

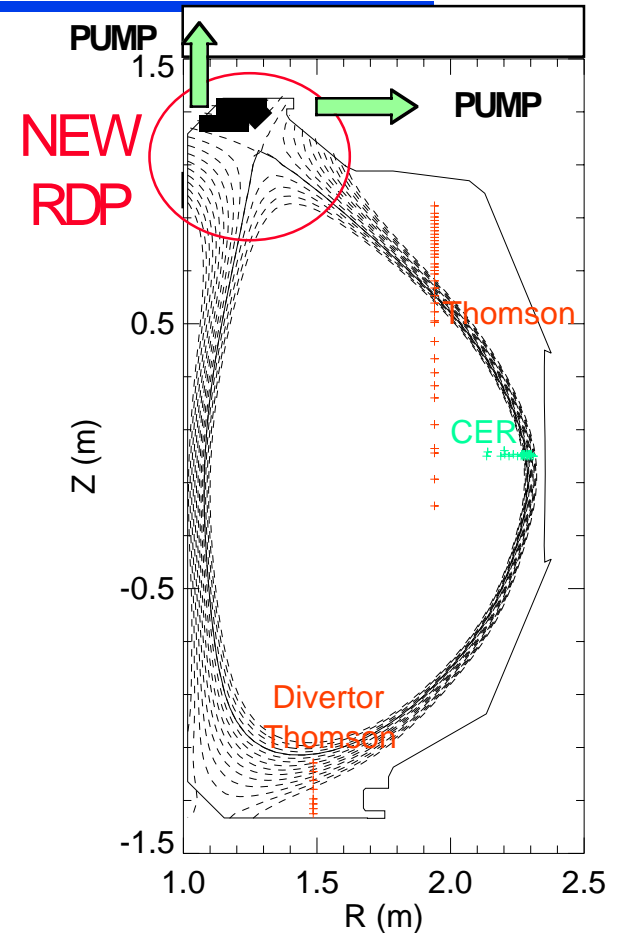
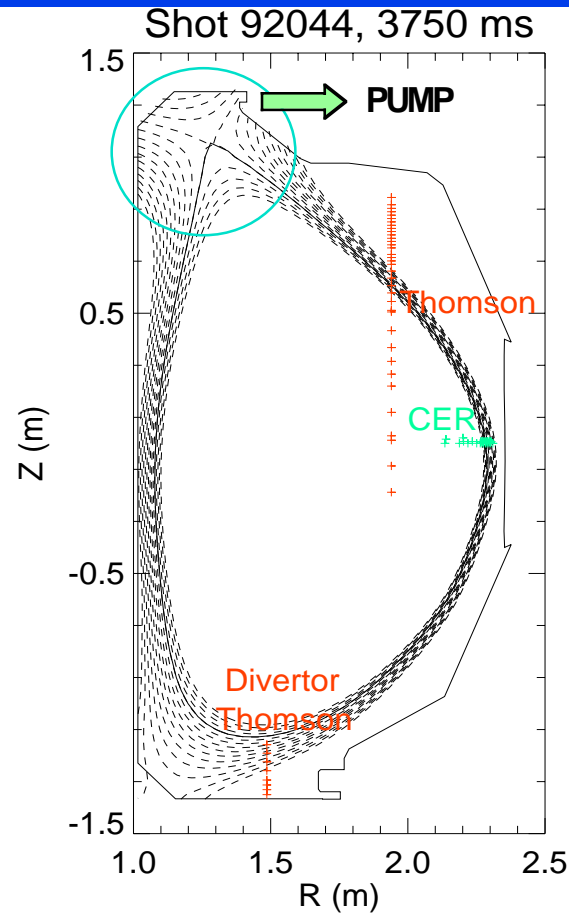
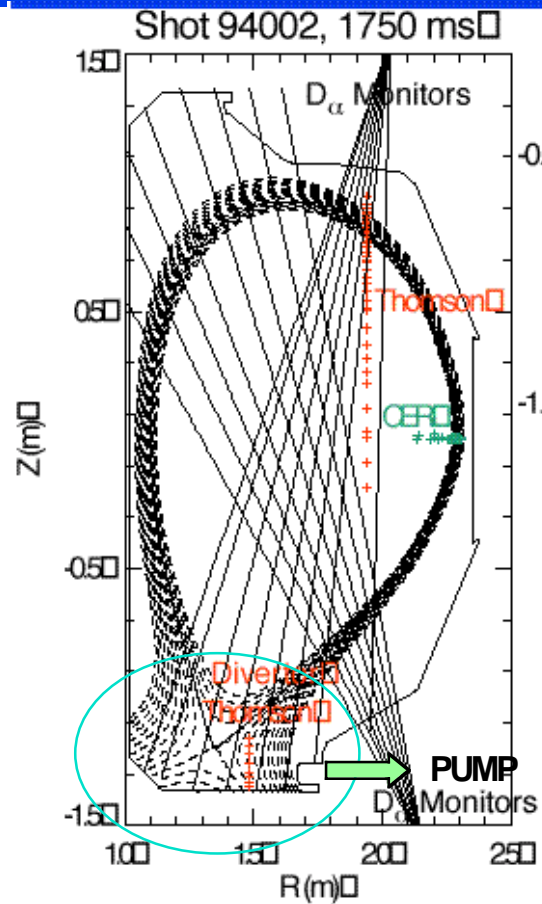
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# **UEDGE Modeling of the Effect of Changes in the Private Flux Wall in DIII-D on Divertor Performance**

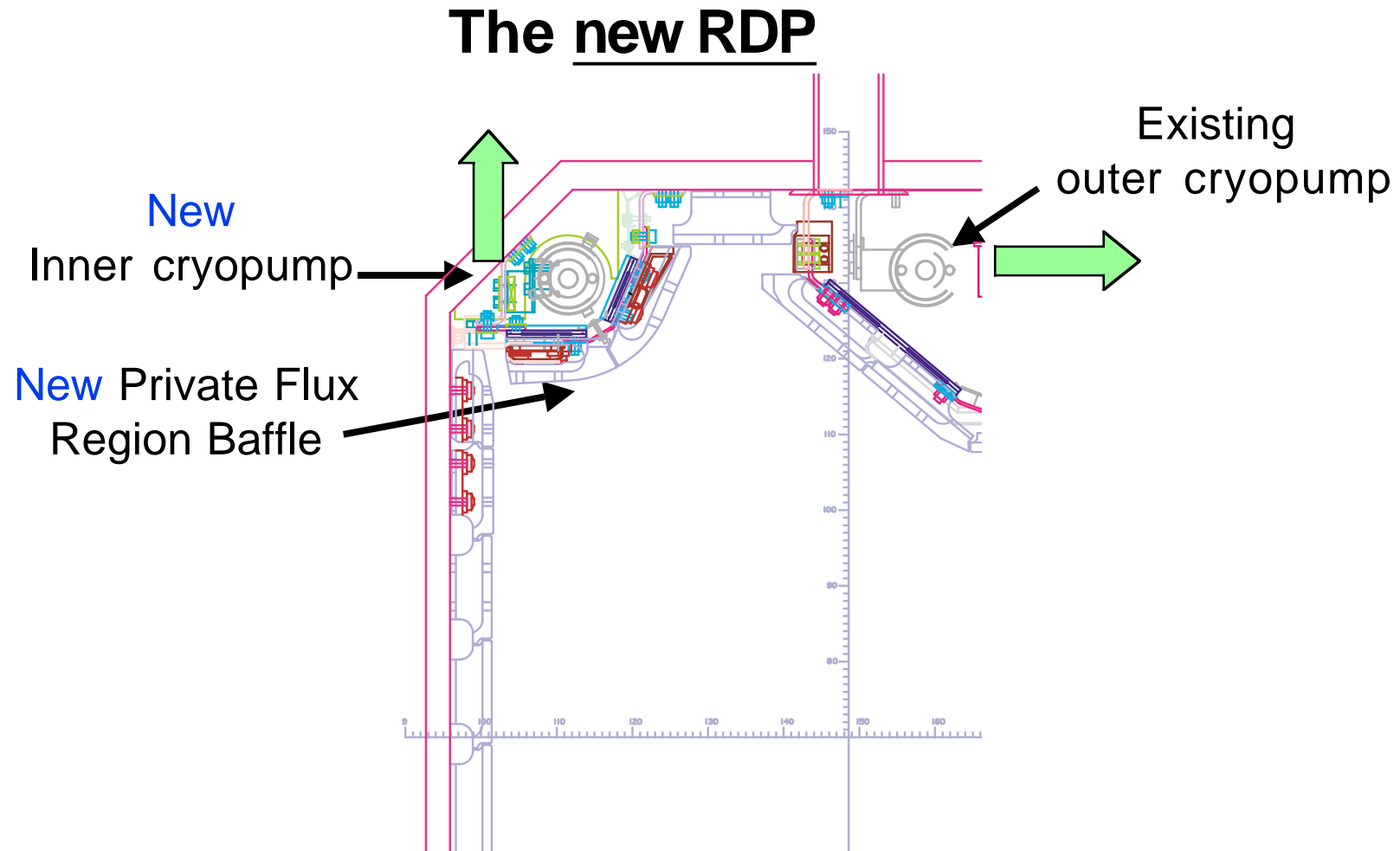
**N.S. Wolf, G.D. Porter, M.E. Rensink, T.D. Rognlien**  
*Lawrence Livermore National Lab,*  
**And the DIII-D team at *General Atomics***

**Presented at the APS-DPP Meeting, Nov. 17, 1999**

# MOTIVATION: determine the effect of changes in the DIII-D upper divertor



# Upper divertor (RDP) now has a dome in the private flux region and a pumped inner leg



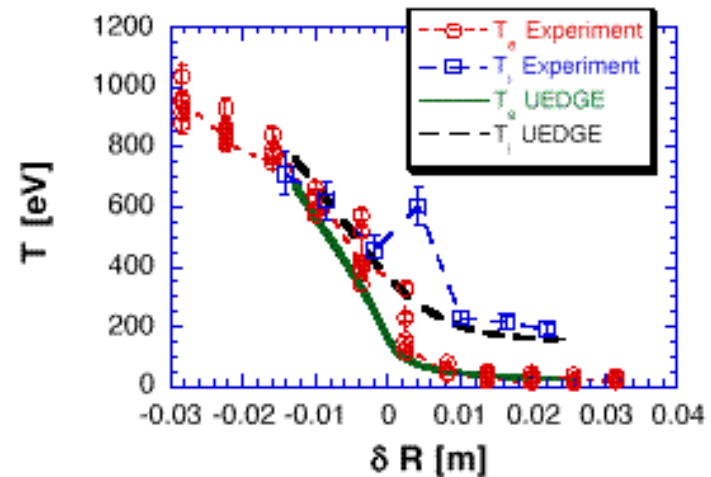
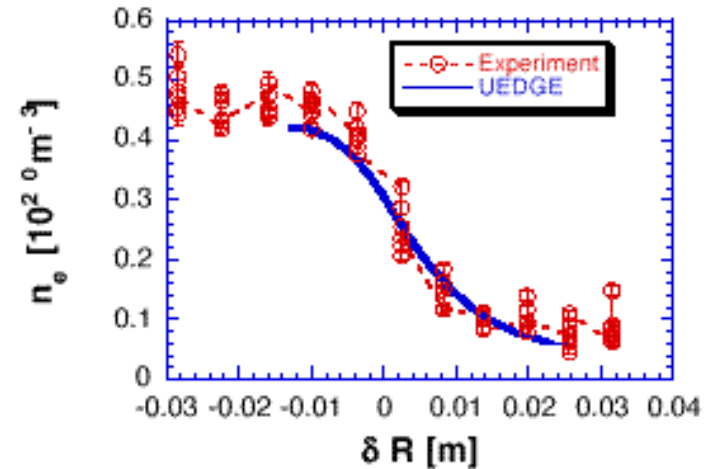
# METHOD: simulate the SOL and divertor plasma with the UEDGE code

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- ◆ UEDGE solves equations for ion continuity, energy and momentum on 2-D domain, simulating the plasma from:
  - 96% flux surface to limiter surface in radial direction,
  - plate to plate in poloidal direction
- ◆ Hydrogenic ion fluid (Braginskii equations)
- ◆ Navier Stokes fluid equations for neutrals
- ◆ Collisional-radiative hydrogenic rates
- ◆ Turbulence-driven perpendicular (radial) transport
- ◆ Carbon source is physical and chemical sputtering from walls, using Univ. Toronto model [Davis & Haasz, J. Nucl. Mater. 241-243, 37,1997]
- ◆ Force balance equations for 6 ionization states of carbon
  - diffusive neutral carbon fluid
  - non-equilibrium coronal impurity radiation

# VALIDATION: simple radial transport model agrees with midplane $n_e$ and $T_e$ profiles

- ◆ UEDGE uses constant turbulence-driven radial diffusion coefficients:  
 $D_{\perp} = 0.1 \text{ m}^2/\text{s}$   
 $\chi_i = \chi_e = 0.4 \text{ m}^2/\text{s}$
- ◆ Radial profiles match **experimental** results for the lower single null plasmas shown
- ◆ These and many other results indicate that UEDGE models the DIII-D experiment well



# SUMMARY of our SIMULATIONS for the new RDP

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- ◆ 1) Core carbon density (and hence  $Z_{\text{eff}}$ ) increases with increasing carbon yield
- ◆ 2) Core carbon density increases with core heating power
- ◆ 3) The radiation fraction is much less than that for similar lower single null plasmas
- ◆ 4) Inner and outer pumping is not independent.

# Specific UEDGE assumptions for new RDP divertor modification simulations

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- ◆ Density at 96% surface specified;  $n_e(\text{core}) = 2.7 \times 10^{19} \text{ m}^{-3}$
- ◆ Radial power across 96% surface in ions and electrons specified
- ◆ Particles removed in two ways:
  - 1) neutral albedo at the plate,  $A_p = 0.98$ , simulates cryopumping at baffle entrances
  - 2) neutral albedo at walls  $A_w = 0.97$  (wall pumping)
- ◆ Spatially constant particle and thermal perpendicular diffusivity
- ◆ Carbon sputtered from walls (as fraction of Davis & Haasz model)

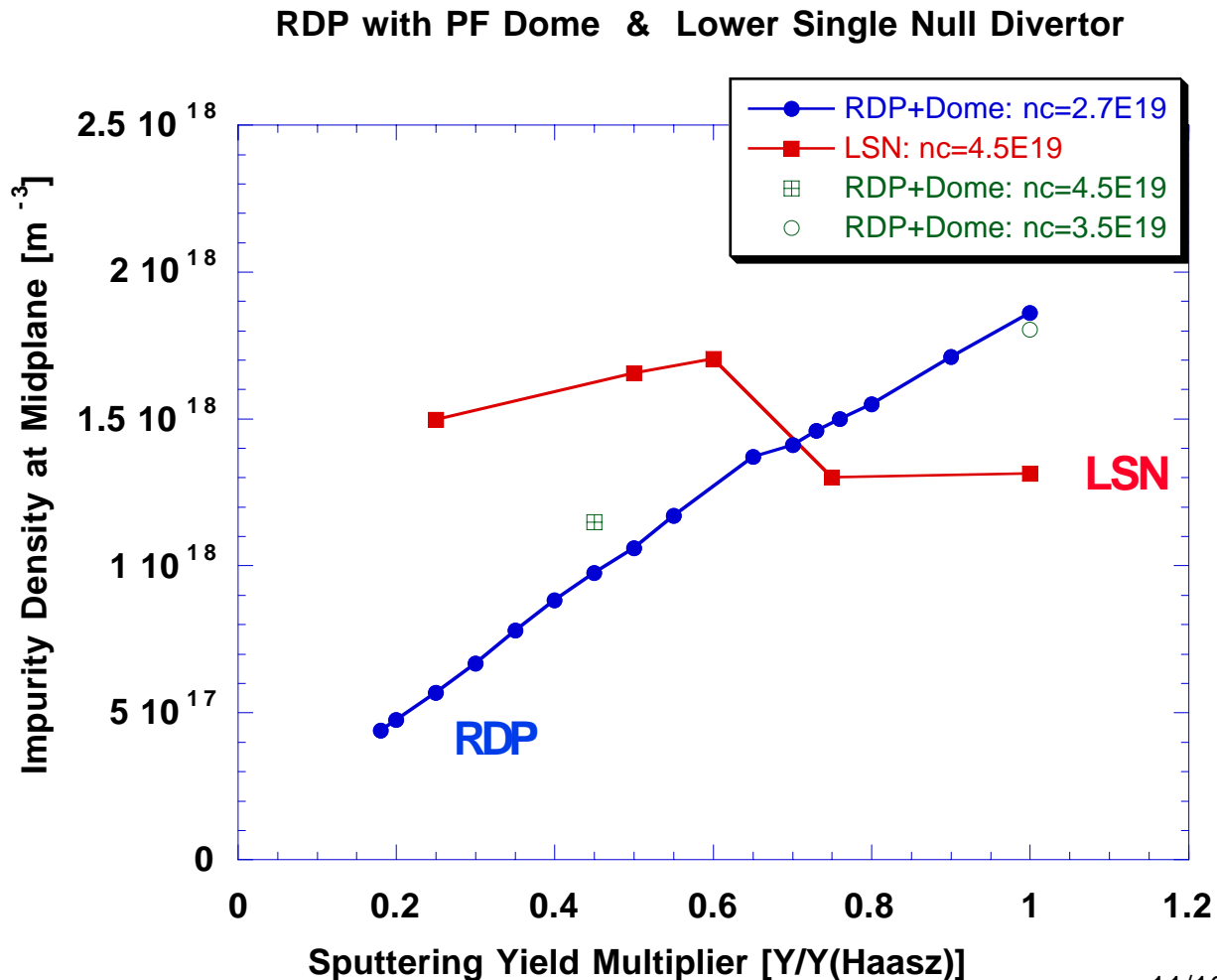
# We examine the effect of changing carbon yield on core impurity density in new RDP

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- ◆ **WHY?** Experiments on DIII-D show a nearly constant core impurity concentration as the **lower divertor** apparent yield has decreased in seven years of operation [see D. Whyte's poster this session]
- ◆ **UEDGE Modeling Results:**
- ◆ **Lower Divertor:** Impurity density remains nearly constant as the carbon yield is lowered {agrees with experiment} [see G. Porter, et al. and also P. West, et al. at this session]
- ◆ **Upper Divertor (New RDP+PF Dome):** Impurity density decreases as carbon yield is lowered {new prediction}

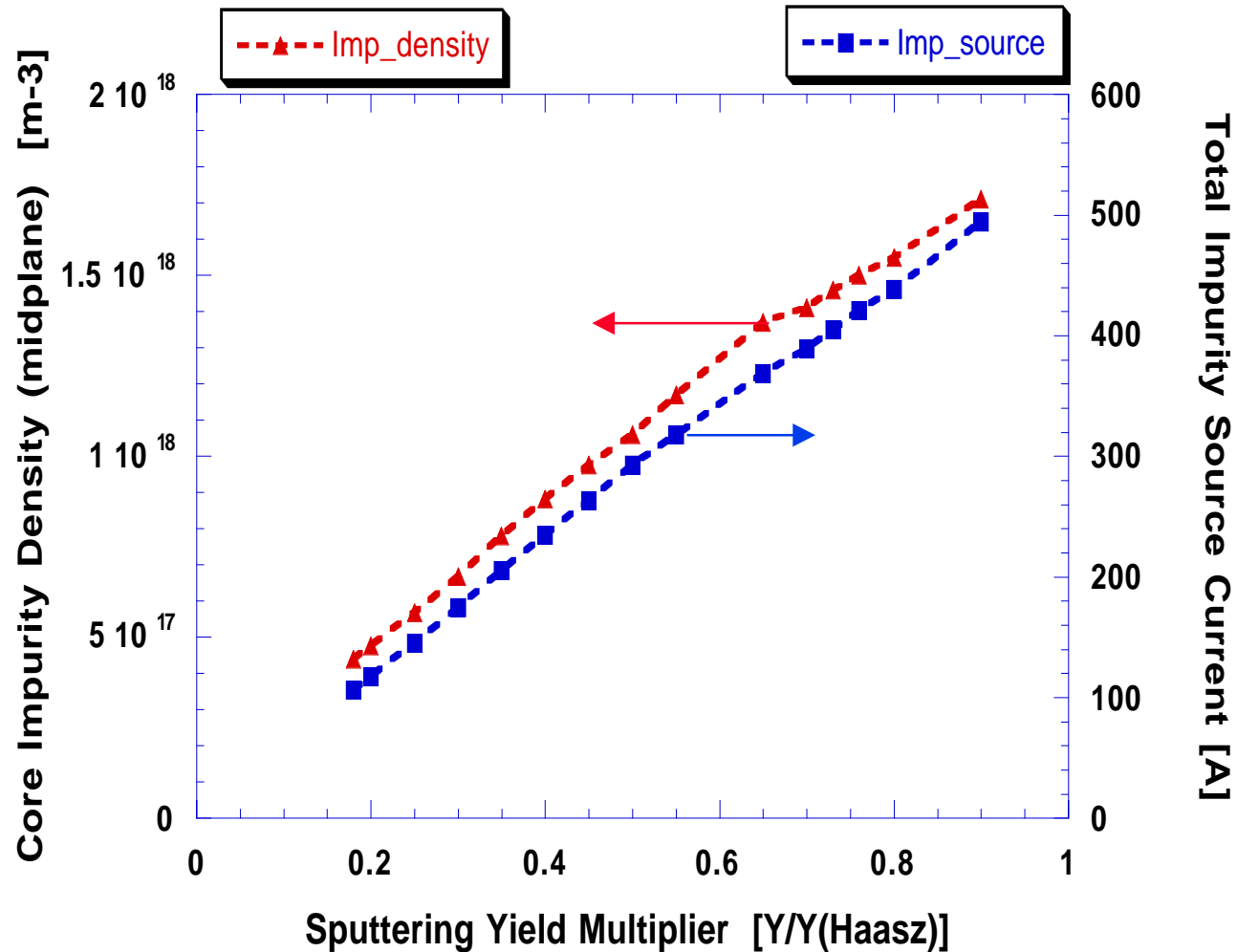


# KEY RESULT: Core impurities insensitive to sputtering with lower divertor, but not RDP



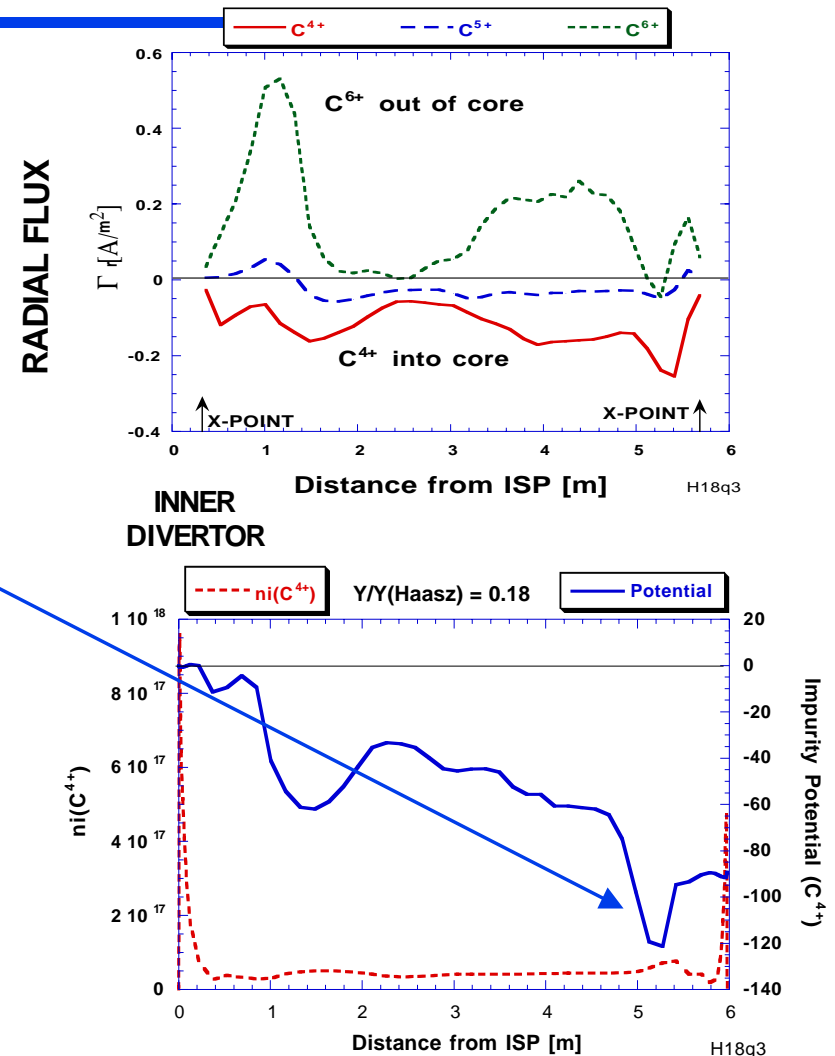
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# Core impurity density is linear with impurity source strength with new RDP



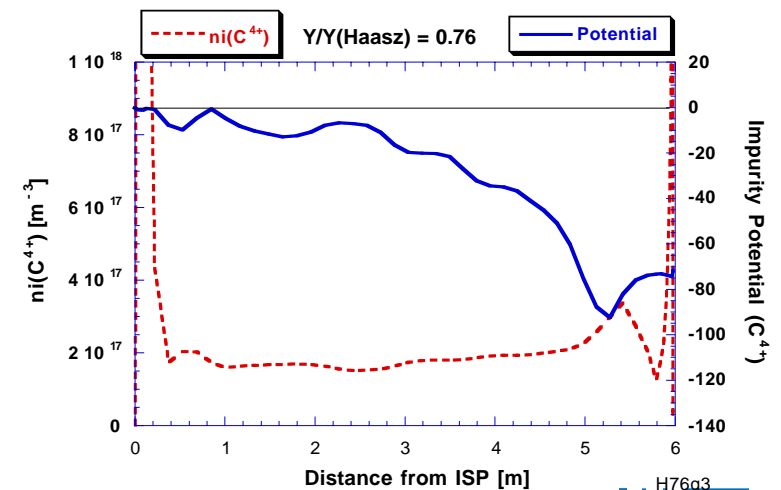
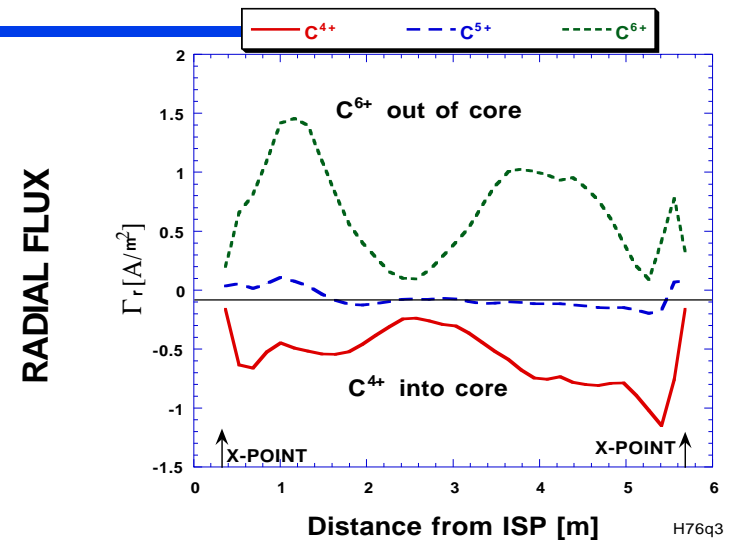
# Is core impurity level much influenced by parallel transport in the new RDP?

- ◆ Carbon is sputtered from ion and neutral impact on all walls:
- ◆  $Y/Y(\text{Haasz}) = 0.18$
- ◆  $\text{C}^{4+}$  flows freely from inner divertor and is attenuated from outer divertor
- ◆ There is some  $\text{C}^{4+}$  accumulation due to local **parallel potential wells**
- ◆ Carbon enters the **core** as  $\text{C}^{4+}$  via radial diffusion, and exits as  $\text{C}^{6+}$
- ◆ The **potential** integrates the parallel net force, which is a balance between drag and  $\nabla T_i$  forces

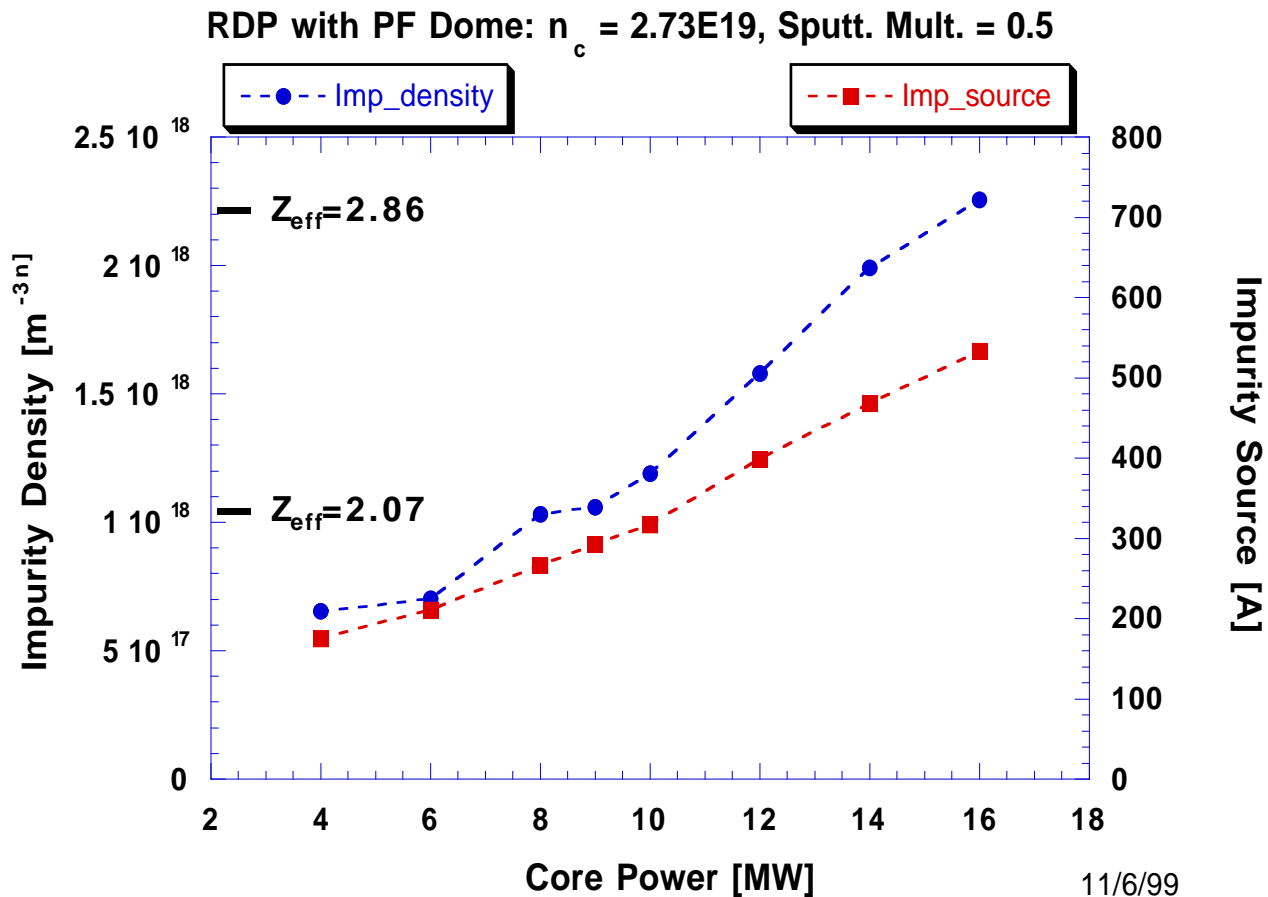


# Potential is not changed by higher sputtering yield in new RDP

- ◆ Carbon is sputtered from ion and neutral impact on all walls:
- ◆  $Y/Y(\text{Haasz}) = 0.76$
- ◆ As before, carbon enters core as  $C^{4+}$  via diffusion, and exits as  $C^{6+}$  (at much larger values than for low yield)
- ◆ But the parallel potential is not much changed from lower sputtering yield value, implying transport is not changed.
- ◆ Therefore the higher core carbon density is dominated by the higher carbon source current, not parallel transport forces.

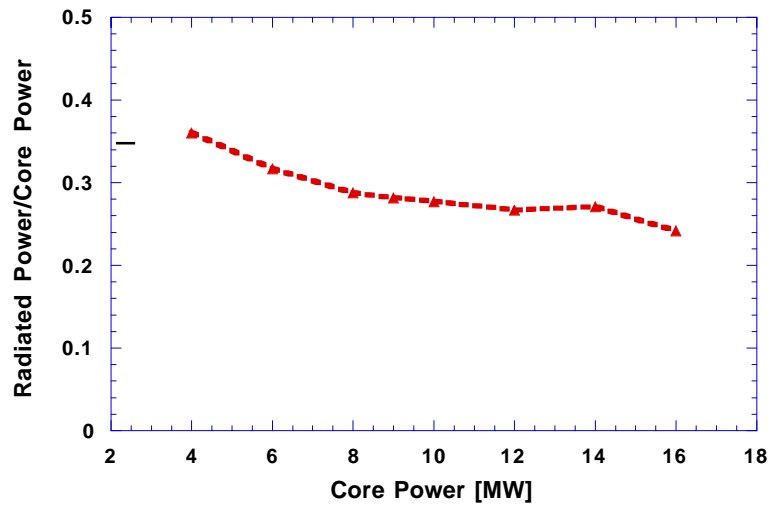
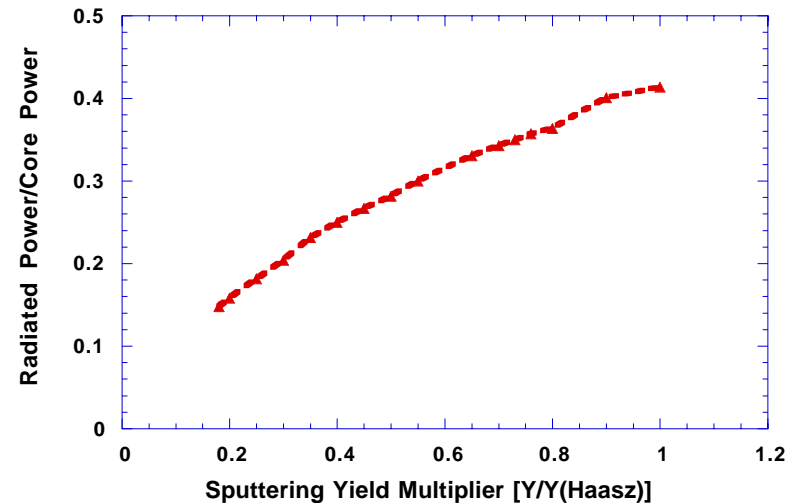


# Core impurity density increases with the core heating power in the new RDP



# Radiation fraction remains below 40% for the new RDP

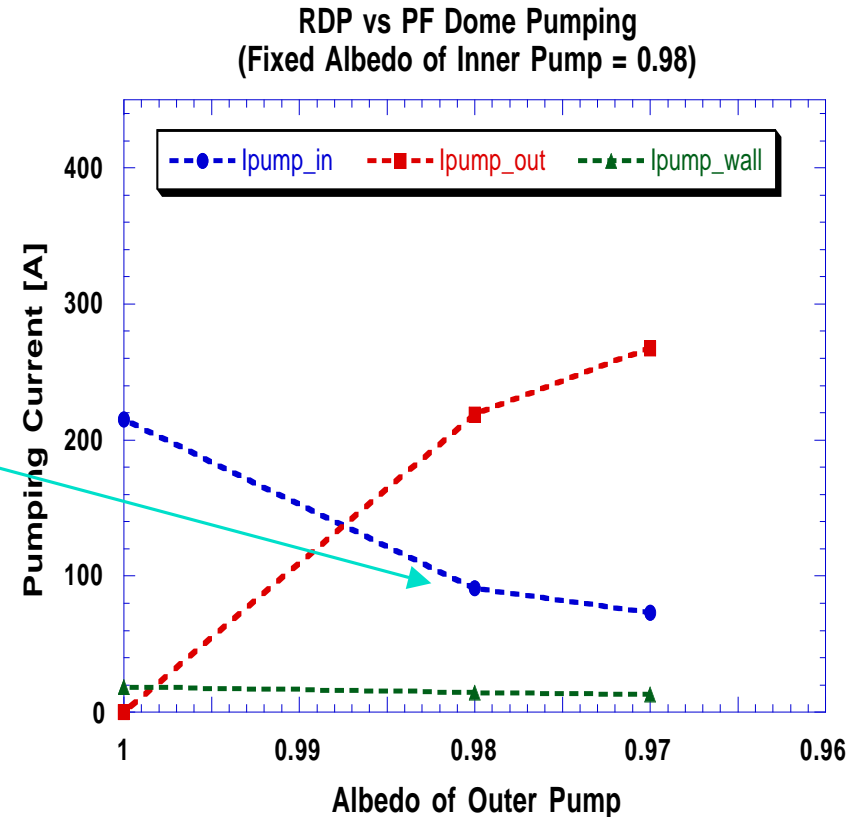
- ◆ Radiation fraction increases with carbon yield (at fixed core power,  $P_c = 9$  MW)
- ◆ Radiation fraction is higher in LSN (usually above 70%)



**Radiation fraction remains between 25% & 35% as core power increases (at fixed yield = 0.5)**

# Inner and outer pumping is not independent in the new RDP

- ◆ Core density fixed:  $n_c = 2.73 \times 10^{19}$
- ◆ Core Power fixed:  $P_c = 9$  MW
- ◆ Carbon yield multiplier = 0.25
- ◆ **Wall pumping is insignificant**
- ◆ The **inner pump exhaust** decreases as outer pumping efficiency (albedo) increases
- ◆ For equal albedos, the outer pump is more effective in particle removal



# Core carbon density **may be more dependent** on wall and plasma conditions in new RDP

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- ◆ 1) Core carbon density (and hence  $Z_{\text{eff}}$ ) increases with increasing carbon yield, indicating that core carbon can be influenced by wall conditioning.
- ◆ 2) Core carbon density increases with core heating power, indicating there may be a problem with high power operation - at low density.
- ◆ 3) Radiation fraction is below 40% (less than that for the lower single null plasma with similar parameters)
- ◆ 4) Inner and outer pumping is not independent.