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**COMPLETE SUPPRESSION OF THE $M/N = 2/1$
NEOCLASSICAL TEARING MODE USING RADIALLY
LOCALIZED ELECTRON CYCLOTRON CURRENT DRIVE
ON DIII-D AND THE REQUIREMENTS FOR ITER**

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ABSTRACT

DIII-D experiments demonstrate the first real-time feedback control of the relative location of a narrow beam of microwaves to completely suppress and eliminate a growing tearing mode at the $q = 2$ surface. Long wavelength tearing modes such as the $m/n=2/1$ instability are particularly deleterious to tokamak operation. Confinement is seriously degraded by the island, plasma rotation can cease (mode-lock) and disruption can occur. The neoclassical tearing mode (NTM) becomes unstable due to the presence of a helically-perturbed bootstrap current and can be stabilized by replacing the “missing” bootstrap current in the island O-point by precisely located co-electron cyclotron current drive (ECCD). The optimum position is found when the DIII-D plasma control system (PCS) is put into a “search and suppress” mode that makes small radial shifts (in about 1 cm steps) in the ECCD location based on minimizing the Mirnov amplitude. Requirements for ITER are addressed.

1. "HYBRID SCENARIO" STATIONARY HIGH-PERFORMANCE DISCHARGES

The suppression of tearing modes in DIII-D was carried out in high performance, long-pulse discharges with normalized beta $[\beta_N (\%)/\beta_p (\text{MA})/a (\text{m}) B_T (\text{T})] \beta_N \approx 2.7$, normalized confinement time (to that of the L-mode scaling) $H_{89p} = 2.6$, $q_{95} = 4.3$ and fraction of plasma current noninductively driven by the bootstrap effect $f_{bs} \approx 0.35$ [1]. These discharges are referred to as a hybrid scenario as they have sufficient bootstrap current to significantly reduce the volt-s consumption but not enough for full noninductive steady state. The key element is the relaxation of the current profile to a stationary state with safety factor on axis $q_{min} > 1$, without sawteeth and fishbones. Under the influence of a small $m/n = 3/2$ tearing mode, the current relaxes to the stationary state maintained for up to 40 energy confinement times τ_E and >2 resistive diffusion times τ_R . The confinement remains well above that of standard H-mode ($H_{89p} \approx 2.6 > 2$) despite the approximate $\lesssim 5\%$ reduction in τ_E due to the $3/2$ tearing mode. Real-time feedback control of the energy content is done by regulation of neutral beam injection (NBI) power using the diamagnetic flux, and control of the particle inventory by gas fueling and active cryopumping based on the CO_2 interferometer. The highest performance in β_N and $\beta_N H_{89p}$ is found to be limited by the $m/n = 2/1$ tearing mode. Requesting a higher diamagnetic flux (and thus beta) such that the NBI power is increased causes an $m/n = 2/1$ NTM to appear. The hybrid scenario promises to be a robust, long-pulse operating regime for physics and engineering tests on ITER, highlighting the importance of stabilizing the $2/1$ NTM.

2. MODIFIED RUTHERFORD EQUATION FOR NTM STABILIZATION BY ECCD

The requirements on the ECCD for complete $m/n = 2/1$ island suppression in DIII-D are well-modeled by the modified Rutherford equation. The NTM is metastable in that the high β_θ plasma without the island must be excited above a threshold island width for the island to grow large and saturate ($dw/dt = 0$). This is shown by solving the modified Rutherford equation [2,3], Eq. (1), evaluated in Fig. 1 for saturated island widths for both no rf and two levels of precisely positioned ECCD [4],

$$\frac{R}{r} \frac{dw}{dt} = \beta_\theta + \beta_\theta^{1/2} \left[\frac{L_q}{L_p} \frac{r}{w^2 + w_d^2} - \frac{r w_{pol}^2}{w^3} - \frac{8 q r \beta_{ec}}{w^2} \frac{j_{ec}}{j_{bs}} \right] \quad (1a)$$

and

$$\beta_\theta = \beta_0 \left(1 + 2 \beta_{ec}^2 / w^2 \right)^{1/2} e^{\left(5 R / 3 \beta_{ec} \right)^2} \quad (1b)$$

with $\beta_\theta = r/R_0$, $L_q = q/(dq/dr)$, $L_p = p/(dp/dr)$, β_θ the poloidal beta and j_{ec}/j_{bs} the ratio of the peak ECCD current density normalized to the local equilibrium bootstrap current density. The rf efficiency β has a coefficient $\beta_0 = 0.4$ for no modulation (as in DIII-D experiments described here) and is reduced if the peak ECCD is not placed precisely ($\Delta R = 0$) on the island O-point and/or if the ECCD width is greater than that of the island. β_{ec} is the full radial width-half maximum (FWHM) of a Gaussian rf current density of width parameter $3\beta_{ec}/5$.

The NTM is particularly well suited to the development of suppression techniques because the mode is linearly stable [$\Delta r \approx -1.3$ is used in Fig. 1 evaluated by fitting to the

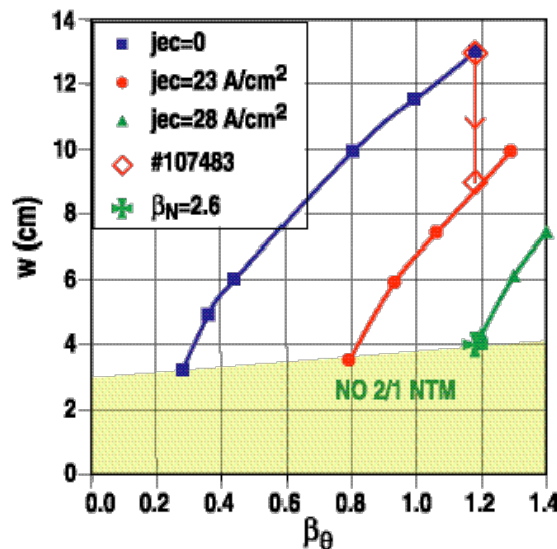


Fig. 1 Calculated full width in DIII-D of $m/n = 2/1$ saturated island from the modified Rutherford equation versus poloidal beta for different levels of precisely aligned rf current density. $\Delta r = -1.3$, $j_{bs} = 14 \text{ A/cm}^2$ at $\beta_\theta = 1.2$ and $\beta_{ec} = 4 \text{ cm}$.

model no rf saturated island width $w_{sat} \approx \sqrt{L_q/L_p} \sqrt{\Delta r}$ with the measured island width from ECE radiometer] although nonlinearly unstable. So if the island can be decreased below a threshold size, the mode will decay and vanish. Here the effective threshold is $w_{th} \approx \sqrt{3(w_{pol}^2 + w_d^2)} \approx 3.9$ cm from both the polarization threshold w_{pol} of order of the ion banana width and from the cross-field transport threshold w_d [5]. Note that all quantities in this paper (w , w_{pol} , w_d , L_q, L_p , $\sqrt{\Delta r}$, etc.) are evaluated at the outboard midplane $q = 2$ location while $\sqrt{\Delta r}$ is the global quantity [5]. Experiments in the 2001 DIII-D campaign could at best achieve only a partial suppression of the 2/1 island with well-aligned ECCD and NBI feedback to keep $\sqrt{\Delta r}$ (and $\sqrt{\Delta r_N}$) constant in the presence of the mode as shown by discharge #107483 marked in Fig.1. The modeling uses peak $j_{ec} \approx 23$ A/cm² with $\sqrt{\Delta r} \approx 4$ cm from the code TORAY-GA with about 2 MW injected rf power. Predictions were that about 25% more j_{ec} is needed at fixed $\sqrt{\Delta r}$ to completely suppress the 2/1 NTM or a somewhat lower $\sqrt{\Delta r}$ for smaller j_{bs} . In the 2002 DIII-D campaign with similar rf power and j_{ec} only slightly higher, $\sqrt{\Delta r}$ was dropped by NBI feedback to just under 1 ($\sqrt{\Delta r_N} = 2.2$) and complete suppression of the $m/n = 2/1$ NTM was achieved as shown in Fig. 2 for discharge #111367. Note that the plasma control system needed to make one $\Delta R \approx 1$ cm position adjustment to obtain complete suppression,

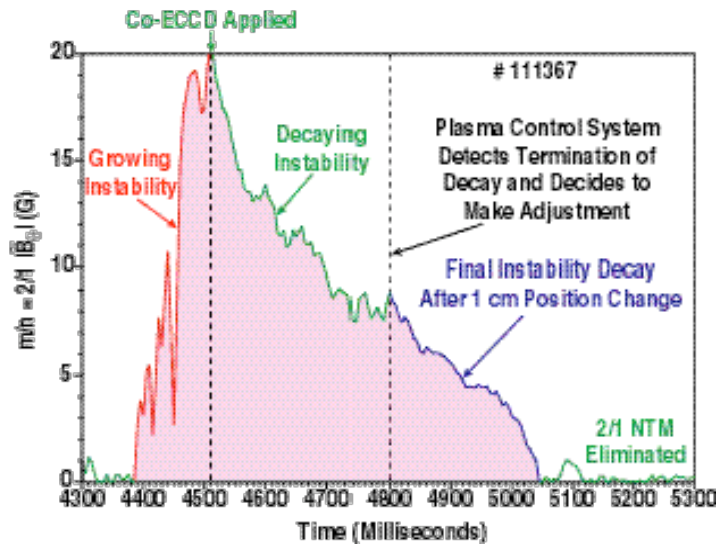


Fig. 2 Applying and adjusting the precise position of co-ECCD stops the growth of a long wavelength tearing mode and then completely eliminates it.

demonstrating both how precise the alignment must be and how close to marginal the rf power and current drive was. Note also that from Eq. (1b), $\exp [-(5\Delta R/3\sqrt{\Delta r})^2] \approx \exp [-(5 \times 1/3 \times 4)^2] \approx 0.84$ or only a 16% reduction in efficiency, while $\Delta R = 2$ cm would be a 50% reduction. Experiments in the 2003 DIII-D campaign are planned with 6 gyrotrons for up to 3 MW of injected power so as to study the complete 2/1 NTM suppression at the unreduced $\sqrt{\Delta r_N} = 2.6$ operating point shown in Fig. 1 chosen as representative of the hybrid scenario in ITER. The DIII-D result shown in Fig. 2 is the first use of ECCD for complete suppression of the $m/n = 2/1$ NTM and follows previous successes with ECCD on the $m/n = 3/2$ NTM in ASDEX Upgrade, JT-60U and DIII-D [6-8].

3. HYBRID SCENARIO IN ITER AND ECCD REQUIREMENTS

The DIII-D hybrid scenario is extrapolated to ITER assuming the same shape, profiles, \bar{n} and q_{95} but with larger major radius [$R_0 = 1.7$ m (DIII-D) becomes 5.7 m (ITER)], higher toroidal field ($B_T = 1.7$ T becomes 5.3 T) and $T_i = T_e$ instead of $T_i = 1.6 T_e$ as the density \bar{n} relative to the Greenwald density [I_p (MA)/ πa (m)²] is assumed to be increased to 1.0 from 0.4 in DIII-D. Because the normalized ion gyroradius $\bar{\rho}_{i*}$ (equal to the ratio of ion gyroradius ρ_i to the minor radius a) decreases at $q = 2$ from 11.9×10^{-3} in DIII-D to 1.9×10^{-3} in ITER (while collisionality is similar if smaller), the relative threshold at $q = 2$ decreases from $w_{th}/r = 3.9$ cm/42 cm = 0.093 to 3.7 cm/127 cm = 0.029, about three times smaller. The effect of this is shown in Fig. 3 which assumes that supplementary heating is adjusted to keep \bar{n}_N and \bar{n}_D fixed. Note that: (1) without rf, the relative saturated island widths are similar as $w_{sat}^2 \gg w_{th}^2$, (2) there is a critical j_{ec} for which all w have $dw/dt < 0$ so the mode is stabilized, and (3) the worst case, i.e. highest dw/dt , is at $w \approx w_{th}$ so the NTM if partially suppressed needs only a little more stabilizing rf current drive to achieve complete suppression by reducing the saturated island ($dw/dt \equiv 0$) to $w \approx w_{th}$. Experiments on DIII-D, so far, have been performed with the nearly optimal $\bar{\rho}_{ec} \approx w_{th} \approx 4$ cm as shown in modeling in Fig. 4.

The predicted optimum $\bar{\rho}_{ec}$ for ITER is only 4–5 cm which may be difficult to execute. Assuming this is achievable, without modulation the required $j_{ec} \approx 40$ A/cm² with $j_{ec}/j_{bs} \approx 3$ and $I_{ec} \approx 250$ kA with $I_{ec}/I_p \approx 0.02$. However if the efficiency of suppression is improved a factor of 2.5 ($\bar{\rho}_0 = 0.4 \rightarrow 1.0$) by modulating the ECCD to drive current only at the island O- point (yet to be demonstrated in existing devices) the requirements at $\bar{\rho}_{ec} = 4$ –5 cm drop to $j_{ec} \approx 17$ A/cm² and $I_{ec} \approx 100$ kA which would allow a tradeoff to larger $\bar{\rho}_{ec}$.

Future work on DIII-D includes increased injected rf power to achieve 2/1 NTM suppression at higher $\bar{\rho}$, pre-biasing with ECCD to avoid the 2/1 NTM or keep it from ever growing to large amplitude (which will include active tracking of the $q=2$ location and ECCD alignment in the absence of the mode) and detailed comparisons of requirements by changing $\bar{\rho}_{ec}$, i.e., trading off j_{ec} and I_e .

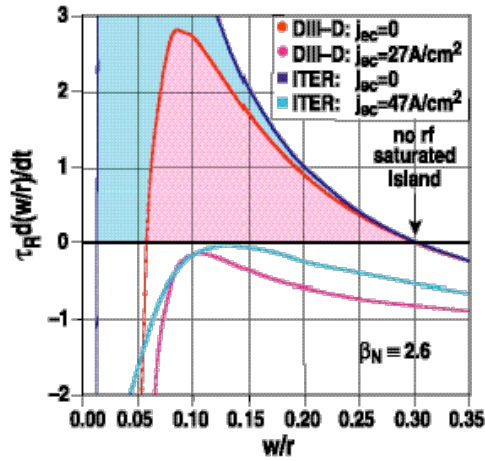


Fig. 3 Growth rate of $m/n = 2/1$ island width w vs. relative island width w/r for both DIII-D and ITER with and without the critical rf current density j_{ec} for stabilization. (Assumed fixed parameters of note are $\beta_N = 2.6$, $\beta_{\parallel} = 1.2$, $\Delta \bar{q} = -1.3$, and FWHM $\delta_{ec} = 4$ cm. Relative NTM threshold island width $w_{th}/r = 0.093$ in DIII-D and 0.029 in ITER and $j_{bs} = 14$ A/cm² in DIII-D and 13 A/cm² in ITER.)

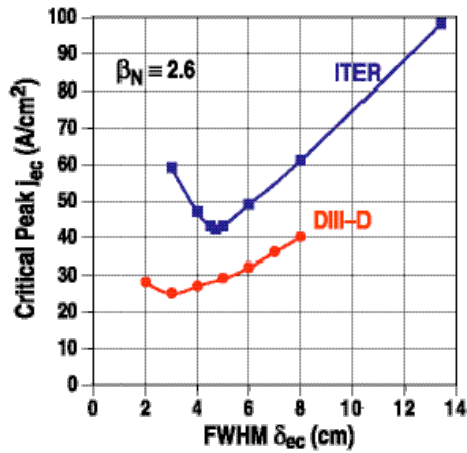


Fig. 4. Calculated critical peak rf current density j_{ec} vs. FWHM width d_{ec} (evaluated at $q = 2$ on outboard midplane) for $2/1$ NTM stabilization by modeling of DIII-D and ITER assuming fixed $\beta_N = 2.6$ ($\beta_{\parallel} = 1.2$), perfect alignment and with relative threshold $w_{th}/r = 3.9 \text{ cm}/42 \text{ cm}$ in DIII-D and $3.7 \text{ cm}/127 \text{ cm}$ in ITER.

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