

Compatibility of the Radiating Divertor with High Performance Plasmas in DIII-D

by
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INTRODUCTION

Introduction

- Issue

Protecting the divertor structure from excessive power loading

- Possible solution

“Seed” the divertor with impurities in order to enhance the radiated power upstream of the divertor targets → more uniform dispersal of power loading → “Radiating divertor”

- Trade-offs

Reducing divertor power loading vs. degrading plasma performance, e.g., impurity accumulation → displacement of fuel ions and degradation in τ_E

- Reduction in impurity accumulation

Enhance deuterium flow in the scrape-off layer → Counters the thermal gradient force that pushes impurities out of the divertor

- **HOW DOES ALL THIS AFFECT “HIGH PERFORMANCE” PLASMA OPS?**

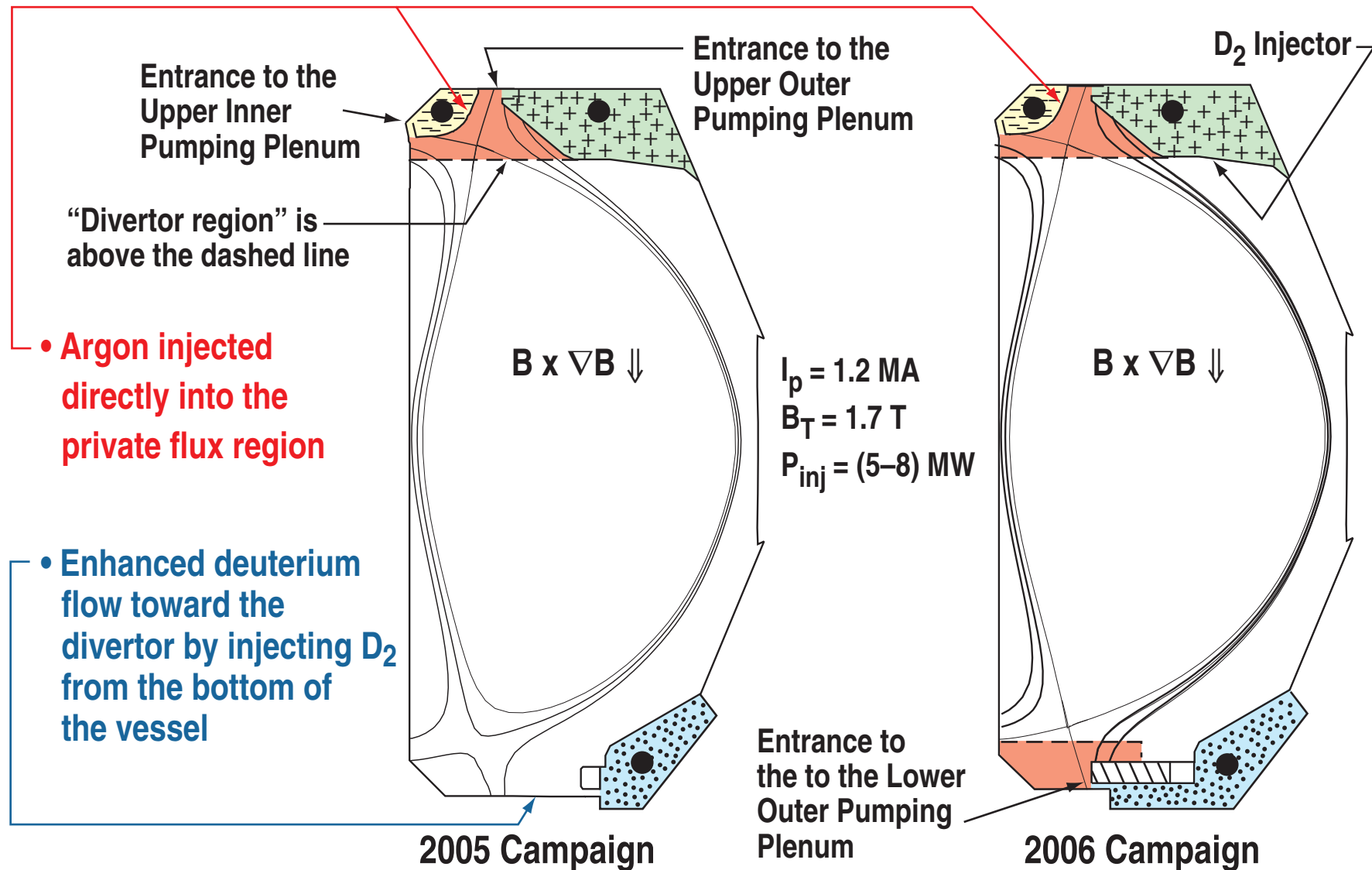
Main Questions

- Is radiating divertor operation compatible with high performance “hybrid” discharges?
- How well can impurities be confined to the “closed” DIII-D divertor?
- How effectively does the radiating divertor reduce power loading at each divertor target?
- Do DNs behave differently than SNs under radiating divertor conditions?

EXPERIMENTAL

ARRANGEMENT

DIII-D Puff and Pump Capability Enhanced by DN Pumping



Experimental Operating Conditions

- Hybrid plasmas are used in this study
 - Similar to ELMing H-mode plasmas with good confinement, e.g., $\tau_E/\tau_{ITER89P} \gtrsim 2$
 - Important difference: absence of sawteeth
 - ⇒ Improved stability and confinement properties
- There are two main impurity species in the core plasma
 - CARBON (intrinsic)
 - Dominant intrinsic impurity in DIII-D discharges
 - Generated by erosion of the graphite armor protecting the vessel interior
 - ARGON (injected)
 - Radiates effectively under hybrid plasma operating conditions
 - Relatively short $\lambda_{MFP} \rightarrow$ good candidate for confining to the divertor
- Inner and outer divertor legs are attached during puffing

ARGON AT TRACE LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

Exhaust enrichment (η_{exh})

$\propto \Gamma_{D2}$ and $\eta_{\text{exh,MAX}} \approx 38$

Exhaust Enrichment is One Measure of How to Characterize the Retention of Injected Impurities in the Divertor

$$[\text{exhaust enrichment}] \equiv [f_{\text{EXH}}]/[f_{\text{CORE}}]$$

where

$$f_{\text{CORE}} \equiv [n_{\text{Z,CORE}}]/[n_{\text{e,CORE}}]$$

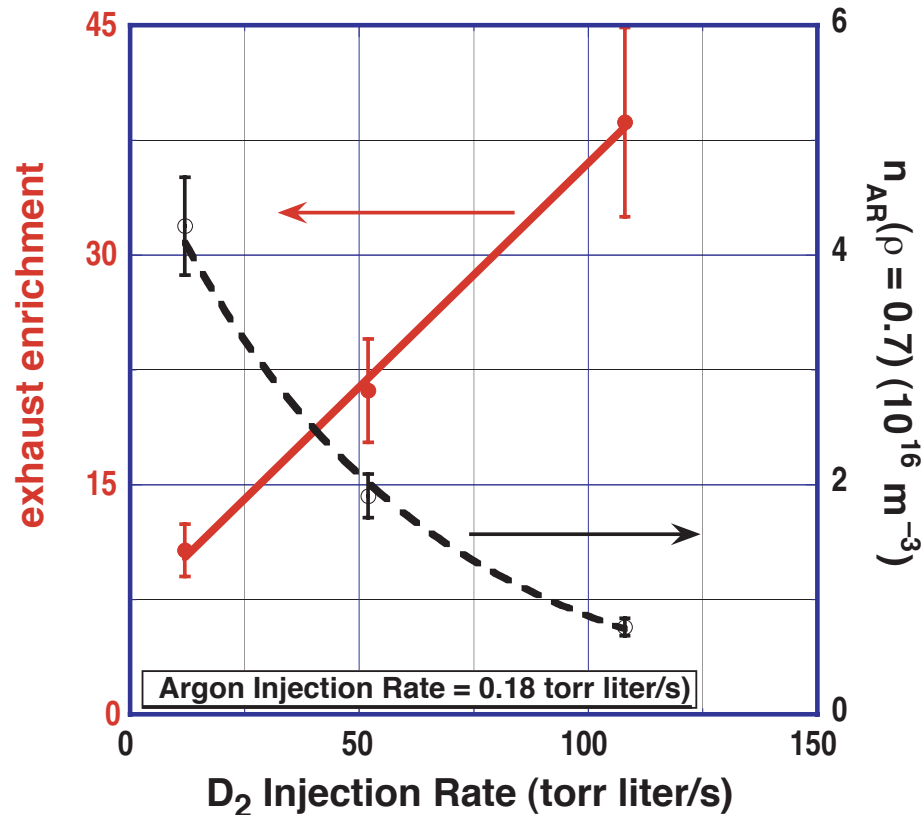
↑ ↑
Thomson scattering
Charge-Exchange Recombination
(Ar⁺¹⁶ and C⁺⁶ profiles)

$$[f_{\text{EXH}}] \equiv [P_{\text{Z,EXH}}]/[2 \times P_{\text{D2,EXH}}]$$

↑ ↑
Modified Penning gauge
(partial pressure of deuterium and argon inside outer baffle)

The Exhaust Enrichment of Trace Argon Increased by a Factor of 3 Over the Range of Γ_{D2} Considered

The argon density decreased by almost a factor of six over the Γ_{D2} range considered



Comparison with a previous DIII-D experiment with trace argon

	1998*	2005
Γ_{D2} (Torr ℓ /s)	84	108
DIV. Config.	“OPEN”	“CLOSED”
$\overline{\mathbf{B}} \times \nabla \mathbf{B}$	Toward Xpt	Away from
Pumping	Outer	Inner + Outer
η_{EXH}	17	38

*M.R. Wade, et al,
J. Nucl. Matter., 266-269 (1999) 44

Argon Enrichment Improves Significantly with Combined D₂ Injection and Pumping

	Case A	Case B	Case C
Γ_{D_2} (Torr ℓ/s)	0	52	107
Γ_{AR} (Torr ℓ/s)	1.3	1.3	1.3
n_{AR}/n_e ($\rho=0.7$) (%)	0.092	0.034	0.013
η_{EXH}	11.4	24.3	35.1
$n_{e,ave}$ ($10^{20} m^{-3}$)	0.47	0.58	0.61
$n_{e,DIV,OUT}$ ($10^{20} m^{-3}$)	0.25	0.40	0.50
$n_{e,DIV,IN}$ ($10^{20} m^{-3}$)	0.29	0.59	1.02

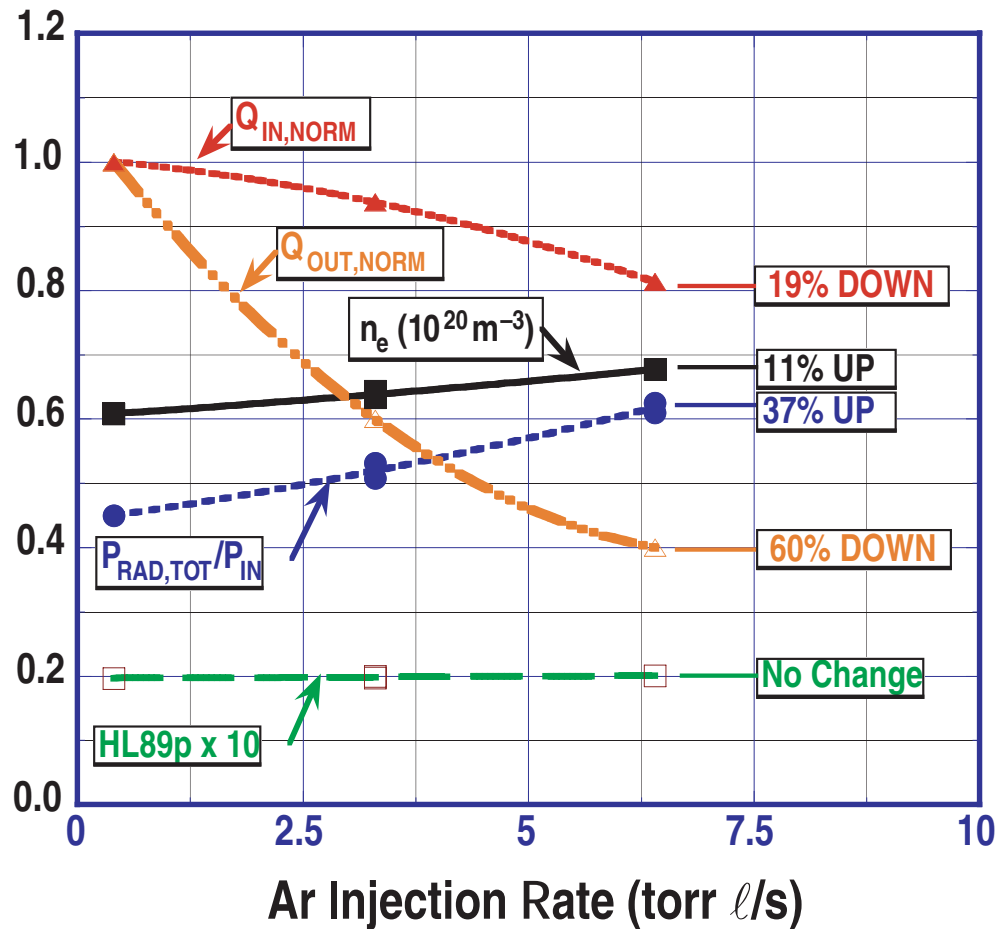
Note: We choose $\rho=0.7$, because MIST impurity transport analysis of the hybrid plasmas under investigation showed that helium-like argon at $\rho=0.7$ was by far the dominant charge state of argon \rightarrow good approximation for the total argon density

ARGON AT PERTURBING LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

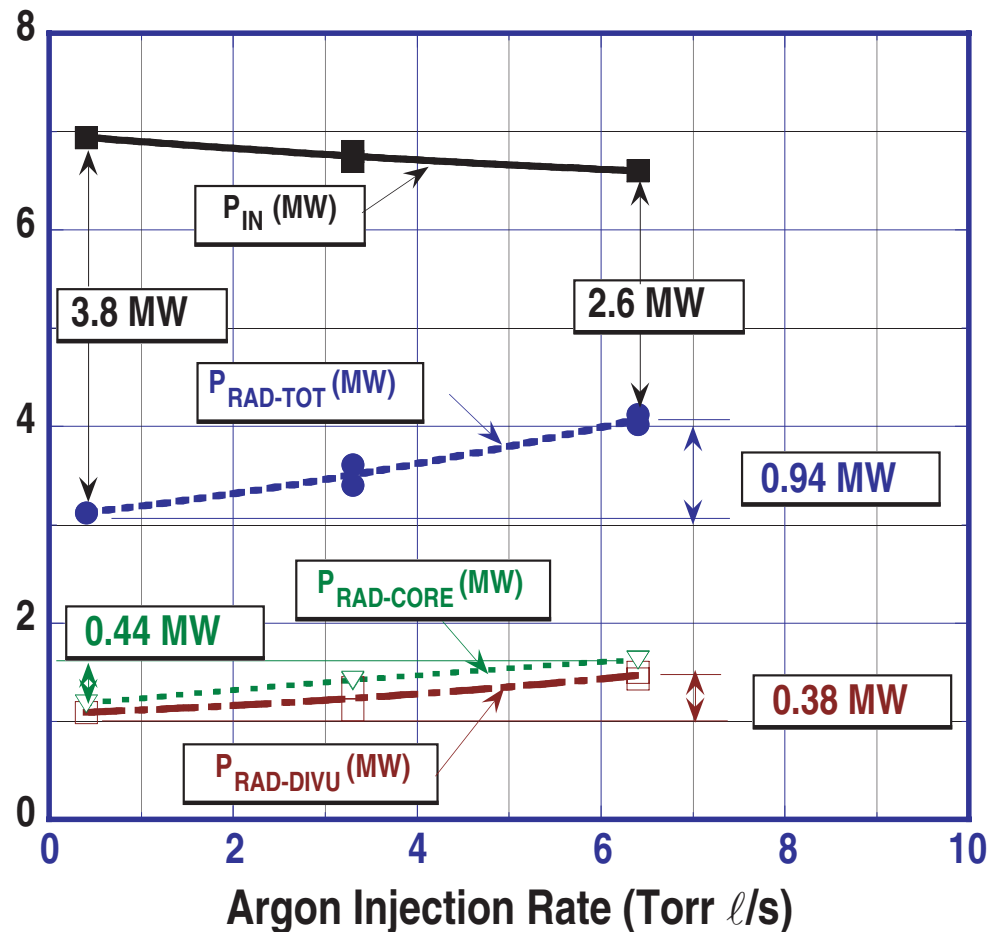
**The heat flux reduction at the
outer divertor target was
much greater than that at the
inner divertor target**

The Peak Heat Flux at the Outer Divertor Target Decreased Much More than at the Inner Divertor Target, as the Argon Injection Rate Increased



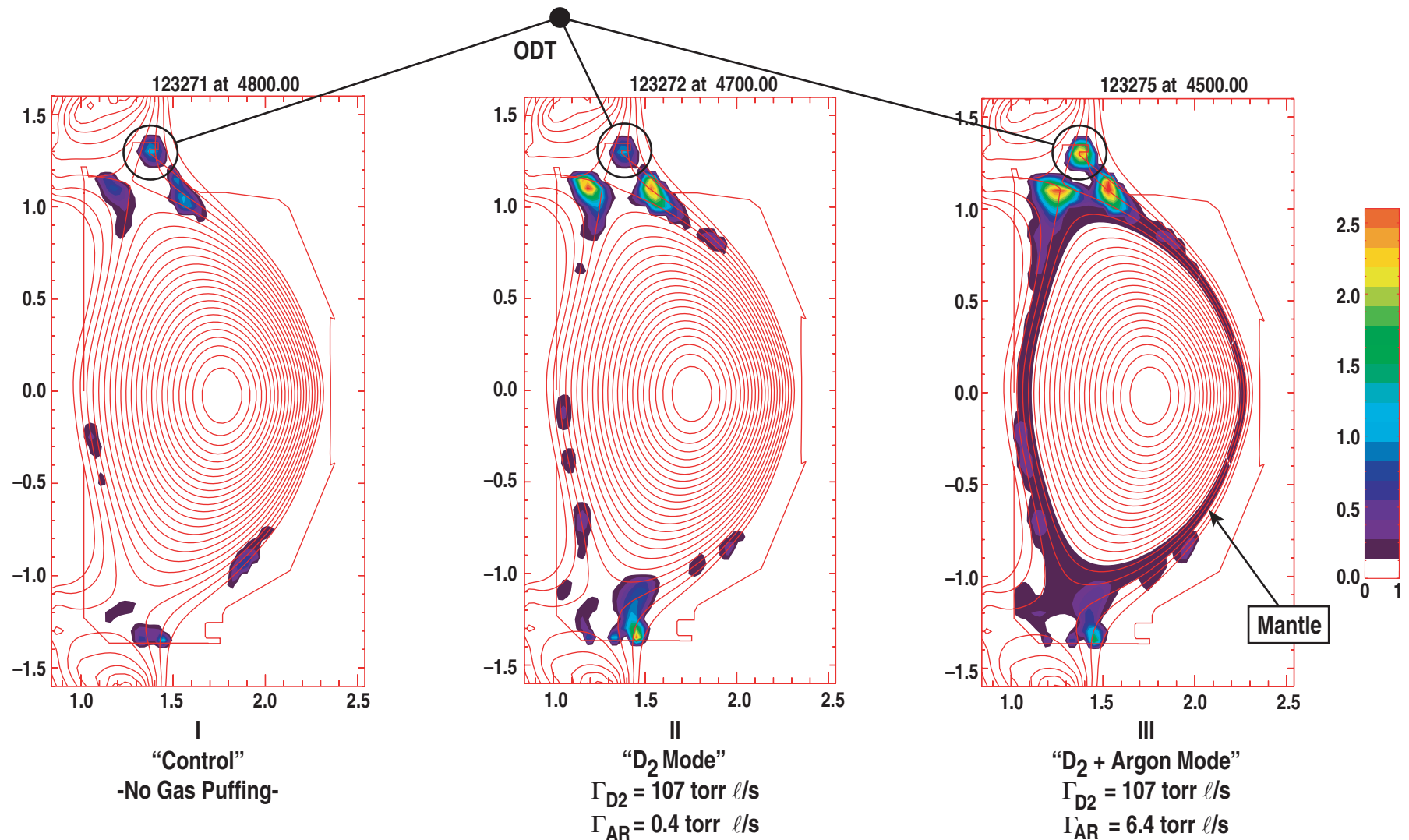
- Modest increase in density with a higher rate of argon injection
- Rise in total radiated power was co-incident with a sharp drop in peak heat flux at the outer divertor target but much less of a drop at the inner divertor target
- Maintain good energy confinement during argon injection

Roughly 40% of the Increase in the Total Radiated Power from High-level Argon Injection was Found in the Divertor

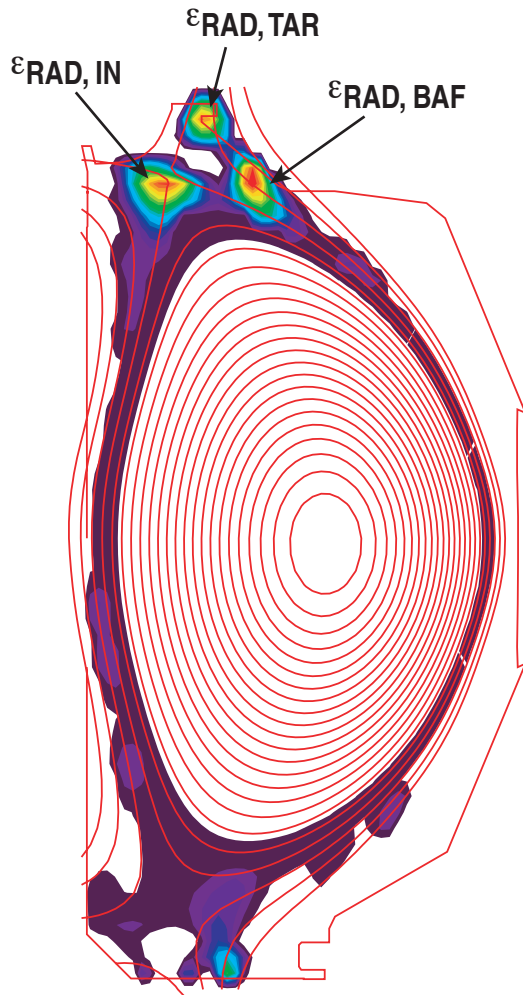


- The increase in both divertor and total radiated powers was linear in Γ_{AR} over the range considered
- About 45% of the increase in $P_{RAD-TOT}$ with high-level argon injection was found in the core

Argon Injection with Enhanced Deuterium Flow in the SOL was Effective in Raising the Radiated Power Near the Outer Divertor Target (ODT)



The Reduction in the Peak Heat Flux at the Outer Divertor Target may be Associated with the Increase in Radiated Power Near the Target



Comparison of peak emissivities for two cases

	$[\epsilon_{\text{RAD,IN}}]_{\text{P}}$ [MW/m ³]	$[\epsilon_{\text{RAD,BAF}}]_{\text{P}}$ [MW/m ³]	$[\epsilon_{\text{RAD,TAR}}]_{\text{P}}$ [MW/m ³]	$[\hat{Q}_{\text{OUT}}]_{\text{P}}$	$[\hat{Q}_{\text{IN}}]_{\text{P}}$
D ₂ Mode	2.95	2.80	1.10	1.0	1.0
D ₂ + Ar Mode	2.85	2.95	2.70	0.37	0.81

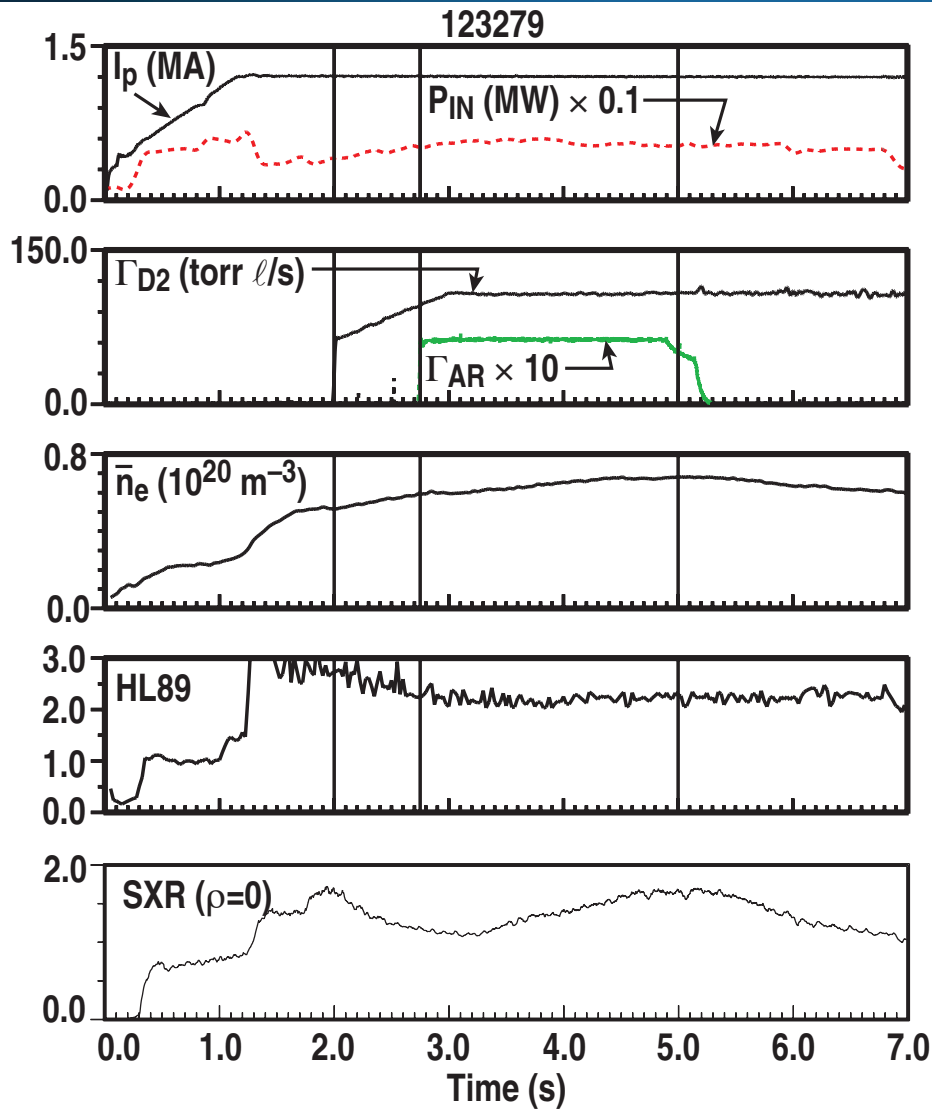
- $[\epsilon_{\text{RAD,TAR}}]_{\text{P}}$ increased by 2-3x for the D₂ + Ar mode
- $[\epsilon_{\text{RAD,BAF}}]_{\text{P}}$ and $[\epsilon_{\text{RAD,IN}}]_{\text{P}}$ were comparable in both cases
 - $[\hat{Q}_{\text{OUT}}]_{\text{P}}$ is the peak heat flux at the outer divertor target normalized to the “D₂ mode” case
 - $[\hat{Q}_{\text{IN}}]_{\text{P}}$ is the peak heat flux at the inner divertor target normalized to the “D₂ mode” case

ARGON AT PERTURBING LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

η_{exh} was insensitive to Γ_{AR}

The Response of a Hybrid-class Plasma to D₂ Injection and to D₂+Argon Injection is Shown



$t \approx 2.0 - 2.8 \text{ s}$ — D₂ injection only

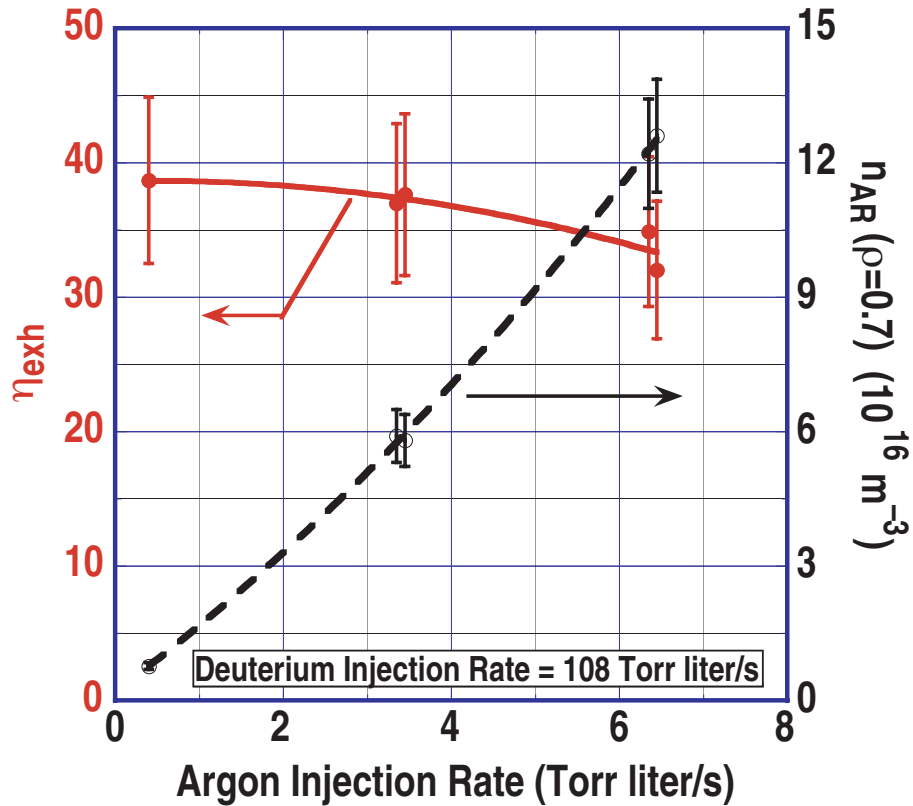
$t \approx 2.8 - 5.0 \text{ s}$ — D₂ + argon injection

$t \approx 5.0 - 7.0 \text{ s}$ — D₂ injection only

- Roughly 10% increase in line-averaged density after argon injection is initiated
- No change in the energy confinement time with the addition argon to D₂
- Minimal sawtooth activity

The Exhaust Enrichment was Insensitive to the Argon Injection Rate at Perturbing Levels

The Argon density increased a little faster than linear



Comparison of Exhaust Enrichment

	1998*	2005
Γ_{D2} (Torr. ℓ)	190	108
Γ_{AR} (Torr. ℓ)	3.8	6.4
\bar{n}_e (10^{20} m^{-3})	0.80	0.67
P_{IN} (MW)	12	6.7
$\tau_E/\tau_{\text{ITER89P}}$	1.7	2.0
$P_{\text{RAD}}/P_{\text{IN}}$	0.72	0.63
$P_{\text{RAD,CORE}}/P_{\text{IN}}$	0.17	0.24
Z_{EFF}	1.85	2.1
η_{EXH}	~5	32

*M.Wade, et al, J. Nucl. Matter.,
266-269 (1999) 44

A Comparison of D₂ and Argon Gas Puffing Modes on “Hybrid” Plasma Behavior

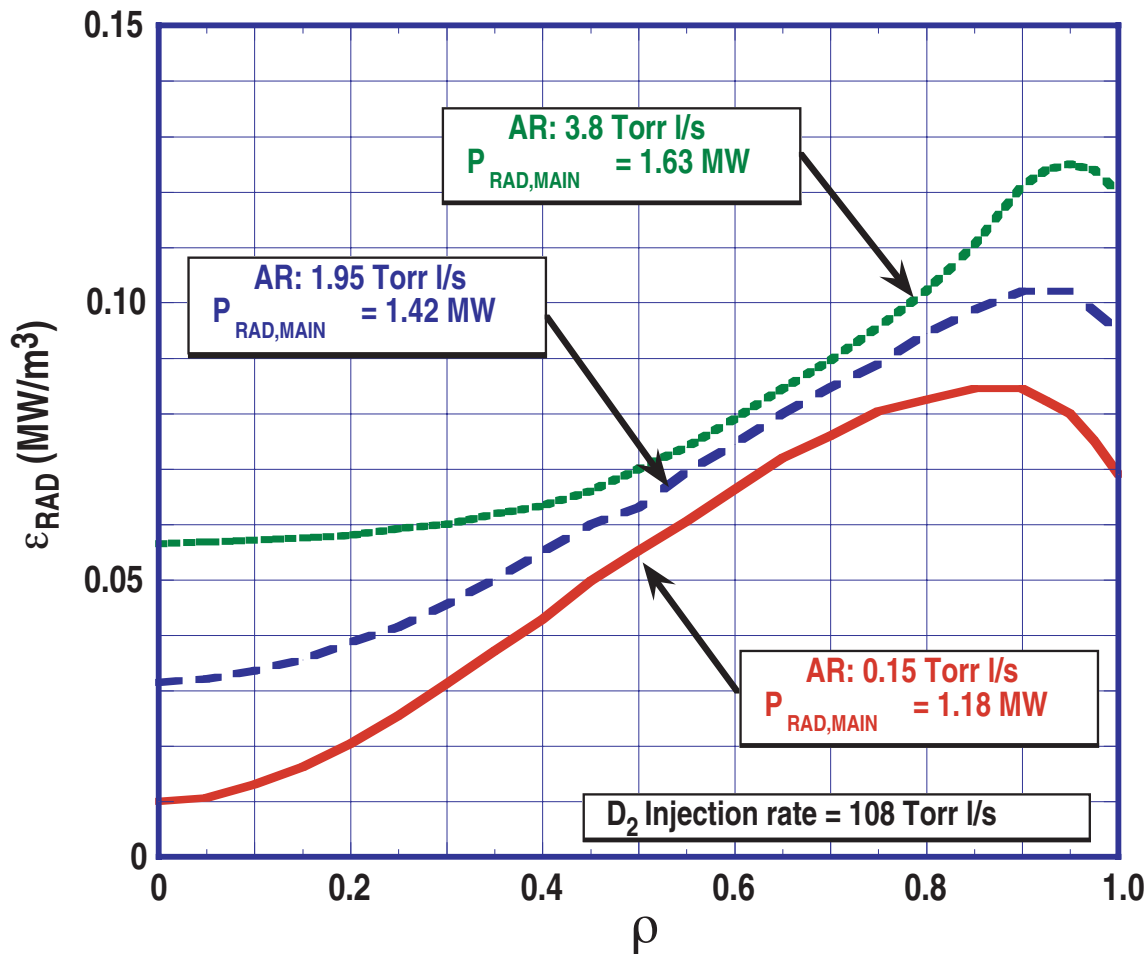
	[CASE 1]	[CASE 2]	[CASE 3]
Γ_{D_2} torr liter/s	108	108	108
Γ_{AR} torr liter/s	0.4	3.4	6.4
\bar{n}_e (10^{20} m ⁻³)	0.61	0.64	0.67
$H_{ITER\ 89P}$	2.0	2.0	2.0
P_{IN} (MW)	6.9	6.8	6.6
$P_{RAD,TOT}/P_{IN}$	0.45	0.52	0.63
$P_{RAD,MAIN}/P_{IN}$	0.17	0.21	0.24
$P_{RAD,DIV}/P_{IN}$	0.16	0.18	0.22
$q_{P,IN}$ (MW/m ²)	1.6	1.5	1.3
$q_{P,OUT}$ (MW/m ²)	3.0	1.8	1.2
$T_{e,IN}$ (eV)	10	10	10
$T_{e,OUT}$ (eV)	22	15	10
ν_{ELM} (Hz)	≈ 80	≈ 75	≈ 70
$n_C/n_e[\rho = 0.7]$ (%)	2.1	2.1	2.2
$n_{AR}/n_e[\rho = 0.7]$ (%)	0.013	0.10	0.20
$Z_{EFF}[\rho = 0.7]$	1.65	1.87	2.15
η_{EXH}	38	37	33

ARGON AT PERTURBING LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

**Roughly 30% of $P_{\text{RAD,CORE}}$
was due to argon**

The Primary Radiator Inside the Core Plasma is Mainly Carbon, Even at the Highest Argon Injecton Rate



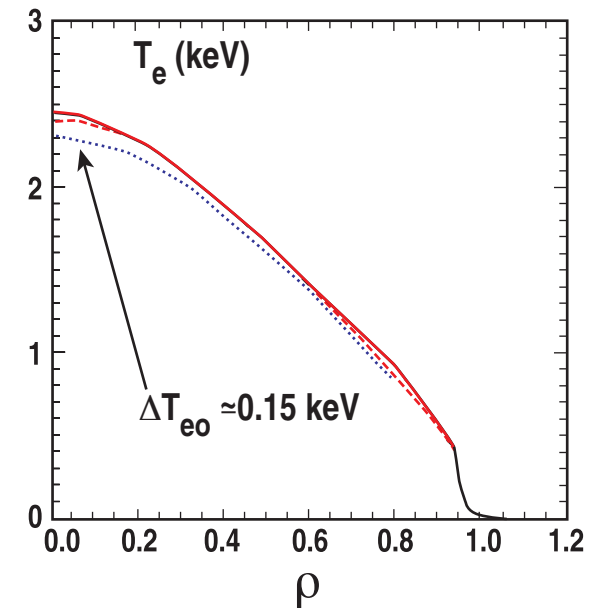
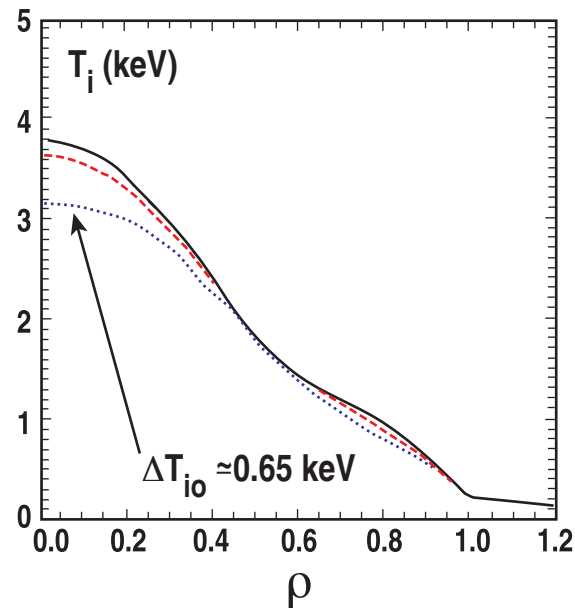
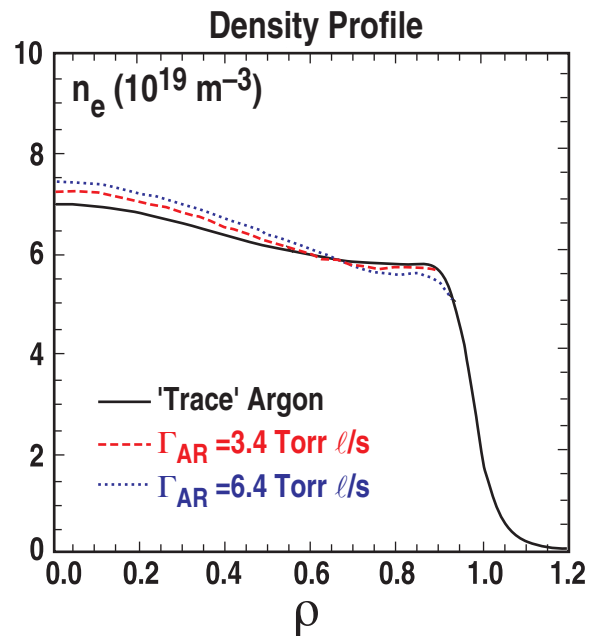
Case 1: “trace argon”
>95% of the radiated power in the core was from carbon

Case 3: “perturbing argon”
25-30% of the radiated power in the core was from argon and the profile was still hollow

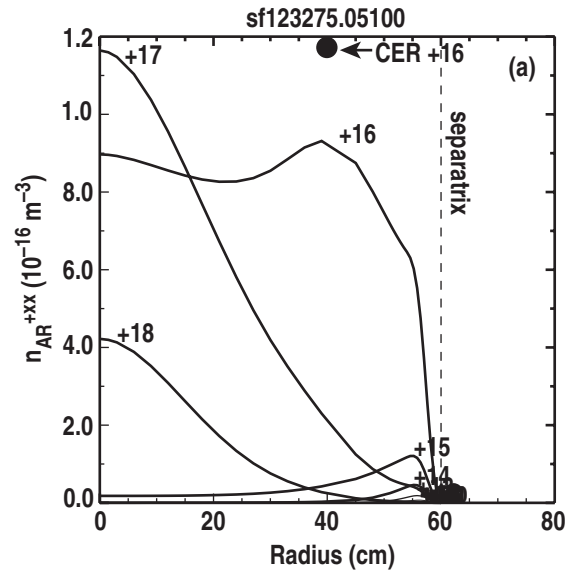
Note: For case 3, 4% of the **deuterium fuel ions** was displaced by the Ar at $\rho=0$

Increasing Γ_{AR} Reduced T_{i0} Much More than T_{e0}

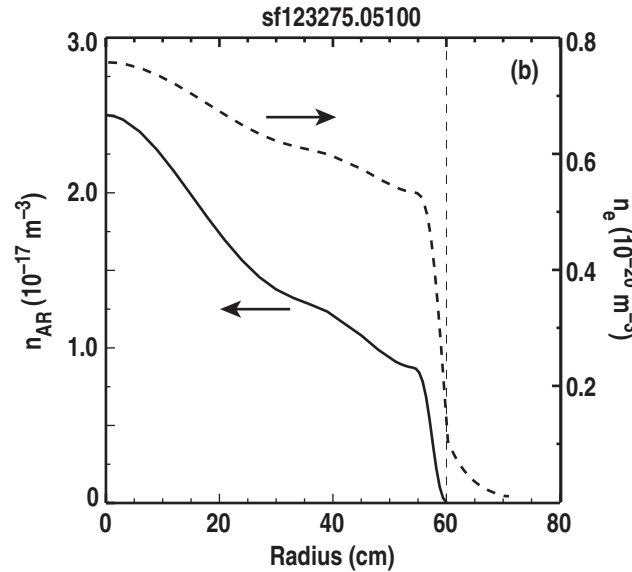
- Density profile slightly more peaked at higher Γ_{AR}
- Total stored energy unchanged



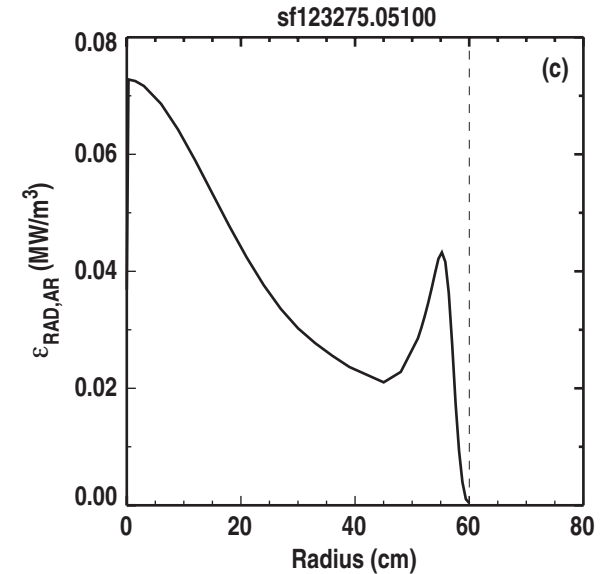
MIST Analysis for “High Γ_{AR} ” (case 3) Shows Important Features of Argon Behavior in the Main Plasma



Ar+16
state dominates
into outer
region of the
plasma, but does
not dominate near
the center



The argon profile
is more
peaked than
the background
electron density
profile



The emissivity profile
from argon is peaked
near the center and
near the edge

ARGON AT PERTURBING LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

The argon concentration was much higher near the outer divertor target than near the inner divertor target

An Alternative Method for Estimating the Relative Argon Concentration at the Inner and Outer Targets

$$\left(\begin{array}{l} \text{Argon flux at the} \\ \text{divertor target} \end{array} \right) \equiv \Phi_{\text{AR}} = \sigma \times I_{\text{ARII}} \times [S/X_B]$$

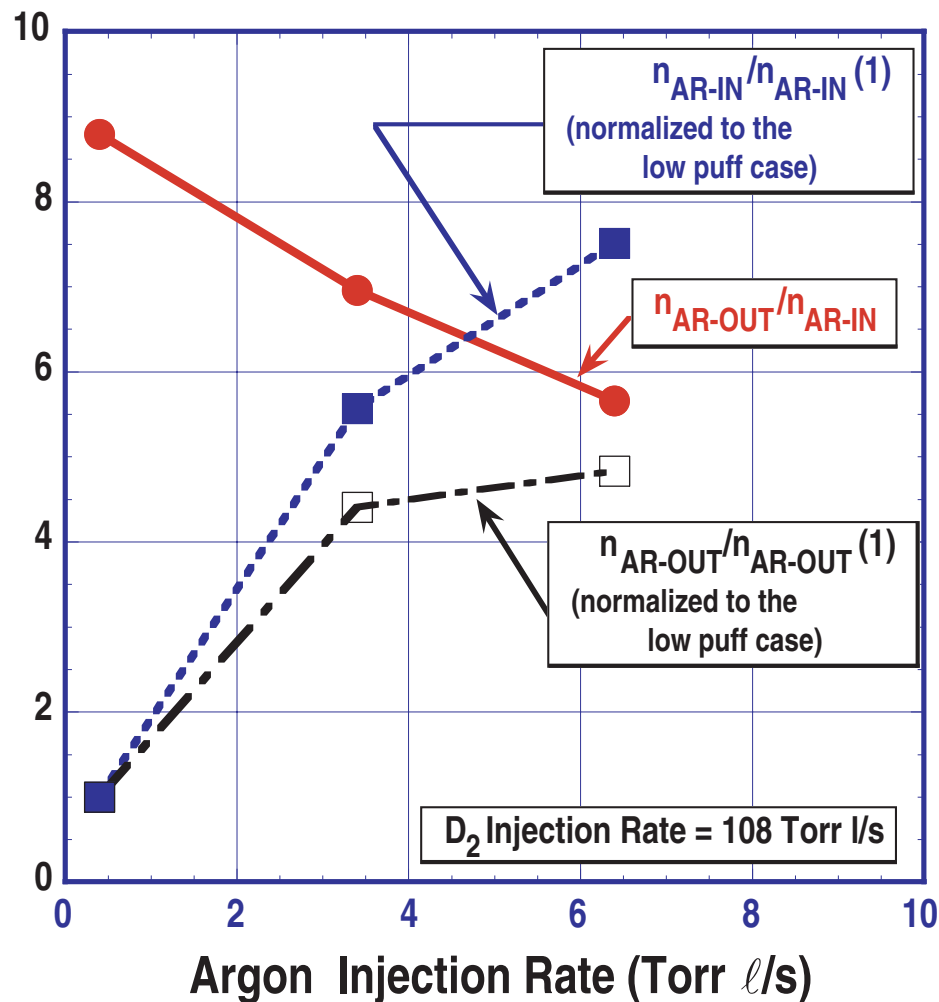
where σ is the ratio of the whole multiplex to measured line 434.8 nm
 I_{ARII} is the measured emission rate of ARII 434.8 nm
 S/X_B is the ratio of ionization to excitation rates computed from
a collisional radiative model [R.C. Isler, Nucl. Fusion 24 (1984) 1599]

Simple example:

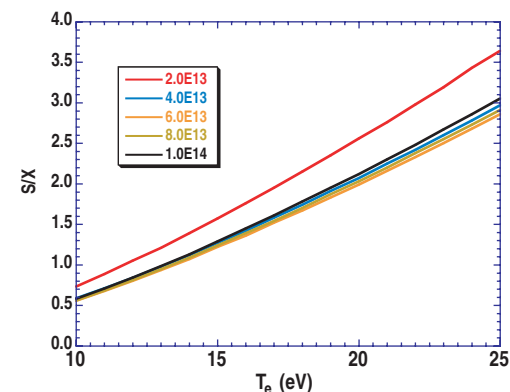
Because both T_e and n_e at the inner and outer targets were comparable at high Γ_{AR} (case 3):

$$\Phi_{\text{AR,OUT}}/\Phi_{\text{AR,IN}} \approx n_{\text{AR,OUT}}/n_{\text{AR,IN}} \approx I_{\text{ARII,OUT}}/I_{\text{ARII,IN}} \approx 6$$

The Argon Asymmetry Between the Inner and Outer Divertor Targets Decreased, as the Argon Injection Rate was Raised



- The argon density at the inner target grew more rapidly than the argon density at the outer target, as Γ_{AR} was raised
- Conditions favoring argon entrainment in the outer divertor evidently deteriorated, as Γ_{AR} was increased



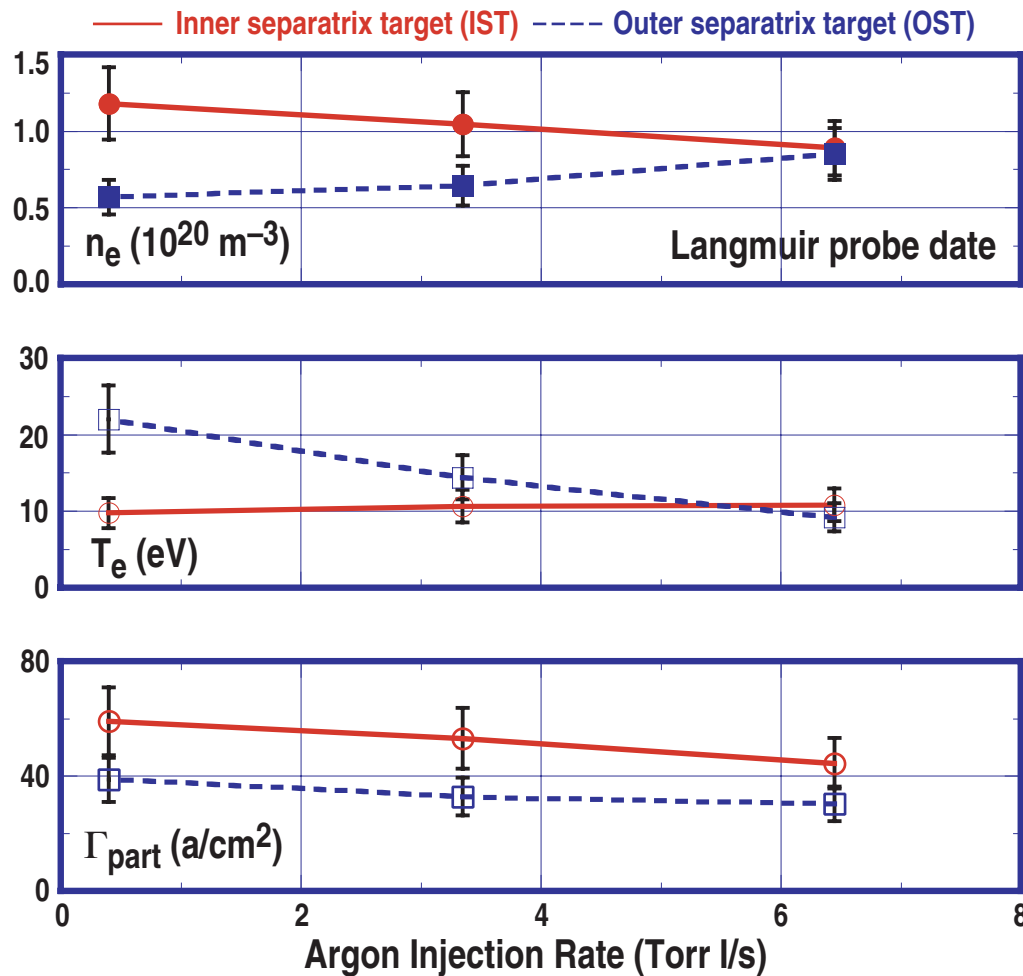
ARGON AT PERTURBING LEVELS

SINGLE-NULL *with* $B \times \nabla B$ DRIFT DOWN

**Carbon was the main
contributor to $P_{\text{RAD,DIV}}$**

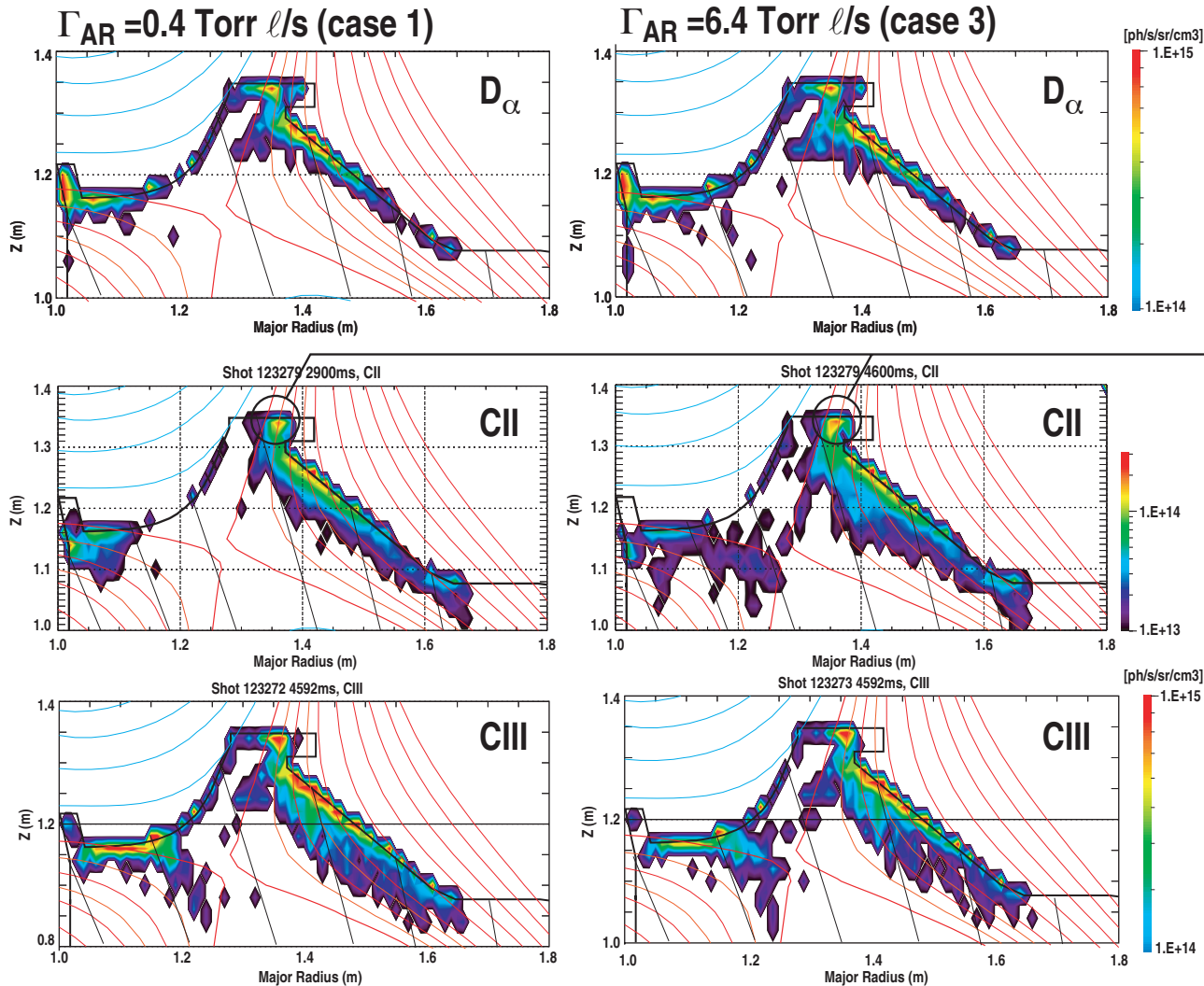
—divertor characterization—

Increasing the Argon Injection Rate Has its Most Pronounced Effect on the Electron Temperature at the Outer Divertor Separatrix Target



- n_e at the IST decreased $\approx 24\%$
- n_e at the OST increased $\approx 17\%$
- T_e at the IST was insensitive to the argon presence
- T_e at the OST decreased more than 2x
- Γ_{part} decreased 20-25% at both IST and OST

Adding Argon Had Little Effect on the Recycling (D_α) and CIII Distributions but Increased CII Radiation Localized Near the Outer Divertor Target



- D_α distribution in the outer divertor shows little change after argon is added
- Increase in CII radiation at the outer target post-argon injection
- Similar CIII distributions [CIII is a good indicator of the location of the dominant radiator CIV lines.]

Argon Was Not the Principal Radiator in Either the Divertor or the Main Plasma

- No direct measurement of the radiated power from argon, carbon, and deuterium
- “Trace” argon (i.e., Case 1) — Expect radiated power to be carbon-dominated
 - Little contribution to radiated power from argon
 - D_{α} radiation distribution is NOT consistent with bolometer data
 - CIII/CIV radiation distribution is consistent with bolometer data
- Perturbing argon (i.e., Case 3) — Expect radiated power to still be carbon dominated
 - CIII/CIV radiation distribution consistent with bolometer data
 - 50% increase in CII signal at the outer divertor target may in part be due to sputtering of the graphite tiles by argon \Rightarrow increase in radiated power at the target likely due to a combination of argon and sputtered carbon
 - *If* the entire increase in divertor radiation between case 1 and case 3 was due to argon, the upper limit of the argon contribution to total divertor radiation in case 3 would be ~ 0.29

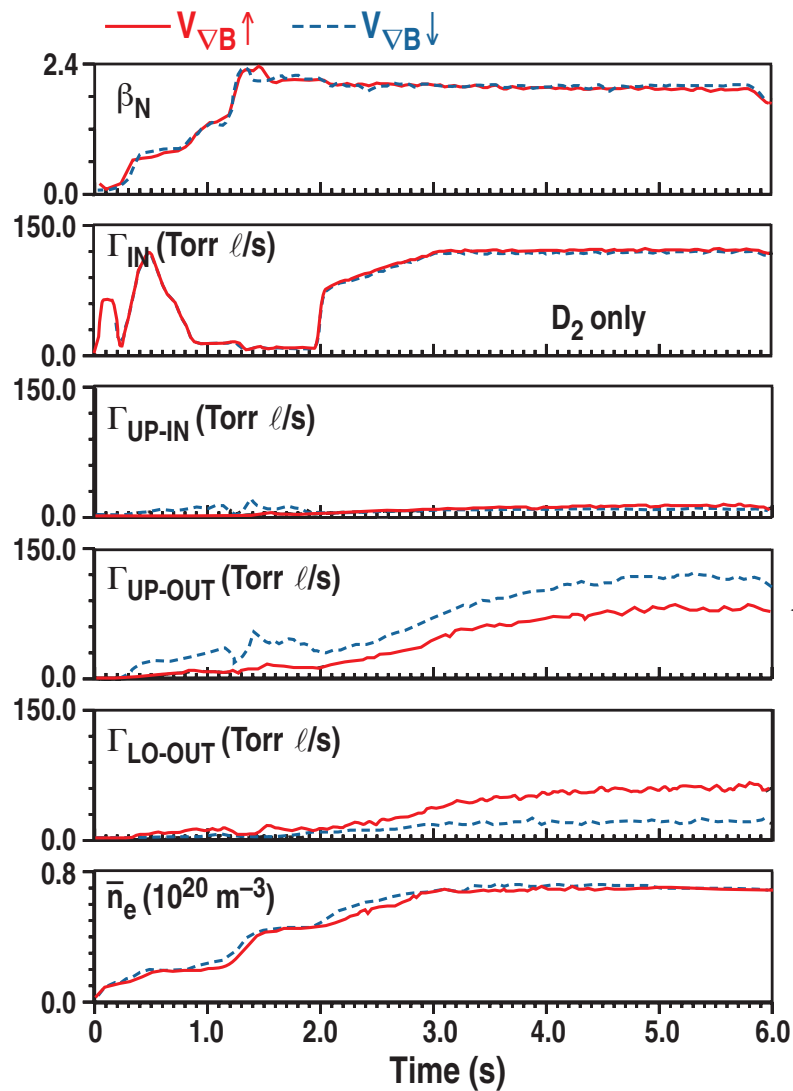
-Recent Data-

SINGLE-NULL vs DOUBLE-NULL

$B \times \nabla B$ DRIFT DOWN

- Argon entered the main plasma more rapidly in DNs
- DNs did not tolerate the higher Γ_{Ar} that SNs did

The Modified Pumping Configuration Enhances the Feasibility of “Puff-and-Pump” Experiments in High- δ Double-null Plasmas



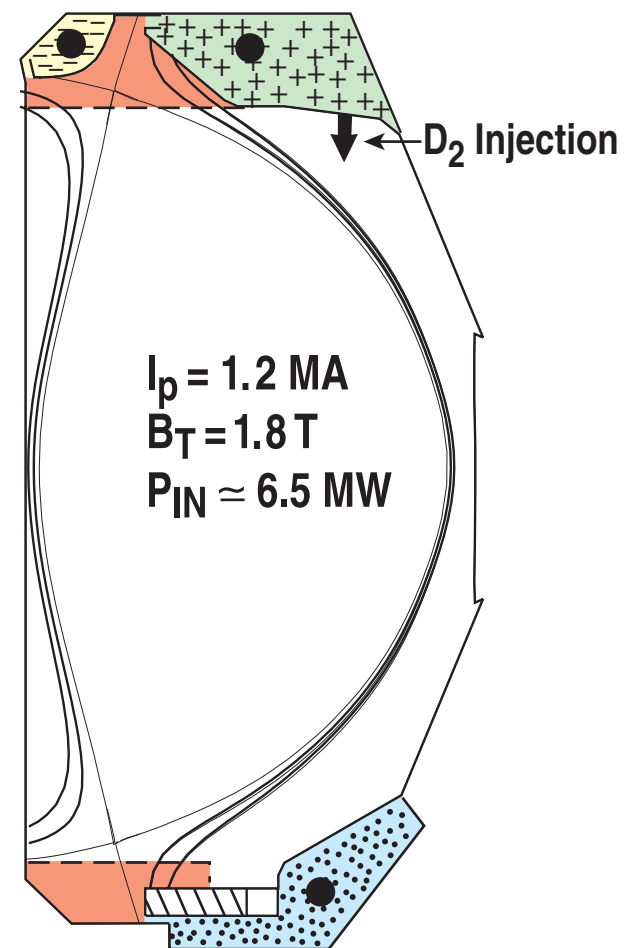
Feedback on B_N

Comparable fueling rate

<8% particle removal

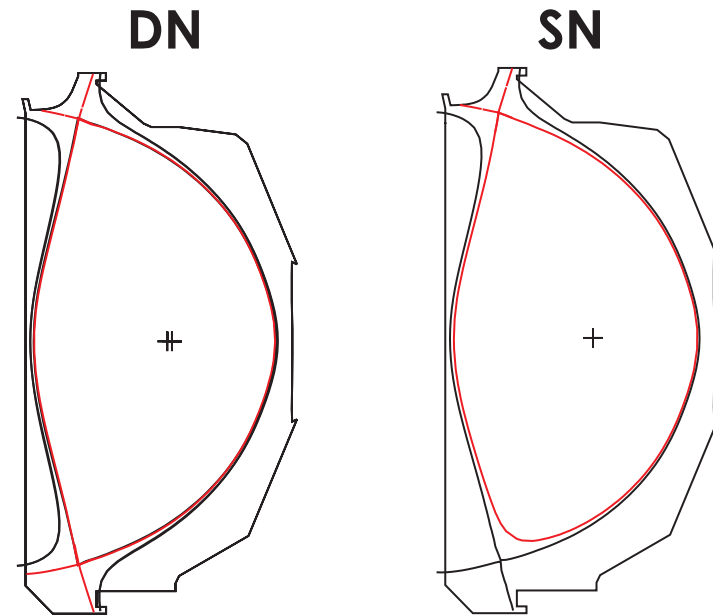
Outer pumps compensate for each other

Comparable final density



– Trace Argon Injection – Argon Accumulation in the DN was Much More Pronounced than in the SN Where $B \times \nabla B$ is Down

	DN	SN
dRsep (cm)	0.0	+1.0
Γ_{AR} (Torr ℓ/s)	0.17	0.17
Γ_{D2} (Torr ℓ/s)	108	108
P_{INJ} (MW)	6.5	6.5
V_{ELM} (Hz)	≈ 130	≈ 130
\bar{n}_e (10^{20} m^{-3})	0.7	0.6
n_{AR}	0.72	0.46

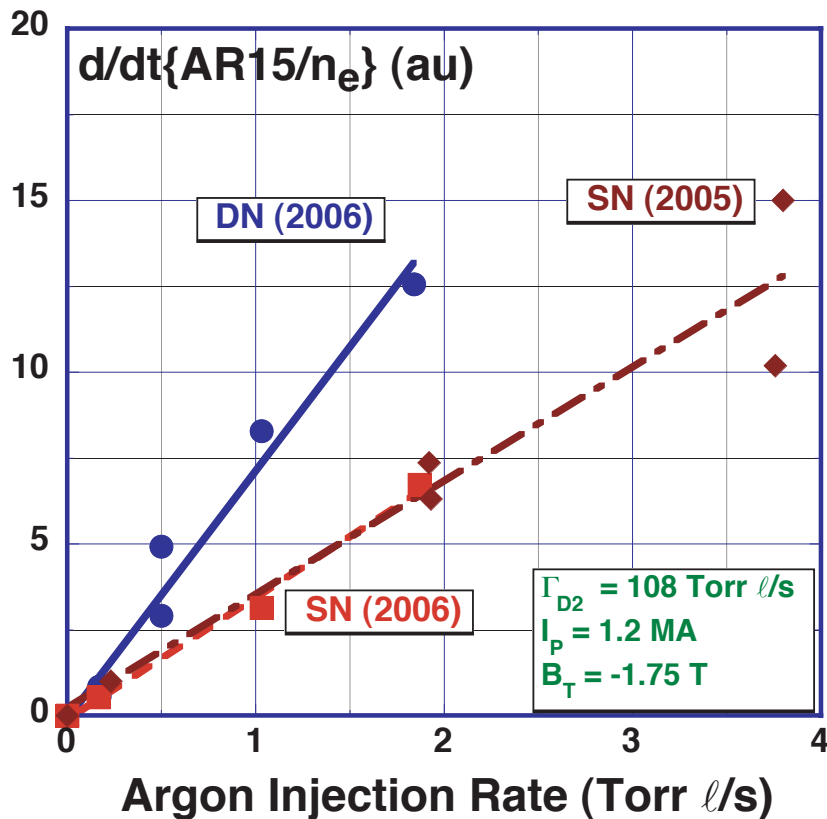


- All three pumps are operational
- D_2 and argon are injected from the midplane and from the upper private flux region, respectively

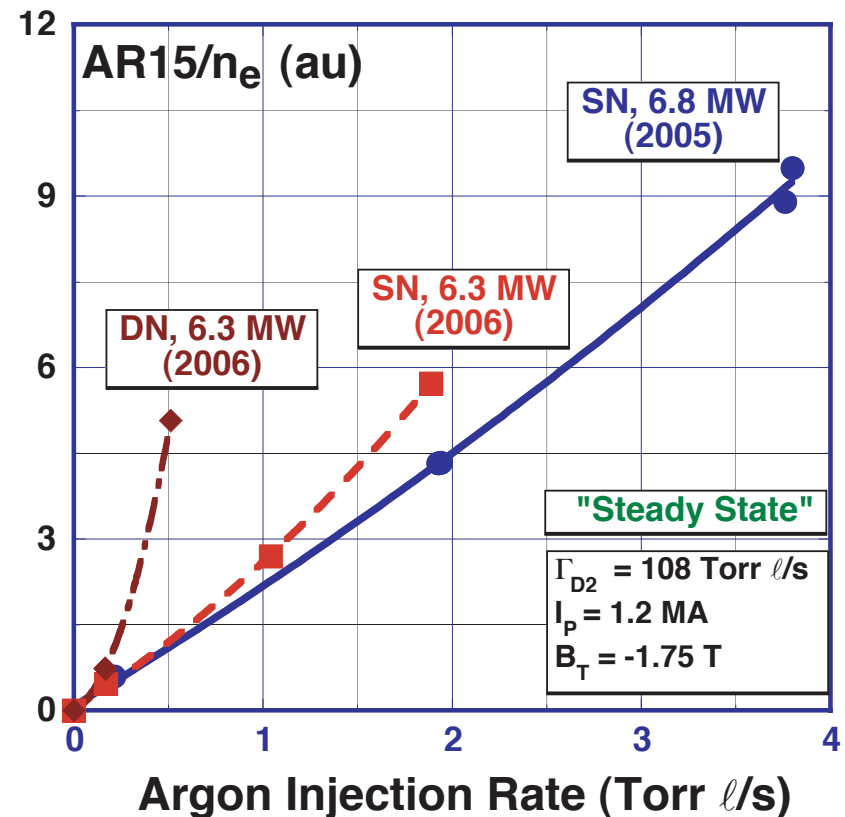
— For a given argon injection rate and $B \times \nabla B$ is down —

Argon Initially Accumulates Faster in DN than SN and Reaches Higher Steady State Values

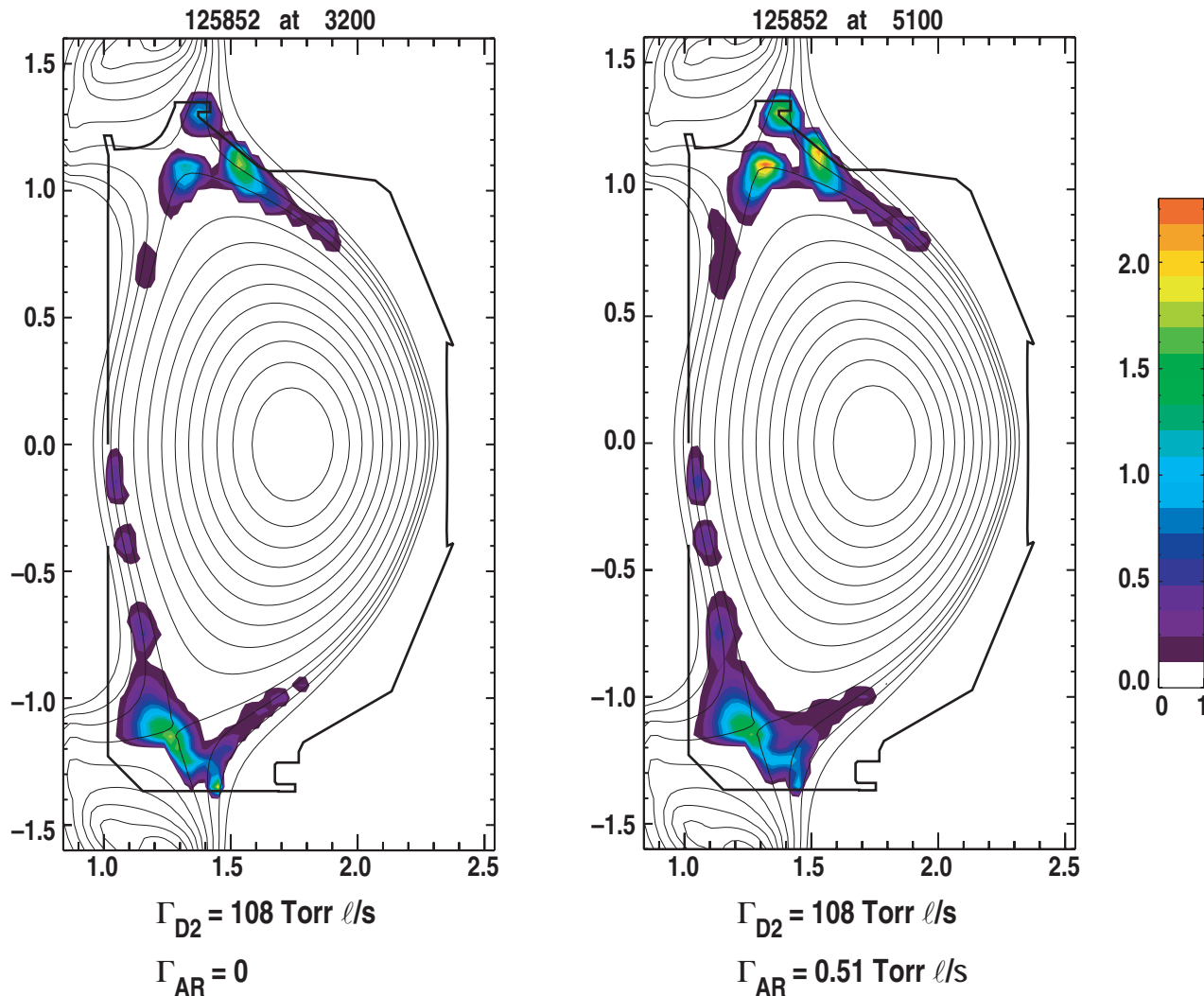
The initial rate at which argon accumulates in a DN is $\approx 2x$ that of a SN, given the same Γ_{AR} and Γ_{D2}



Argon accumulates in DNs to a much higher steady state value than in SNs, given the same Γ_{AR} and Γ_{D2}



The Argon Injection Increased Radiated Power Much More in the Upper Divertor Than in the Lower Divertor In the DN Configuration Where $B_x \nabla B$ is Down

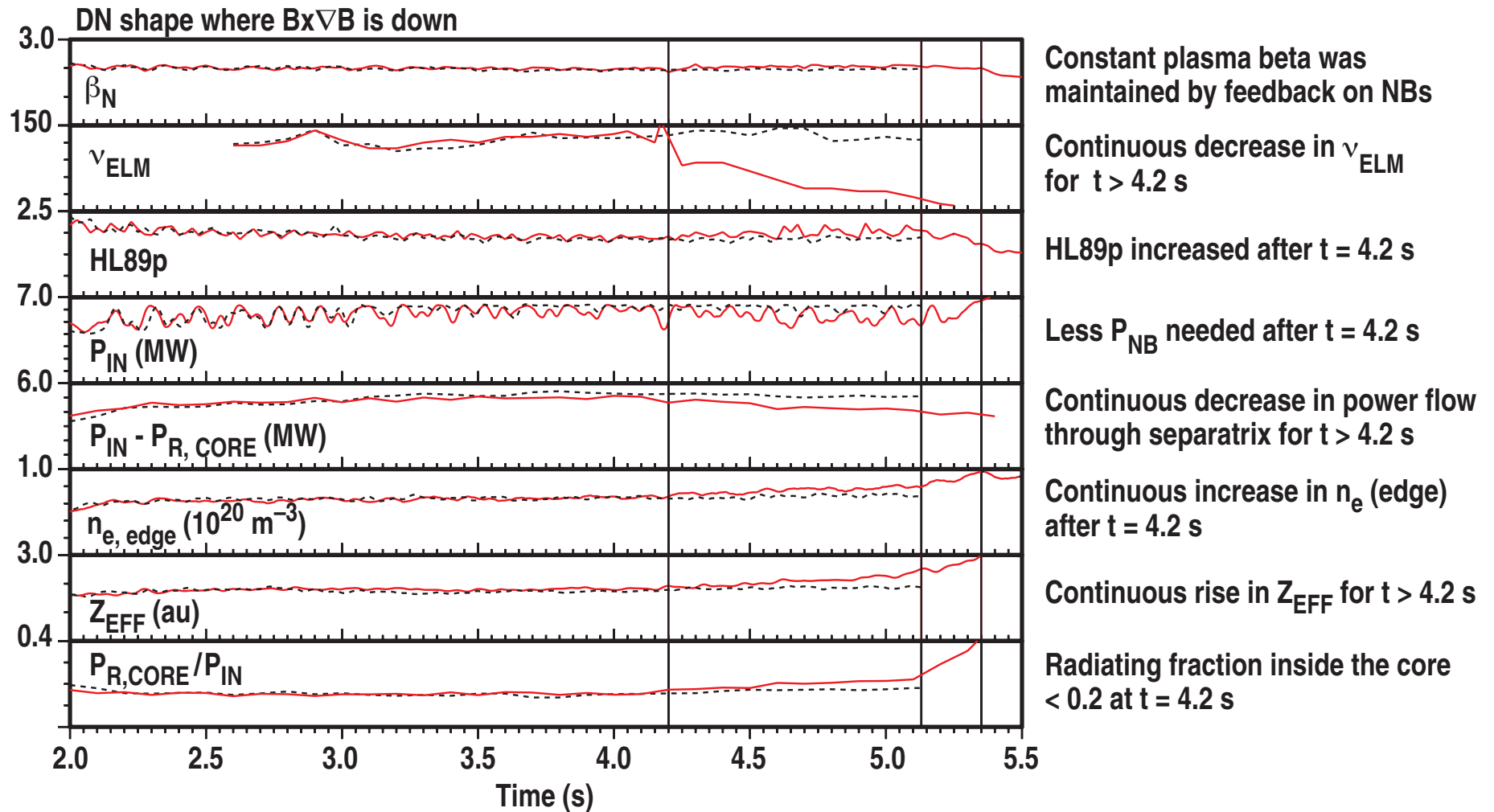


Γ_{AR} (tl/s)	0	0.51
P_{INPUT} (MW)	6.0	6.1
$P_{R, CORE}$ (MW)	0.85	1.09
$P_{R, SOL}$ (MW)	0.20	0.42
$P_{R, UP, DIV}$ (MW)	0.67	0.99
$P_{R, LO, DIV}$ (MW)	0.70	0.75

Note: Argon was injected into the upper divertor

Decreased ELMing Activity Triggered Processes Leading to the Eventual Loss of H-Mode During Puff-and-Pump Operation

Dashed line \Rightarrow stable puff-and-pump Solid line \Rightarrow "identical" but unstable puff-and-pump



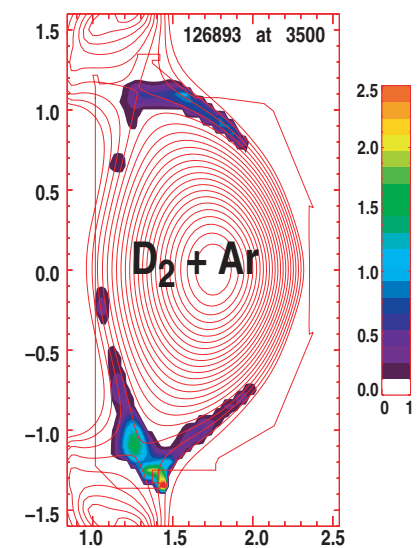
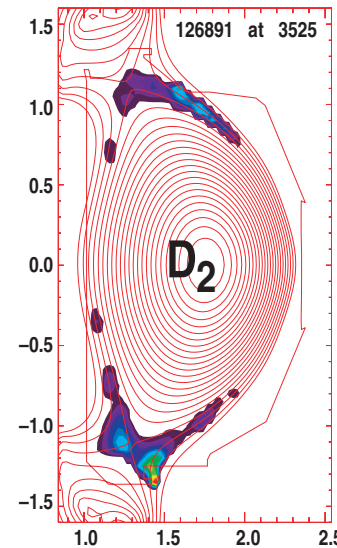
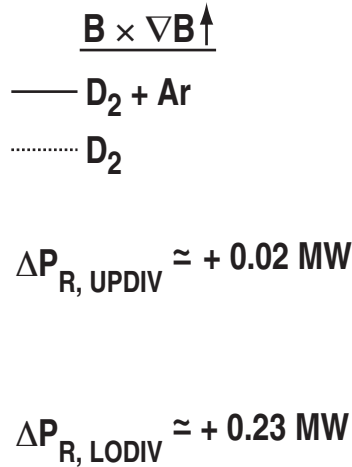
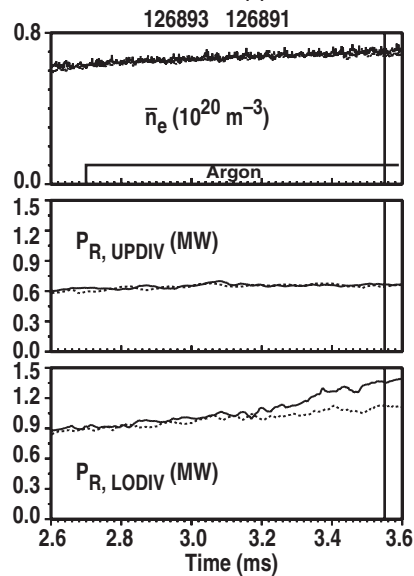
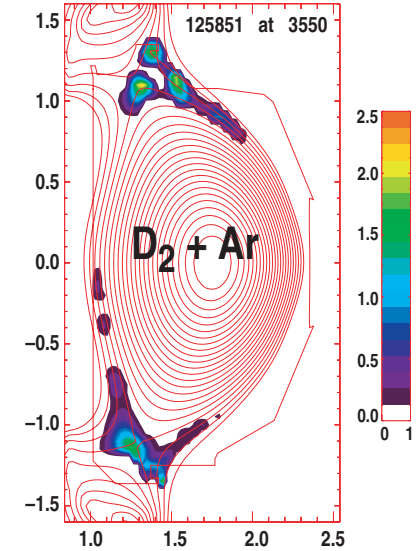
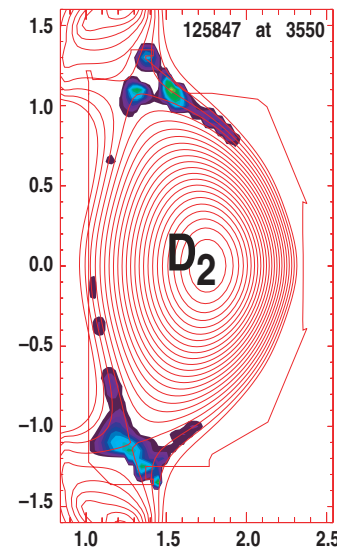
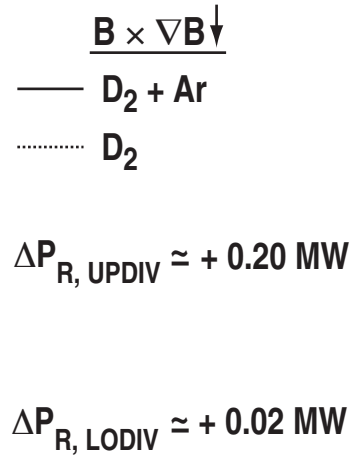
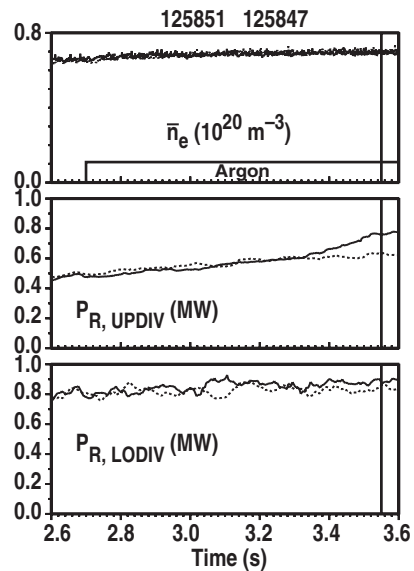
-Recent Data-

SINGLE-NULL vs DOUBLE-NULL

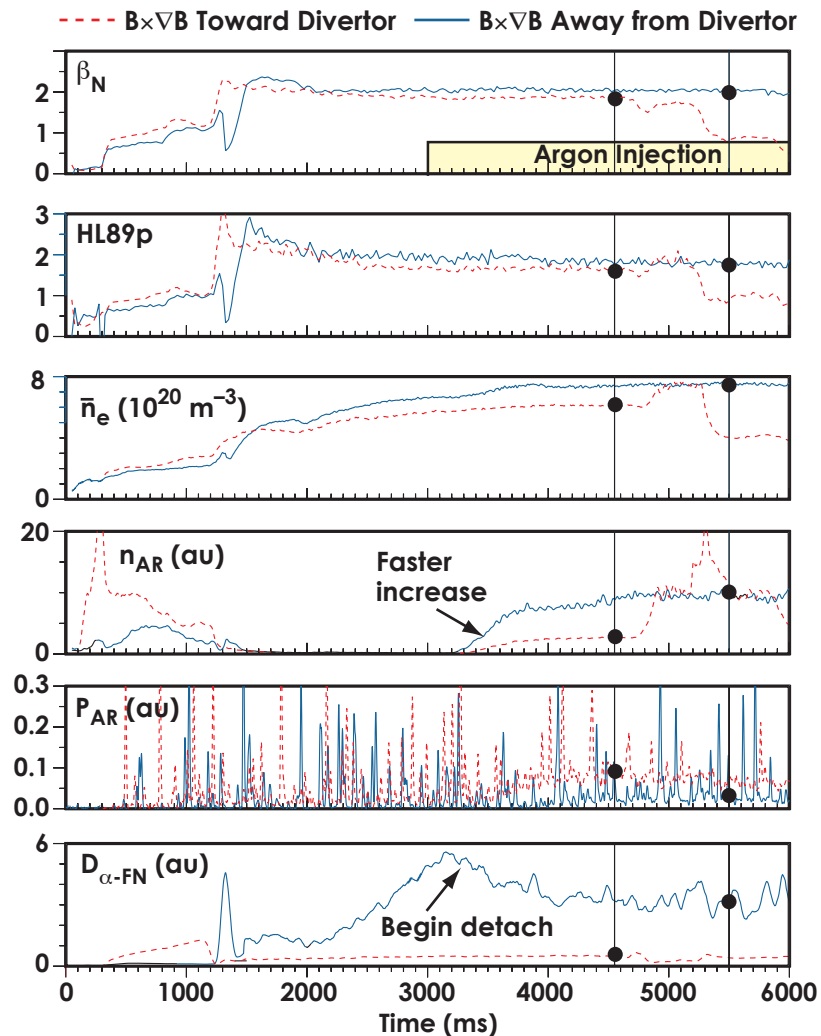
$B \times \nabla B$ DRIFT DOWN and UP

- The distribution of the radiated power and the argon containment in the divertor changed when the $B \times \nabla B$ drift direction changed

Measureable Increases in Radiated Power Were Observed First in the Divertor OPPOSITE the $B \times \nabla B$ Ion Drift Direction in DN



– Upper Single Null Divertor Case – Argon Escapes Much More Quickly from the Divertor Region and Reaches a Higher Steady State Concentration in the Core when the $B \times \nabla B$ Ion Drift is Toward the Divertor



$$\Gamma_{AR} = 0.85\text{--}1.00 \text{ Torr } \ell/s$$

$$\Gamma_{D2} = 108 \text{ Torr } \ell/s$$

Feedback on β_N with neutral beams

$$HL89p \approx 1.7\text{--}1.9$$

Line-averaged density was steady
at the two times of interest

“ n_{AR} ” was 2–3 \times greater in the
“ $B \times \nabla B$ toward the divertor” case

The argon pressure in the upper baffle
was much lower in the “ $B \times \nabla B$ toward” case

Upper inner divertor in the “ $B \times \nabla B$ toward”
case showed evidence of detaching shortly
after argon injection started

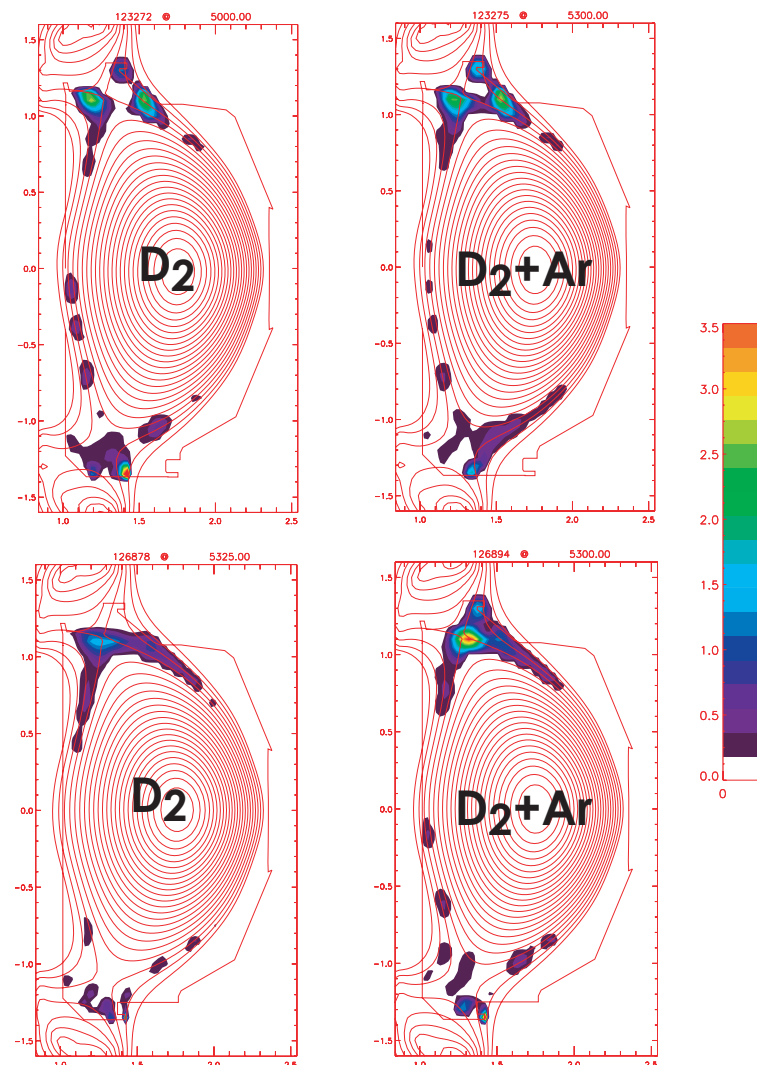
The Emissivity Distribution in the Divertor of SN Plasmas Changed Markedly When the $B_x \nabla B$ Ion Direction was Reversed

$B_x \nabla B$ toward lower divertor

- Three main radiating regions in the divertor were observed
- Outer divertor target region was most affected by argon injection

$B_x \nabla B$ toward upper divertor

- One main region of emissivity lay near the X-point during D_2 phase
- Radiated power from the X-point region continued to be dominant during argon injection



DISCUSSION

Discussion

Heat flux reduction in SNs ($B \times \nabla B \downarrow$)

- $q_{P,OUT}$ was reduced $\approx 2.5X$ between case 1 and case 3, but $q_{P,IN}$ by only $\approx 20\%$
- Greater increase in ϵ_{RAD} near the outer divertor target than near the inner induces this “asymmetry”
- Greater concentration of argon near the outer divertor target induces greater change in ϵ_{RAD}

Argon asymmetry at the divertor targets in SNs ($B \times \nabla B \downarrow$)

Several factors may have contributed to the asymmetric argon distribution between divertors

- Geometry: The argon source was located in the PFR near the outer divertor target and was adjacent to a major sink for the argon, i.e., the entrance to the outer baffle pumping plenum. For argon neutrals, direct flight across the PFR from the outer divertor target to the inner was blocked by the dome over the inner cryopump
- Particle drifts: The *ionized* argon in the PFR near the separatrices would be preferentially dragged from the inner target toward the outer divertor target by $E_R \times B$ -induced ionic flow across the PFR
- Induced D_2 flows in the SOL: Leakage of argon out of the closed outer divertor was impeded by the enhanced deuterium flow in the SOL directed into that divertor.
- Additional pumping: Argon that *does* make it to the inner target can be exhausted by the dome cryopump.

Discussion (continued)

Argon accumulation in the main plasma of SNs ($B \times \nabla B \downarrow$)

- n_{AR} was almost linear with Γ_{AR}
 - => $n_{AR} \propto \Gamma_{AR} - \Gamma_L(v_{ELM})$, where $\Gamma_L(v_{ELM})$ is the time-averaged argon losses during ELMs
 - If $\Gamma_L(v_{ELM})$ is constant as Γ_{AR} increases, n_{AR} is linear with Γ_{AR}
 - As more argon accumulates in the main plasma, $P_{RAD,MAIN}$ increases $\rightarrow v_{ELM}$ decreases [(i.e., $H \approx 80$ Hz (case 1) to $H \approx 70$ Hz (case 3))] $\rightarrow \Gamma_L(v_{ELM})$ decreases $\rightarrow n_{AR}$ rises faster than linear in Γ_{AR}
- The 3/2 NTM did not prevent the n_{AR} -profile from becoming more peaked than the n_e -profile. Even so, $\epsilon_{RAD}(\rho)$ was not peaked on axis and there was no observed degradation in τ_E

Comparison of two radiating divertor conditions in SNs

The above results can be compared with those from a previous, well-documented DIII-D puff-and-pump experiment, where argon was injected into the PFR of a standard ELMing H-mode plasma (Wade *et al.*)

- *Similarities:* I_p , B_T , q_{95} , and line-averaged density
- *Differences:* (1) No dome structure in the PFR and the divertor was more “open,” (2) the particle pumping was done only at the outer divertor target, and (3) the $E_R \times B$ -induced ion particle flow across the PFR was directed *toward* the inner divertor target
- *Trace argon:* $\eta_{exh}(Wade)$ was only $\approx 50\%$ of that reported here, even though Γ_{D2} was higher in Wade
- *Perturbing argon:* (1) inner divertor leg “detached” and (2) $\eta_{exh}(Wade)$ degraded significantly with Γ_{AR}

Discussion (continued)

Double-null vs single-null shapes ($Bx\nabla B\downarrow$)

- Argon penetrates DN much faster than it does for SN
- Expected: D2 fuelling in DN more efficient than SN \Rightarrow likely similar result for argon injection
 - Narrower SOL for DN on inboard side
 - Quiescent SOL for DN on inboard side (no ELMing)
 - Detached lower inner leg in DN

$Bx\nabla B\downarrow$ vs $Bx\nabla B\uparrow$

- Single-null: argon escapes divertor much more readily when $Bx\nabla B$ is toward the divertor
 - Inner divertor leg detaches more easily in $Bx\nabla B\uparrow$
 - Argon escape is easier with detached inner divertor leg
- Double-null: The increase in radiated power due to argon was stronger in the divertor opposite the $Bx\nabla B$ drift direction
 - Argon is not well contained in the upper divertor when $Bx\nabla B\uparrow$
 - Strong evidence that particle drifts are important in DN puff and pump experiments
 - Results suggest it will be difficult to achieve equal radiated power in both divertor

PRELIMINARY
CONCLUSIONS

The Radiating Divertor Concept Shows Compatibility with Hybrid Regime Operation Under Certain Conditions

$B \times \nabla B \uparrow$ direction

- The puff and pump approach in SN was effective in reducing peak power loading at the outer divertor target but much less so at the inner target
- Argon presence was MUCH stronger in the outer divertor of the SN, possibly explaining why heat flux reduction was much stronger at the outer divertor target
- $\eta_{EXH} \propto \Gamma_{D2}$ at trace argon levels, in SNs and was weakly dependent on Γ_{AR} at fixed Γ_{D2}
- Argon accumulated in DNs at a much faster rate than in SNs, given the same Γ_{AR}

$B \times \nabla B \uparrow$ and $B \times \nabla B \downarrow$ directions

- Argon escapes to divertor more readily in SNs with $B \times \nabla B$ toward the divertor
- The increase in $P_{RAD, DIV}$ due to argon for DNs was stronger in the divertor opposite the $B \times \nabla B$ drift direction \rightarrow difficulty in achieving equal radiated power in both divertors