GA-A26008

## INERTIAL CONFINEMENT FUSION

**Annual Report** 

October 1, 2006 through September 30, 2007







GA-A26008

## RESEARCH AND DEVELOPMENT AND FABRICATION OF INERTIAL CONFINEMENT FUSION TARGETS, COMPONENTS, AND COMPONENT TECHNOLOGY

### ANNUAL REPORT TO THE U.S. DEPARTMENT OF ENERGY FOR THE PERIOD OCTOBER 1, 2006 THROUGH SEPTEMBER 30, 2007

by PROJECT STAFF

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#### **1. INTRODUCTION**

This report documents General Atomics' (GA) fiscal year (FY) 2007 activity for Inertial Confinement Fusion (ICF), a research and development program of the U.S. Department of Energy (DOE) National Nuclear Security Administration (NNSA). The program goals are controlled nuclear fusion at laboratory scales using large laser and pulsed power facilities in the U.S., and conducting experiments relevant to high energy density physics (HEDP) using those same facilities. GA is registered in the ISO 9001:2000 program and maintained excellent communication with the users of the targets to continually improve the performance of the team. As well as getting extensive and generally very positive feedback from its customers in FY07, the GA staff authored a number of papers in refereed journals and presented work at major international conferences. Highlights of the GA ICF technology work performed under DOE Contract No. DE-AC52-06NA27279 in FY07 comprise the subject of this report. Comments and requests for further information may be directed to the current GA Inertial Fusion Technology Program Manager, Abbas.Nikroo@gat.com (858) 455-2931.

ICF relies on inertia to confine a mixture of deuterium and tritium (DT) for the time required to create a self-sustained fusion reaction. This also requires that the DT be highly compressed (about 1000 times solid density) and heated to about 100,000,000 deg. The ICF Ignition and High Yield Campaign supports the NNSA's goal to develop laboratory capabilities to create and measure extreme conditions of temperature, pressure, and radiation density. Achieving HEDP conditions is critical to validate codes and to study high energy density conditions.

The strategy to accomplish this long-term goal is centered on four objectives:

- 1. Achieve ignition in the laboratory and develop it as a scientific tool.
- 2. Support execution of HEDP experiments necessary to provide advanced assessment capabilities.
- 3. Develop advanced technology capabilities that support long-term needs of NNSA.
- 4. Maintain robust national program infrastructure and attract scientific talent to the programs.

The ICF Campaign, which includes the National Ignition Campaign (NIC) and HEDP experiments, is presently executed at six sites: Los Alamos National Laboratory (LANL), Lawrence Livermore National Laboratory (LLNL), Sandia National Laboratories (SNL), the University of Rochester Laboratory for Laser Energetics (UR/LLE), the Naval Research Laboratory (NRL) and GA. General Atomics concentrates on making the targets and doing the R&D for the targets for experiments which are carried out at several laser and pulsed power facilities. In this, GA supports all four of the above strategies of NNSA's ICF Campaign.

There are three major ICF facilities: the OMEGA glass laser at UR/LLE, the Z pulsed-power facility at SNL, and the National Ignition Facility (NIF) at LLNL. This 192-beam laser is not quite 100% complete but has done preparatory experiments with a few prototype beams and will perform Early Opportunity Shots within the next year. These facilities are supplemented by LANL's Trident laser, NRL's Nike laser and other smaller lasers.

In FY07, GA continued its support of NNSA's ICF program by on time delivery of more than 4000 fully characterized target components and targets, necessary to enable experiments at the various facilities. The OMEGA laser accounted for the majority of experiments for ICF and HEDP. Each shot requires a new target and generally there is a completely different type of tightly specified and well-characterized target for each day or half day of shots. The Z facility paused operation during the summer of FY06 for a major refurbishment and came back online in the late fall of CY2007. In FY07, GA produced components for these facilities consisting of many different types (Section 2). Many of the components are novel and were made by techniques requiring significant development. As the targets are the initial conditions for the experiments, the targets and components need to be accurately measured and characterized for each shot, which destroys the target.

In Section 2 of this report, we summarize the target deliveries for these facilities. By the nature of experiments, there is always the question of specifying the target well enough in advance for complete manufacture and characterization of the target to specification. The experimentalists may delay specifying the target, pending analysis of previous experiments and computer simulations, but several months are often required for fabrication, which often requires some development and characterization. In FY07, GA worked closely with LLNL — and the other sites — to manage the rolling specification of hundreds of targets per year required for OMEGA.

In Section 3, we summarize research and development work for the ignition campaign on the NIF (NIC Target Development) and supporting current deliveries for OMEGA (NIC x-ray drive target production and NIC direct drive target production), and Z (SNL Target Development and Production). This development work has been presented to peers in the inertial fusion and HEDP community at major international conferences (e.g., Inertial Fusion Sciences and Applications, IFSA, in Kobe, Japan and the American Physical Society Division of Plasma Physics, APS/DPP, in Orlando, Florida, USA). Section 3 has selected presentations from these major meetings; also included in this technical section is closely related target work on fast ignition and inertial fusion energy funded via related contracts.

Demonstration of laboratory ignition is the highest priority and a major objective of NNSA. This work is encompassed in the NIC which is an enhanced management activity of the NNSA, managed with the rigor of a project. There is a point design for the ignition target for the NIC. Major R&D is required to produce this target for 2010 due to the demanding specification on the ignition targets, the cryogenic capability required for ignition, and the higher quality standards required for experiments on the NIF.

In FY07, GA was the major program participant in the development of the non-cryogenic components of the new NIC targets. These include fuel capsules with graded doped ablators with micron-scale fill tubes. The specifications on the surface finish, roundness, uniformity, doping fraction, fill tube fillet, etc., are demanding. The cryogenic hohlraum that contains the capsules is continuing to evolve. GA is fabricating the prototypes and pieces used in current cryogenic fuel layering experiments. An accelerated program of R&D and preparing for facilitization to produce hundreds of targets per year is ongoing to ensure the success of the NIC. GA also supports the Cryogenic Target System (CTS) for the NIF by supplying LLNL-onsite engineering and technician staff.

Development for current x-ray drive targets on OMEGA includes surrogate target components that are shot on OMEGA in preparation for NIC development work. For current direct drive targets on OMEGA, development includes novel ways of attaching fill tubes to direct drive targets, ways of making targets to achieve enhanced implosion performance and x-ray yield for backlighting. Research for SNL includes a design to create targets for Z with many fill tubes on the large Z targets enabling several experiments on one shot to help examine the way the fill tube itself perturbs an implosion.

#### 2. DELIVERIES

GA and Schafer supplied a wide range of ICF components to LLNL, LANL, SNL, UR/LLE, and others in FY07. Tables 2-1 summarizes these deliveries by quarter.

	FY07 DELIVERIES	BROKE	N DOWN	BY GA C	ENTER.	BY LAB	ORAT	ORY, AN	ID BY C	<b>NARTER SHI</b>	PPED		
Sum of Numb	ber Shipped	Lab											
Quarter										FI			Grand
shipped	Center	LANL	LLE	LLNL	NLUF	NRL	SNL	AWE	CEA	consortium	ILE	U Mich	Total
Q1	Capsules	73	229	6	12	0	9						329
	Micromachining	110	35	145	16		Ŋ						311
	Foams												
	Coatings												
	Development												
Q1 Total		183	264	154	28	0	11						640
Q2	Capsules	0	215	29	40	11	9						301
	Micromachining	284	181	361			9	63					895
	Foams		20	30	37					14		16	117
	Coatings			30									30
	Development												
Q2 Total		284	416	450	77	11	12	63		14		16	1343
Q3	Capsules	73	228	21	18	0	0						340
	Micromachining	298	101	210	78		2	20		71			780
	Foams		27		0			101					128
	Coatings												
	Development	12	16	14									42
Q3 Total		383	372	245	96	0	2	121		71			1290
Q4	Capsules	28	178	27	40	0	0						273
	Micromachining	110	76	133	111				12	22			464
	Foams		19		17					12	29		77
	Coatings												
	Development	4											4
Q4 Total		142	273	160	168	0	0		12	34	29		818
Grand Total		992	1325	1009	369	11	25	184	12	119	29	16	4091

Project Staff

TABLE 2-1

6 GENERAL ATOMICS REPORT GA-A26008

#### 3. DEVELOPMENT

#### 3.1 Target Development and Manufacturing

This section reports monthly accomplishments and progress for the National Ignition Campaign (NIC), as described in NIC Progress Reports for FY07.

The response of a cryogenic DT ice layer to the room temperature radiation that is encountered during clamshell shroud opening was characterized. The spherical interferometer developed for full area inspection of ablator capsules is now in operation and has been used to demonstrate that full-thickness graded germanium CH (hydrocarbon) ignition capsules meet the isolated defect specification for exterior surfaces of this capsule type. A new cryogenic experiment was initiated to directly compare x-ray phase contrast characterization of a DT ice surface with optical shadowography of the ice in the same capsule at the same time. Test artifacts were developed in order to calibrate x-ray phase contrast radiography.

First article parts for the NIC Thermo-Mechanical Package (TMP), as shown in Fig. 1, were produced in FY07. We then completed the first prototype assembly of a thermal mechanical package (TMP), as shown in Fig. 2. Also in FY07, a cryogenic experiment demonstrated significant improvement in the surface quality of a DT ice layer at 18.3 K by rapidly cooling the layer from 19.5 to 18.3 K.

Ion-assisted sputtering was demonstrated to be a considerable improvement in the beryllium coating process in FY07. Adequate gas retention in full-thickness NIF Be capsules using ion-assisted sputtering was demonstrated. Two batches of shells were coated using this process, and all of the



Fig. 1. First prototype assembly of a hohlraum inside of the thermal mechanical package.



Fig. 2. Two components of the thermomechanical package; a silicon equalizer glued to the TMP can and a TMP can before assembly.

shells tested from these batches were proven to be leak free. In addition, the use of Be mandrels was demonstrated to reduce the uptake of oxygen in Be shells.

Ionized physical vapor deposition (IPVD) was tested on Au/U cocktails and was shown to improve the shelf life of the coating and the joint at the waist of the hohlraum. Installation was completed of a new LLNL-designed station for precise assembly of micro fill tubes onto ignition capsules. A versatile electron-beam and sputter deposition coating system was transferred from LANL to GA to improve beryllium capsule development capability.

A milestone to develop a preliminary NIF/NIC target component binning strategy that addresses target parameter variability and provides the required manufacturing and assembly flexibility to meet campaign requirements was completed. CH capsules doped with Ge that meet NIC ignition specifications and measured a batch yield of 40%–75% were manufactured. We also completed a capsule and fill tube assembly for a multi-view radiography experiment, as shown in Fig. 3. The first ignition prototype NIC target assembly was fabricated and cooled to 18 K, demonstrating cryogenic performance and completing a milestone, as shown in Fig. 4.



Fig. 3. A 2-mm Be capsule and fill tube assembly for a multi-view radiography experiment showing the tapered fill tube and the transition to the fill line to the reservoir.



Fig. 4. Top view of the first NIC ignition prototype target assembly showing the Si cooling arms and the tented capsule.

We developed a process for bonding fill tubes to Be shells that optimizes the surface treatment of the components and the epoxy to maximize the strength of the bond by more than 10x. Pure uranium NIC-scale hohlraums, with a thin electroplated gold protective liner, were tested for lifetime and oxygen pickup for over seven weeks and met specifications.

A baseline plan for NIF target assembly flow, including sub-assembly at GA and assembly and proofing at LLNL was completed. The first gold-boron co-sputtered hohlraums for experiments at OMEGA, which successfully demonstrated reduction in wall backscatter, were delivered to UR/LLE. A milestone for the transfer of fill tube assembly technology from LLNL to GA was completed. We completed a Level 2 DOE milestone to demonstrate a scientific prototype ignition capsule with fill

tube, and produced a cocktail hohlraum with the shelf life needed for ignition experiments. A plan was completed for design and fabrication of all assembly point workstations that is consistent with a start of pilot production in 2008. We demonstrated component pre-pilot production for capsules, fill tube assemblies, Au hohlraums and thermo-mechanical package (TMP) components, and completed a second station for subassembly of hohlraums and TMP components.

A batch of prototype Laser Entrance Hole (LEH) windows was received and successfully leak checked to establish the viability of this design for cryogenic NIF targets. We completed assembly of an ignition prototype target for testing with tritium in the Hohlraum Test System (HTS). A non-destructive radiography technique was developed to allow the measurement of both argon and copper content in Be capsules with a spatial resolution of 2 micrometers and a sensitivity of 0.15 atom %.

We produced the first hohlraum component with a gold-boron liner for NIF Early Opportunity Shot experiments, as shown in Fig. 5.



Fig. 5. Hohlraum components for NIF Early Opportunity Shot experiments.

#### 3.2 Target Development

In this section, attachments of technical presentations summarize the research and development work, and the progress, on the NIF (NIC Target Development) and supporting current deliveries for OMEGA (NIC x-ray drive target production and NIC direct drive target production), Z (SNL Target Development and Production) and the NRL laser target development. These presentations represent work discussed at major international conferences including the 5th International Conference on Inertial Fusion Sciences and Applications in Kobe, Japan, and the 49th Annual Meeting of the APS Division of Plasma Physics in Orlando, Florida, USA. These attachments are selected presentations from these major meetings; also included in this technical section is closely related target work on fast ignition and inertial fusion energy funded via related contracts.

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- Akli, K.U., "Laser Heating of Solid Matter by Light Pressure-Driven Shocks at Ultra-Relativistic Intensities," 49<sup>th</sup> American Physical Society DPP Meeting, Orlando, Florida, November 12–16, 2007.
- Alexander, N.B., "Mass Production Layering for IFE," US/Japan Workshop, San Diego, California, March 5-6, 2007.

- Alexander, N.B., "IAEA CRP on IFE," IFE Science and Technology Strategic Planning Workshop, San Ramon, California, April 24–27, 2007.
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- Back, C.A., "OMEGA Ordering/Z and NLUF Targets," US Department of Energy Target Fabrication Review, San Diego, California February 7, 2006.
- Back, C.A., "Overview of GA Plans for New SNL Targets," presentation to Sandia National Laboratories, San Diego, California, July 11, 2007.
- Back, C.A., "Integrated Target Scheduling," OMEGA FY08 Scheduling Meeting, Rochester, New York, June 27, 2007.
- Back, C.A., presentation given at University of San Diego, La Jolla, California, July 31, 2007.
- Back, C.A., "Current and Projected Needs for OMEGA," VanFleet Review, San Diego, California, August 28, 2007.
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- Blue, B.E., "Astrophysical Jet Experiments on Inertial Confinement Fusion Machines," 5<sup>th</sup> International Conference on Inertial Fusion Sciences and Applications (IFSA), Kobe, Japan, September 9–14, 2007.

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- Buckingham, R.T., "Production of Hydrogen Using Nuclear Power by the Sulfur=Iodine Hydrogen Cycle," Bi-Annual Steering Committee Meeting, Korea, May 16, 2007.
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- Hund, J.F., "IFE Target Fabrication Update," HAPL Meeting, Washington, DC, October 29, 2007.
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- Nikroo, A., "Progress Towards Fabrication and Metrology of Ignition Design Capsules," 5<sup>th</sup> International Conference on Inertial Fusion Sciences and Applications (IFSA), Kobe, Japan, September 9–14, 2007.
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- Wilkens, H.L., "Holhraums Energetics and Symmetry," IET VTC with Lawrence Livermore National Laboratory, April 21, 2007.
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- Zimmerer, Z., "Thermal Mechanical Package (TMP) Subassembly," Pilot Production Meeting, Livermore, California, July 19, 2007.

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#### **ATTACHMENTS**

- "Recent Success in Fabrication of Depleted Uranium and Cocktail Hohlraums for the National Ignition Facility," by H. Wilkens, presented at the 5th International Conference on Inertial Fusion Sciences and Applications, Kobe, Japan, September 9-14, 2007.
- "Progress Towards Fabrication and Metrology of Ignition Design Capsules," by A. Nikroo, presented at the 5th International Conference on Inertial Fusion Sciences and Applications, Kobe, Japan, September 9-14, 2007.
- "Progress in Demonstrating Feasibility of the Target Supply for Laser Fusion," by J. Kilkenny, presented at the 5th International Conference on Inertial Fusion Sciences and Applications, Kobe, Japan, September 9-14, 2007.
- "Astrophysical Jet Experiments on Inertial Confinement Fusion Machines," by B. Blue, presented at the 5th International Conference on Inertial Fusion Sciences and Applications, Kobe, Japan, September 9-14, 2007.
- "Laser Drilled Counterbored Fill Holes in Beryllium Capsules," by A. Forsman, presented at the 49th Annual Meeting of the Division of Plasma Physics, Orlando, Florida, November 12-16, 2007.
- "Ultra-Intense Laser Beam Interactions in Cone Geometry for Fast Ignition," by R.B. Stephens, presented at the 49th Annual Meeting of the Division of Plasma Physics, Orlando, Florida, November 12-16, 2007.
- "Laser Heating of Solid Matter by Light Pressure-Driven Shocks at Ultra-Relativistic Intensities," by K. Akli, presented at the 49th Annual Meeting of the Division of Plasma Physics, Orlando, Florida, November 12-16, 2007.
- "Fabrication and Metrology of Ignition Design Copper Doped Beryllium Capsules With Fill Tubes," by A. Nikroo, presented at the 49th Annual Meeting of the Division of Plasma Physics, Orlando, Florida, November 12-16, 2007.

## Recent success in fabrication of depleted uranium and cocktail hohlraums for the National Ignition Facility





## Heather Wilkens General Atomics

5th International Conference on Inertial Fusion Sciences and Applications September 14, 2007 Kobe, Japan



## Collaborators

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**J. Cooley** Los Alamos National Laboratory

### And many others...







# The NIF target design calls for a uranium or "cocktail" hohlraum to minimize wall losses



- Composite has higher net opacity than constituents
  - Higher opacity = more re-emission
  - Provides margin for ignition on NIF
- Addition of U to Au hohlraum:
  - Radiation losses reduced by 17%







## Developments for NIF are focusing on meeting hohlraum can design specifications



Must withstand handling and a <u>minimum of 2 week exposure to air</u> for final assembly





# Keeping the depleted uranium from oxidizing is the greatest experimental challenge



# The multi-layers are made by rotating the substrate between separate Au and U sputter sources



45° Sputter source

**View-ports**<sup>1</sup>/

Rotating arm

Rotating mandrel onto which material is sputtered

### Oxygen mitigation:

- Base pressure high 10<sup>-8</sup> Torr
- Monitor chamber with residual gas analyzer




### Sputter deposition system



• Use this system to deposit cocktails or U-only hohlraums





### Schematic of the basic sputtering process

- Sputter deposition is a type of physical vapor deposition
  - Film quality dependent on the energy of the particles arriving at the substrate surface







# Concerns over poor yield and shelf-life prompted change in deposition technique

- Yield was <40% intact post leach
- Shelf-life limited to 2-3 days
- Yield of parts with required lifetime of >2 weeks = 0%



Example of failure during leach





# Cocktail coatings on flat substrates fared better with time than those on mandrels

- Microstructure is weaker along barrel
- Coatings on flat substrates pick up less oxygen over time than freestanding hohlraums
- Coating at oblique angles is known to induce selfshadowing
  - Low density, porous films





# Transmission electron microscopy images support concerns over self-shadowing



Cocktails on flat substrates are planar, uniform, & have well-defined interfaces



Growth on mandrel barrel is non-uniform, angled, and sometimes porous





### Recent alterations to coating geometry result in dramatically improved yield and shelf-life

- Ion assist promotes better mobility of adatoms
- Improvements in density and structural integrity has allowed:
   UPDATE #s
  - 93% yield through fabrication
  - 70% of these parts have a shelf-life of >4 weeks in air (higher % >2 weeks)
    - Minimal oxygen uptake

Produced cocktails that had shelf-lives of several weeks Yield of intact parts increased from <40% to ~70% Focused on U only at the beginning of R&D effort







# U-only design is preferable from a fabrication standpoint

### Small hit in radiation temperature

- Some energetics penalty in replacing Au/U with U (U gives ~75% of the cocktail benefit)
- U performance is relatively less sensitive to passivating layer thickness
- Easier fabrication, higher yield
  - Explain





# Uranium-only hohlraum halves now exceed the shelf-life specification





#### • Part cut for AES after 4 weeks in air

- 0.2 µm sputtered Au liner
- No visible signs of degradation under microscope
- Au appears in bulk because of overlap in secondary AES peaks





### Much progress has been made on NIF hohlraums...

- Demonstrated ability to produce NIF-scale cocktail and uranium-only hohlraum halves
- U-only design preferable from fabrication standpoint
- NIF "early opportunity shots" begin next year
  - Au, U and cocktail shots are planned (L. Suter talk)





# Progress towards fabrication and metrology of ignition design capsules

Abbas Nikroo IFSA 07 Sept 9-14 , Kobe Japan



#### Almost all of Be shell specifications have been met

Fill tube details are being addressed currently

 Reproducibility, reliability and yield of processes is major focus currently

Capsule outer radius, tolerance	± 5µm
Ablator composition	Ве
Ablator layer thicknesses	see table
Ablator layer dopant concentration	see table
Ablator oxide layers	
Ablator – average mass density	± 3% absolute, ± 1.5 % relative to campaign average
Ablator layer density	see table
Ablator – voids	< 3% void fract, < 0.1 µm3 void volume
Ablator – measurement of x-ray optical depth variations	accuracy <0.01%
Ablator thickness non- uniformity	see table
Ablator inner surface figure	see table
Capsule surface isolated defects	see figure
Capsule cleanliness	See isolated defects
Ablator – Low level impurities	sum(atomic fraction)*Z <sup>2</sup> < 0.1
Gas retention	> 7 day half life at room temp



#### Three ablator designs are being currently considered



## We have produced graded Cu-doped Be capsules at NIF-scale by sputter deposition



# Ionized physical vapor deposition was utilized to obtain gas retentive shells



- Argon content of shells is also increased from <0.1 at% to as much as 2 at% (spec 0.25 ± 0.1 at %)
- A coater configuration identified that leads to ~ 0.25 at% Ar in gas retentive shell meeting specifications
  - Current effort focused on understanding the parameter space to extend to other coating systems

# USAXS measurements indicate reduced bulk porosity using IPVD

- USAXS shows that the pore fraction has been significantly reduced
  - Low scattering intensity at intermediate q implies that voids are significantly lower

 IPVD works by creating a dense structure by creating additional ions that are then accelerated toward the target



IPVD sputter deposition sharply reduces the intergranular porosity and hence permeability

## Current precision radiography indicates shells meet 10<sup>-4</sup> optical depth uniformity spec

- Precision radiograph examines azimuthal optical depth uniformity of the shells
- For graded Be:Cu two factors can lead to OD variations
  - Roughness at Cu doped interface
  - Void agglomeration
- Much data has been collected
  - Meet current assumed specification
- A power spectrum based specification is being developed
- Isolated features can dominate OD power spectrum



#### X-ray transmission vs angle



#### Graded doped Be:Cu shell

### Polished Be capsules are approaching NIF ignition surface finish requirements



- Polishing reduces as coated shell high mode roughness to well below spec
- Low mode mainly dominated by mandrel
  - Mandrel selection mitigates that issue
  - Polishing does not increase low mode





## Be shells have met outer surface isolated defect feature requirement

- Shells examined by phase shift diffractive interferometer (PSDI)
- Patches taken around surface
- 60% of data analyzed
- No major features found
- RMS also below NIF curve requirement
- Need to collect more data

   We are collecting more data on inner surface with PSDI nearly in production mode



## Inner surface of shells made using ion assist are below or near the NIF spec



PSDI Patch scans ~ 500  $\mu$ m dia

- Destructive test
- Inner surface determined by mandrel and its removal process
- More data will be taken as unit is available in production mode



#### Fill holes have been drilled to specification



- Hole volume/mass defect meets spec
- Fill hole focused on counterbore needs
   development



foil test

Counterbore hole

16/MAY/07

Forsman FPo46

# NIF scale fill tubes have been attached to beryllium shells

Multiple capsule and fill tube assemblies have been built and tested for



- Leak, pressure and openness of tube testing integrated into process
- However, assemblies have failed during transport

#### **CH** capsules have met all NIF specifications

- Tens of graded CH:Ge capsules have been produced and characterized that meet all specifications including:
  - NIF outer surface power spectrum
  - Wall thickness uniformity
  - Doping levels and layer thicknesses specifications



- Isolated defects
  - Shells made in batches of ~
     9 shells meet the isolated defect specification



#### Almost all of Be shell specifications have been met

Fill tube details are being addressed currently

 Reproducibility, reliability and yield of processes is major focus currently

Capsule outer radius, tolerance	± 5µm
Ablator composition	Ве
Ablator layer thicknesses	see table
Ablator layer dopant concentration	see table
Ablator oxide layers	
Ablator – average mass density	± 3% absolute, ± 1.5 % relative to campaign average
Ablator layer density	see table
Ablator – voids	< 3% void fract, < 0.1 µm3 void volume
Ablator – measurement of x-ray optical depth variations	accuracy <0.01%
Ablator thickness non- uniformity	see table
Ablator inner surface figure	see table
Capsule surface isolated defects	see figure
Capsule cleanliness	See isolated defects
Ablator – Low level impurities	sum(atomic fraction)*Z <sup>2</sup> < 0.1
Gas retention	> 7 day half life at room temp



### **End Of presentation**

# Inner surface of full thickness shells made also meets NIF specification



 Again more data needs to be taken with PSDI now available for routine examination

## Spherical Interferometer allows mapping of the outside and inside of shells

- Phase sensitive diffractive interferometry (PSDI) has been adapted to provide complete mapping of exterior capsules surface
  - Best tool to quantify isolated defects





- Data propagation is manual and slow
  - Automation in process
- Shell flipper under development and construction — Automation of data acquisition
- Above will increase throughput

# Failure mechanism of glue joint to Be was identified and remedied

- Glue-Be joint identified as weak joint
- Glue joint strength optimized
  - Optimization of the adhesive type (Dymax)
  - Surface preparation (ultraclean and activated)
- Allows us greater safety margin for handling 10μm scale assemblies
- Improvements observed at 20 µm fill tube dimension
  - Extending to 10 µm tubes currently
  - We have not DT filled capsule with < 20 μm fill tube yet</li>







Failure at 28 mN

166mN



### Progress in Demonstrating Feasibility of the Target Supply for Laser Fusion

#### Presented by Joe Kilkenny

at the Fifth International Conference on Inertial Fusion Sciences and Applications Kobe, Japan September 9-14, 2007



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#### UCLA - Robin Garrell

Lawrence Livermore - John Perkins

**General Atomics -** Dan Goodin, Neil Alexander, Amy Bozek, Graham Flint, Dan Frey, Remy Gallix, Jared Hund, Abbas Nikroo, Reny Paguio, Ron Petzoldt, Diana Schroen, Sheida Saeidi, Emanuil Valmianski

Los Alamos - Jim Hoffer, Drew Geller, John Sheliak

*Top-level objective = show feasibility of economical target fabrication for commercial fusion* 



# *Our objective is to develop the "target factory" for HAPL*



### IFE Ignition Targets - "Beyond the Basics"

- Potential manufacturing processes that are adaptable to mass-production identified
- An experimental demonstration program for each process step laid out and initiated
- A "baseline" target design identified and good progress made on its fabrication ....

#### Basic process steps

- 1. Fab foam capsule
- 2. Overcoat foam
- 3. Fill/layer fusion fuel
- 4. Inject
- 5. Track and engage



#### "Beyond the basics" on foam capsules



*IFE-sized (~4 mm OD) divinybenzene (DVB) foam capsules* 



FTF-sized (~2.4 mm OD) DVB foam capsules

- Optimization of rotobeaker "curing" to improve Non-Concentricity (NC)
- Yields of DVB foam capsules at 1 to 3% NC improved dramatically



### Checklist of foam capsule progress

Attribute	Value	Tolerance	Meet?	Comments
Composition	DVB	(Low O/N)	Yes	DVB is original baseline foam
Diameter	4.6 mm	±0.2	Yes	<b>Controlled by process flows Characterization: optical</b>
Wall thickness	176 µm	±20	Yes	Controlled by process flows
Density	≤100 mg/cc	[25%]	Yes	Calculated, measured optically
Pore size	~1 µm	<3 μm	Yes	Qualitative by SEM - 1 to 3 $\mu m$
Out of round	<1 % of radius		Yes	Limited data, but never an issue
Non- concentricity	< 1-3% wall th.		Yes	Basic feasibility demo'd, yields 5 to 60%

### So does this mean we're finished? (no...)

#### **Overcoats** for the foam capsules are a current focus!

Status - for polyvinyl phenol on DVB foam (original baseline, made by interfacial polycondensation)

Attribute	Value	Toleran ce	Meet?	Comments
Composition	CH +	O/N OK	Yes	Polyvinyl phenol was "baseline", others possible
Thickness	1 μm	±1	No	Originally 1 μm, ~10 microns may be acceptable
Surface finish	<50 nm		No	
Permeability	Holds DT at cryo		No	Low yield of overcoats, shrinkage, implosion, "microcracks" common
Strength	For filling		Not yet shown	

A major difficulty is overcoating (sealing) hi-aspect ratio shell at wet stage

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## Alternate approaches to the original, baseline method for overcoats have been evaluated

#### Evaluated two major approaches..

- 1. Two-step process fill DVB pores with PVP then GDP coat
- 2. Switch to smaller-pore foam like resorcinol formaldehyde (RF)

#### PVP overcoated with GDP



Cross section of coated DVB shell



#### ...the simpler approach turns out to be best


#### The first gastight HAPL-sized foam capsule - GDP on RF

Half-life with deuterium testing confirms permeation
 flow - not "pinholes"



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#### A cryogenic fluidized bed has been constructed to demo mass-production layering

- Static controlled
- Scoping tests show good randomization
- Initial cryostat cooldowns to ~ 11K
- Method to "grab" one shell for characterization has been done at cryogenic conditions



Unfilled shells at 11 Kelvin



# Target injection now has several acceleration options ...

#### Previously demonstrated:

-Velocity  $\geq$ 400 m/s, time jitter 0.5 ms, 2-piece sabot separation in vacuum -Target placement accuracy of 10 mm at 17 meters standoff (1 $\sigma$ )





Magnetic diversion reduces gas in chamber, reduces heating, and allows slower injection

#### Range of options, including:

- 1. Gas-gun for >400 m/s
- 2. "EM Slingshot" concept for 50-100 m/s



Improved accuracy demo'd at 50 m/s (without 2-piece sabot)  $\rightarrow$  4 mm at 17 m (1 $\sigma$ ), and done with ~1 mg projectiles



#### Tracking - optical table demo of "hit-on-fly" engagement

Engagement of Driver with 4mm Target

4 mm target

2000

4000

4000

2000

2000

X-axis (um)

-2000

- IFE requirement is alignment of lasers and target to 20 μm
- System using lasers, optics and fast steering mirror
- Also "glint" from target ~1 ms before the shot aligns optical train (target itself is the reference point)



-axis (um)

200

-4000

**Target Engagement Results** 

X-axis (um)

20 um goal

100\*

200

(-axis (um)

-200





- Scaled experiment, velocity ~ 5 m/s
- Accuracy of hitting "onthe-fly" is 110-150 microns now (1σ)
- Working toward 20 micron goal for demo



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## Summary/Conclusions

- 1. Moving "beyond the basics" in demonstrating laser fusion target supply
  - Mass-production identified for each step
  - Demo programs underway with good progress
  - Advanced methods being evaluated
- 2. Basic foam capsules can be made
  - Focus now on yield curves and detailed specifications
- 3. Working to get gastight, smooth overcoats first one made
- 4. Mass production demo for layering now undergoing cold checkouts
- 5. A range of target injection methodologies available
- 6. Tracking and engagement table-top demo is closing in on our goal of 20 micron alignment in a scaled experiment



## Astrophysical Jet Experiments on Inertial Confinement Fusion Machines

#### by B. Blue

Presented at the 5th International Conference on Inertial Fusion Sciences and Applications Kobe, Japan

September 9-14, 2007



#### Summary

- We have developed a target platform to study high Mach number, compressible, turbulent plasma flows
- Scaled experiments allow us to study deep nonlinear dynamics relevant to astrophysical phenomena in the laboratory
- A series of experiments has been performed to study:
  - The transition to turbulence and its effect on global hydrodynamic evolution
  - Jet interaction dynamics
  - Shock interactions with spherical objects



# Several fundamental questions about astrophysical jets remain unanswered



We are not recreating all of the physical processes in an astrophysical jet. Rather, we are isolating specific subset of the physics and testing them via a combination of experiments and simulations.



## Euler scaling permits us to study astrophysical jets in the laboratory



#### 50 ns in the laboratory corresponds to 100 years in space



## Radiography was used to diagnose the jet's temporal evolution



## By observing the jets at different times, we can diagnose their turbulent evolution







## By varying target components, we were able to study different aspects of jet physics

#### 5.2 keV V Backlighter



# 4.7 keV Ti Backlighter

#### 0.1 um cell size foam







# Targets were constructed to address the physics of a jet deflecting off a gas cloud





# 3D RAGE simulations accurately model the large scale hydrodynamic motions



## Significant target characterization is needed to constrain the simulations



## A large number of well characterized targets were shot to study jet deflection physics



## Targets were constructed to study the physics of a shock interacting with a spherical object

TIM3 and TIM5 500  $\mu$ m dia. Al<sub>2</sub>O<sub>3</sub> sphere, embedded in CH(Br) and CH 0.3 g cm<sup>-3</sup> RF foam ablator Scale-1 Shock in foam hohlraum

**Dual-axis backlighting :** 







## The experiment shows more breakup of the ball than predicted by the simulations





# Characterization of assembled targets is necessary for interpreting experimental results





**Characterization impossible after the shot - Target destroyed** 



# Characterization of individual target components is critical before the target has been assembled

#### Images of hole before and after polishing





Characterization is necessary for high-quality targets

# Foam Perturbations

#### Cast foam surface finish





## Our collaboration is using observation time on the Hubble Space Telescope to study jet dynamics



HST project to obtain 3<sup>rd</sup> epoch to follow instabilities, clumps, and shear

3 targets: HH 1&2, HH 34, HH47 Data to be taken August 2007 – January 2008



#### Summary

- We have developed a target platform to study high Mach number, compressible, turbulent plasma flows
- Scaled experiments allow us to study deep nonlinear dynamics relevant to astrophysical phenomena in the laboratory
- A series of experiments has been performed to study:
  - The transition to turbulence and its effect on global hydrodynamic evolution
  - Jet interaction dynamics
  - Shock interactions with spherical objects



#### Laser drilled counterbored fill holes in beryllium capsules

#### A. Forsman, E. Lundgren, A. Komashko, K. Moreno

General Atomics, San Diego, USA



# Ideal fill holes have > 30:1 depth : diameter aspect ratio.

- The holes need to be ~ 5 um in diameter.
  - Allowed mass defect is 125% of an ideal 5 um hole.
  - Hole needs to allow for pyrolysis.
- 175 um of multilayered Be and 15 um thick GDP mandrel.
  - The drilling process is more akin to drilling a pipe than a hole.
- Drilling process produces a reasonable approximation to the ideal shape.





#### Nanosecond lasers form the hole and the counterbore

- Technique proven for fuel injectors
- Nanosecond lasers (Sierra)
  - Reliable & maintenance free
  - 532 nm, 4 ns



- 25 mm laser focusing lens
  - Good standoff
  - Survivability & depth of focus.





## Formatted laser pulses enable the drilling of the fill holes

- Double pulse format outperforms conventional technique
  - Trademarked by GA as SuperPulse
  - Forsman et al., J. Appl. Phys 98 033302-1 (2005)
- Conventional approach reduces
  ablation debris
  - Femtosecond lasers
  - Gas assist jets
- Double pulse format uses ablation debris
  - Increases basic material removal rate.
  - Improves ejection of ablation products.





1 mm type 304⁄ stainless steel

deneral



#### The counterbore is also drilled using the laser in situ.

- In-situ drilling is fast and accurate
  - Eliminates need for ultra-precise tool
- The tapered bottom prevents the fill tube from blocking the hole





#### A sacrificial foil is used to control surface debris

- Debris from ablation will normally accumulate on the surface around the hole.
  - This is undesirable.
- A thin foil is placed in imminent contact with the capsule at the drill site.
  - External debris accumulates on the foil
  - The foil is removed after drilling



#### $5 \ \mu m$ hole entrance





## Present process development work is focused on parasitic processes that limit aspect ratio and quality

- Parasitic processes arising due to small, high aspect ratio holes:
- Unwanted laser energy deposition
  - Occurs in the bore walls of the high aspect ratio hole.
  - Can be thought of as transmission losses.
- Unwanted plasma thermal deposition.
  - Hot (100 000 K) plasma flows out through a small, relatively long hole.

#### Hole enlargement due to plasma

 Radially expanding plasma can ablate the bore walls next to the target point

#### Internal debris management

- How to control redeposition



## Parasitic processes, continued

- 1<sup>st</sup>-order EM waveguide model shows that 70% transmission losses at the hole bottom should be expected.
  - Cannot experience losses less than this for a cylindrical hole.
  - Can reduce hole taper through more energetic primary pulses.
  - Hole taper would increase unwanted laser deposition.
- Adjusting the durations and timing of the laser pulses allows us to influence the temperatures and the durations of the ablation plasmas.
  - Can also affect material redeposition.
- Becomes multi-dimensional process optimization.



## The double pulse technique already mitigates these parasitic processes

- Improved ablation rates and material ejection efficiency mean that
  - Fewer laser shots are used → less overall energy applied..
  - Redeposition is reduced
- Each laser pulse is less intense than it would have to be if a conventional technique was used
  - Ablation plasmas are less energetic and hence cause less damage as they exit the hole.
  - Absolute transmission losses are smaller and thus undesirable laser energy deposition is reduced.
- Further process optimization is underway



## A limit on the aspect ratio for small holes ?

- 30:1 or 40:1
  - $-5\,\mu m$  hole
  - Beryllium & Aluminum
  - 4 ns laser
    pulses
  - Double
    pulse format
  - 532 nm



Laser Power



## Ultra-Intense laser beam interactions in cone geometry for Fast Ignition

#### **R.B. Stephens, General Atomics**

49th Annual Meeting of the Division of Plasma Physics November 12-16, 2007 Orlando, FL

This work was performed under the auspices of the U.S. Department of Energy under contracts No.DE-FG02-05ER54834 and W-7405-Eng-48.



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IFT\P2007-005

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#### Abstract

#### FI pulses are absorbed inside cone - complex geometry -hard to understand

- Reflect light?
- Create forward e current?

#### Expts at 10<sup>20</sup> W/cm<sup>2</sup> to measure reflectivity and electron creation

- Preliminary results show
  - High reflectivity at glancing incidence (~40x)
  - Lower electron generation at glancing incidence (~10x)
    - --> Minimal light absorption at glancing incidence
  - No Electrons generated fluorescence forward from laser beam (Escaped electrons carry insignificant energy)
- $\Rightarrow$  Dominant cone effect is focusing light
- $\Rightarrow$  Energy mostly absorbed on near-normal incidence

Design cones for concentrating light in glancing incidence reflection

#### Ignitor pulse converted to electrons inside cone

- High conversion efficiency demonstrated in ILE core heating expt.
- What is the role of the cone geometry?


#### 1) Cone walls reflect and concentrate light at tip

 Particle in cell (PIC) modeling with sharp interfaces show side wall interactions strongly reflect light at FI intensity 10<sup>19</sup> to 10<sup>20</sup> Wcm<sup>-2</sup>



### 2) Electrons formed in sidewalls flow toward tip and concentrate there

Surface Magnetic Field and Sheath Field are excited on Inner Surface



 $\Rightarrow$ Electrons are flowing toward the tip.

#### Created LPI with simplified geometry to investigate effect

- Titan laser pulse f/3 10<sup>20</sup> W/cm<sup>2</sup>, 1 psec, ~150 J
- Focused f/3 beam to 10  $\mu$ m
- Incident at 28° and 75° from surface normal s-polarized
- Target 0.5x0.5 mm<sup>2</sup> x 25  $\mu$ m thick
- Detect reflectance by light scattered off Spectralon<sup>™</sup> surface
- Detect electrons using Bragg mirror to image  $K\alpha$  reflectance
- Count electrons with single hit ccd (data not yet analyzed)



### Reflectance low at near normal

- Still working on calibration
- Reflection ~ Independent of prepulse





#### Reflection at glancing incidence 20-40X larger



### Fluorescence shows no evidence of forward directed hot electrons

- Normal incidence shows symmetric electron spread
- Glancing incidence shows no electrons forward from beam
- Effect seems independent of plasma gradient





### Electron generation much lower at glancing incidence (s polarization)



### Any significant electron flow would be visible

#### A few electrons can leave target without a trace

- Depends on target size preplasma expansion can increase numbers.
- Forward directed surface electrons detected with electron spectrometer.

#### Most electrons are trapped on the target

- Losing 2x10<sup>11</sup> electrons charges 1/2 mm sphere to MV
- If all MeV electrons, loss of 30 mJ
- Current flowing up support stalk insignificant ~10<sup>6</sup> electrons 4.0

#### All trapped electrons can be seen

- Target only 25 μm thick so
- Scattering cross section

No significant e flows along the surface

. In be seen . Inick so . Inorescence Jung cross section ~ independent of energy down to threshold so we follow them a 10 rough their entire lifetime 2 3 10 10 10

Kinetic Energy (keV)

T.Yabuuchi et al., Plasm & Fus Res 1,1 (2006)

H. Habara et al., Phys. Rev. Lett 97, 095004 (2006)

## Maximize efficiency with Winston non-imaging light concentrator

- High reflection at glancing incidence, minimal electron generation
- Low reflection at normal incidence, maximum electron generation
- No significant electron flow along surface
- ⇒ Maximize light intensity at tip
- Winston Collector has the right properties
  - Single bounce gets all light to the tip
  - Concentrates light proportional to f/number

See also:

QI1.00003 Linn Van Woerkom - Intense laser plasma interactions on the road to fast ignition

CO6.00012 T. Yabuuchi - Influence of sheath fields on hot electron emission from small foils irradiated by intrise laser pulses

GO6.00015 Andrew MacPhee - Short pulse laser coupling efficiency to hot electrons for fast-ignition studies



### Laser heating of solid matter by light pressure-driven shocks at ultra-relativistic intensities

Kramer Akli General Atomics 49th Annual Meeting of the Division of Plasma Physics Orlando, Florida November 12-16, 2007



This work performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344

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#### **Co-Authors and Acknowledgements**







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F. N. Beg, S. Chen, T. Ma

C. Stoeckl, W. Theobold, M. Storm.

P.A. Norreys, J. S. Green, K. Lancaster, C.D. Murphy G. Gregori.

### Abstract

Heating by irradiation of a solid surface in vacuum with  $5 \times 10^{20} W cm^{-2}$ ,  $0.8 \ ps$ ,  $1.05 \ \mu m$  wavelength laser light is studied by x-ray spectroscopy of the K-shell emission from thin layers of Ni, Mo and V. A surface layer is heated to ~ 5 keV with an axial temperature gradient of 0.6  $\mu m$  scale length. Images of Ni  $Ly_{\alpha}$  show the hot region has a ~ 25  $\mu m$  diameter. These data are consistent with collisional particle-in-cell simulations using pre-formed plasma density profiles from hydrodynamic modeling, which show that the  $> 100 \ Gbar$  light pressure compresses the preformed plasma and drives a shock into the solid heating a thin layer.

### Experimental setup



### Mo/Ni/V multi-layered targets were used to study laser-generated electrons transport and the associated isochoric heating



# Two Highly Ordered Pyrolytic Graphite (HOPG) Crystal spectrometers were used to obtain x-ray spectra: "Rear HOPG" and "Front HOPG"





### Ni Ly<sub> $\alpha$ </sub> images indicate that the hot surface region has a 25 µm diameter (much smaller than the region of cold K<sub> $\alpha$ </sub> emission).



### Two XUV imagers at 68 eV and 256 eV recorded spatial patterns of thermal emission from the rear surface of the targets



The rear surface temperature was determined to be  $\sim 400 \text{ eV}$ 

### The collisional-radiative model SCRAM was used to generate Ni spectra









### K-shell emission spectra showing the reduction of thermal lines intensity with Mo overlay



#### Temperature profile obtained using thermal line intensity ratio



The rear surface temperature is consistent with both spectroscopic modeling and xuv results

# Hydrodynamic modeling of the Vulcan laser pre-pulse shows that the pre-plasma extends $2 - 3 \mu m$ between critical and solid density



W. Theobald et al. Phys. Plasmas 13, 043102 (2006)

#### 1D PIC simulations of 5µm solid density Mo<sup>+5</sup> slab target with preplasma at two different laser intensities



Results of 1D PIC simulation: ion density profile at time 1ps for two different laser intensities. Also shown is the intial ion density profile

### 2D collisional Particle-in-Cell (PIC) simulations of a 5 µm thick Molybdenum target



The laser pulse is modeled as Gaussian in space and top-hat in time

The simulation box has a total size of  $30 \ \mu m \ x \ 60 \ \mu m$  at a resolution of  $80 \ cells \ per \ \mu m$  and 10 ions plus 50 electrons per cell

Results of 2D PIC simulation:

- (a) electron energy density (arbitrary units)
- (b) azimuthal magnetic field in units of B0=2MG at time 100fs.

#### PIC simulations suggest light pressure-driven electrostatic shock as a heating mechanism



#### **Results of 2D PIC simulation :**

- (a) longitudinal ion phase space.
- (b) electric potential (solid), and electron density (dashed) along laser irradiation axis; average over 0.25um.
- (c) energy spectrum of all electrons at time 100fs

### The amount of energy in the hot surface layer is $\sim 0.3$ J which is < 1% of the laser energy.

### Conclusion

• Heating of a sub micron thick layer at near solid density to  $\sim$ 5keV temperature by 5x10<sup>20</sup>wcm<sup>-2</sup>, 0.8 ps laser irradiation is attributed to the light pressure-driven shock.

• Such shock heating is expected only when the light pressure and pulse duration are sufficient to sweep up preformed plasma.

• The heating is interesting in its own right for creation of high energy density states of matter. It is not a major drain of electron energy and therefore does not adversely affect fast ignition.



## Fabrication and metrology of ignition design copper doped beryllium capsules with fill tubes

Abbas Nikroo APS/DPP 07 Nov 12-16 , Orlando Florida





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Lawrence Livermore National Laboratory



### Three ablator designs are being currently considered for ignition campaign







### All Be shell specifications have been demonstrated



<b>↑</b>	Capsule outer radius, tolerance Ablator composition	± 5µm Be	
Dimensional and dopant	Ablator layer thicknesses	see table	
	Ablator layer dopant concentration	see table	Capsule and fill tube specs
↑	Ablator – average mass density	± 3% absolute, ± 1.5 % relative to campaign average	have been met
	Ablator layer density	see table	
Voids	Adiator – Volds	< 3% void fract, < 0.1 µm3 void volume	Haan spec table
and density	Ablator – measurement of x-ray optical depth variations	accuracy <0.01%	
	Ablator thickness non- uniformity	see table	
Ť	Ablator inner surface figure	see table	
Surface	Capsule surface isolated defects	see figure	
•	Capsule cleanliness	See isolated defects	
Opacity <sup>↑</sup>	Ablator – Low level	sum(atomic fraction)*Z <sup>2</sup> < 0.1	
Gas retention	Impurities Gas retention	> 7 day half life at room temp	

 Process reproducibility, reliability and yield are major focus currently as we move into pilot production



### We produce graded Cu-doped Be capsules at NIF-scale by sputter deposition





AN-111607 APS/DPP07

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- Weak structure and accumulated stress in coating led to nano-cracks in shells
- Nano-cracks led to rapid leakage of gas out of the shell


## Ion assisted deposition was utilized to obtain gas retentive shells





Previous process

- Argon content of shells is also increased from <0.1 at% to as much as 2 at% (spec 0.25 ± 0.1 at %)
- Coater configuration used that leads to ~ 0.25 at% Ar in gas retentive shell meeting specifications



**Previous process** 

- •Density increase also observed ~ 1.82 ± 0.2 g/cc
- X-ray scattering confirms total void and size (<500nm) reduction



# Polished Be capsules meet NIF ignition surface finish requirements





- Polishing reduces as coated shell high mode roughness to well below spec
- Low mode mainly dominated by mandrel
  - Mandrel selection mitigates that issue
  - Isolated defects within specifications





## Inner surface of shells made using ion assist are below or near the NIF spec





#### PSDI Patch scans ~ 500 $\mu$ m dia

- Destructive test
- Inner surface determined by mandrel surface
- Blistering of inner surface has been mitigated by adjustment to removal temperature



 Effect of isolated features being modeled



# Current precision radiography indicates shells meet 10<sup>-4</sup> optical depth uniformity spec

- Precision radiograph examines azimuthal optical depth uniformity of the shells
- Three factors can lead to OD variations
  - Thickness variations
  - Void agglomeration
  - Roughness at Cu doped interface
- A more rigorous power spectrum specification is being developed
  - Sputtered shells meet nominal





#### X-ray transmission vs angle



#### Graded doped Be:Cu shell





### Fill holes have been drilled to specification





- Used super pulse nano-sec laser technique
  - Fuel injector drilling
- Hole volume/mass defect meets spec
  - 5 µm through hole
  - 15 µm counterbore
- 10 µm fill tube

A. Forsman, YO5-9



#### Bond joint meets NIF mass defect spec

Be capsule with bonded fill tube





### All Be shell specifications have been demonstrated



<b>↑</b>	Capsule outer radius, tolerance	± 5µm	
Dimensional and dopant	Ablator layer thicknesses	see table	
	Ablator layer dopant concentration	see table	Capsule and fill tube specs
<b>↑</b>	Ablator – average mass density	± 3% absolute, ± 1.5 % relative to campaign	have been met
	Ablator layer density Ablator – voids	see table	← Haan snor tahlo
Voids and density	Ablator – measurement of x-ray optical depth variations	< 0.1 µm3 void volume accuracy <0.01%	< Haan Spec table
	Ablator thickness non- uniformity	see table	
	Ablator inner surface figure	see table	
Surface	Capsule surface isolated defects	see figure	
▼ ▲	Capsule cleanliness Ablator oxide layers	See isolated defects	
Opacity	Ablator – Low level	sum(atomic fraction)*Z^2 < 0.1	
Gas retention	Gas retention	> 7 day half life at room temp	

 Process reproducibility, reliability and yield are major focus currently as we transition into pilot production

