

# Recent Advances in the Theory and Simulation Of Pellet Ablation and Fast Fuel Relocation In Tokamaks

P.B. Parks,<sup>1</sup> L.R. Baylor,<sup>2</sup> R. Ishizaki,<sup>3</sup> S.C. Jardin,<sup>4</sup> and R. Samtaney<sup>4</sup>

<sup>1</sup>General Atomics, P.O. Box 85608, San Diego, California 92186-5608, USA

<sup>2</sup>Oak Ridge National Laboratory, Oak Ridge, Tennessee 37381, USA

<sup>3</sup>National Institute for Fusion Science, Toki, Japan

<sup>4</sup>Princeton Plasma Physics Laboratory, Princeton, New Jersey

20th IAEA Fusion Energy Conference  
Vilamoura, Portugal  
November 1–6, 2004



IAEA 2004



# Outline of Topics

---

- Pellet Ablation

- New 2-D Eulerian code **CAP** treats multi-phase pellet-cloud dynamics. [Phys of Plasmas **11**, 4064 (2004)]. Magnetic field interaction now partially included.
- Ionized cloud pushes B-field away forming a diamagnetic cocoon around pellet. Diverts plasma energy flux around pellet, prolonging its lifetime.

- $\nabla B$  induced cloud drift using **PRL** code (GA-A24807 submitted to Phys Rev Lett)

- Included **plasma pressure profile variations** on drifting cloudlet
- Showed that the  **$M \sim 1$  parallel ablation flow** furthers cloudlet penetration
- Elucidated the effect of **rotational transform** on cloudlet drift
- Discovered how **magnetic shear** causes cloudlet “mass shedding” and dispersal
- Generalized theory to include arbitrary poloidal angle of pellet entry

- 3-D MHD simulations of  $\nabla B$  cloud drift using Adaptive Mesh Reduction code **AMR**

- Preliminary results verify that pellet cloud drifts in large- $R$  direction

# CAP code: Numerical Approach and Assumptions

---

## ● Geometry

- Axisymmetric cylindrical coordinates  $(r, \theta, z)$  with  $\theta$  ignorable, and background (undisturbed) magnetic field  $B_\infty$  parallel to  $z$  axis.
- Magnetic field  $\rightarrow B_r, B_z$ , flow velocity  $\rightarrow v_r, v_z$ , current  $J_\theta$ , electric field  $E_\theta$

## ● Rectangular $(r,z)$ Computational Box

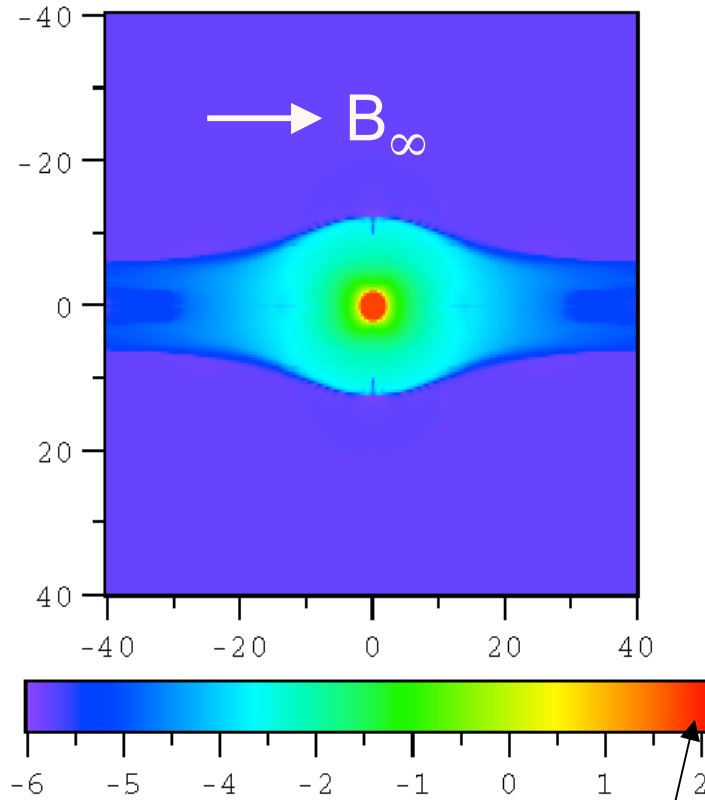
- Ideally conducting wall boundary at  $r_{\text{wall}} \approx 20 r_{\text{pell}}$
- Reflecting (outflow) boundary conditions at end faces  $z_{\text{end}} \approx \pm 20 r_{\text{pell}}$

## ● Some Physical Assumptions Made:

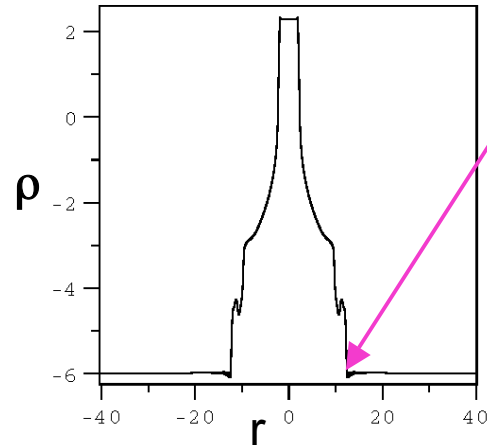
- Solve magnetic flux equation with simple Ohms law,  $E_\theta = -v \times B + J_\theta / \sigma_\perp$ .
- Use step-function heat flux to pellet (realistic pellet entry has gradual increase).
- Artificially high electrical resistivity  $\eta_\infty$  in background plasma is needed to eliminate significant currents and  $J \times B$  forces, which are “continually erased” by fast magnetosonic adjustments on the slow cloud evolution time scale.

# Magnetic Field Force Limits Transverse Cloud Dimension

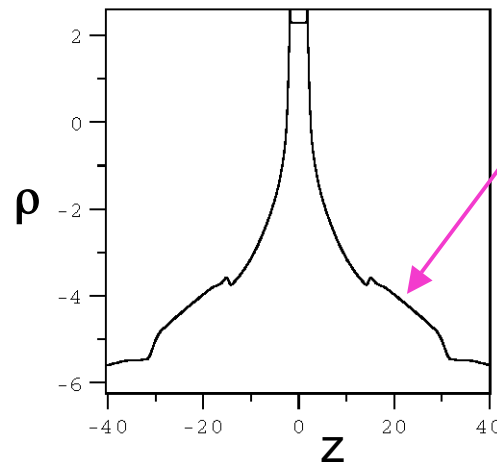
Density  $\rho$  Contours  $\log_{10} \text{ kg/m}^3$   
at  $0.4 \mu\text{s}$



Pellet density  $200 \text{ kg/m}^3$



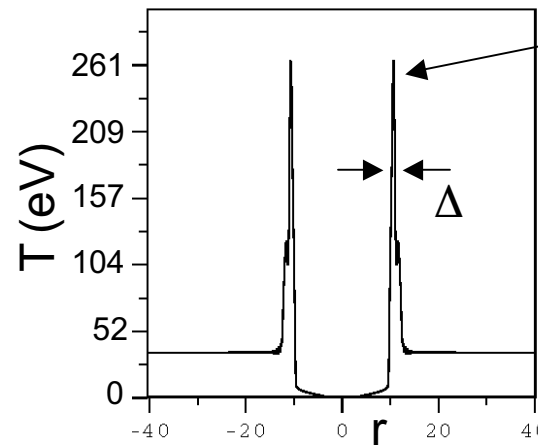
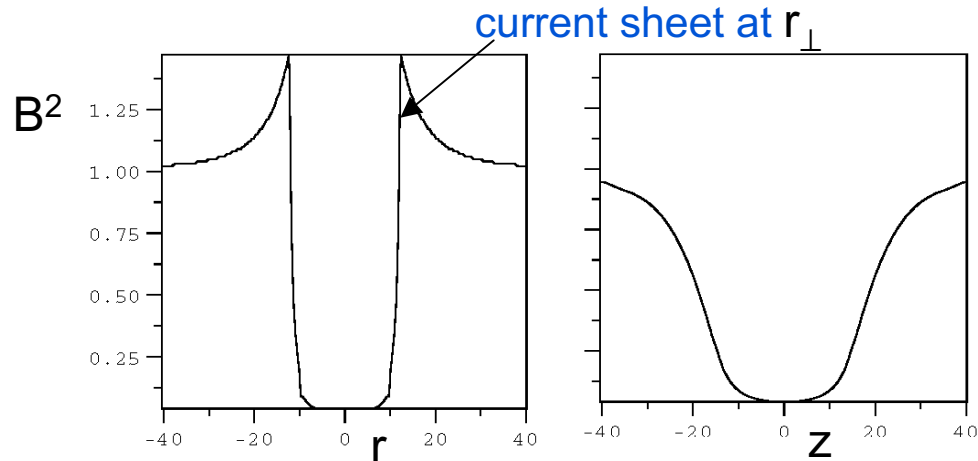
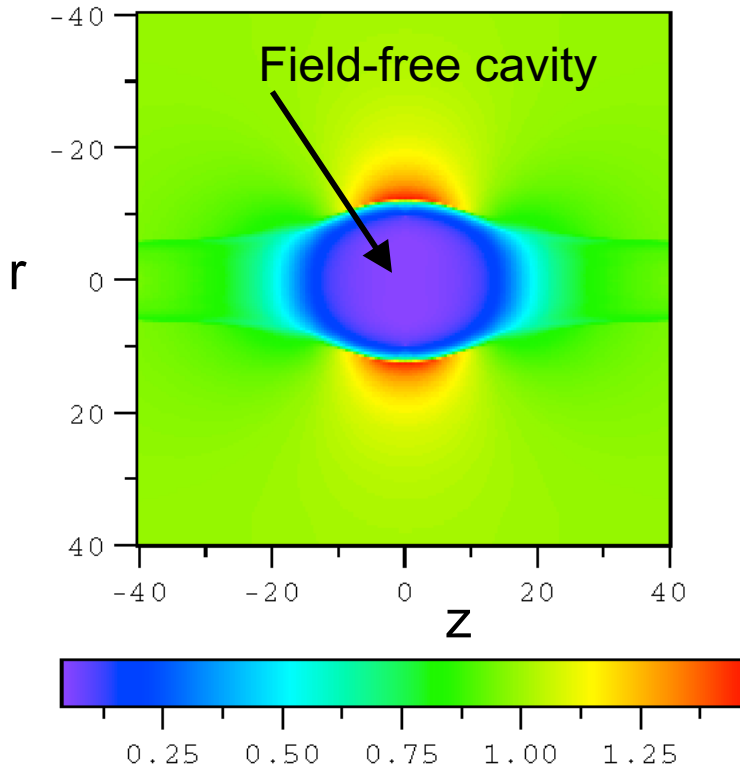
Transverse expansion  
of cloud limited to  $r_\perp =$   
10 mm ( $5 r_{\text{pell}}$ ) by  $\mathbf{J} \times \mathbf{B}$   
force.



Parallel expansion  
is free, but not yet  
fully developed  
after only  $0.4 \mu\text{s}$

# $\beta \sim 1$ Diamagnetic Cavity Can Divert Heat Flux Around Pellet

Contours of  $B^2$  at  $0.4 \mu\text{s}$



**Hot ring** and **current sheet** formed as rarefied ablation front is compressed against magnetic field by impact with the dense flow behind front.

**Hot ring** can potentially maintain field-free cavity over the long skin time  $\tau_{\text{skin}} = \mu_0 \sigma_{\perp} \Delta r_{\perp} \sim 60 \mu\text{s} > r_{\perp} / v \sim 1 \mu\text{s}$ . **Distorted field lines can potentially divert heat flux around pellet, reducing ablation rate.**

# Basic Ingredients of $\nabla B$ Cloud Drift & Fast Fuel Relocation Model

- Ordering and scales

- **Cloudlet** is like a strongly localized cylindrical **pressure perturbation**

$$\nabla_{\perp} \sim 1/r_c \ll 1/R, 1/a, \quad \delta \equiv r_c/qL(t) \sim v_c/qc_s \ll 1 \quad (\text{key expansion parameter})$$

$v_c = E/B$  drift velocity  $\sim 10^3\text{--}10^4$  m/s,  $c_s =$  cloudlet sound speed  $\sim 10^4\text{--}10^5$  m/s,

- Transverse force balance (no fast time-scale magnetosonic waves  $v_c \ll c_{A\infty}$ )

$$0 \equiv \nabla_{\perp}(\delta p + B_{\infty}\delta B/\mu_0) + O(r_c/R) \quad \longrightarrow \quad \delta p = -B_{\infty}\delta B/\mu_0$$

$$\delta p = p_c - p_{\infty} \quad p_c = \text{cloud pressure, "}\infty\text{"} = \text{ambient plasma quantity}$$

“excess pressure” is  
source of curvature drive

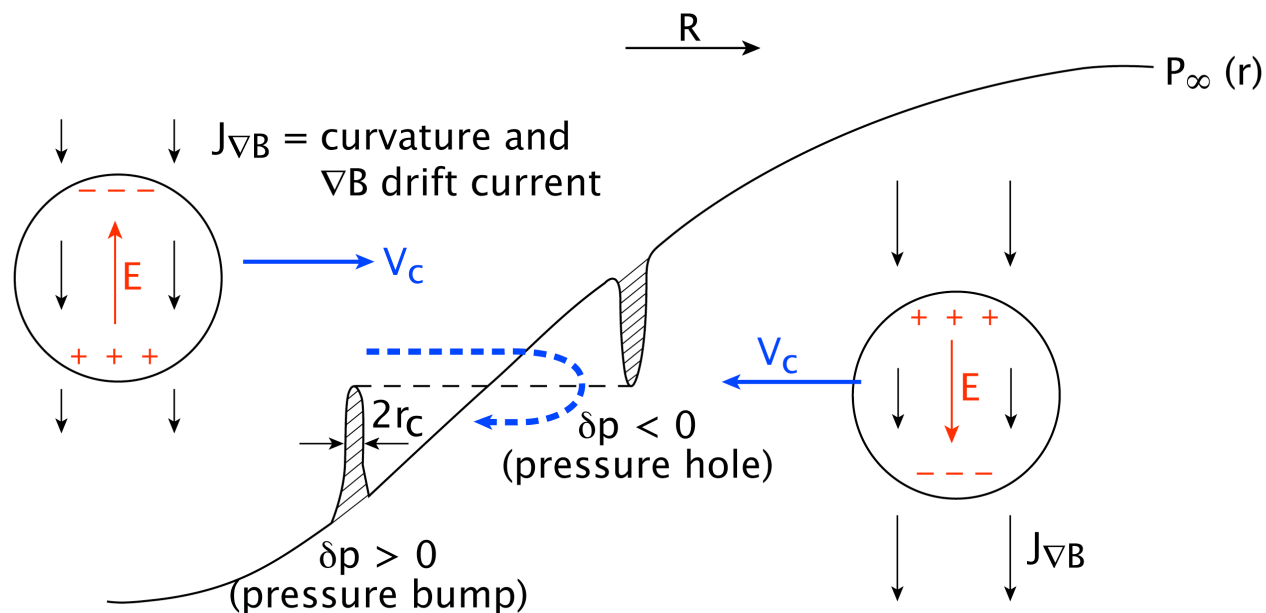
- Parallel expansion flows relax pressure perturbation  $\delta p$

- **Pressure Relaxation Lagrangian (PRL)** code (Parks, PoP 2000)

- End boundary condition applied on a drifting cloudlet

$$p_c(z = L) = p_{\infty}(\rho = \rho_c) \quad \rho_c(t) = \text{minor radius of cloud centroid}$$

# Pressure Profile Variation Works Against Penetration



- A local positive **pressure bump** ( $\delta p > 0$ ) is necessary to start the inward drift  $V_c$ . In doing so the pressure bump could change to a **pressure hole** ( $\delta p < 0$ ), causing drift reversal. **Pellet penetration well past edge pedestal region seems to be necessary for good cloud penetration.**

# Beginning Point: Perturbed Parallel Vorticity Equation

- Evolution of plasma vorticity [Hazeltine, 1992]

$$\frac{\hat{b}}{B} \cdot \nabla \times mn \frac{d\vec{v}}{dt} = (\vec{B} \cdot \nabla) \frac{J_{\parallel}}{B} - \frac{(\hat{b} \times \vec{\kappa}) \cdot \nabla_{\perp} B^2}{\mu_0 B}$$

where  $\hat{b} = \vec{B}/B$ ,  $\kappa = \hat{b} \cdot \nabla \hat{b}$  (curvature),  $B^2 = B_{\infty}^2 + 2B_{\infty} \delta B$ ,  $J_{\parallel} = J_{\parallel\infty} + \delta J_{\parallel}$ .

- Perturbed result with substitution  $-2\delta p = 2B_{\infty} \delta B / \mu_0$

$$\frac{\hat{b}}{B} \cdot \nabla \times mn \frac{d\vec{v}}{dt} = (\vec{B} \cdot \nabla) \frac{\delta J_{\parallel}}{B} + \frac{2(\hat{b} \times \vec{\kappa}) \cdot \nabla_{\perp} \delta p}{B}$$

(Inertial Forces)      (Alfven Waves)      (Curvature Drive)

- Inertial term becomes **exactly** **Coriolis force** **Centrifugal force**

$$\frac{d\vec{v}}{dt} = \hat{b} \left( \frac{\partial v_{\parallel}}{\partial t} + v_{\parallel} \frac{\partial v_{\parallel}}{\partial s} + \vec{v}_{\perp} \cdot \nabla v_{\parallel} - v_{\parallel} \vec{\kappa} \cdot \vec{v}_{\perp} \right) + v_{\parallel} (\nabla \times \hat{b})_{\parallel} \hat{b} \times \vec{v}_{\perp} - v_{\parallel} \hat{b} \times \nabla \times \vec{v}_{\perp} + v_{\parallel}^2 \vec{\kappa} + \frac{D\vec{v}_{\perp}}{Dt}$$

$\frac{\hat{b}}{B} \cdot \nabla \times mn(\quad) \rightarrow O(\delta) \text{ neglect}$

$= \frac{\partial}{\partial t} + \vec{v}_{\perp} \cdot \nabla$



# Vorticity Equation Yields Electrostatic Potential $\Phi$ and Cross-Field Cloud and Plasma Drifts Near Cloud

$$\vec{v}_\perp = \hat{b} \times \frac{\nabla \Phi}{B} \longrightarrow \nabla_\perp \cdot \left( \frac{mn}{B^2} \frac{D \nabla_\perp \Phi}{Dt} \right) = (\vec{B} \cdot \nabla) \frac{\delta J_\parallel}{B} + \frac{(\hat{b} \times \vec{\kappa}) \cdot \nabla_\perp (2\delta p + mn v_\parallel^2)}{B}$$

Centrifugal force driving term operates, even after  $\delta p \rightarrow 0$

- Tokamak coordinate system  $(\rho, \chi, \phi)$  for poloidal plane  $(\rho, \chi)$  variations

$$\hat{b} \times \vec{\kappa} = -(\hat{\chi} \cos \chi + \hat{\rho} \sin \chi) / R$$

- Helical magnetic-field-line-following (MFLF) coordinate system  $(x, y)$  or  $(r, \vartheta)$  for local cloud variables:  $\nabla_\perp (2\delta p + mn v_\parallel^2) = \partial / \partial r (2\delta p + mn v_\parallel^2) \hat{r}$

$$\longrightarrow (\hat{b} \times \vec{\kappa}) \cdot \hat{r} = \frac{-1}{R} (\cos \chi \sin \vartheta + \sin \chi \cos \vartheta)$$

$$\chi(z, t) = \chi_0 + \int_0^t \frac{v_\chi(t')}{\rho(t')} dt' \pm \frac{z}{qR}$$

$$\longrightarrow = \chi_c(t)$$

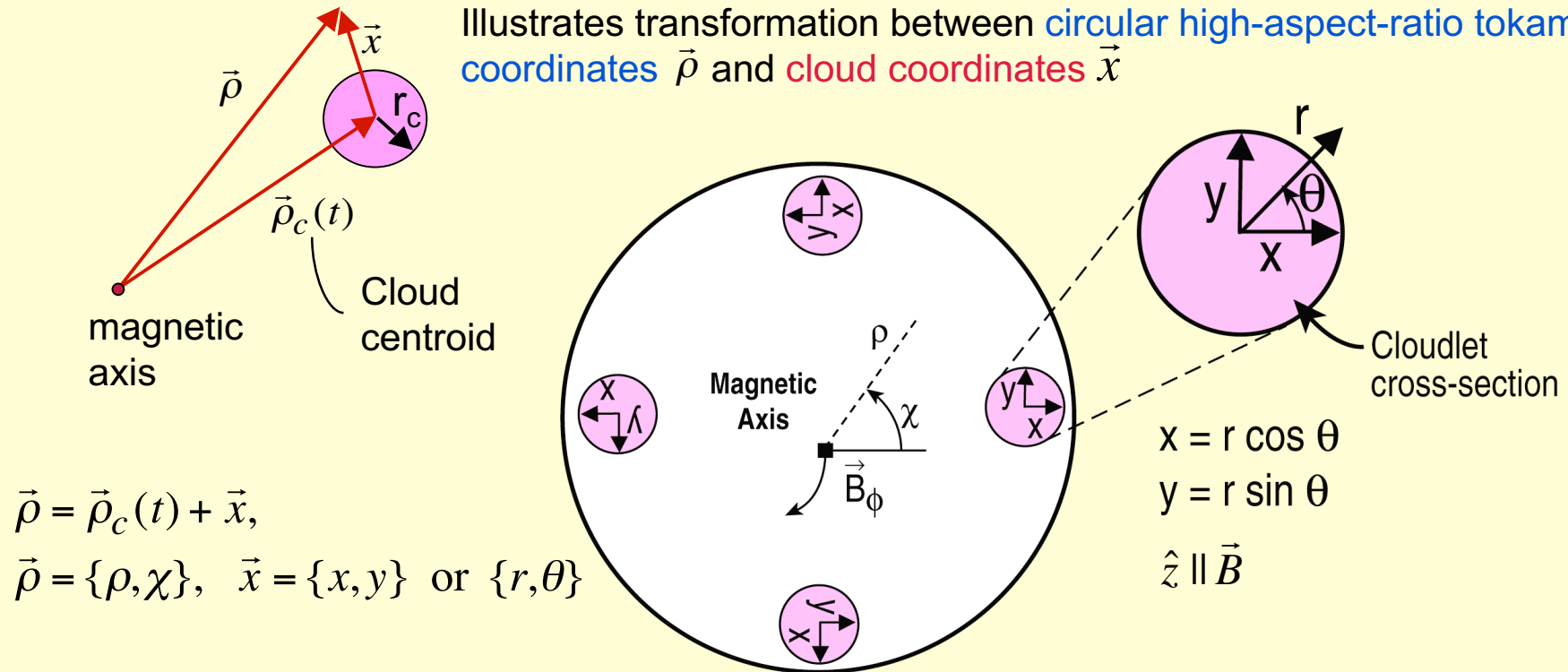
How Toroidicity modifies curvature drive

$q$  = safety factor  
 $\chi_0$  = pellet launch angle

Position of cloud centroid ( $x = y = z = 0$ )

# Helical Magnetic-Field-Line Following (MFLF) Coordinates $\vec{x}$ Suitable for Local Cloud Variables

Illustrates transformation between circular high-aspect-ratio tokamak coordinates  $\vec{\rho}$  and cloud coordinates  $\vec{x}$



$$\vec{\rho} = \vec{\rho}_c(t) + \vec{x},$$

$$\vec{\rho} = \{\rho, \chi\}, \quad \vec{x} = \{x, y\} \text{ or } \{r, \theta\}$$

$$x = r \cos \theta$$

$$y = r \sin \theta$$

$$\hat{z} \parallel \vec{B}$$

- Local cross-field coordinates  $(x, y)$  affixed to cross-section of cloud:  $x = \text{const}$ ,  $y = \text{const}$  identify a field line. Due to rotational transform, the coordinates rotate counter-clockwise with longitudinal distance  $z$

$$\nabla_{\parallel} \Phi \approx 0 \text{ so } \Phi(x, y) \text{ is frozen to B-field lines in cloud}$$

## Field-Line-Average Along Cloudlet Length

- Match parallel end-current  $\delta J_{||}$  with the current carried off by shear Alfvén wave excited by motion in ambient plasma  $E_{||} = -ik_{||}\Phi + i\omega A_{||} = 0$  (Parks, PoP 2000)

→

$$\nabla_{\perp} \cdot \vec{\Gamma} = S(r, \vartheta) \equiv \frac{2}{BR} \delta(r - r_c) [\sin \vartheta \cos \chi_c(t) + \cos \vartheta \sin \chi_c(t)] \Psi(t)$$

$$\vec{\Gamma} = \frac{m\tau}{B^2} \frac{D\nabla_{\perp}\Phi}{Dt} + \frac{\nabla_{\perp}\Phi}{\mu_0 c_{A\infty}}$$

Shear Alfvén wave part

Assumed flat radial cloud profiles

Line-averaged inertial (polarization) drift current

$$\tau = \int_{-L_c}^{L_c} n dz, \quad \tau_{cloud} \sim 10^3 \tau_{plasma}$$

- Drive integral folds **parallel (z) variations** with changing direction of  **$\nabla B$ -drift current**

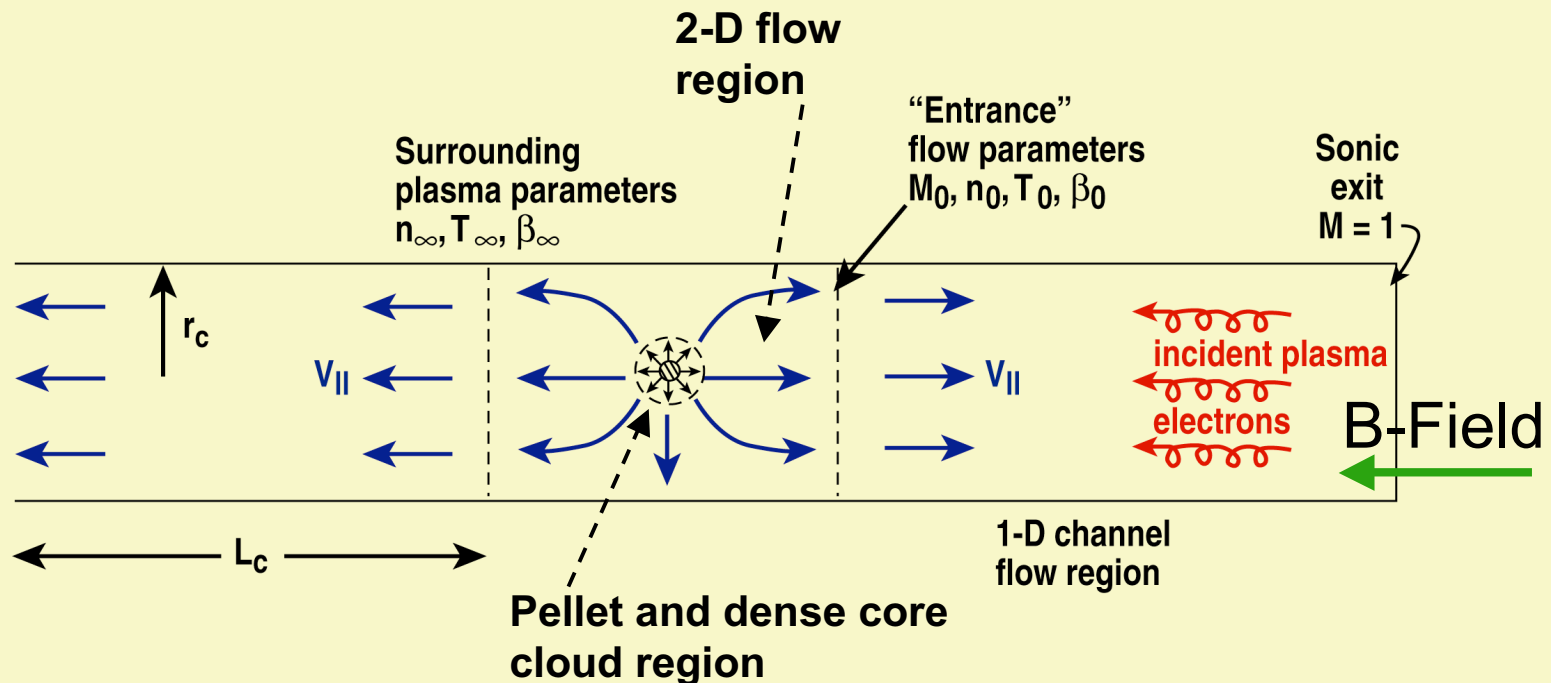
$$\Psi(t) = \int_0^{L_c(t)} \left[ p_c(z, t) [1 + M_c^2(z, t)/2] - p_{\infty}(t) \right] \cos(z/qR) dz$$

- Boundary condition on electrostatic potential at “infinity”

$$\Phi(\vec{x}, t) \rightarrow -E_{\rho\infty}[\rho_c(t)]x$$

Radial ( $\rho$ ) electric field in tokamak at cloud centroid

# Nondimensional Drift Equations Use Parameters of 1-D Ablation Channel Flow Formed around Solid Pellet



- $$\tilde{t} = \frac{t}{(L_c/c_0)}, \quad \tilde{\rho}_c = \rho_c/a, \quad u_\rho = \frac{v_\rho}{c_0}, \quad u_\chi = \frac{v_\chi}{c_0}, \quad u_E = \frac{v_{\perp\infty}^{E \times B}}{c_0}, \quad c_0^2 = \frac{2T_0}{m}$$

- Normalized curvature drive integral 
$$\tilde{\Psi} = \frac{\Psi(t)}{p_0 L_c}, \quad p_0 = 2n_0 T_0$$

## Non-dimensional Drift Equations

---

- Radial and Poloidal velocities and coordinates  $\rho_c(\tilde{t}), \chi_c(\tilde{t})$  are coupled

$$\tilde{M}(\tilde{t}) \frac{du_\rho}{d\tilde{t}} = -v_{drag} u_\rho + g \tilde{\Psi}(\tilde{t}) \cos \chi_c(\tilde{t}) + w \tilde{M}(\tilde{t}) \frac{u_\chi^2}{\tilde{\rho}_c(\tilde{t})}$$

Centripetal force  
Coriolis force

$$M(\tilde{t}) \frac{du_\chi}{d\tilde{t}} = -v_{drag} [u_\chi - u_{\perp\infty}^{E \times B}(\tilde{\rho}_c)] - g \tilde{\Psi}(\tilde{t}) \sin \chi_c(\tilde{t}) - w \tilde{M}(\tilde{t}) \frac{u_\rho u_\chi}{\tilde{\rho}_c(\tilde{t})}$$

Alfven drag coefficient

Normalized Curvature

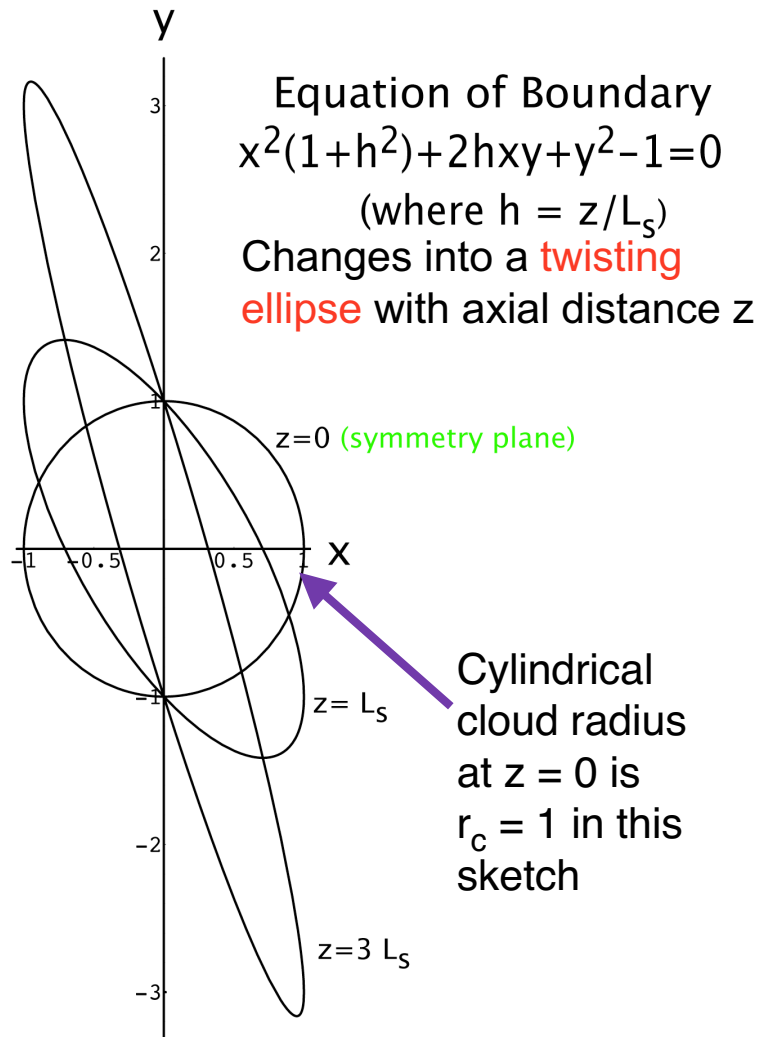
Normalized Cloud mass

$$v_{drag} = \left( \frac{L_c}{L_{skid}} \right), \quad g = \frac{2L_c}{\bar{r}R}, \quad w = \frac{L_c}{a}, \quad \tilde{M} = \frac{M(t)}{M(0)}$$

**"Skidding Length"** =  $r_{gi} n_0 e \mu_0 c_{A\infty} L_c / (2B)$  *N. Brennen J. Geo. Res. 1991*  
*P. Parks NF 1991*

- Cloud mass loss  $\frac{d\tilde{M}}{d\tilde{t}}$  comes from "Mass Shedding"

# Magnetic Shear Leads to “Mass Shedding”



- Elliptical compression and rotation re-orient polarization charges
- Leads to small **differential poloidal drift** increasing with  $z$
- Limits axial extent of drift response
- “Mass shedding” results

$$L_s = qR / \hat{s} \quad \text{magnetic shear length}$$

$$\hat{s} = \frac{\rho}{q} \frac{dq}{d\rho} \quad \text{shear parameter}$$

# Phenomenological Model Of Mass Shedding

- Natural “twisted basis” coordinates for a flux tube cloud filament, where  $x_* = \text{const}$ ,  $y_* = \text{const}$  identifies a field line

$$x_* = x, \quad y_* = y - \frac{xz}{L_S}$$

- Transform internal cloud electrostatic potential solution without shear  $\Phi^0(x,y)$  to an approximate one with shear by simple mapping  $\Phi_{in}^0(x,y) \rightarrow \Phi_{in}(x_*,y_*)$

- For this representation  $\frac{\partial \Phi_{in}}{\partial x} = \frac{\partial \Phi_{in}}{\partial x_*} - \frac{\partial \Phi_{in}}{\partial y_*} \frac{z}{L_S}$ ,  $\frac{\partial \Phi_{in}}{\partial y} = \frac{\partial \Phi_{in}}{\partial y_*}$

$\rightarrow \vec{v}_{in} = v_{\rho}^0 \hat{x} + v_{\chi}^0 \hat{y} + v_{\rho}^0 \frac{z}{L_S} \hat{y}$ 
← Cloud acquires small differential poloidal drift ( $z < L(t) \ll L_S$ )

- The coherent cloud drift is effectively limited in longitudinal extent when

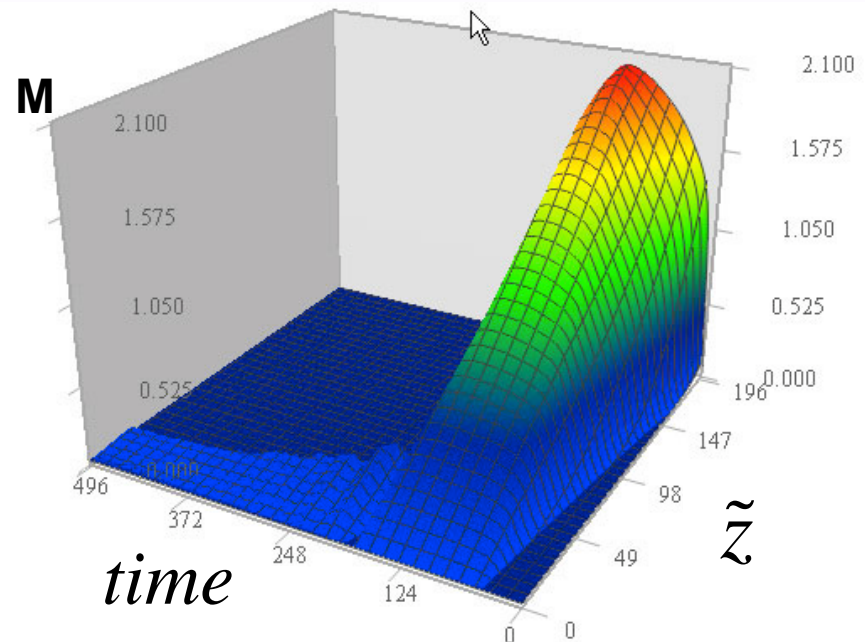
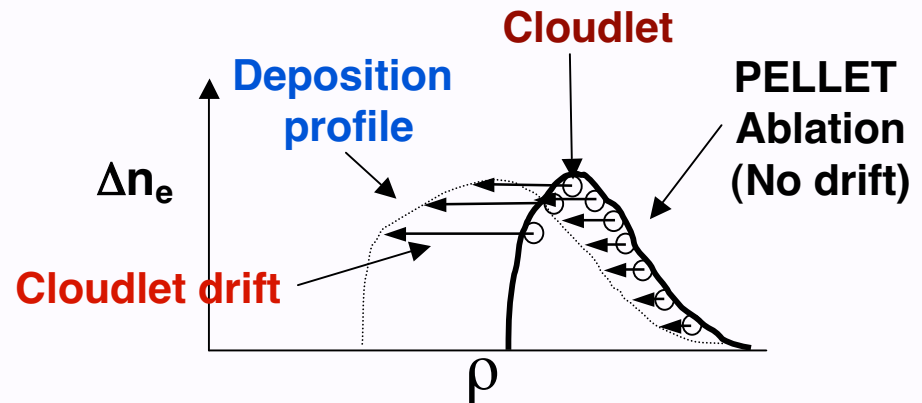
$$2r_c = \int_0^{t_S(z_0)} \frac{v_{\rho}^0(t) z(z_0, t) dt}{L_S[\rho_c(t)]}$$

Shedding time  $t_S(z_0)$  for fluid element with Lagrangian coordinate  $z_0$

- Mass loss rate  $\frac{d\tilde{M}}{dt} = \frac{d\tilde{M}}{dz_0} \frac{dz_0}{dt_S}$  decreases with weaker shear (larger  $L_S$ )

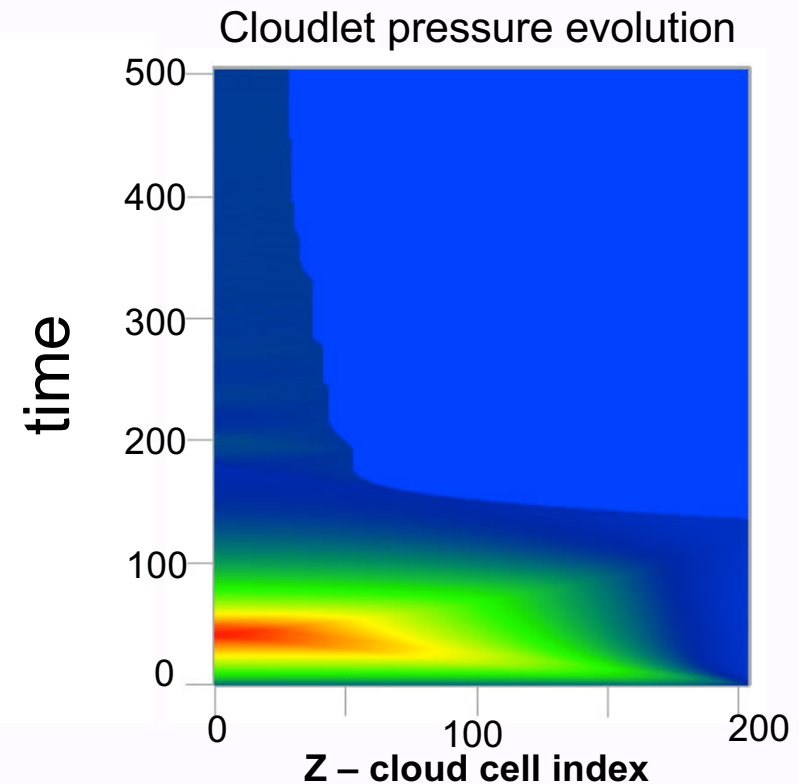
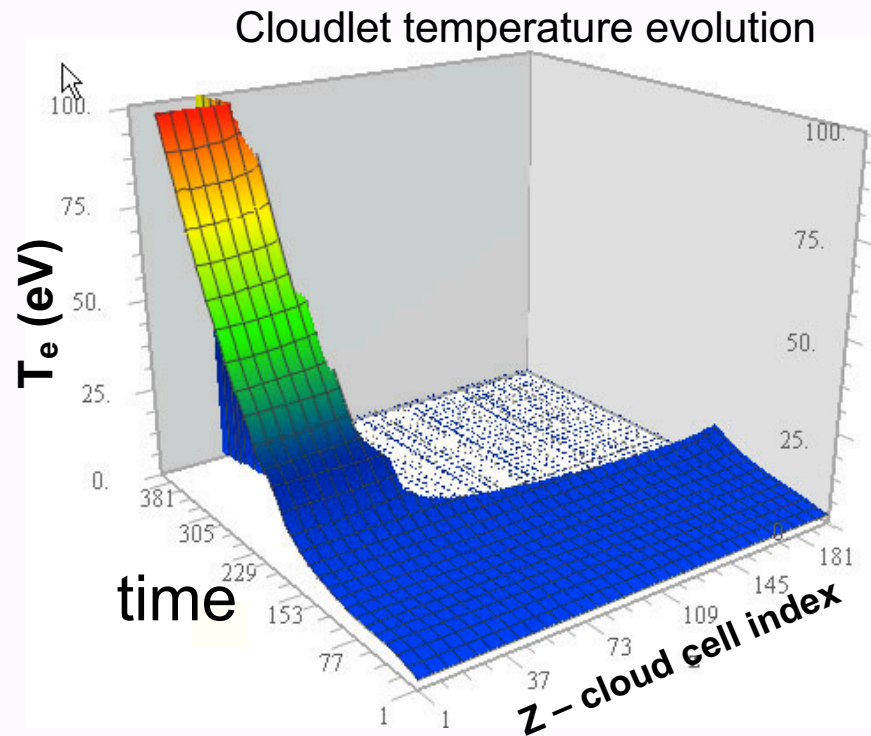
# Pressure Relaxation Lagrangian (PRL) Code Solves Coupled Drift and Parallel Dynamics for a Series of Cloudlets

- The PRL code uses the pellet size and plasma parameters at each point along the ablation track determined by PELLET code [Houlberg, 1988] to initialize the cloudlet parameters using model of Parks et al PoP 2000.
- The experimental plasma profiles are used by PRL to calculate the subsequent cloudlet pressure relaxation and drift velocity.
- The deposition profiles from each cloudlet are summed, yielding a **net  $\Delta n$  profile**.
- Parallel Mach number  $M$  for a single cloudlet (DIII-D 98796) is shown as a function of normalized time and Lagrangian coordinate  $\tilde{z}$ .





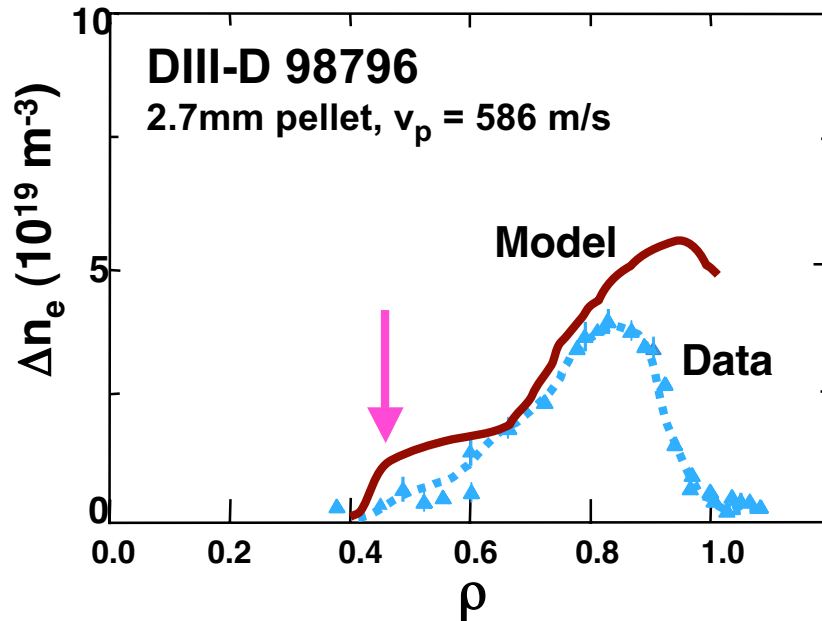
# Simulation of Temperature and Pressure Inside Cloudlet with Mass Shedding



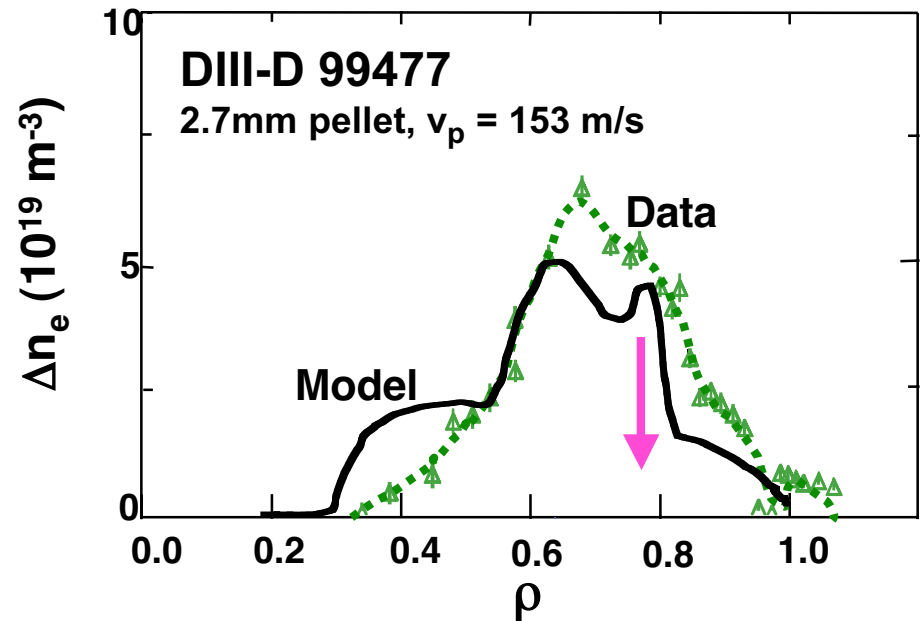
- Temperature and pressure evolution for typical cloudlet in DIII-D 98796. The cloudlet mass shedding can be seen by the reduced number of cells that starts at  $t_{cycle} = 150$  (3  $\mu$ sec). The cloudlet pressure builds quickly then decays as the density decays due to expansion along the field lines.

# Theory and DIII-D Experiments Agree

Outside launch



Inside launch (45 deg above mid-plane)



- Vertical arrows indicate pellet burnout point.

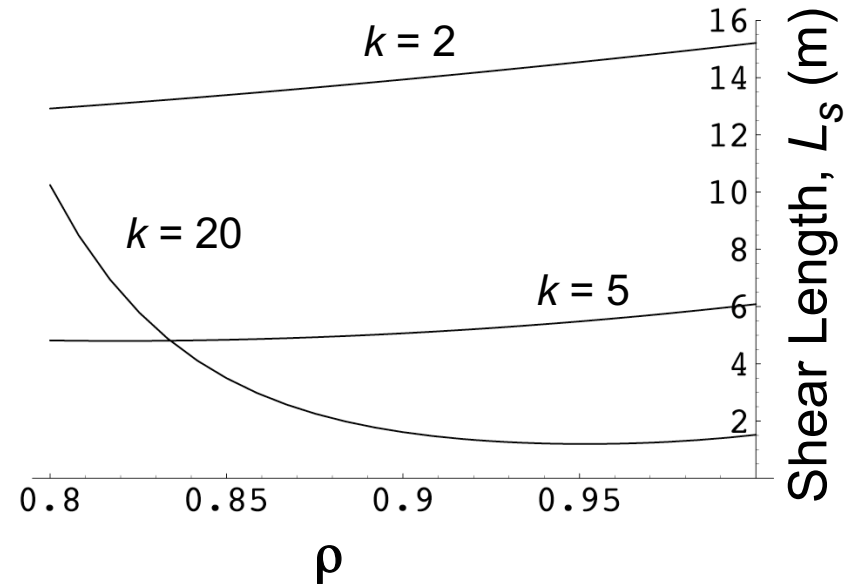
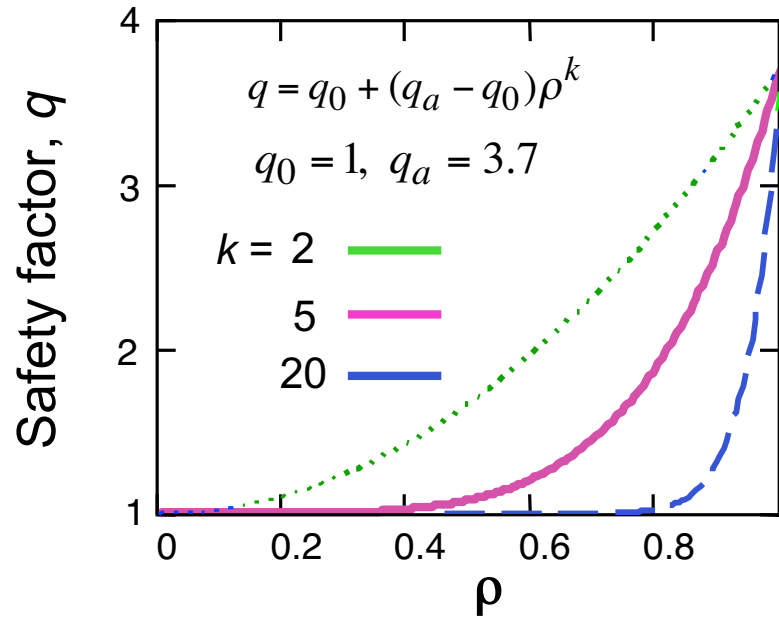
- Fueling efficiency for inside launch is much better (even with slower pellets)

outside launch  $\eta_{\text{theory}} = 66\%$  ,  $\eta_{\text{exp}} = 46\%$  (discrepancy due to strong ELM)

inside launch  $\eta_{\text{theory}} = 100\%$  ,  $\eta_{\text{exp}} = 92\%$  (discrepancy due to weak ELM)

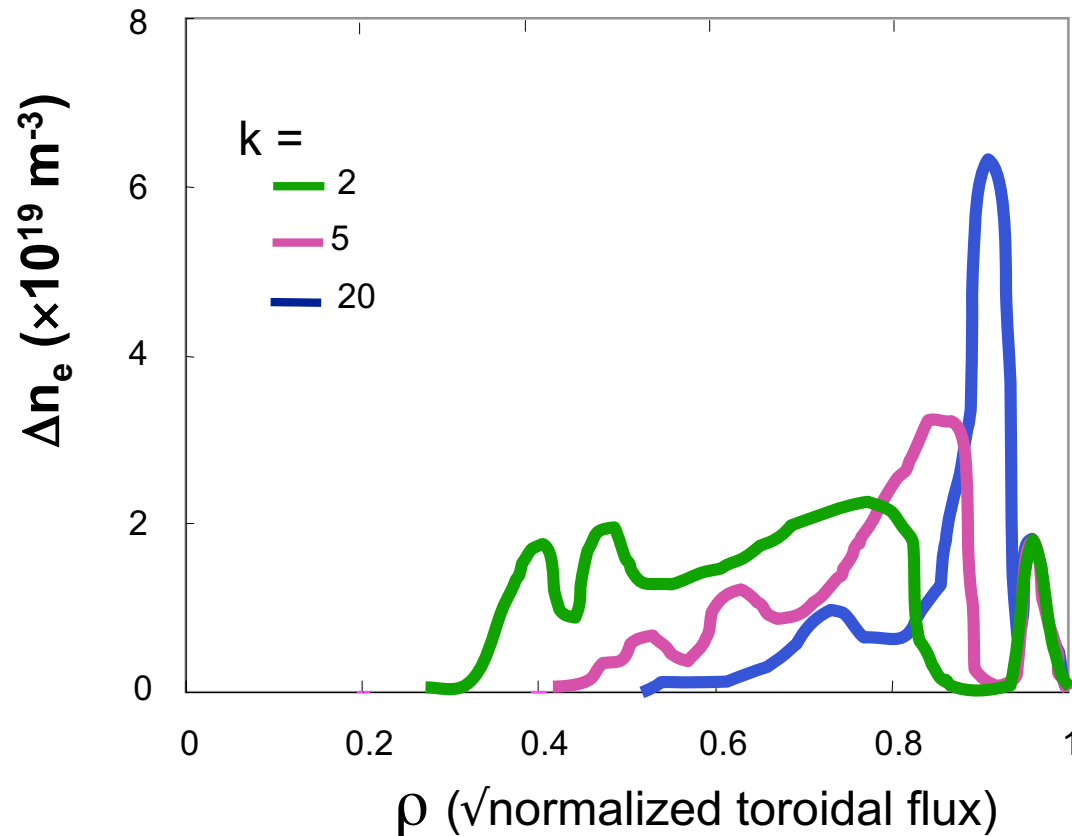
# Parameters for the Following ITER Calculations

$a = 2 \text{ m}$ ,  $R_0 = 6 \text{ m}$ ,  $n_e = 10^{14} \text{ cm}^{-3}$  (flat),  $T_e = (\text{P.B. Snyder profile NF 2004})$



- In ITER, pellets ablate near plasma edge, forming  $\sim 10$ - $20$  cloudlets. We find that the cloudlet drift distance is sensitive to  $L_s$  near edge

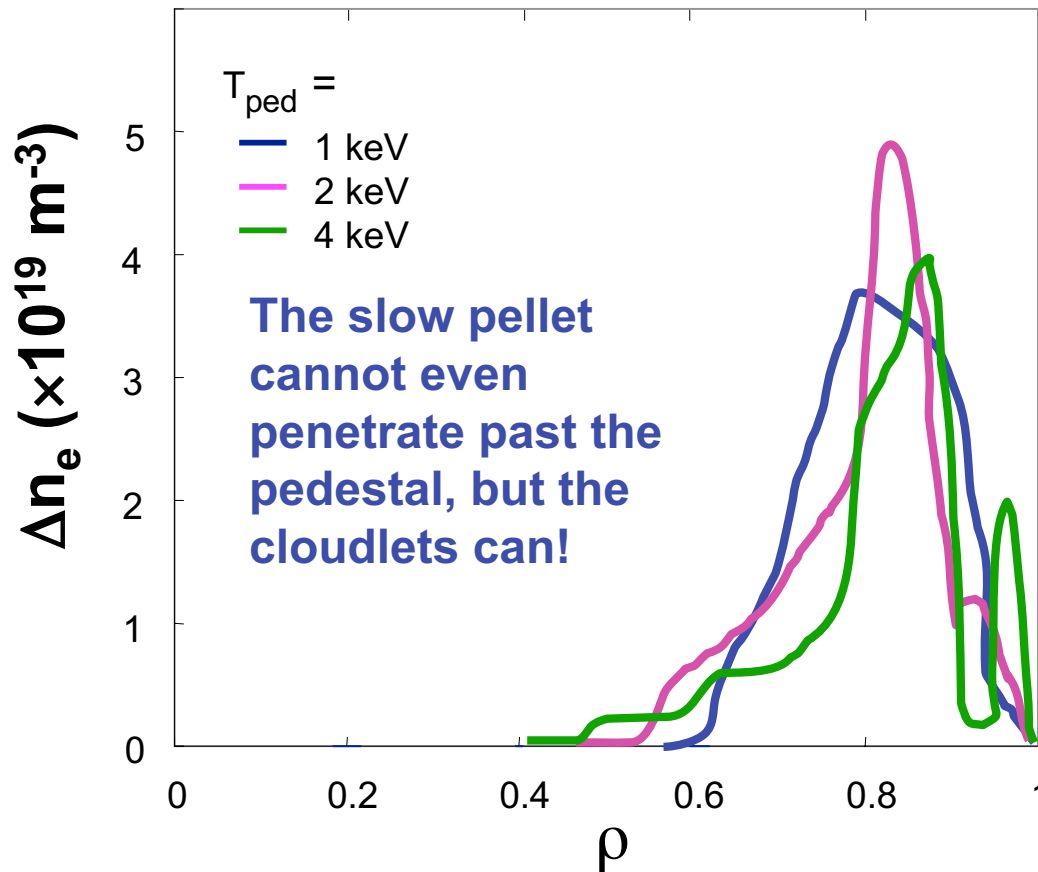
## How ITER Deposition Changes with q-Profile



6 mm D2 pellet  
 $T_0 = 20 \text{ keV}$   
 $T_{\text{ped}} = 4 \text{ keV}$   
 $v_p = 300 \text{ m/s}$   
Inner Wall (45 deg)  
Launch:

— The strong shear case near the edge ( $k = 20$ ) leads to early mass shedding and less penetration.

# ITER Deposition Profile Insensitive to $T_{ped}$ for Finite $\Delta_{ped}$



$\Delta_{ped} = 8$  cm

$T_0 = 20$  keV

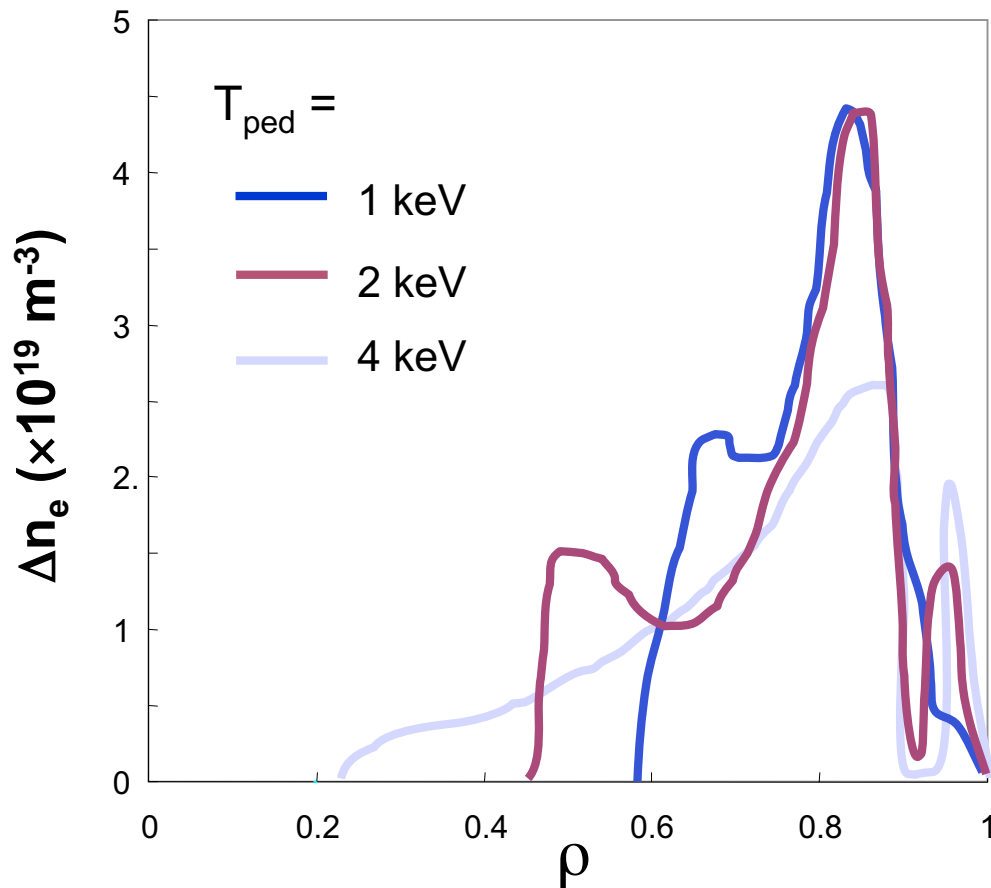
6 mm  $D_2$  pellet,  $v_{pell} = 300$  m/s,

45 deg below midplane entry

q-profile with  $k = 5$

• As  $T_{ped}$  increases, the temperature where pellet burns out  $T_{burn}$  increases as  $T_{burn} \sim T_{ped}^{3/8}$ , forming higher cloudlet pressures... However penetration is more shallow, so the cloudlets have to drift further up the pedestal. These **two effects almost cancel.** → Deposition remains fairly constant.

# ITER Deposition Improves with $T_{ped}$ for zero $\Delta_{ped}$

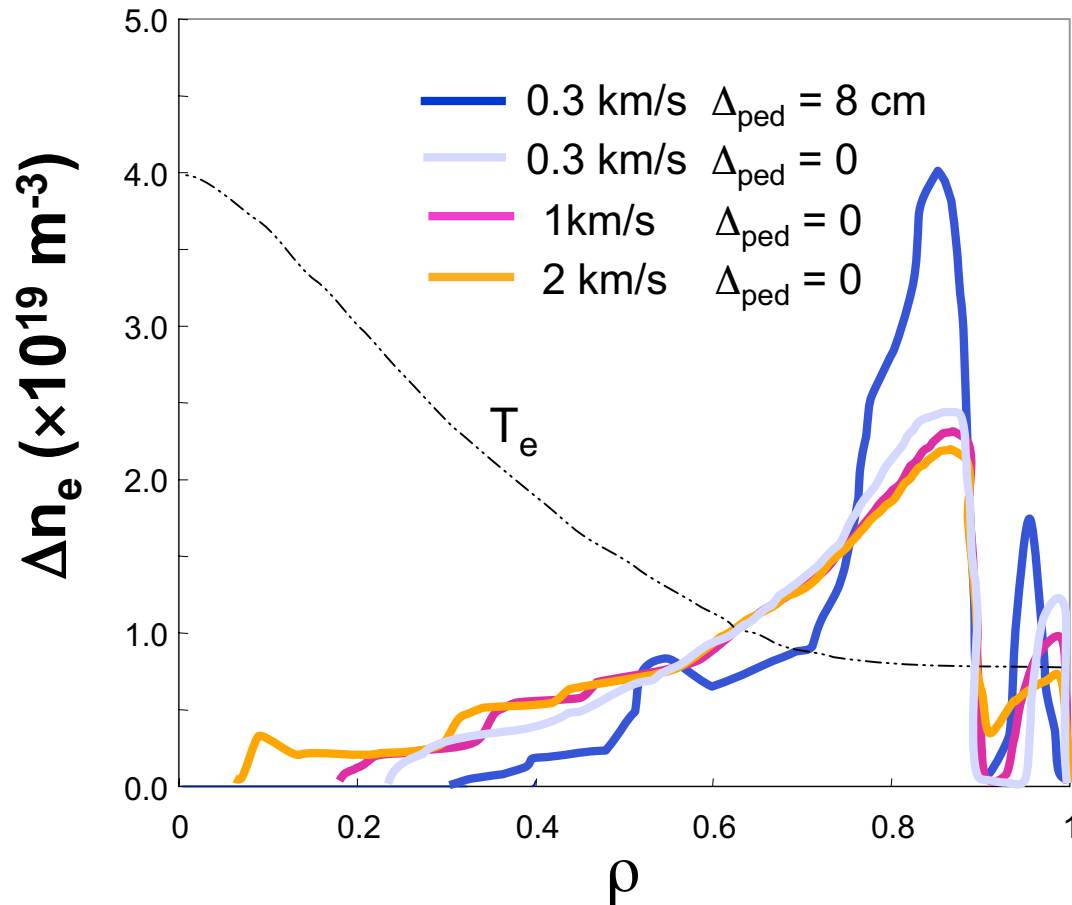


$T_0 = 10 \text{ keV}$ ,  
6 mm  $D_2$  pellet,  $v_{pell} = 300$   
m/s, 45 deg below  
midplane entry

➤ Higher  $T_{ped}$ , leads to  
deeper fuel penetration

➔ makes higher  
pressure cloudlets which  
drift further

# ITER Inner Wall (45 deg) Deposition Versus Pellet Speed



$T_0 = 10 \text{ keV}$ ,  $T_{ped} = 4 \text{ keV}$   
 6 mm  $D_2$

*Zero Pedestal width*

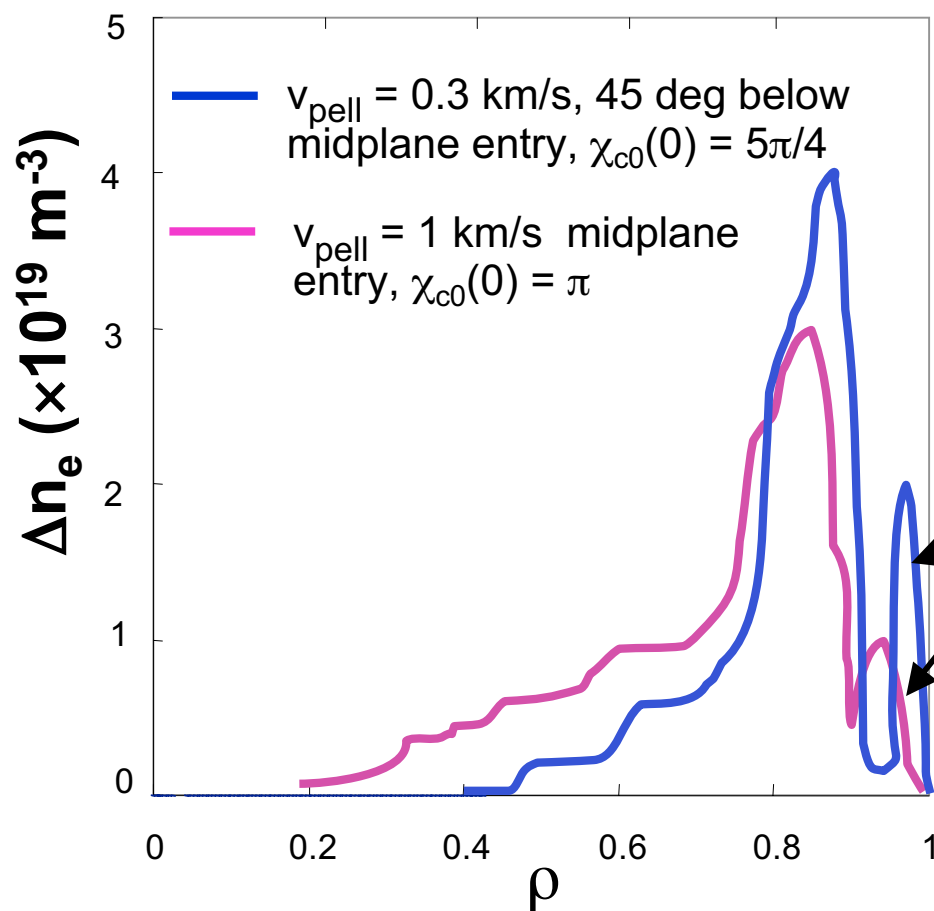
▶ Pellet velocity makes scant difference in fuel deposition profile, because pellet penetration in a 4 keV edge plasma is poor anyway!

*Finite Pedestal width*

▶ Higher velocity pays off: helps pellet punch through pedestal layer

→ making higher pressure cloudlets, which drift further

# ITER Deposition Profiles for Two Pellet Injection Scenarios



$T_0 = 20 \text{ keV}$ ,  $T_{\text{ped}} = 4 \text{ keV}$

$\Delta_{\text{ped}} = 8 \text{ cm}$

6 mm  $\text{D}_2$  pellet

$q$ -profile with  $k = 5$

10% of ablated material is assumed to be **locally deposited** (no drift)

• A high-velocity inner-bore (midplane) pellet injector promotes deeper fueling (F.Perkins APS 2004) .



## 3-D AMR code: Numerical Approach and Assumptions

---

- Detailed 3D AMR simulations of pellet injection using the MHD equations— pellet treated as moving density source
  - Ratio of pellet size to device size is  $\sim O(10^{-3})$
- Phased approach to understand the basic physics of mass redistribution with varying degrees of complexity
  - Simple Cartesian geometry (Samtaney, Jardin, Colella and Martin, Sherwood Fusion Theory Conference 2003)
  - Toroidal geometry (ICNSP 2003 Invited talk. To appear in Comput. Phys. Comm.)
- Physical assumptions
  - Pellet ablation rate uses a semi-analytical model
  - Instantaneous heating of ablated mass by plasma electrons
    - Finite rate heating using kinetic model (Parks, PoP 2004) is in progress
  - Single fluid MHD equations describe plasma
  - Plasma pressure and B-field initialized by a Grad-Shafranov equilibrium solution  $\rightarrow p_{\infty}(\Psi), T_{\infty}(\Psi), n_{\infty} = \text{const}$



## Equations and Mathematical Model

- Equations in conservation form + source terms

$$\frac{\partial U}{\partial t} + \frac{\partial F_j(U)}{\partial x_j} = \frac{\partial F_{v,j}(U)}{\partial x_j} + S_T(U) + S_{\nabla \cdot \mathbf{B}}(U) + S_{\text{pellet}}(U)$$

- Flux vector
  - $B_T$  is the toroidal component of the equilibrium magnetic field

$$F_j(U) = \left\{ \begin{array}{l} \rho u_j \\ \rho u_i u_j + p_t \delta_{ij} - B_i B_j + B_T B_3 \delta_{ij} - B_i B_T \delta_{3j} - B_j B_T \delta_{i3} \\ u_j B_i - u_i B_j + B_T \delta_{i3} u_j - B_T \delta_{3j} u_i \\ (e + p + \frac{1}{2} B_k B_k) u_j - B_j (B_k u_k) + B_T B_3 u_j - (B_k u_k) B_T \delta_{3j} \end{array} \right\}$$

- Equation of state

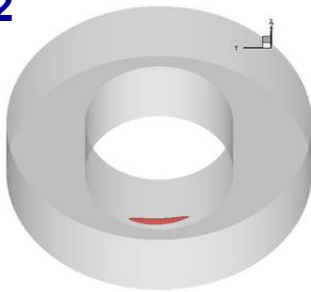
$$e = \frac{p}{\gamma - 1} + \frac{\rho}{2} u_k u_k + \frac{1}{2} B_k B_k$$

# Preliminary AMR Code Results Using NSTX Machine Parameters

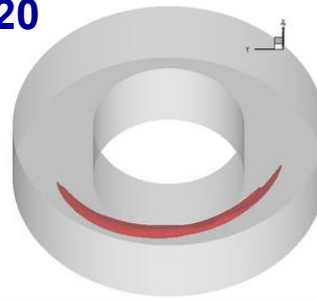
—  $n = 1.5 \times 10^{13} \text{ cm}^{-3}$ ,  $B = 0.23 \text{ T}$ ,  $a = 0.26 \text{ m}$ ,  $r_p = 1 \text{ mm}$ ,  $v_{\text{pell}} = 3200 \text{ m/s}$

Density iso-surface shows pellet cloud expanding along B-field

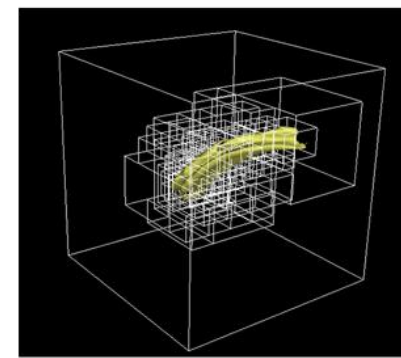
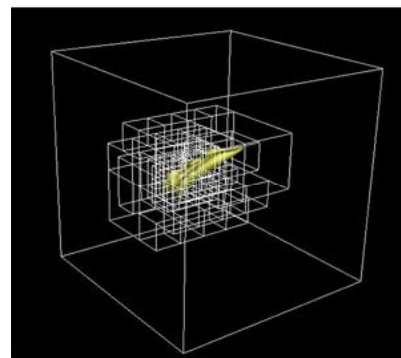
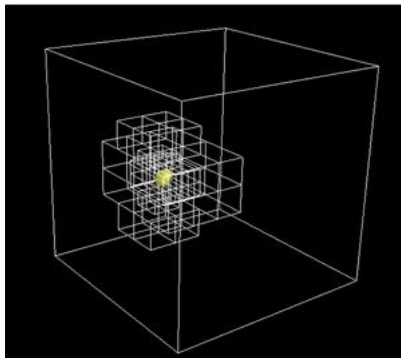
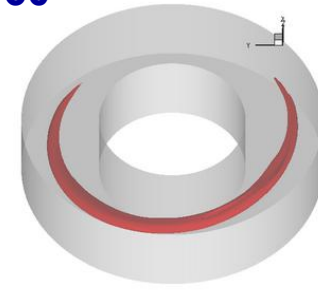
$t/t_A = 2$



$t/t_A = 20$

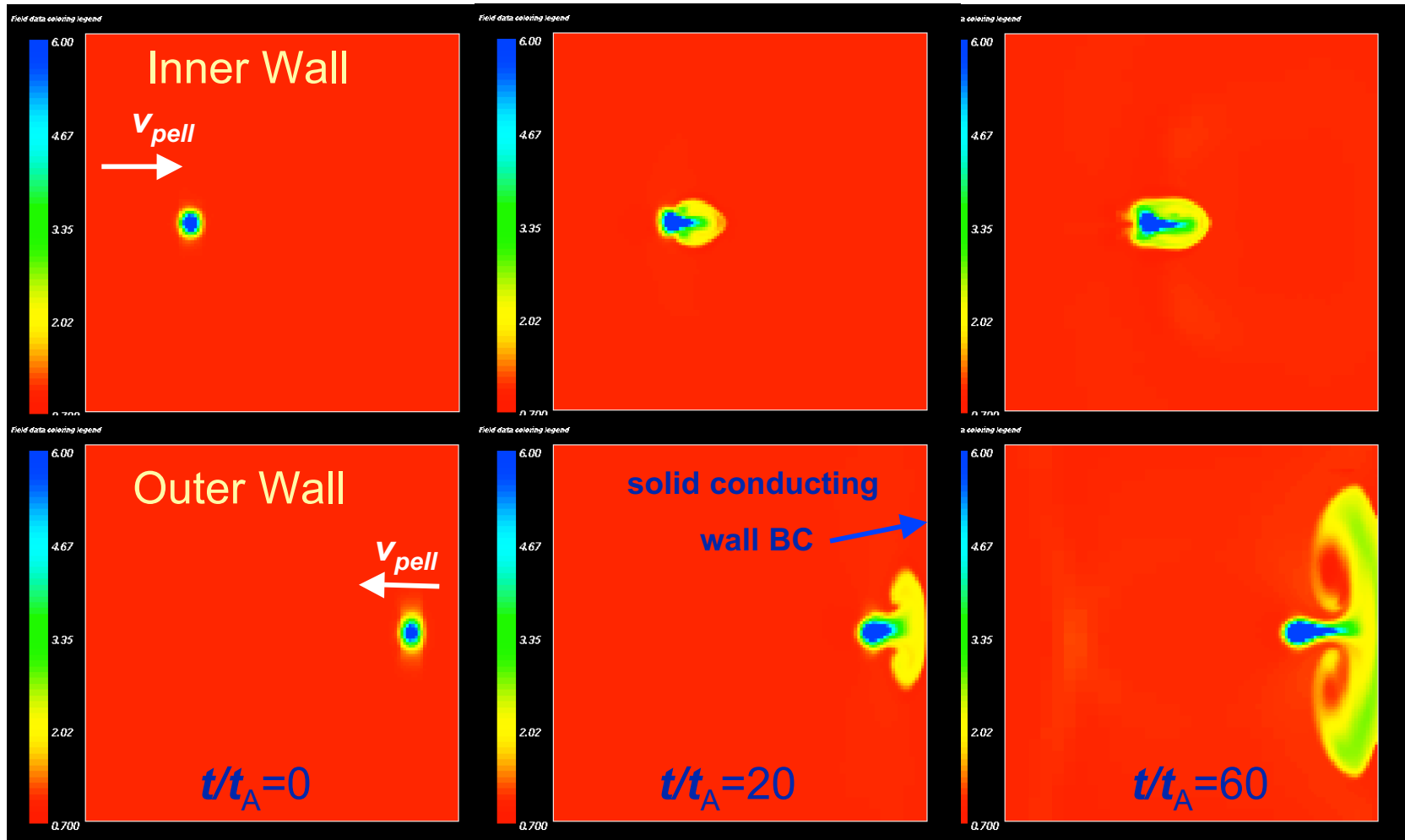


$t/t_A = 60$



Adaptive Mesh Tracks Elongating Cloud

# Inner Wall vs Outer Wall Pellet Injection (Midplane Entry)



- Density contours of pellet cloud (at cloud midplane cross section) indicate significant large- $R$  displacement relative to instantaneous pellet position.

## Summary and Conclusions

---

- Pellet Ablation used 2-D **CAP** code, the most sophisticated ablation code which is now including the interaction of the ablation flow with the magnetic field
  - Showed that a  $\beta \sim 1$  cavity can be formed around pellet by the high ablation pressure. This will reduce heat flux to pellet, but it contradicts previous quasi-steady ablation models in which  $B$ -field is only slightly distorted.
    - However **CAP** used a “switch-on” heat flux, described just the initial transient period to  $0.4\mu\text{s}$ , and kept heat flux  $\parallel$  to  $z$ , NOT DIVERTED AROUND  $B$  (which would reduce  $p, T$  and  $\sigma$ . “Switch-on” heat flux might apply to step-function high- $T$  pedestal.
- The theoretical  $\nabla B$  drift model has been reformulated with new physics
  - **PRL** code was validated by inner and outer wall pellet injection experiments on the DIII-D tokamak. Good agreement was found!
  - For ITER, **PRL** showed much better penetration of pellet material for inner wall injection, but penetration is sensitive to  $L_s$ ,  $T_{\text{ped}}$ , and  $\Delta_{\text{ped}}$ .
- 3-D numerical simulations of  $\nabla B$  pellet cloud drift using **AMR** code are underway, verifying drift in the large- $R$  direction for both inner- and outer-wall injection.