

# Experiment and Modeling of ITER Demonstration Discharges in the DIII-D Tokamak

by  
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Presented at the  
Twenty-Third IAEA Fusion Energy Conference  
Daejeon, Republic of Korea

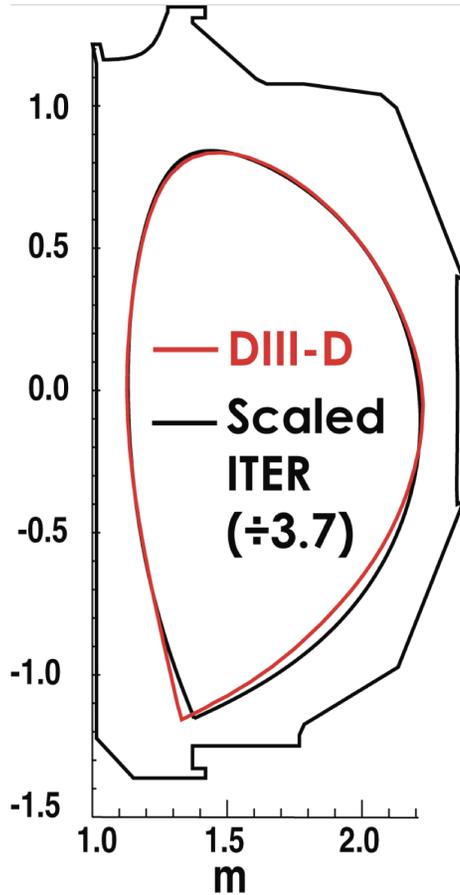
October 11–16, 2010



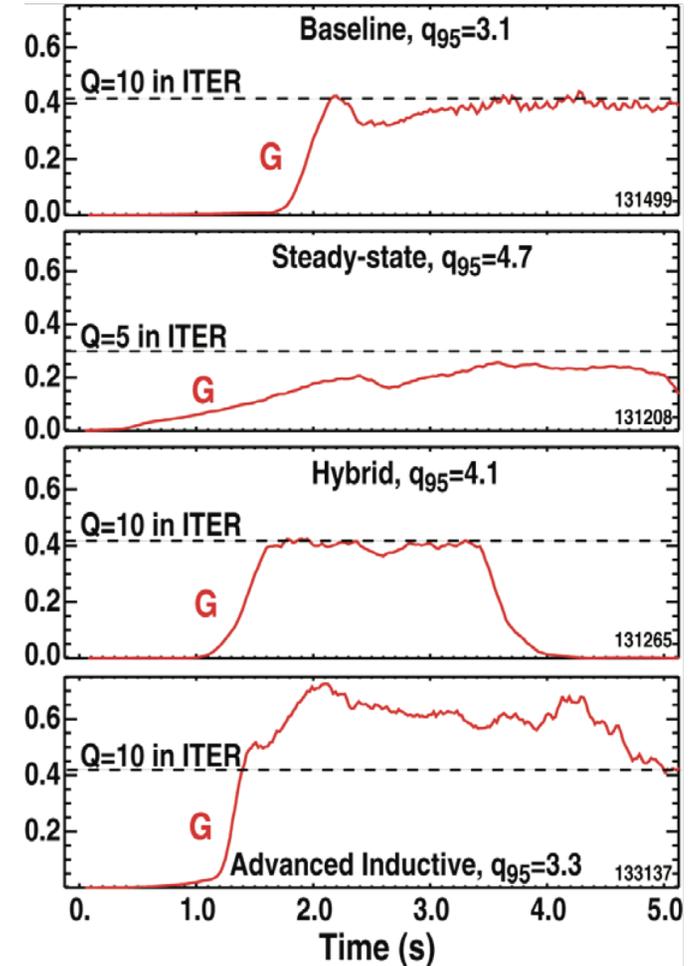
# OUTLINE

- **Recent progress on the ITER demonstration experiment made since 2008 IAEA and integrated theory-based modeling for ITER projection**
- **Baseline scenario:**
  - Improved match to the expected ITER parameters including:
    - Edge pedestal collisionality and rotation
  - Modeling implication for ITER:
    - Change in confinement, transport, and ELM characteristics in ITER regime of low collisionality and rotation
- **Steady state scenario:**
  - Demonstration of fully noninductive operation in ITER shape
    - Strong dependence of confinement, stability, and noninductive fraction on  $q_{95}$
  - Modeling implication for ITER:
    - Optimizing  $q$  profile crucial to simultaneously achieving the fully noninductive ( $f_{NI}=1$ ) and  $Q=5$  goal

# DIII-D Is Providing Suitably Scaled Experimental Evaluations of the Four Primary ITER Operational Scenarios



- With size reduced by factor of 3.7, the DIII-D discharges match the ITER design values for
  - Plasma cross-section
  - Aspect ratio
  - Normalized current  $I/aB$
- DIII-D demonstration discharges meet ITER normalized performance target
  - Target values for  $\beta_N$  and  $H_{98}$  were matched or exceeded



$G \equiv \beta_N H_{98} / q_{95}^2$  is a measure of fusion performance

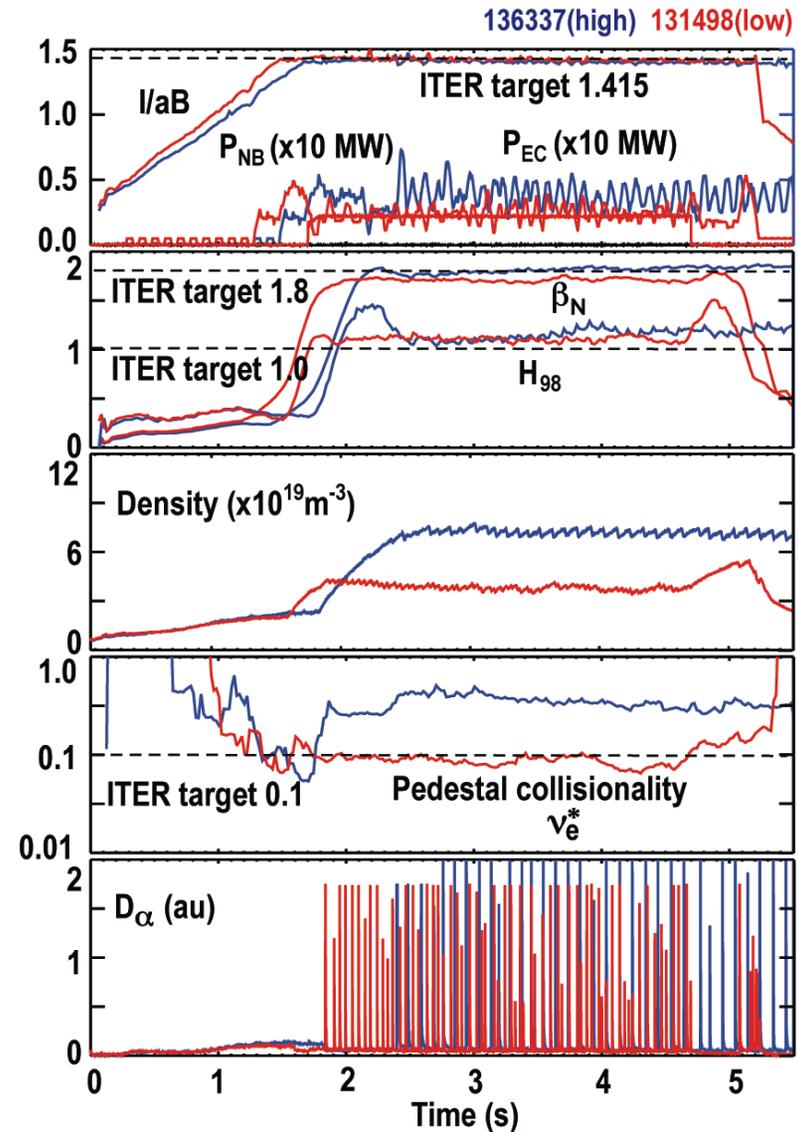
[E. Doyle, IAEA 2008 (NF2010)]

# BASELINE SCENARIO

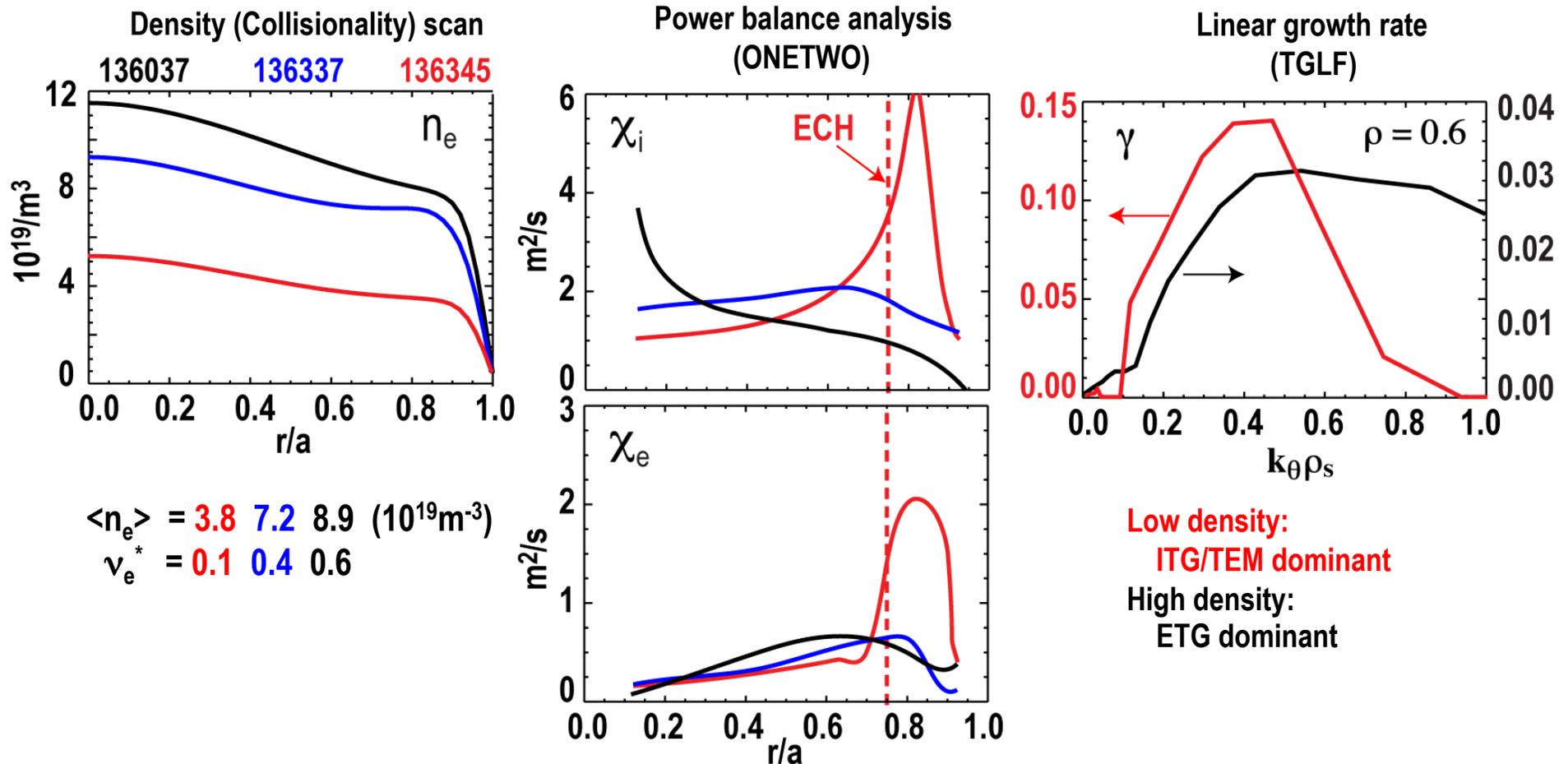


# Lower Density Baseline DIII-D Discharge Developed to Match Edge Pedestal Collisionality

- **Density reduced by more than factor 2 and temperature raised by:**
  - Lowering  $I_p$  (keeping  $I/aB=1.415$ )
  - Application of ECH
- **Target values for  $\beta_N$  and  $H_{98}$  maintained with lower collisionality/density operation**
  - No loss in fusion performance
- **Significant change observed in ELM characteristics**
  - More frequent smaller ELMs
- **ECH is multi-purpose**
  - Suppressing 2/1 NTM by EC current drive
  - Electron dominant heating
- **Improved density control and stationarity**



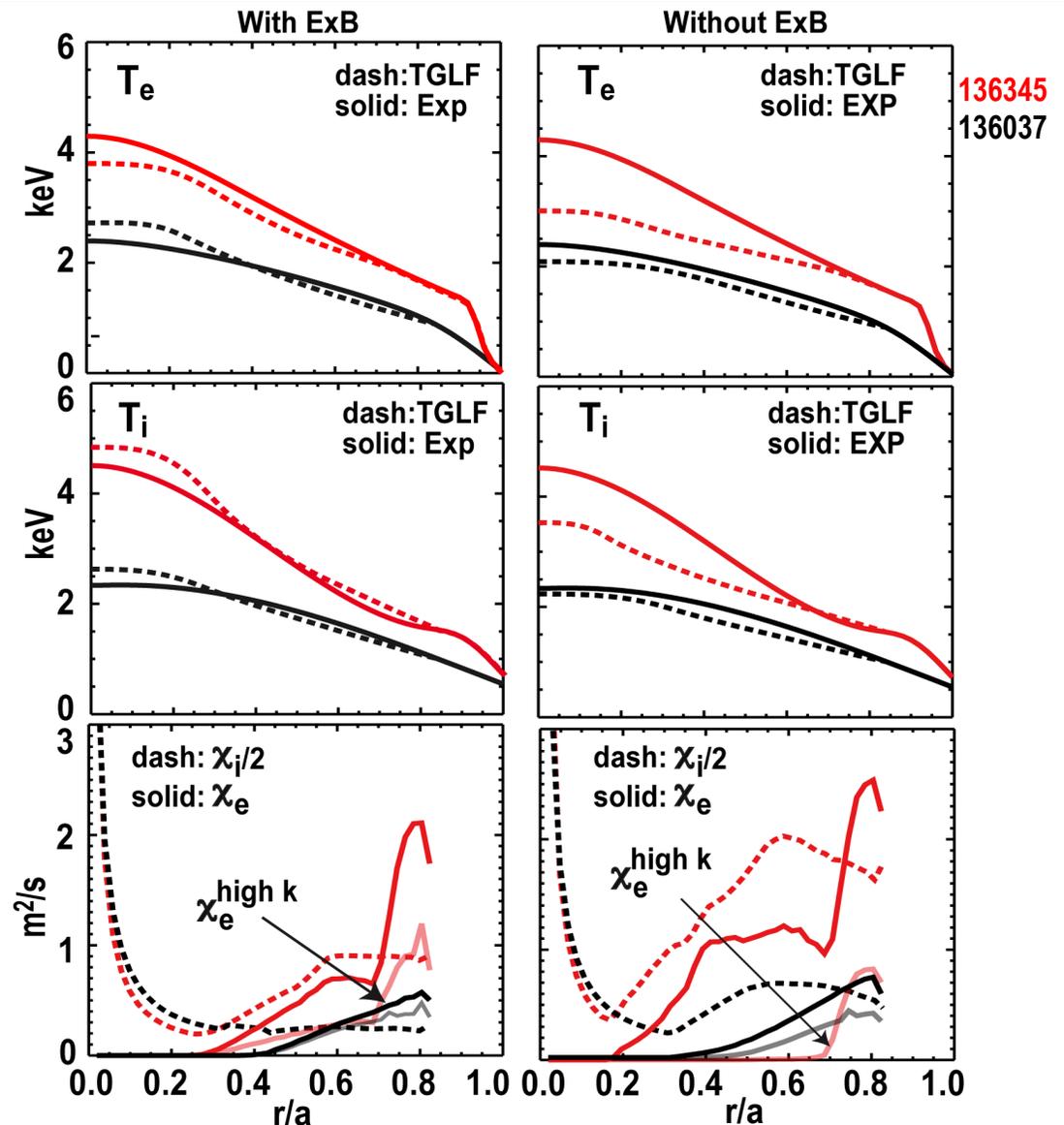
# Transport Mechanism Changes Dramatically in ITER Regime of Low Collisionality and Localized Electron-Dominant Heating



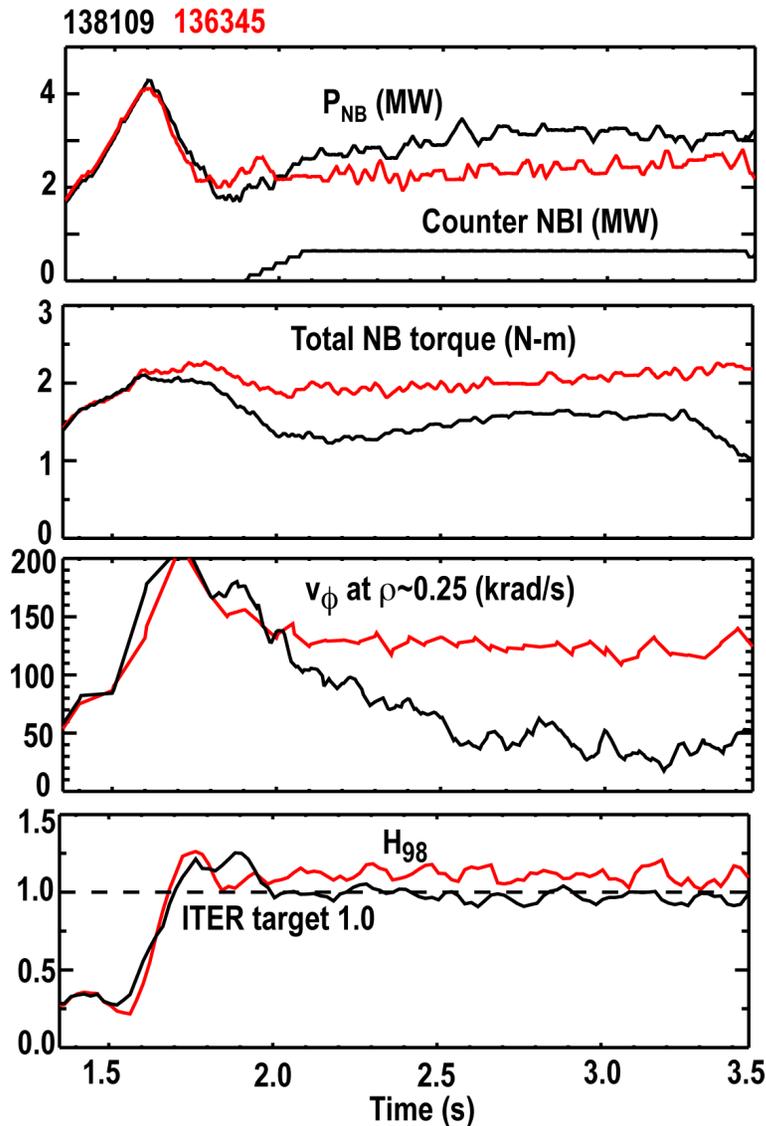
- Same normalized global energy confinement ( $H_{98} \sim 1$ ), but significant change in local transport characteristics
  - Collisionality plays a key role in transport
- Localized electron-dominant heating increases energy transport significantly

# TGLF Transport Simulation Reproduces Change in Transport Processes As Observed in Experiment

- **TGLF modeling of  $T_e$  and  $T_i$** 
  - Used experimental density and pedestal
  - Profiles from 80-100 % of ELM cycles
  - Boundary condition at  $\rho = 0.84$
  - Miller geometry, electrostatic
  - $E \times B$  shearing rate from CER measurement of rotation
  - FASTRAN transport solver
- **Low density**
  - ITG/TEM dominant (low  $k$  mode)
  - Good agreement only when the  $E \times B$  shear stabilization included
- **High density**
  - ETG dominant (high  $k$  mode)
  - Relative small effects of  $E \times B$  shear stabilization

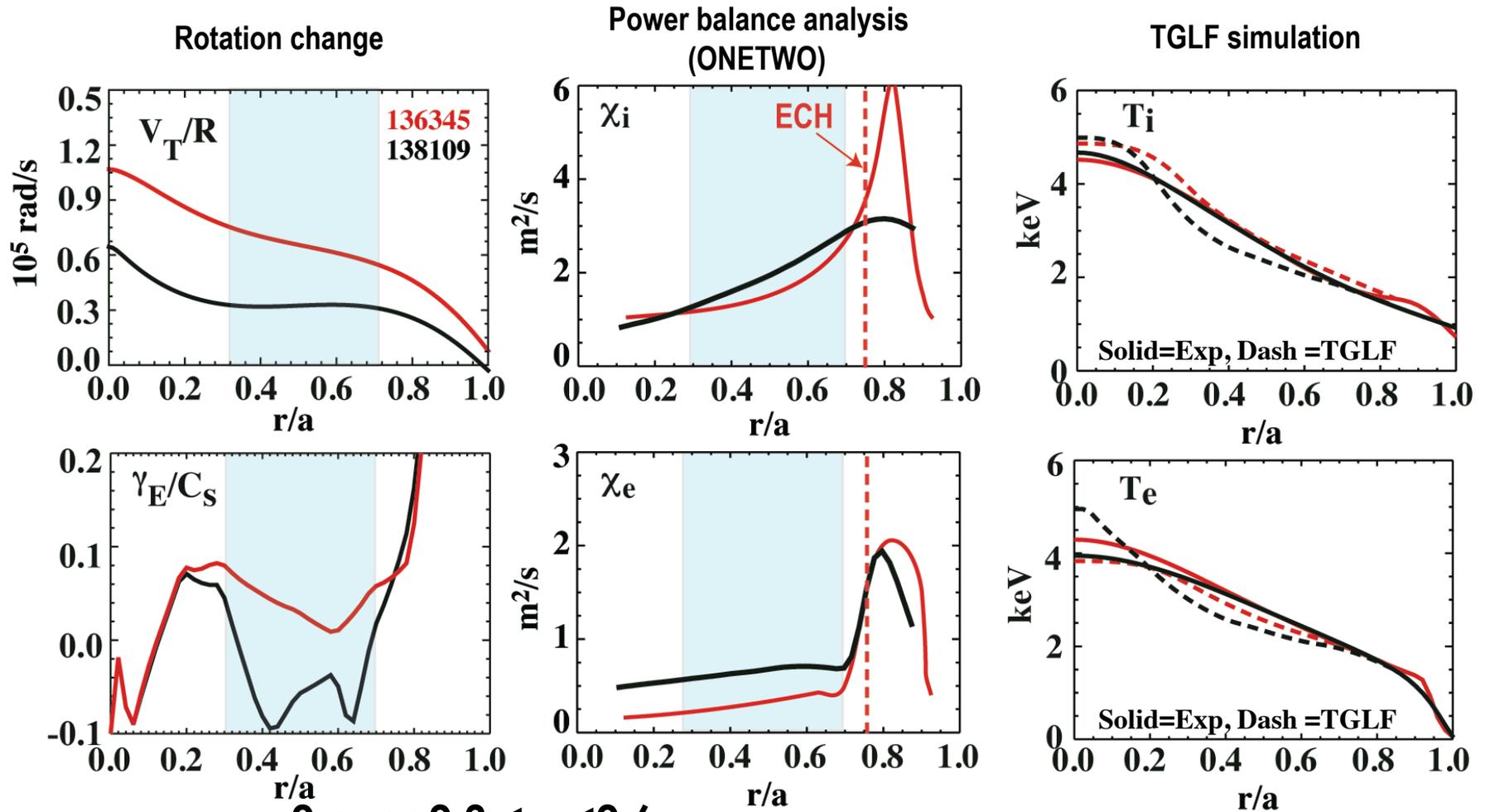


# Plasma Rotation Reduced by Adding Counter-NBI in Low Collisionality Discharge



- Initiated study on effect of reduced plasma rotation on confinement
- Modest 1/4 counter-beam changes rotation substantially
- Confinement factor  $H_{98}$  reduced by  $\sim 15\%$ , but remains ITER target  $H_{98} \sim 1$

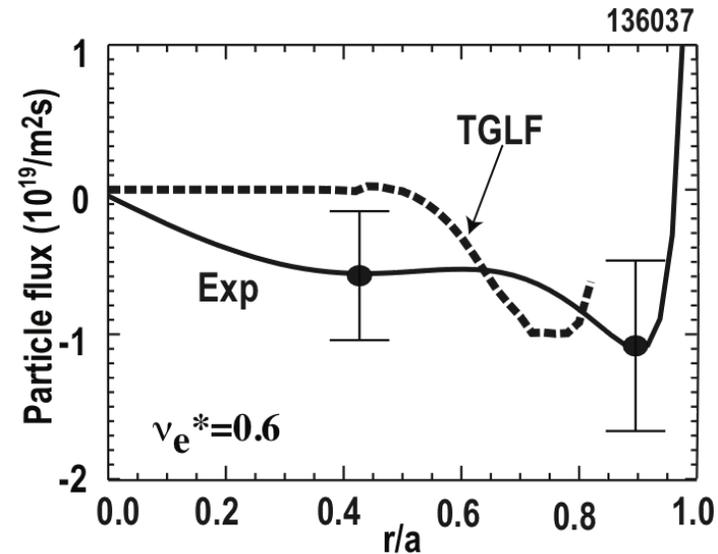
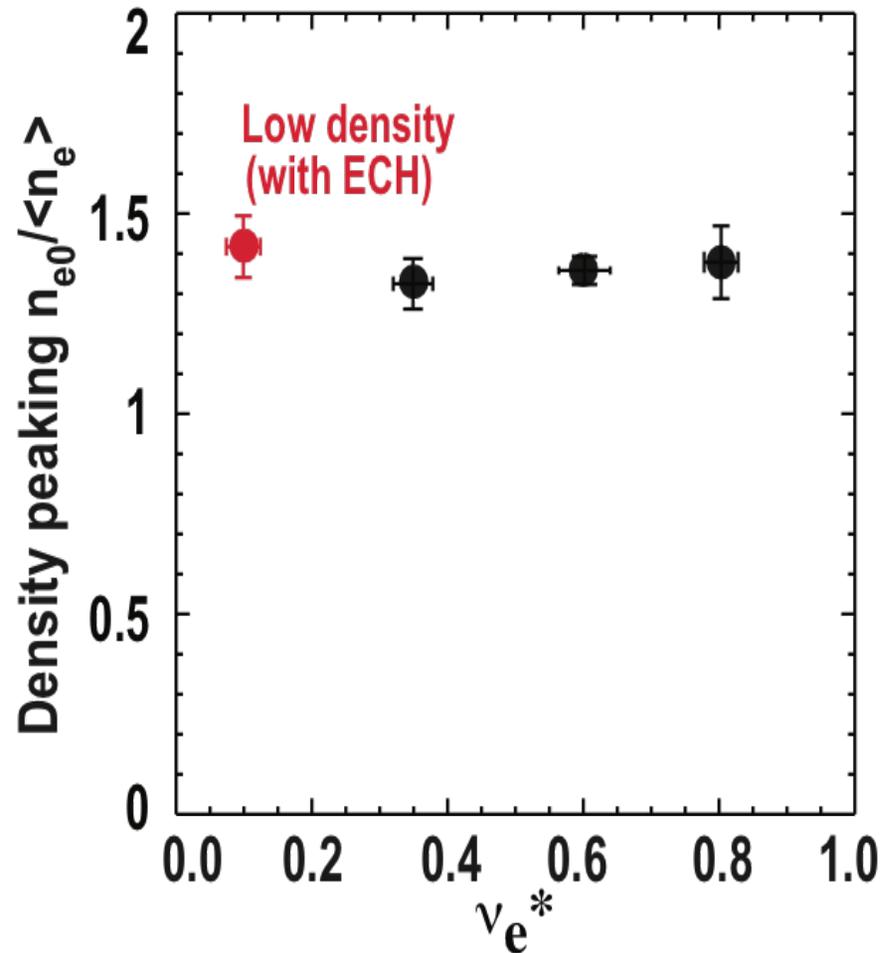
# Initial Data Indicates that Reduced Plasma Rotation Reduces Confinement in Baseline Scenario



- $\gamma_E \sim 0$  over  $0.3 < \rho < 0.6$
- Thermal diffusivity increases with reduced rotation
- **Indicate need for performance margin in projection to ITER**

# Density Profile Is Substantially Peaked for the Baseline Discharge while Insensitive to Collisionality

- Less sensitive to the collisionality than recent AUG and JET observation, which do not use ECH at low density



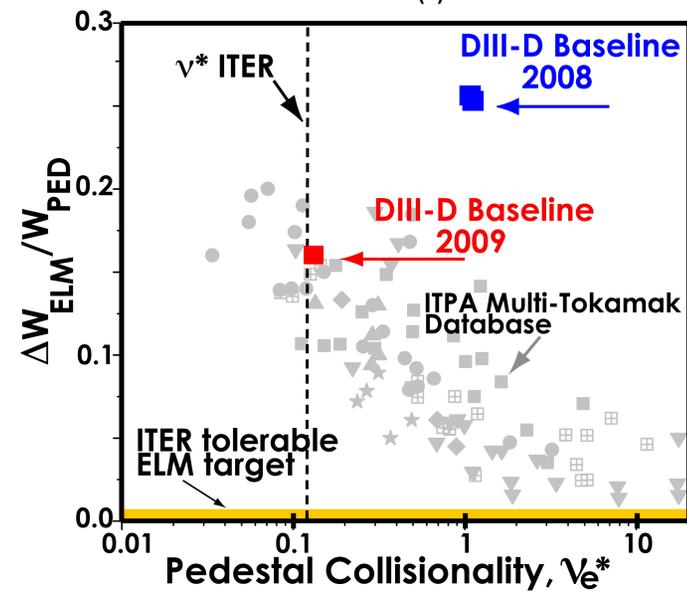
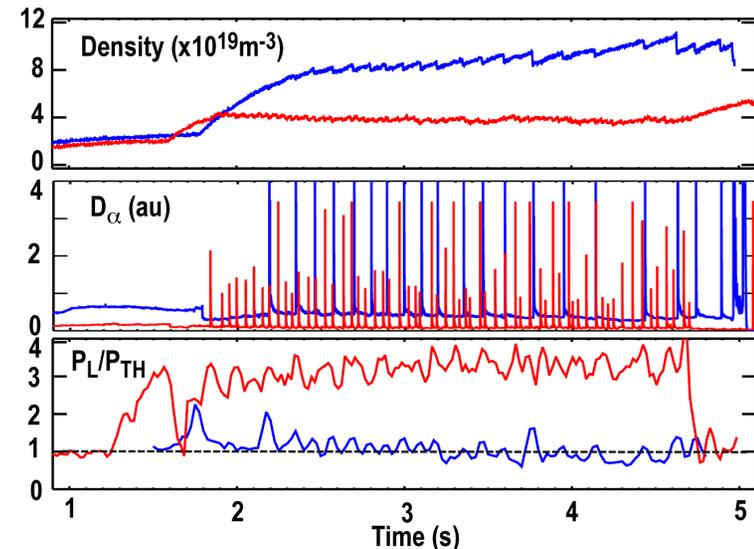
- **Density peaking affected by:**
  - NBI core fueling
  - ECH particle pumping
  - ELM characteristics
- **Particle balance analysis indicates inward particle flux**
  - Consistent with TGLF modeling

# Lower Density Results in Smaller and More Frequent ELMs

- **Significant change in ELM characteristics**
  - More frequent smaller ELMs for low density discharges
- **The change in  $P_L/P_{TH}$  is likely to affect the ELM characteristics**
  - Empirical scaling for L-H power threshold (Y. Martin, et. al, 2008)

$$P_{TH} = 0.049 \chi n^{0.72} B^{0.8} S^{0.9}$$

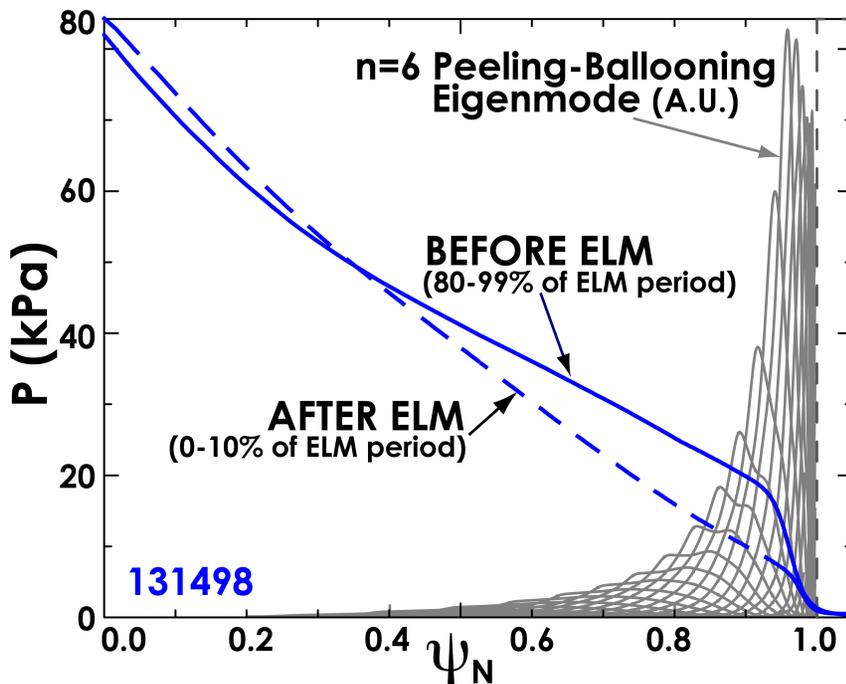
- **Reduction of energy loss at lower collisionality is counter to scaling obtained in ITPA database**
- **Fractional energy loss at ELMs substantially exceeds ITER limit**



# Magnitude of ELM Energy Loss Correlated With the Shape of Unstable Peeling-Ballooning Modes

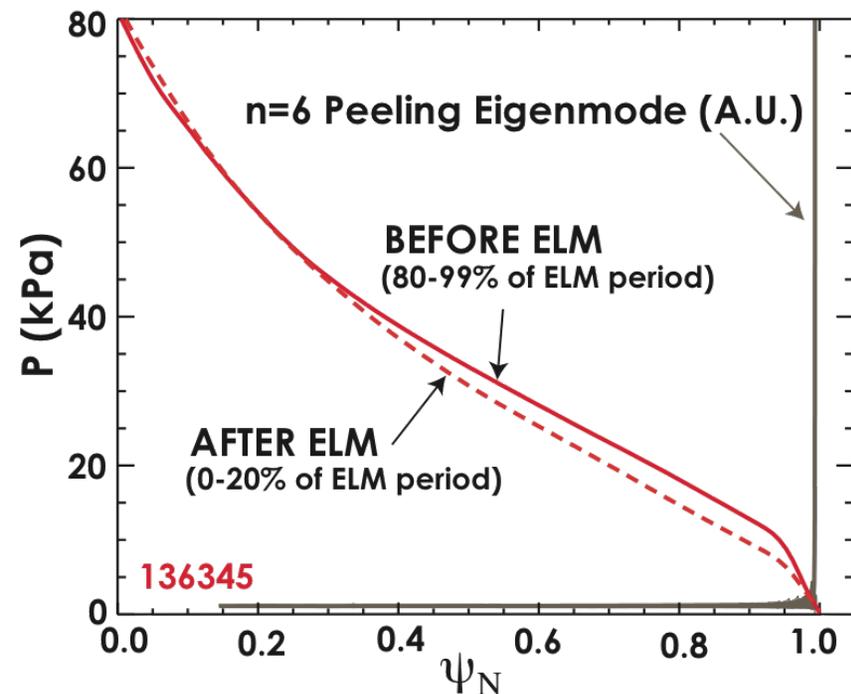
- **High density**

- Coupled peeling-ballooning mode
- ELM-affected region extends deep into the plasma



- **Low density**

- More peeling-like mode
- Narrow mode structure
- Smaller and more frequent ELM



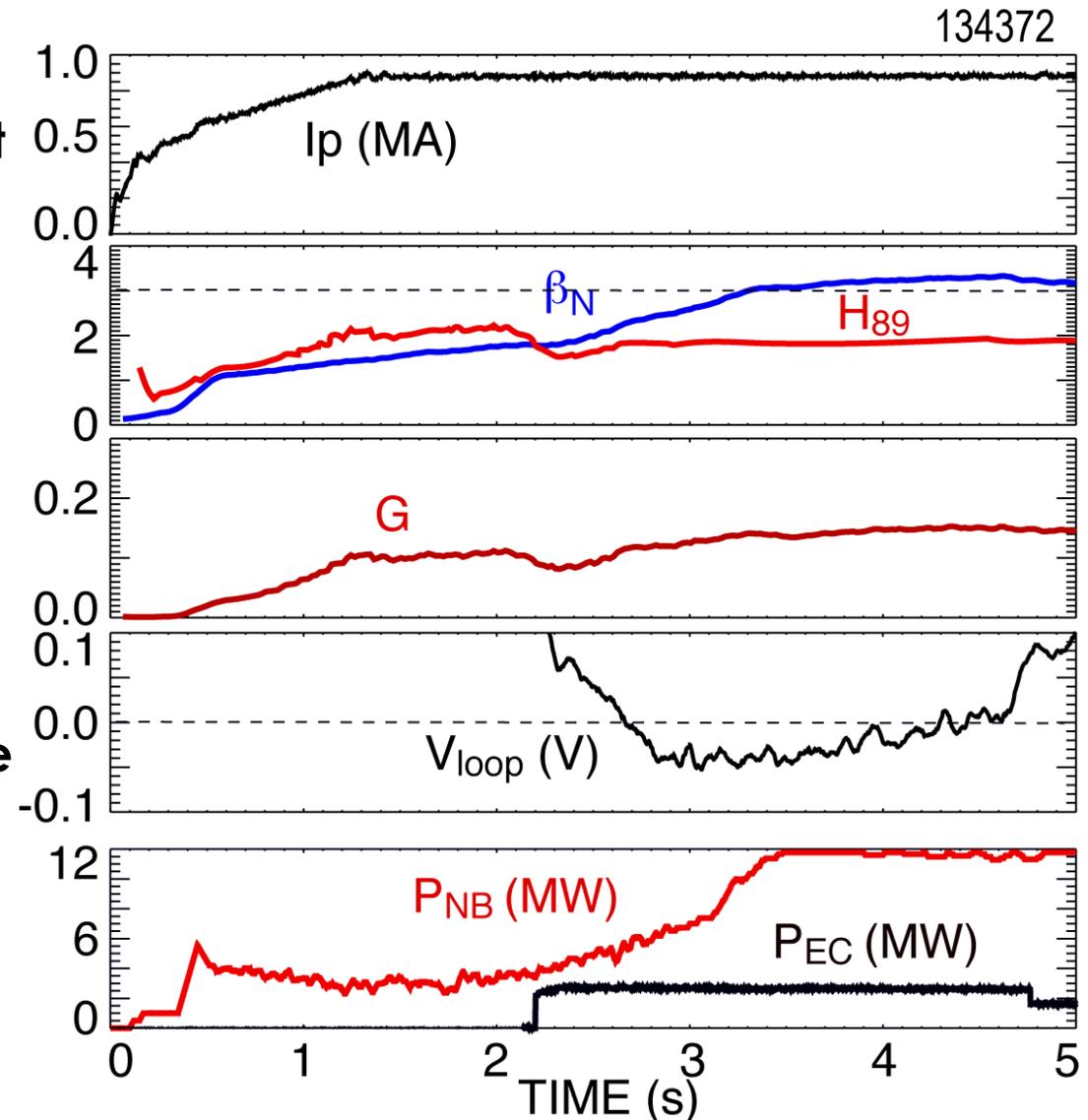
- **Eigenmode structure calculated by ELITE stability code**

# STEADY STATE SCENARIO

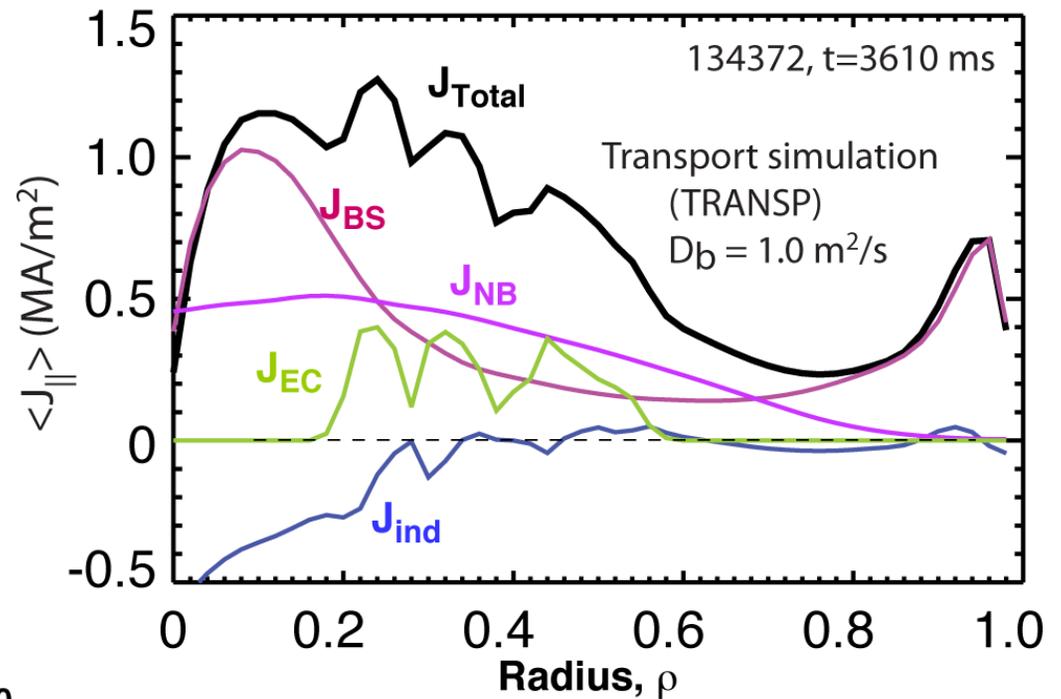
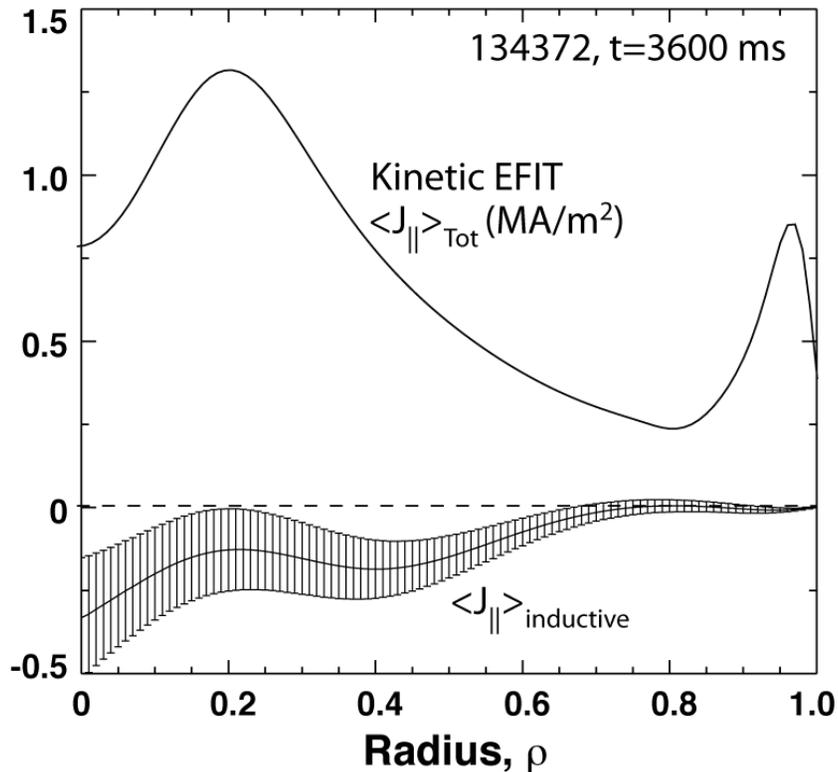


# Fully Noninductive Operation Demonstrated in ITER Shape

- Fully noninductive operation obtained in 8.5 MA equivalent discharge with  $\beta_N = 3.1$ 
  - $q_{95} = 6.3$
  - High bootstrap fraction (~70%)
  - Relatively low fusion performance
  - Not stationary
- Standard DIII-D prescription
- Steady-state discharges utilize off-axis ECCD to maintain stable q-profile with  $q_{\min} \geq 1.5$
- $G = \beta_N H_{89} / q_{95}^2$ 
  - Measure of fusion performance



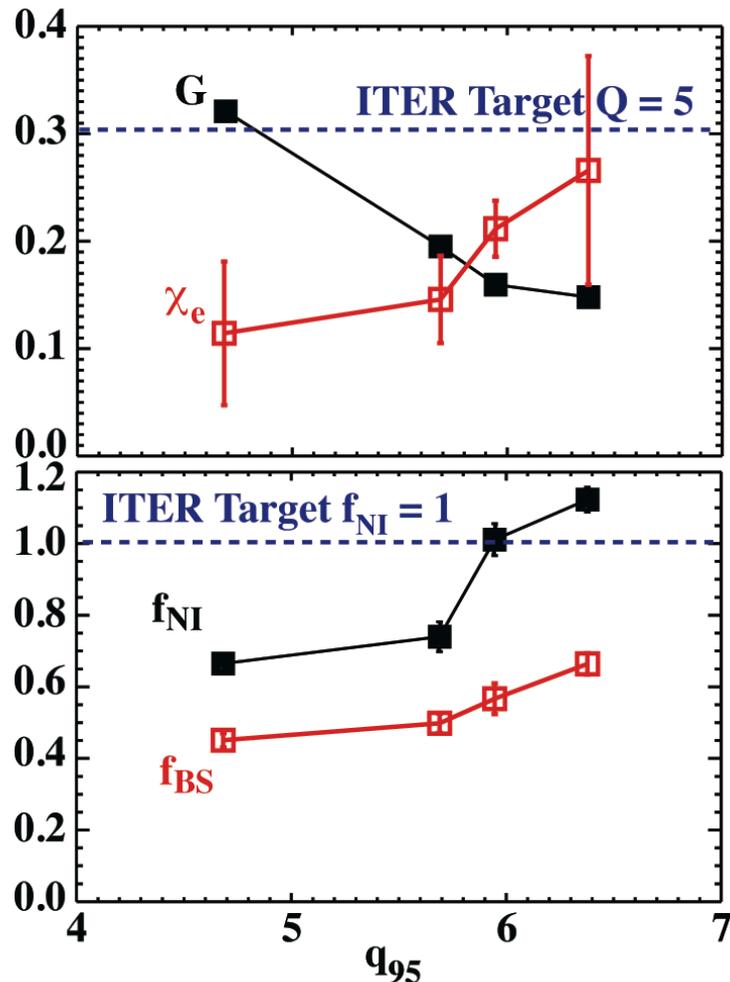
# Measurement and Simulation Show that Inductive Current Density is Small Everywhere



- Measurement of inductive current density - loop voltage analysis

- Transport code simulation

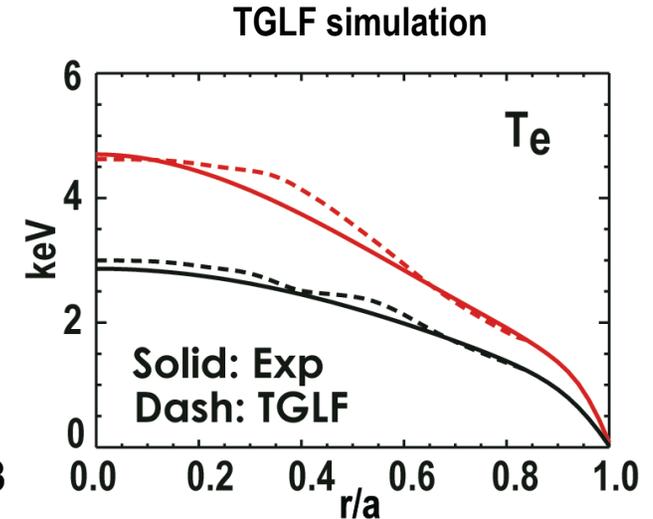
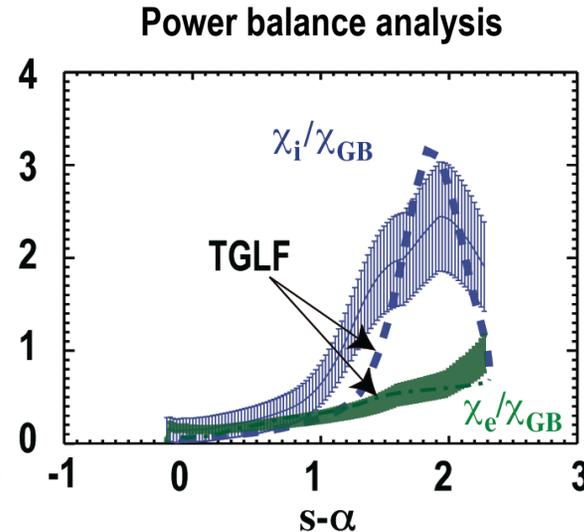
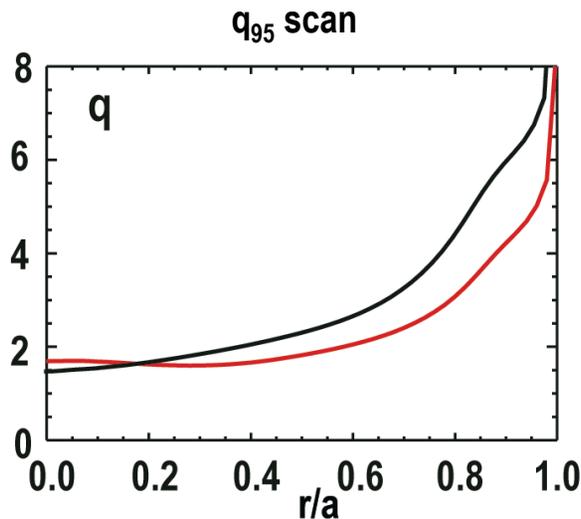
# Noninductive Fraction Increases while Fusion Performance Decreases with $q_{95}$



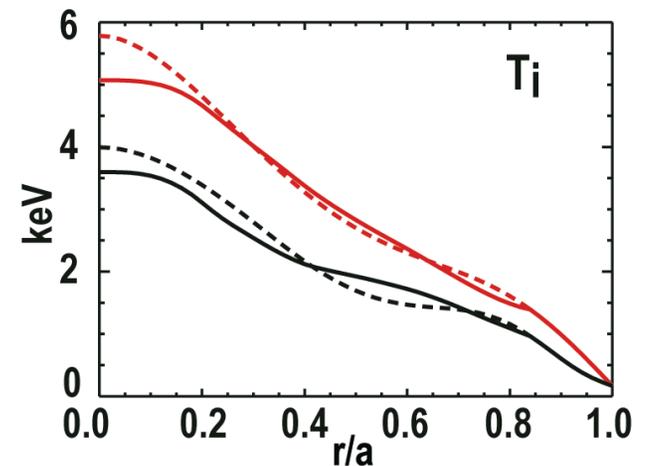
- Thermal energy confinement time decreases with  $q_{95}$ 
  - Generally follow the scaling of  $H_{98}$
- $f_{NI}$  and  $f_{BS}$  increase with  $\beta_N q_{95}$
- Edge pedestal provides typically ~40% of the total bootstrap current
  - Pedestal height and width depend on  $q_{95}$
- Theory-base (GLF23) projection using the scaled edge profiles shows the same trade-off between  $f_{NI}$  and  $Q$  with variation of  $q_{95}$  [M. Murakami: ITR P1-35]

- Indicate need for optimizing  $q_{95}$  in projection to ITER

# Electron and Ion Thermal Diffusivities Correlated Mainly with Magnetic Shear

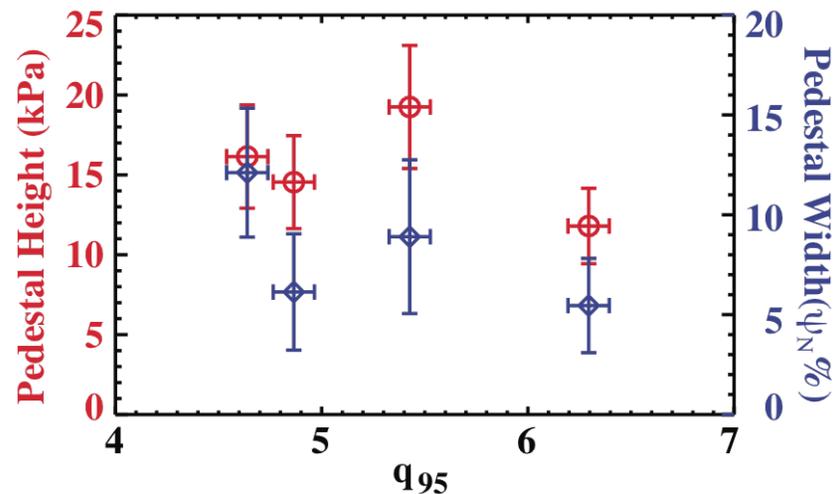
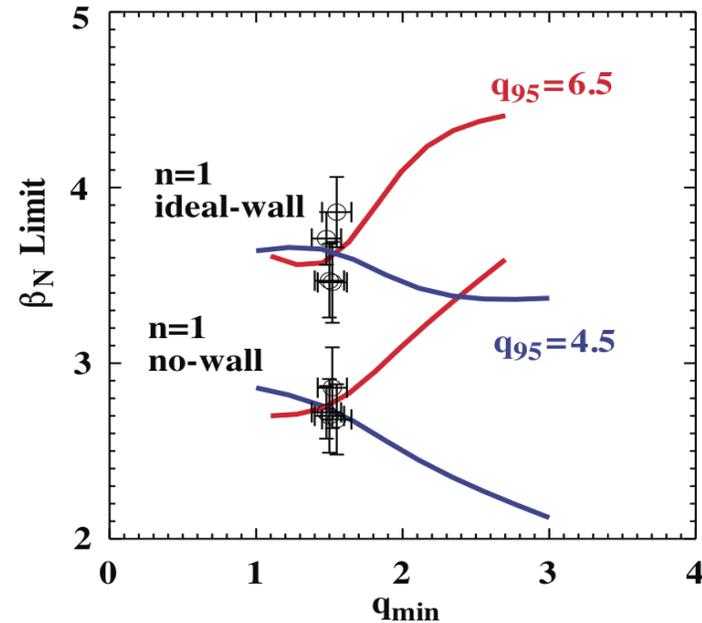


- Electron and ion thermal diffusivities correlated mainly with magnetic shear both in the power balance analysis by TRANSP and in the TGLF modeling
- TGLF transport simulation reproduces the transport dependency on  $q_{95}$
- Predictive simulation suggests that a larger radius of minimum q with weak magnetic shear can reduce turbulent transport significantly



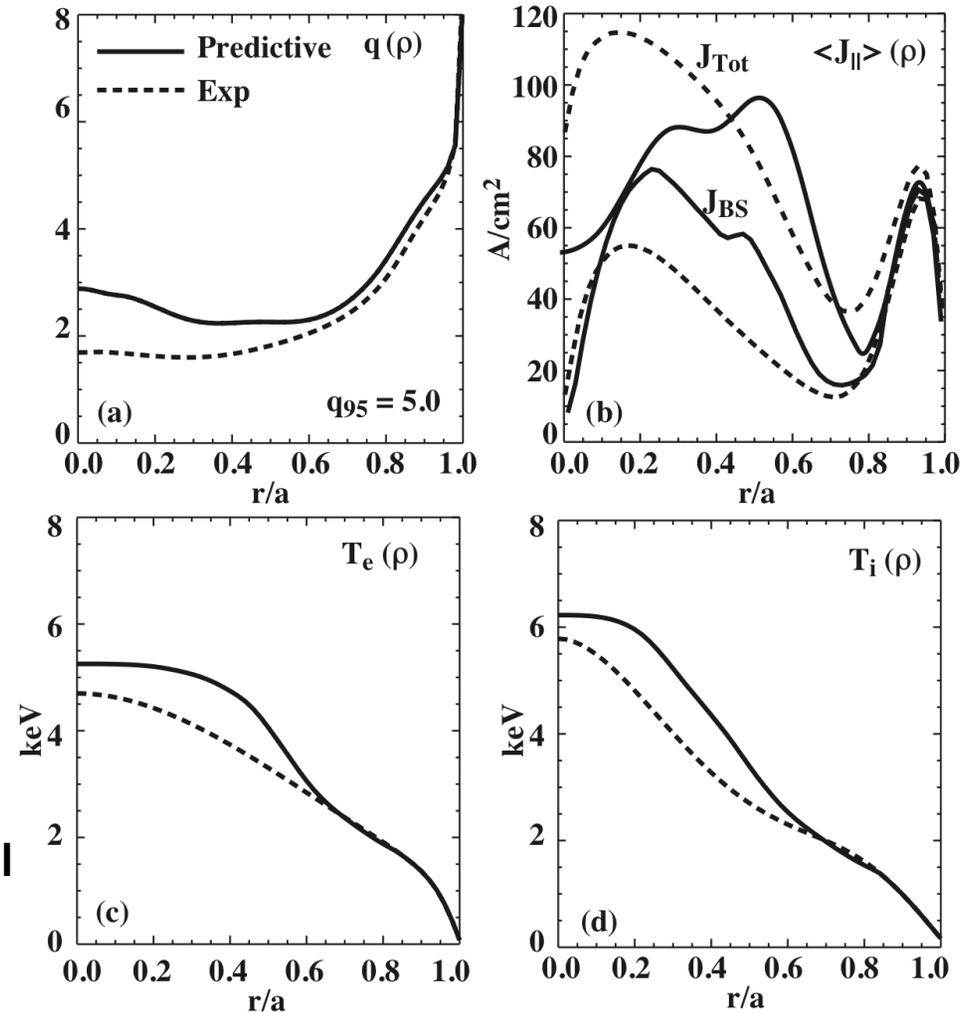
# Experiment and Modeling Show Dependence of Stability and Edge Pedestal on $q_{95}$

- **Calculated ideal  $\beta_N$  limit using experimental profiles and equilibria**
  - $n=1$  no-wall  $\sim 2.8$
  - $n=1$  ideal-wall  $\sim 3.7$
- **Predictive modeling indicates:**
  - $\beta_N$  Limit decrease (increase) with  $q_{\min}$  at  $q_{95} = 4.5$  ( $6.5$ )
  - Tradeoff between stability and confinement to achieve higher  $\beta_N$  at lower  $q_{95}$
- **Edge pedestal provides typically  $\sim 40\%$  of the total bootstrap current**
  - Key role in optimizing steady-state scenario
- **Pedestal height and width decrease with  $q_{95}$** 
  - Consistent with EPED prediction



# Optimum Scenario Studied by Integrated Theory-based Modeling to Achieve the $f_{NI}=1$ and $Q=5$ Goals Simultaneously

- **Newly developed iterative steady-state solution procedure:**
  - Iterative numerical method to find a steady state solution ( $d/dt=0$ ) of core transport (TGLF) using FASTRAN with self-consistent calculation of equilibrium (EFIT) and heating/CD sources (NUBEAM, TORAY, CURRAY)
- **Predictive simulations suggest:**
  - A larger radius for  $q_{min}$  helps to increase both the fusion performance and  $f_{NI}$  at  $\beta_N$  limit calculated from ideal wall stability
- **Maximally utilize the benefits of low magnetic shear and higher pedestal pressure from the increased  $\beta_p$**



# Low $q_{95}$ (High $I_p$ ) Operation is Important to Reach the $f_{NI}=1$ and $Q=5$ Goals Simultaneously

- **Optimum  $q$  profile scan starting from the experimental condition:**

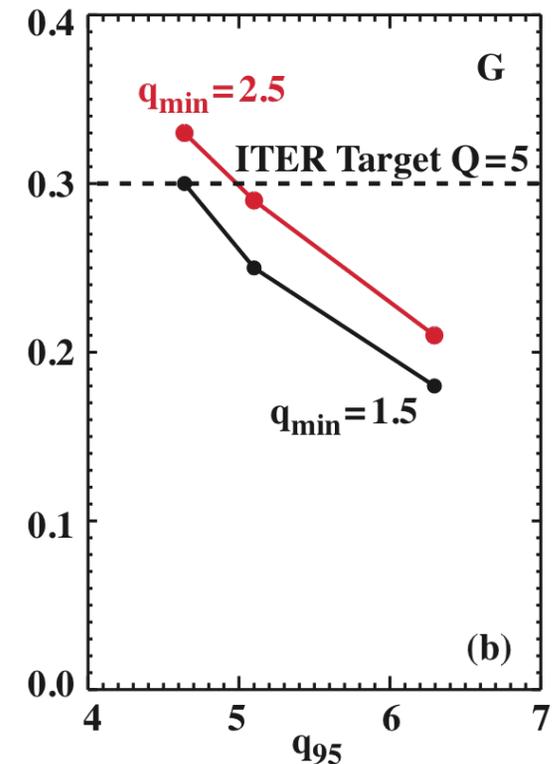
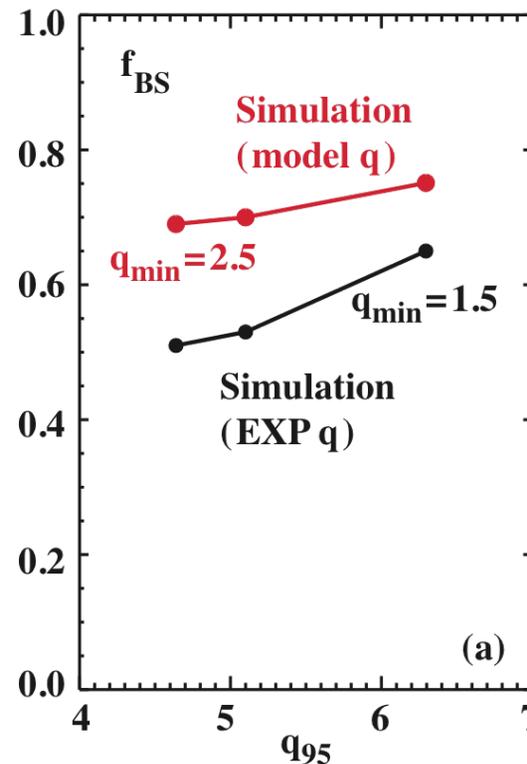
- Modest improvement of fusion performance for  $4.5 < q_{95} < 6.5$

- **Higher  $q_{95}$  (lower  $I_p$ )**

- Maximum improvement of plasma confinement factor is not sufficient to reach  $G=0.3$  for the  $Q=5$  goal

- **Lower  $q_{95}$  (higher  $I_p$ )**

- Significant increase of  $f_{BS}$  with a larger radius of  $q_{min}$
- At  $q_{95}=5.0$  ( $q_{min} \sim 2.5$ ), reach  $f_{BS} = 0.72$  with  $G=0.3$  at the calculated ideal wall stability limit



# SUMMARY AND FUTURE WORK

- **Baseline scenario:**
  - Substantial progress made in improving the match to the expected ITER parameters including edge pedestal collisionality and rotation
  - Significant change in confinement and ELM characteristics in ITER regime of low collisionality and rotation indicates need for performance margin in ITER projection
- **Steady state scenario:**
  - Noninductive operation demonstrated but with relatively low fusion performance, indicating need for  $q_{95}$  optimization in ITER projections
  - Optimization of current profile is crucial to simultaneously achieving the fully noninductive ( $f_{NI}=1$ ) and  $Q=5$  goals
- **Future work:**
  - Apply new tools for better match to the ITER parameters (off-axis NBI, higher power EC, and FW current drive)
  - Develop steady state scenario with higher fusion performance and bootstrap fraction
  - Theory-based ITER projection using validated models against the DIII-D ITER demonstration discharges