## COMPARISON OF IDEAL MHD STABILITY PREDICTIONS WITH MHD BEHAVIOUR IN DIII-D

A.D. Turnbull, L.L. Lao, E.J. Strait, M.S. Chu, J.R. Ferron, T.H. Osborne, P.A. Politzer,
R.D. Stambaugh, T.S. Taylor, A.M. Garofalo, E.A. Lazarus, J.D. Callen, and K. Comer

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COMPARISON OF IDEAL MHD STABILITY PREDICTIONS WITH MHD BEHAVIOR IN DIII-D<sup>1</sup> A.D. TURNBULL, L.L. LAO, E.J. STRAIT, M.S. CHU, J.R. FERRON, T.H. OSBORNE, P.A. POLITZER, R.D. STAMBAUGH, T.S. TAYLOR, General Atomics, A.M. GAROFALO, Columbia U, E.A. LAZARUS, ORNL, J.D. CALLEN, K. COMER, UW-Madison, B.W. RICE, LLNL — New diagnostics in DIII-D have greatly improved equilibrium reconstructions over the past decade. This, coupled to a corresponding improvement in ideal MHD stability code accuracy and capabilities, has resulted in a convergence between the predicted MHD stability limits and the observed limits. The comparisons have evolved beyond global scalings to detailed comparisons of the stability predictions of unstable mode structures and growth rates for individual discharges. These demonstrate that ideal MHD predictions are remarkably accurate --- to within a few percent --- for a wide range of discharges. Several prominent examples include infernal modes, resistive wall modes, and intermediate *n* ideal edge modes in H–Mode discharges, VH--Mode and NCS H--Mode discharges, and n = 1 ideal modes in L--Mode NCS discharges.

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### IDEAL MHD CAN PREDICT MANY OF THE FEATURES OBSERVED IN TOKAMAK DISCHARGES

- Reliable prediction of b limit scaling
- In many cases ideal MHD predicts details of unstable modes when stability limits are violated
- Accurate prediction of stability of individual discharges requires
  - Comprehensive equilibrium diagnostics for accurate equilibrium reconstruction
  - Accurate reproduction of details of the equilibrium
    - ★ Cross section shape
    - **\*** Profiles
    - ★ Stabilizing wall



## IDEAL MHD HAS HISTORICALLY PROVIDED RELIABLE GUIDANCE FOR TOKAMAK CURRENT AND $\beta$ STABILITY LIMITS

• Troyon limit  $\beta^{crit} = \beta_N^{crit}$  I/aB:  $\beta_N^{crit} \sim 3$  from numerical optimization studies (1984)



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## CALCULATIONS INDICATE $\beta_{\text{N}}$ CAN SIGNIFICANTLY EXCEED TROYON LIMIT WITH HIGH $\textbf{I}_{i}$ AND BROAD PRESSURE

- n = 1 kink limit exceeds the ballooning limit for optimized profiles (Howl et al. 1992)
  - Wall stabilization is negligible for the optimized profiles





### EXPERIMENTS CONFIRM $\beta_N$ SCALING WITH $\ell_i$



• 
$$\beta_N^{crit} \sim 4 \ell_i$$

 4 ℓ<sub>i</sub> scaling provides better limit than simple Troyon scaling

> Exceptions can be explained by wall stabilization (1994)



## ACCURATE PREDICTION OF STABILITY OF INDIVIDUAL DISCHARGES REQUIRES COMPREHENSIVE EQUILIBRIUM DIAGNOSTICS



#### **Profile Data:**

36 Channels MSE Thomson  $T_e$ ,  $n_e$ CER  $T_i$ ,  $\Omega$ ECE  $T_e$ SXR axis shift

#### **External Magnetic Data:**

50 Poloidal Bp probes 40 Poloidal flux loops Diamagnetic loop Rogowski loop

Other Constraints: SXR rational surfaces

 MSE is crucial to obtaining well constrained current profile

### NEW 36 CHANNEL MSE DIAGNOSTIC PROVIDES DETAILED INTERNAL CURRENT PROFILE INFORMATION

- Multiple viewing angles allow resolution of Er and Bz:
  - Internal j is well resolved





### DETAILED MEASUREMENTS ENABLE ACCURATE STABILITY SCIENCE





### STABILITY CALCULATIONS REQUIRE ACCURATE REPRODUCTION OF DIII-D VACUUM VESSEL WALL FOR RELIABLE PREDICTIONS





• Wall parameterize by

$$R_{w} = R_{o} + \alpha a_{w} \sum_{k=1}^{N} a_{k} \cos (k_{\theta})$$
$$Z_{w} = Z_{o} + \alpha \kappa_{w} a_{w} \sum_{k=1}^{N} b_{k} \sin (k_{\theta})$$

R<sub>0</sub>, Z<sub>o</sub>, a<sub>w</sub>,  $\kappa_w$ , and the coefficients a<sub>k</sub>, b<sub>k</sub>, k = 1 N, are kept fixed such that  $\alpha$  = 1.0 is the best fit to the real DIII–D wall (N = 26)

 $\alpha$  is then used as an expansion parameter to vary the wall radius R\_{wall} / R\_DIII–D

 1997 upper divertor hardware reproduced by modified fit (up-down asymmetric)

### STABILITY CALCULATIONS INCORPORATE ESSENTIAL DETAILS OF CURRENT PROFILE AND THE PLASMA AND WALL SHAPE

- Realistic DIII-D wall:
  - Plasma boundary set within 10<sup>-4</sup> of separatrix
  - Up-down asymmetry



• Mesh packing used to resolve the edge





## AXISYMMETRIC (n = 0) LIMITS ON ELONGATION AGREE WITH IDEAL MHD TO 2% ACCURACY WITH MODELED DIII–D WALL



- Ideal n = 0 stability calculation reproduces axisymmetric shift measured from magnetic data
- For broad current profiles and high triangularity, non-rigid effects are important
  - They limit elongation to about 80% of the rigid-shift prediction
  - Without m = 3 the comparison is poor



### IDEAL MHD STABILITY PREDICTIONS FOR INDIVIDUAL CASE STUDIES DEMONSTRATE AGREEMENT WITH OBSERVATIONS AT SEVERAL DIFFERENT LEVELS

- Single equilibrium reconstruction ⇒ possible explanations of observed MHD behavior
- Parameter scan of nearby equilibria ⇒ plausible explanations of observed MHD behavior
- Complete sensitivity study with respect to all possible equilibrium reconstructions consistent with allowable variations in equilibrium data
  - ⇒ Well constrained ideal MHD explanations of observed MHD behavior (with caveats re: non MHD effects)

Case studies from DIII–D exhibit varying degrees of these levels over a wide range of discharge types and for a wide range of MHD phenomena

- Fast disruptions
- b collapses
- Edge instabilities
- Core instabilities
- Wall modes



## **CASE STUDY #1**

**HIGH**  $\epsilon\beta_P$ 

## **DIII–D DISCHARGE**

67700



Case Study #1

High εβ #67700

## 

• A fast ( $\mu$ s)  $\beta$  collapse occured at 1765 ms



- No MSE data available at 1750 ms
  - Sensitivity to  $1 \cdot 1 \le q_0 \le 2.0$ and 0.4 MPa  $\le$  P<sup>'</sup>edge  $\le$  0.7 MPa in equilibrium reconstructions





Case Study #1 High  $\epsilon\beta_p$  #67700

## PREDICTED n = 1 INSTABILITY AT 1750 ms IS A PRESSURE DRIVEN KINK BALLOONING MODE





## **CASE STUDY #2**

**HIGH**  $\epsilon\beta_P$ 

## **DIII–D DISCHARGE**

77676



 $\begin{array}{l} \text{Case Study #2} \\ \text{High } \epsilon\beta_p \\ \text{#77676} \end{array}$ 

# DISCHARGE #77676 REACHED HIGH $\epsilon\beta_p$ and maintained quasi-steady state from neutral beam and bootstrap current drive



- MHD activity appeared
  - Before 2 s, in bursts
  - Between 2.8 s and 3.2 s and
  - After 3.8 s
- Transport barrier formed between
   3.2 s and 3.8 s while q<sub>o</sub> > 2



Case Study #2 High  $\epsilon\beta_p$  #77676

## MHD BURSTS IN HIGH $\epsilon\beta_p$ DISCHARGE #77676 RESULT FROM OHMIC CURRENT EVOLUTION





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### STABILITY COMPUTED FOR EQUILIBRIA RECONSTRUCTED FROM DISCHARGE DATA AT SEVERAL TIMES IS IN AGREEMENT WITH OBSERVED MHD ACTIVITY

- 8 Channel MSE and Thomson  $\rightarrow$  profiles
- Equilibrium reconstructed at 5 times slices



**CASE STUDY #3** 

## **VH–MODE**

## **DIII-D DISCHARGE**

75121



Case Study #3 VH–mode #75121

## VH–MODE IS TYPICALLY TERMINATION BY AN n $\sim$ 3–5 MHD BALLOONING-LIKE KINK MODE





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Case Study #3 VH–mode #75121

### IDEAL MHD STABILITY CALCULATIONS ARE CONSISTENT WITH THE OBSERVED X EVENT



 Unstable n = 2, 3, 4 modes computed with edge localized "peeling" structure but strongly ballooning on outboard side



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### VH MODE TERMINATION EVENT IS DRIVEN BY COMBINATION OF p'edge and jedge

Parameter scans of nearby equilibria show stability threshold in p'<sub>edge</sub>, j<sub>edge</sub>
 Threshold for p'<sub>edge</sub>
 Threshold for j<sub>edge</sub>



• Typically higher n are unstable first:

- n = 1 is usually stable unless  $q_0 \rightarrow 1$ 



**CASE STUDY #4** 

## H-MODE

## **DIII–D DISCHARGE**

92001



### PLASMA IS PREDICTED UNSTABLE TO LOW n KINK - PEELING MODE BEFORE TYPE I ELM FOR DISCHARGE #92001

• Equilibrium and low n (n = 1 through 5) stability analysis performed at 1693 msec and 2075 msec





Case Study #4 H–mode NCS #92001

## <sup>cs</sup> ACCURATE EQUILIBRIUM RECONSTRUCTION PROCEDURE FOR EDGE PRESSURE AND CURRENT IS CRUCIAL

### WITHOUT BOOTSTRAP CURRENT





### WITH BOOTSTRAP CURRENT





IAEA F1-CN-69/EX6/2 Granetz/Osborne



### PROFILES FOR DISCHARGE #92001 SHOW A LARGE P'edge IN ELM FREE PERIOD AND JUST BEFORE THE ELM

#### • ELM Free Period







### STABILITY CALCULATIONS FOR n=1 AND n=2 SHOW COMPLETE STABILITY

- Best fit to equilibrium data at 1693 msec yields  $q_0 = 1.02 \pm 0.1$ 
  - Unstable to n = 1 quasi-interchange mode
    - » increasing  $q_0$  to  $1.05 \Rightarrow$  stable to n = 1 with or without wall
  - Stable to n = 2 with or without a wall

- Best fit to equilibrium data at 2075 msec yields  $q_0 = 1.13 \pm 0.1$ 
  - Stable to n = 1 with or without a wall
  - Stable to n = 2 with or without a wall



### UNSTABLE IDEAL n=3 MODE JUST BEFORE TYPE I ELM IS A KINK-PEELING MODE

• Mode displacement



• Fourier decomposition





### UNSTABLE IDEAL n=4 AND n=5 MODES ARE ALSO KINK-PEELING MODES

• Mode displacement

• Fourier decomposition









### ELM IS MORE RADIALLY LOCALIZED THAN VH MODE TERMINATION INSTABILITY

• Mode width appears to correlate with width of high p' region





## **CAUTIONARY REMARKS**

- Ordinary Type I ELM instability is not always found from calculations:
  - Stability depends sensitively on jedge
  - Requirement of 'reasonable' alignment of jBS and jedge in order to impose consistency with ballooning stability does not fully constrain jedge
    - » jedge depends on the fraction of the full collisionless bootstrap current jBS that is used
    - » **jBS is reduced by collisional effects**
    - » full alignment of jBS and jedge may not always be realized in individual discharges
- Limited comparison of predicted mode with experimental data is possible in this case:
  - Experimental identification of ELM toroidal mode number, real frequency, or growth, is difficult
  - In the few available cases, n has been measured between 2 and 9



## **CASE STUDY #5**

## L-MODE

## **DIII-D DISCHARGE**

87009



## PERFORMANCE IN STRONGLY PEAKED PRESSURE NCS DISCHARGES IS LIMITED BY FAST GROWING MHD INSTABILITIES AT $\beta_N \leq 2$



M.S. Chu, Phys. Rev. Lett. 77, 2710 (1996)

- DIII–D L–mode NCS discharges develop internal transport barrier
  - Leads to strong central pressure peaking  $\Rightarrow$  invariably leads to disruption at  $\beta_N \leq 2$ near calculated ideal and resistive  $\beta$  limits



#### Case Study #5 L-Mode NCS #87009 FAST-GROWING n=1 INSTABILITY CAUSES DISRUPTION

- Rapid growth:  $\gamma^{-1} \sim 0.15$  ms
- Large amplitude:  $\tilde{B}_{\theta}/B_{\theta}$  = 10% at outer wall
- Strongly ballooning toward low field side







Case Study #5 L-Mode NCS #87009

## STABILITY CALCULATIONS SHOW SENSITIVITY TO PRESSURE STEEPNESS IN MINIMUM SHEAR REGION

- Standard fit indicates discharge 87009 is 25% below ideal  $\beta$  limit
- Fit with pressure steepened by 15% at r~0.3 finds marginal stability





Case Study #5 L-Mode NCS #87009

## EXPERIMENTAL $\beta$ LIMITS CONSISTENT WITH CALCULATED DEPENDENCE ON $p_0/\langle p \rangle$

- DIII–D high  $p_0/\langle p \rangle \sim 6.0$  (L–mode):  $\beta_N \lesssim 2.5$ 
  - Limited by fast n = 1 disruption
- Discharge #87009 disrupted as it approached ideal stability boundary at high p<sub>0</sub>/(p)
- DIII–D low  $p_0/\langle p \rangle \sim 1.5$  (H–mode): reach  $\beta_N \lesssim 4$ 
  - No disruption limited by ELM-like activity from finite edge pressure gradients





<sup>L-mode</sup> <sup>#87009</sup> OBSERVED MODE GROWTH IS CONSISTENT WITH IDEAL n = 1 KINK DRIVEN THROUGH INSTABILITY THRESHOLD

• Driven instability model (Callen et al, 1999)

 $\gamma \sim \exp \left[ (t/\tau)^{3/2} \right] \quad \tau \sim (2/3)^{2/3} \hat{\gamma}_{MHD}^{-2/3} \gamma_h^{-1/3}$ 

•  $\hat{\gamma}_{MHD}$  predicted from stability calculations ~3 × 10<sup>5</sup> s<sup>-1</sup>

Case Study #5



• Growth fits model with



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#### Case Study #5 L-mode #87009 COMPUTED INSTABILITY WITH STEEPENED PRESSURE IS A GLOBAL n = 1 KINK PEAKED IN THE CORE

- Steepened fit is consistent with diagnostics
- Predicted ideal kink:  $p^{I}$  ( $\rho = 0.3$ ) steepened by 15%

 $\beta_N$  increased by 10% above marginal





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## **CASE STUDY #6**

## **L-MODE NCS**

## **DIII-D DISCHARGE**

92691



Case Study #6 L-mode #92691

## DISCHARGE #92691 WITH LOW q<sub>min</sub> AND HIGH p<sub>0</sub>/(p) DISRUPTED WHEN THE IDEAL STABILITY BOUNDARY WAS CROSSED

• Ideal simulations using GATO based on equilibrium at 2.2 s with  $P_0/\langle P \rangle = 6.6$ 





### INTERNAL MODE STRUCTURE IS CONSISTENT WITH IDEAL INSTABILITY

- The observed instability has an ideal MHD character
  - No evident island structure
- Radial structure is confirmed by SXR and BES measurements



GATO Simulation

Strait, APS, 1997



## **CASE STUDY #7**

## **H–MODE NCS**

## **DIII-D DISCHARGE**

87937



Case Study #7 H-mode NCS #87937

## INTERNAL n = 3 MODE LIMITS THE CENTRAL PRESSURE IN SOME H–MODE NCS DISCHARGES

- Rapid growth =  $\gamma^{-1} \sim 0.2 \text{ ms}$
- Initial energy loss occurs in the plasma core





#### Case Study #7 H-mode NCS #87937 IDEAL n = 3 INFERNAL MODE IS PREDICTED MOST UNSTABLE

- n=3 becomes unstable when β is raised to 1.05 times the experimental value. (n=1 and 2 remain stable)
- Dominant m/n = 4/3 agrees with experimental mode identification
- Centrally peaked mode structure is consistent with observed energy loss



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## **CASE STUDY #8**

## **H–MODE NCS**

## **DIII-D DISCHARGE**

87099



#### Case Study #8 H-mode NCS #87099 MODERATE n MODES LIMIT EDGE PRESSURE GRADIENT IN HIGHEST PERFORMANCE H-MODE NCS DISHARGES

• Early heating creates broad current density profile (I<sub>i</sub> ~ 0.75)



## EDGE-DRIVEN MODE HAS A LOCALIZED/BALLOONING CHARACTER

- Instability consists of a single pulse
  - Wavelength corresponds to n ~ 5
- Amplitude peaks at the low field side (out board midplane)
- Rapid growth:  $\gamma^{-1} \leq 0.15$  ms
- Rotation in the electron diamagnetic direction is consistent with localization near the plasma edge



### NCS H MODE TERMINATION INSTABILITY LESS LOCALIZED THAN STANDARD H MODE ELM





## **CASE STUDY #9**

## WALL STABILIZATION

## **DIII-D DISCHARGE**

870111



#### Case Study #9 Wall Stabilization PREVIOUS DIII-D EXPERIMENTS ARE #80111 CONSISTENT WITH WALL STABILIZATION

Experimental β value never exceeds stability limit computed with an ideal wall but often exceeds limit computed with no wall (E.J. Strait, et al., EPS 1988)



Stabilization from well known profile effects could not be ruled out



Case Study #9 Wall Stabilization #80111

### DIII-D WALL STABILIZATION EXPERIMENTS IN 1994 EXCEEDED THE EARLIER 4I<sub>i</sub> SCALING

 Previous β<sub>N</sub> ~ 4l<sub>I</sub> scaling for DIII-D is an operational β limit for plasmas with moderate to high l<sub>I</sub>

• Wall stabilization experiments used current ramp and strong shaping to increase coupling between plasma and wall





Case Study #9 Wall Stabilization #80111

### DISCHARGE 80111 IS WALL STABILIZED FOR 30 WALL PENETRATION TIMES

- Discharge 80111 is wall stabilized for at least 60 ms, from 640 to 704 msc
- No ideal or resistive mode observed during this time

 Equilibrium reconstructions and ideal stability calculations performed at 5 time slices





#### Case Study #9 Wall Stabilization #80111 COMPLETE EQUILIBRIUM RECONSTRUCTION AND SENSITIVITY STUDIES DEMONSTRATE DISCHARGE 80111 IS ABOVE NO WALL LIMIT



Case Study #9
Wall Stabilization
#80111 PREDICTED IDEAL INSTABILITY WITH NO

### WALL IS A GLOBAL n = 1 KINK MODE

Mode Displacement



Fourier Decomposition

$$X = \xi \cdot \nabla \Psi / |\nabla \Psi|$$





Case Study #9 Wall Stabilization #80111

### β COLLAPSE IS DUE TO A SLOWLY ROTATING AND SLOWLY GROWING 3/1 MODE





#### Case Study #9 Wall Stabilization #80111 SADDLE LOOPS CONFIRM SLOWLY GROWING INSTABILITY IS AN m/n = 3/1 MODE



Case Study #9 Wall Stabilization #80111

### COLLAPSE AT HIGH $\beta_N$ OCCURS WHEN PLASMA ROTATION NEAR q = 3 HAS DECAYED

Theory predicts wall stabilization is lost when the plasma stops rotating





## CASE STUDY #10

## WALL STABILIZATION

## **DIII-D DISCHARGE**

92544



Case Study #10 Wall Stabilization IDEAL KINK MODE STABILIZED BY ROTATION AND #92544 RESISTIVE WALL ABOVE NO-WALL  $\beta_N$  LIMIT FOR > 30  $\tau_wall$ 

- Wall stabilization sustained with  $\beta_N$  up to 1.4  $\times \beta_N^{no-wall}$  computed by equilibrium reconstruction and full stability calculation
- Resistive wall mode grows when rotation drops below a critical value





#### Case Study #10 Wall Stabilization #92544 NO-WALL GA

## NO-WALL GATO STABILITY ANALYSIS FINDS GLOBAL n = 1KINK MODE UNSTABLE DURING HIGH- $\beta$ PHASE

- Instability little affected by edge current density within constraints of experimental data
- Mode near marginal stability at maximum experimental β<sub>N</sub> with perfectly conducting wall at position of DIII-D wall
- Experiment clearly exceeds the n = 1 ideal stability limit calculated with wall at infinity



#### Case Study #10 Wall Stabilization #92544 RESISTIVE WALL MODE RADIAL STRUCTURE PREDICTED FROM GATO CODE AGREES IN DETAIL WITH MEASURED ECE T<sub>e</sub> FLUCTUATIONS

- Similar discharge #96519
- Predicted  $\delta T_e$  profile from  $\delta T_e \propto \xi \nabla T_e$ with  $\xi$  from ideal stability calculation
- Amplitude and toroidal phase of calculated eigenfuction scaled from magnetic saddle loop data





### CONCLUSIONS

- Ideal MHD can predict many of the detailed features of the fastest growing instabilites in DIII-D
- Accurate reconstruction of the discharge equilibria is crucial to obtaining agreement in many cases
  - The more constrained the equilibrium, the better the agreement between predictions and observations
- Extensive equilibrium diagnostics and attention to details in the equilibrium reconstructions and stability calculations are the keys to accurate predictions

