

# Stability Modeling of DIII-D Discharges with Transport Barriers

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**Stability Modeling of DIII-D Discharges with Transport Barriers**<sup>1</sup> L.L. LAO, J.R. FERRON, Y.R. LIN-LIU, E.J. STRAIT, A.D. TURNBULL, T.S. TAYLOR, General Atomics, M. MURAKAMI, Oak Ridge National Laboratory — The stability of DIII-D discharges with transport barriers is systematically studied by modeling the pressure profiles using a hyperbolic tangent representation with various radii, widths, and amplitudes. The  $q$  profiles are modeled using a spline representation with varying  $q(0)$ ,  $q_{\min}$ , and  $\rho_{q_{\min}}$ . The equilibria are computed using the EFIT and the TOQ codes based on the parameters from a strongly shaped high trianguality DIII-D long pulse high performance discharge. Stability against the ideal low  $n = 1$  and 2 modes is evaluated using the GATO code with a conducting wall at  $1.5 a$ . The results show that the stability improves with increasing transport barrier width and radius but varies weakly with  $q(0)$ . When the transport barriers are L-mode like and have narrow widths in the plasma core, the stability is limited by the  $n = 1$  mode. When they are H-mode like and have large widths extending toward the edge, the stability is limited by the  $n = 2$  mode.

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Prefer Oral Session  
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# MOTIVATION

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- Strong local pressure gradients are often observed in discharges with internal transport barrier (ITB) which can lead to instability at low beta
- Previous stability modeling studies have been mostly discussed in terms of  $P(0)/\langle P \rangle$
- Goals
  - Explore stable path to configurations with both ITB and high normalized beta  $\beta_N$
  - Check sensitivity of stability limit to variations in  $q$  and ITB profiles

# OUTLINE / KEY RESULTS

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- **Stability limit improves with transport barrier width and radius**
- **Wall stabilization is crucial for ITB with large radius**
- **Stability limit varies weakly with  $q(0)$**
- **$n = 2$  modes are more unstable in ITB with large radius and width**

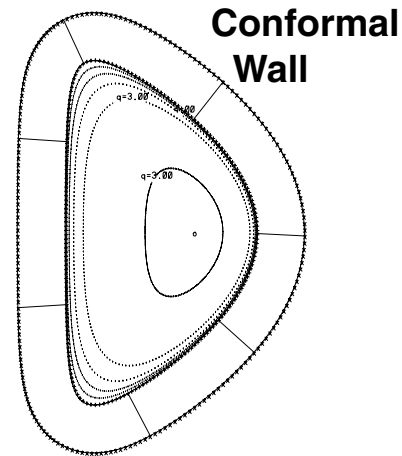
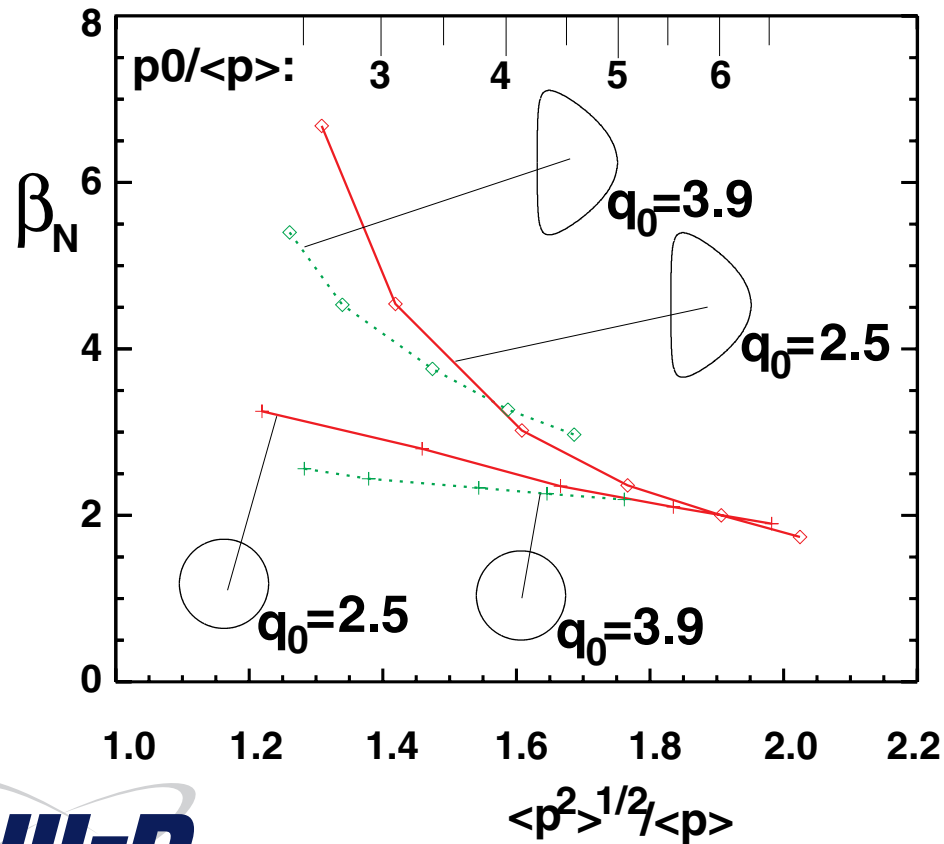
# APPROACHES

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- **Ideal stability with a conducting wall**
- **Simulated equilibria with model  $q$  and pressure profiles based on spline and hyperbolic tangent representations**
- **Simulated equilibria with  $q$  and pressure profiles from self-consistent transport simulations**

# PREVIOUS STABILITY STUDY IS DISCUSSED MOSTLY IN TERMS OF $P(0)/\langle P \rangle$

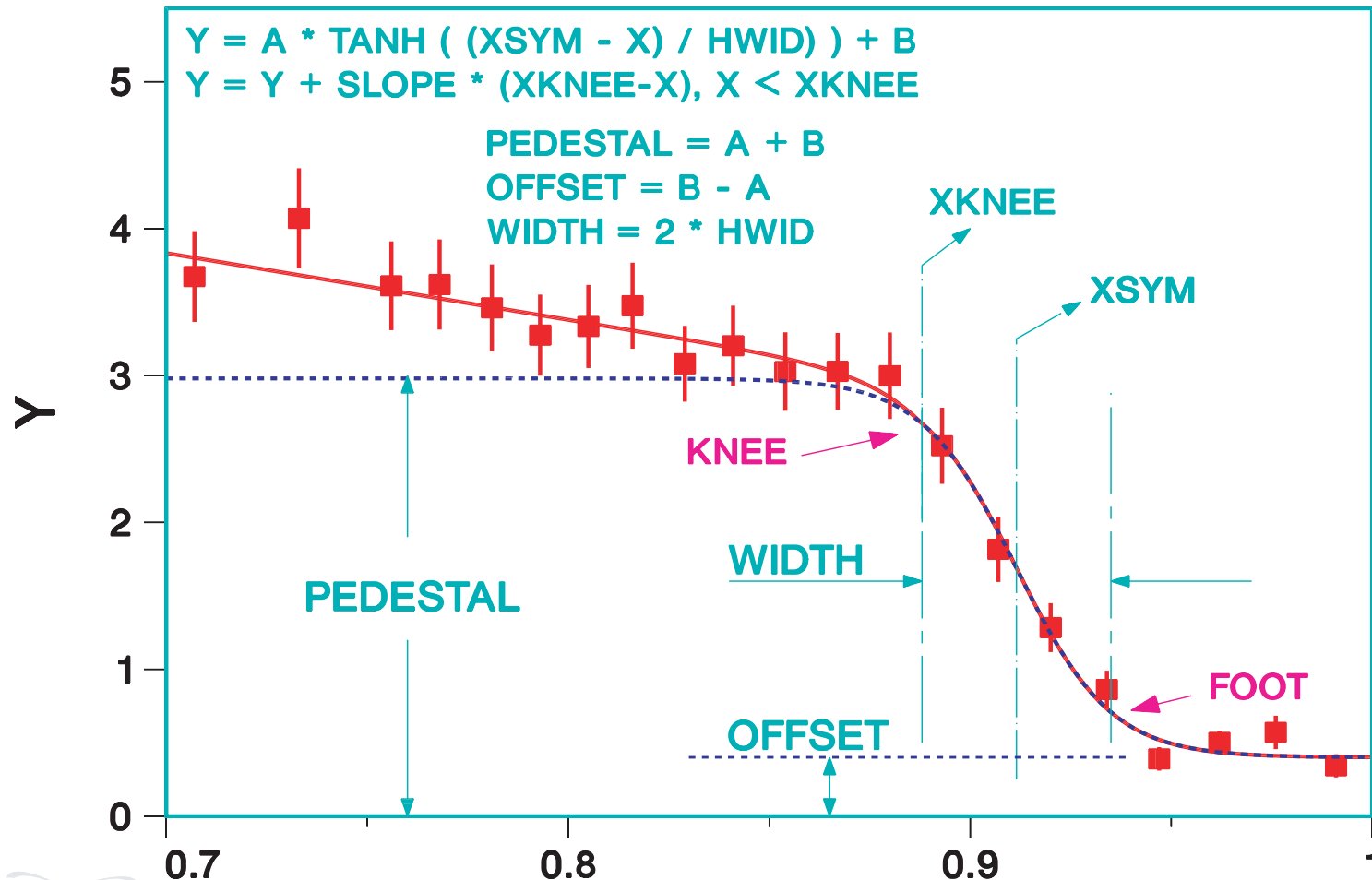
- $P(\psi) = P_0 (1 - \psi)^m$ ,  $q_{95} = 5.1$ ,  $\rho_{q_{min}} = 0.65$ ,  $q_{min} = 2.1$  and  $1.5$
- Vary pressure profile peakedness by varying  $m$



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# HYPERBOLIC TANGENT PROVIDES GOOD PARAMETRIZATION FOR PRESSURE PROFILES WITH TRANSPORT BARRIER

- 3 parameters amplitude, radius, and width



# ANALYSIS METHODS

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- **Equilibrium**
  - ToQ, EFIT
  - Up-down symmetric DND based on long pulse high performance shot 95983
  - Pressure profiles modeled using hyperbolic tangent representation with various radii, widths, and amplitudes
  - $q$  profiles modeled using spline representation with various  $q(0)$ ,  $q_{\min}$ , and  $\rho_{q\min}$
  - Fixed  $q_{95} \sim 5.1$
  - Single transport barrier
- **Stability**
  - Low  $n$  modes evaluated using GATO with a conducting wall at  $1.5a$
  - High  $n$  ballooning evaluated using BALOO



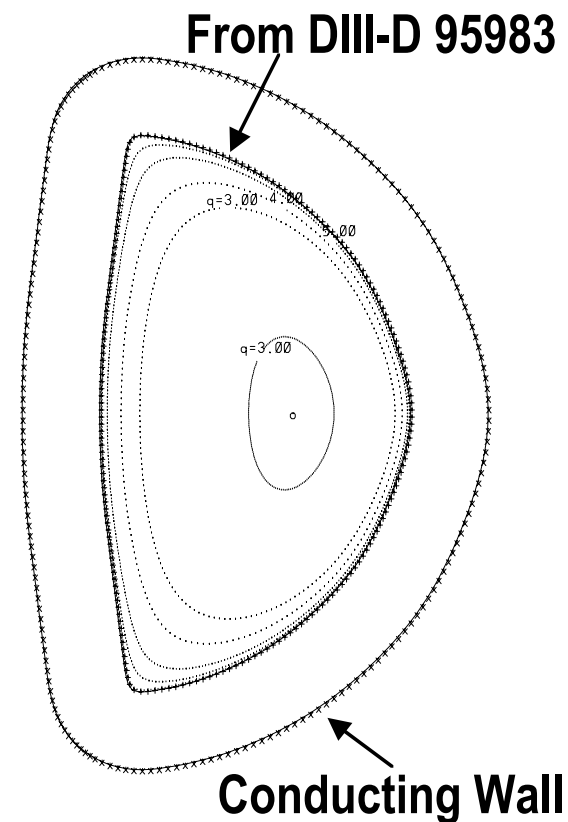
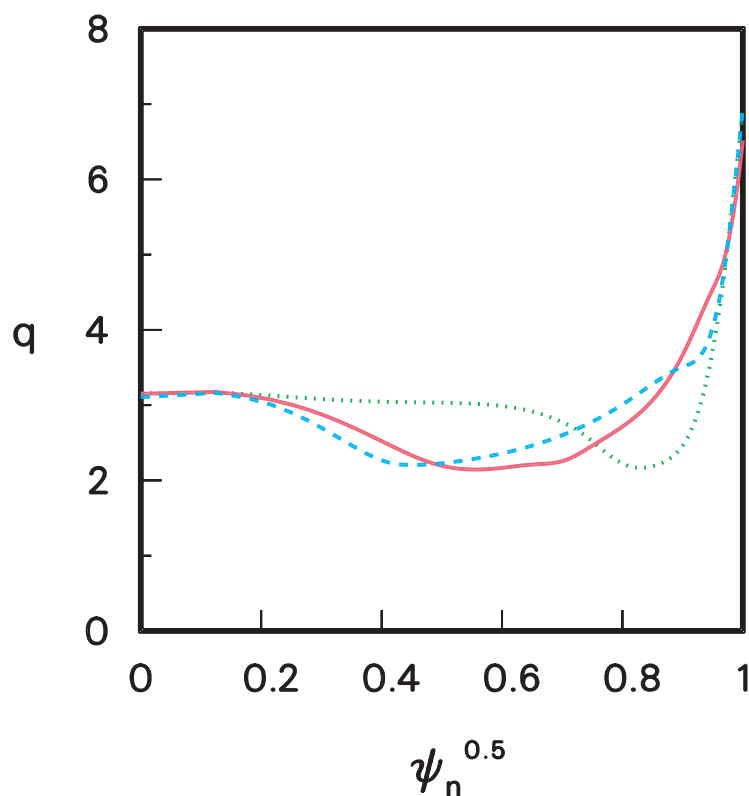
# SCANS

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- ITB radius  $\rho_{ITB}$ 
  - Fixed shape
  - Fixed  $q(0)$ ,  $q_{min}$ ,  $q_{95}$ ,  $\rho_{qmin} = \rho_{ITB}$
  - Hyperbolic tangent pressure with fixed half width  $W_{ITB}$
- ITB half width  $W_{ITB}$ 
  - Fixed shape
  - Fixed  $q(0)$ ,  $q_{min}$ ,  $q_{95}$ ,  $\rho_{qmin} = \rho_{ITB}$
  - Fixed  $\rho_{ITB}$
- $\rho_{qmin} = \rho_{ITB}$ 
  - Fixed shape
  - Fixed  $q(0)$ ,  $q_{min}$ ,  $q_{95}$
  - Hyperbolic tangent pressure with fixed half width  $W_{ITB}$ ,  $\rho_{ITB}$
- $q(0)$ ,  $q_{min}$

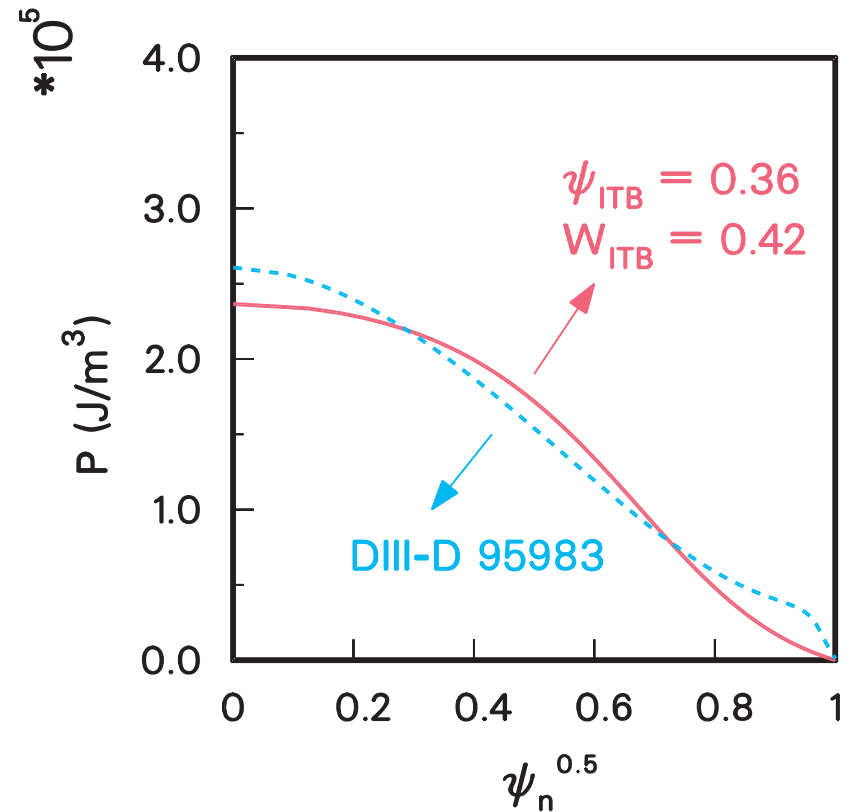
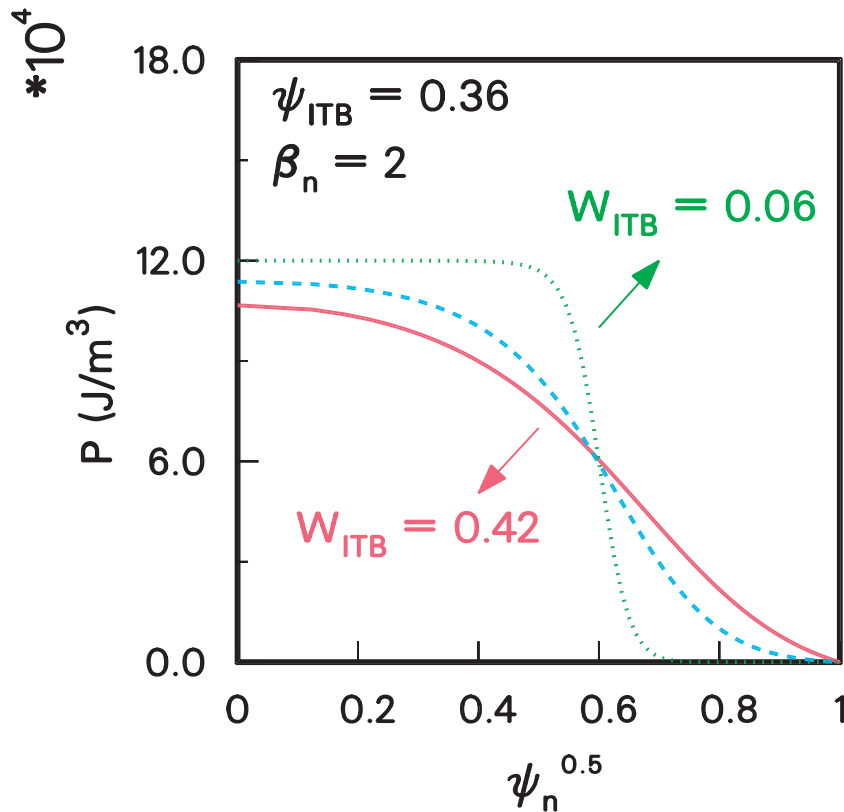
# PLASMA SHAPE IS BASED ON A DIII-D LONG PULSE HIGH PERFORMANCE DISCHARGE

- Up-down symmetric with a conducting wall at 1.5a
- q profiles are modeled using spline representations



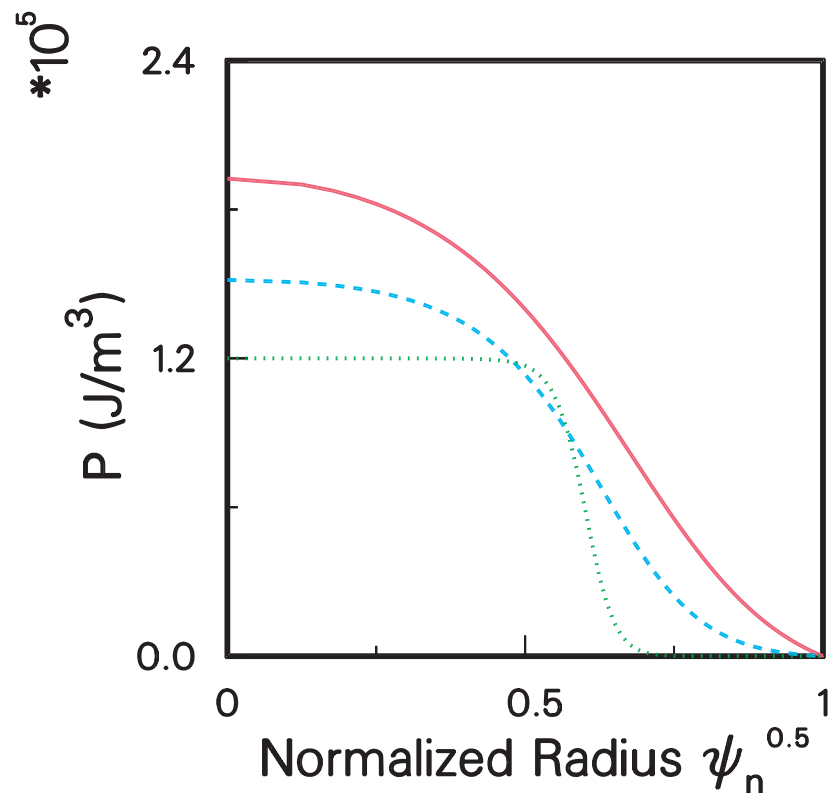
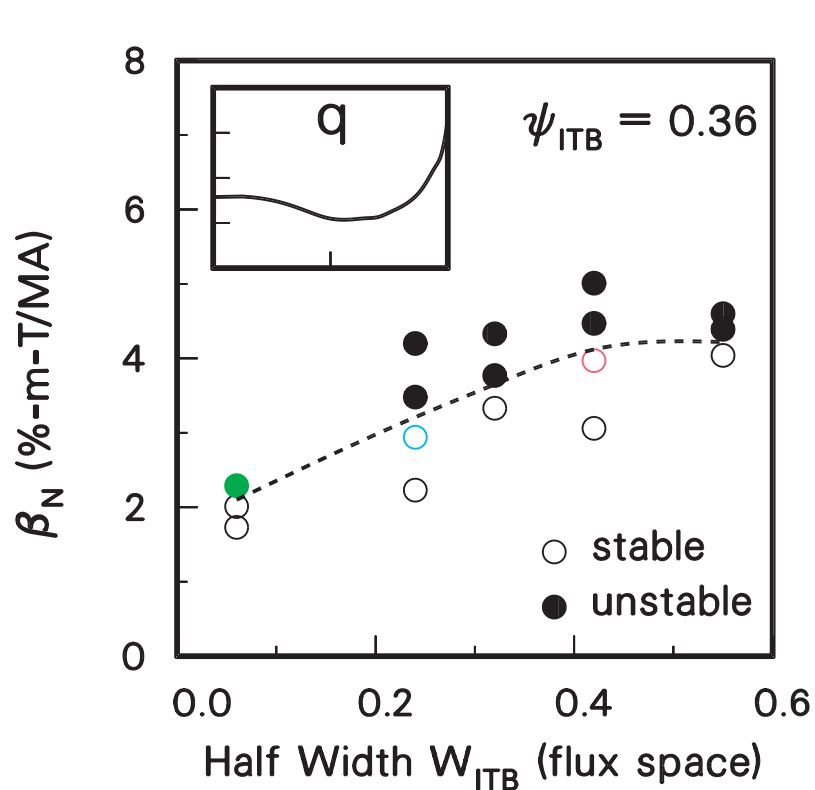
# LARGEST PRESSURE GRADIENT IS REDUCED AS TRANSPORT BARRIER WIDTH IS INCREASED AT CONSTANT $\beta$

- $$P(\psi) = P_0/2 \{ 1 - \text{TANH}[(\psi - \psi_{ITB})/ W_{ITB}] \} - P_0/2 \{ 1 - \text{TANH}[(1 - \psi_{ITB})/ W_{ITB}] \}$$



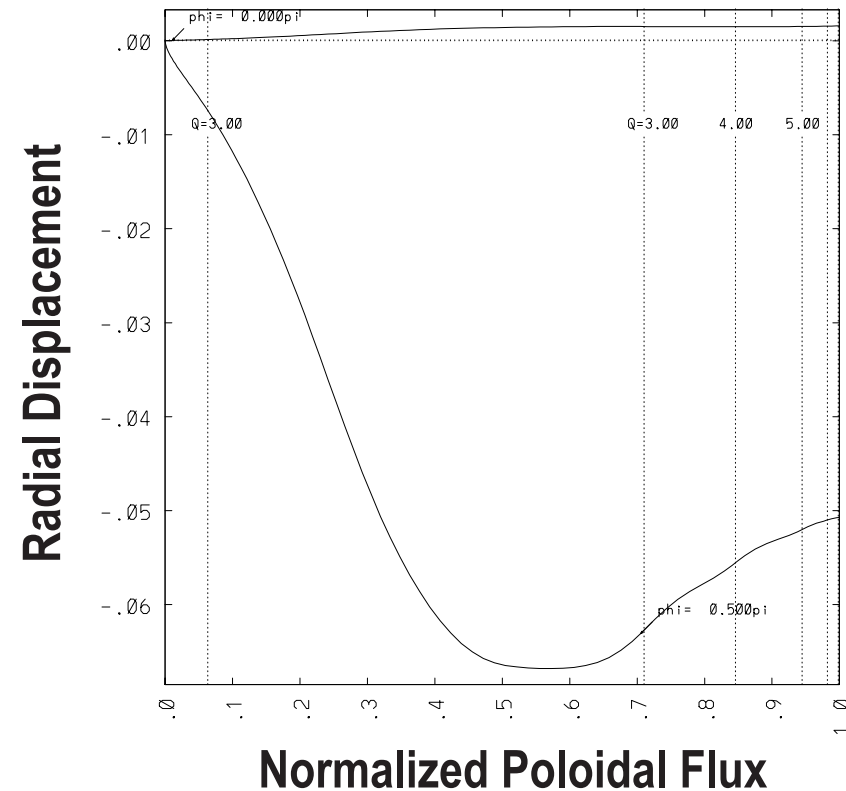
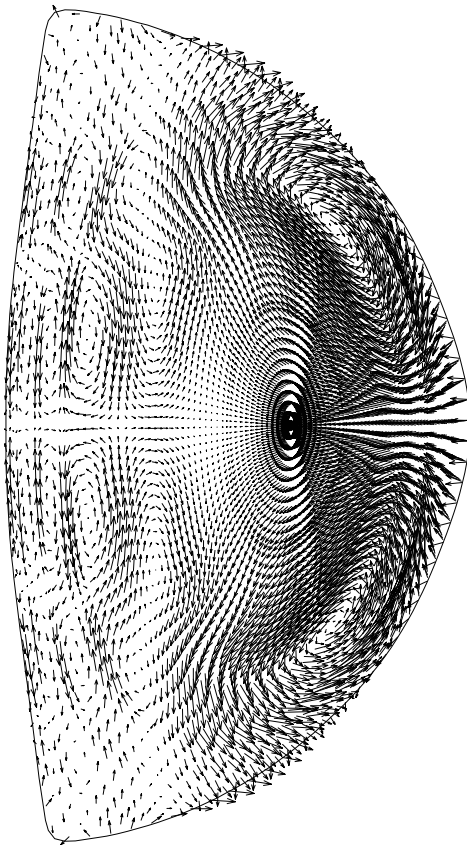
# STABILITY LIMIT IMPROVES WITH INTERNAL TRANSPORT BARRIER WIDTH

- fixed shape DND,  $q_{95} = 5.1$ ,  $q(0) = 3.2$ ,  $q_{\min} = 2.2$
- ideal  $n = 1$  with wall at  $1.5a$ ,  $\psi_{q_{\min}}^{0.5} - \psi_{ITB}^{0.5} = 0.05$
- stability improves due to geometric effect, closer to wall, and stronger shear



# THE $n = 1$ UNSTABLE MODE HAS A GLOBAL RADIAL STRUCTURE

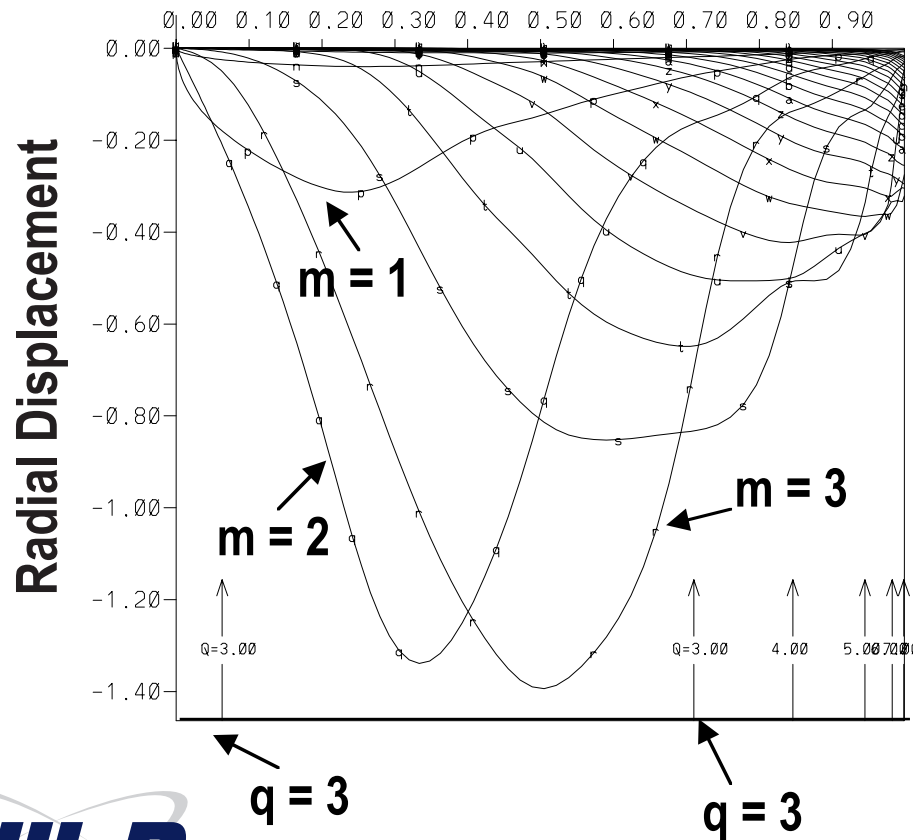
- $\beta_N = 4.3$ ,  $W_{ITB} = 0.24$ ,  $\psi_{ITB} = 0.36$ ,  $q(0) = 3.2$ ,  $q_{min} = 2.2$ ,  $q_{95} = 5.1$ ,  $\psi_{qmin} = 0.42$
- Computed using GATO with a conducting wall at 1.5a



# THE $n = 1$ UNSTABLE MODE HAS AN INFERNAL MODE STRUCTURE

- $\beta_N = 4.3$ ,  $W_{ITB} = 0.24$ ,  $\psi_{ITB} = 0.36$ ,  $q(0) = 3.2$ ,  $q_{min} = 2.2$ ,  $q_{95} = 5.1$ ,  $\psi_{qmin} = 0.423$
- Computed using GATO with a conducting wall at  $1.5a$

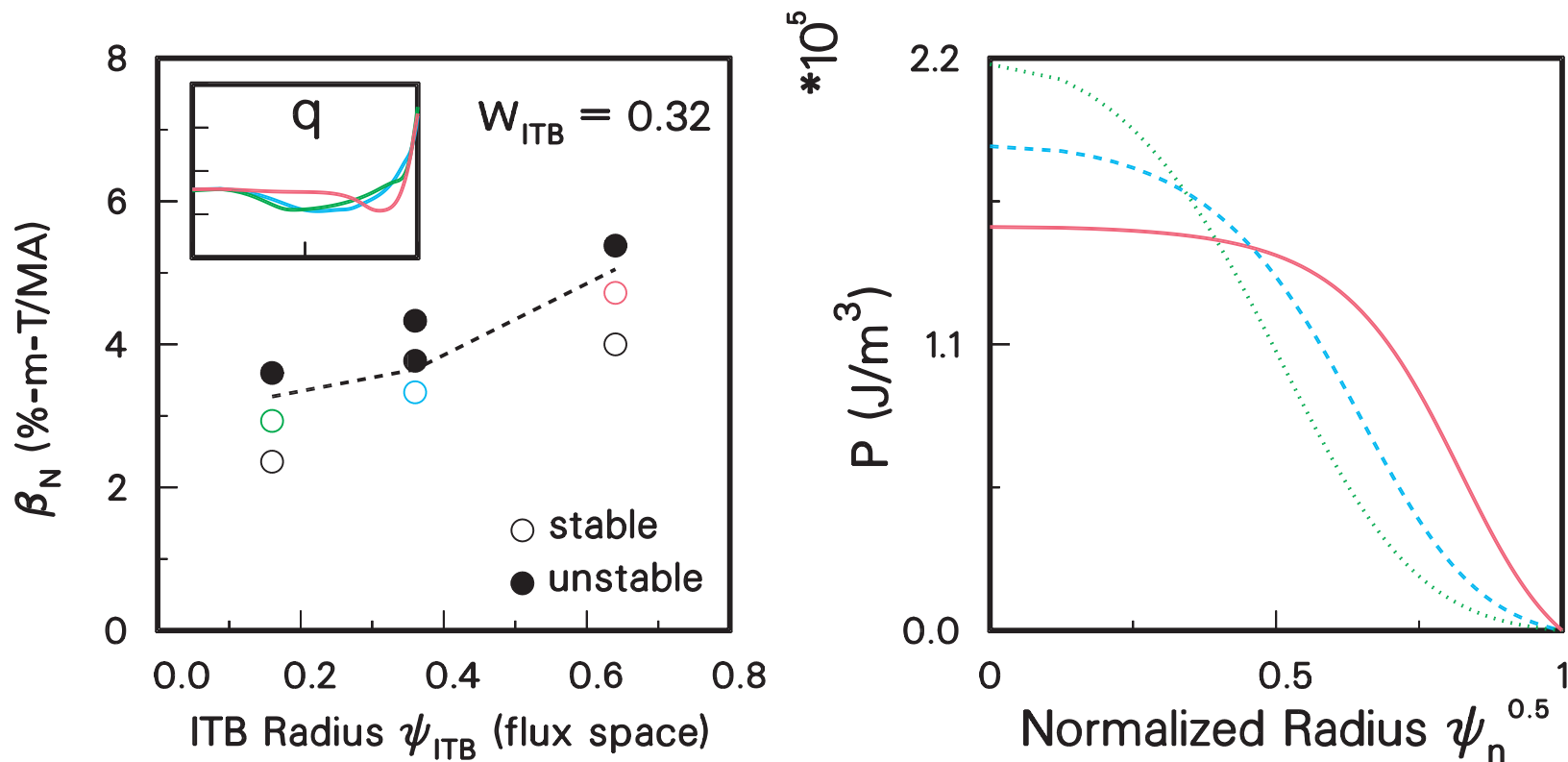
## Normalized Poloidal Flux



- Large  $m = 1, 2$  components although no  $q = 1$  and  $2$  surfaces

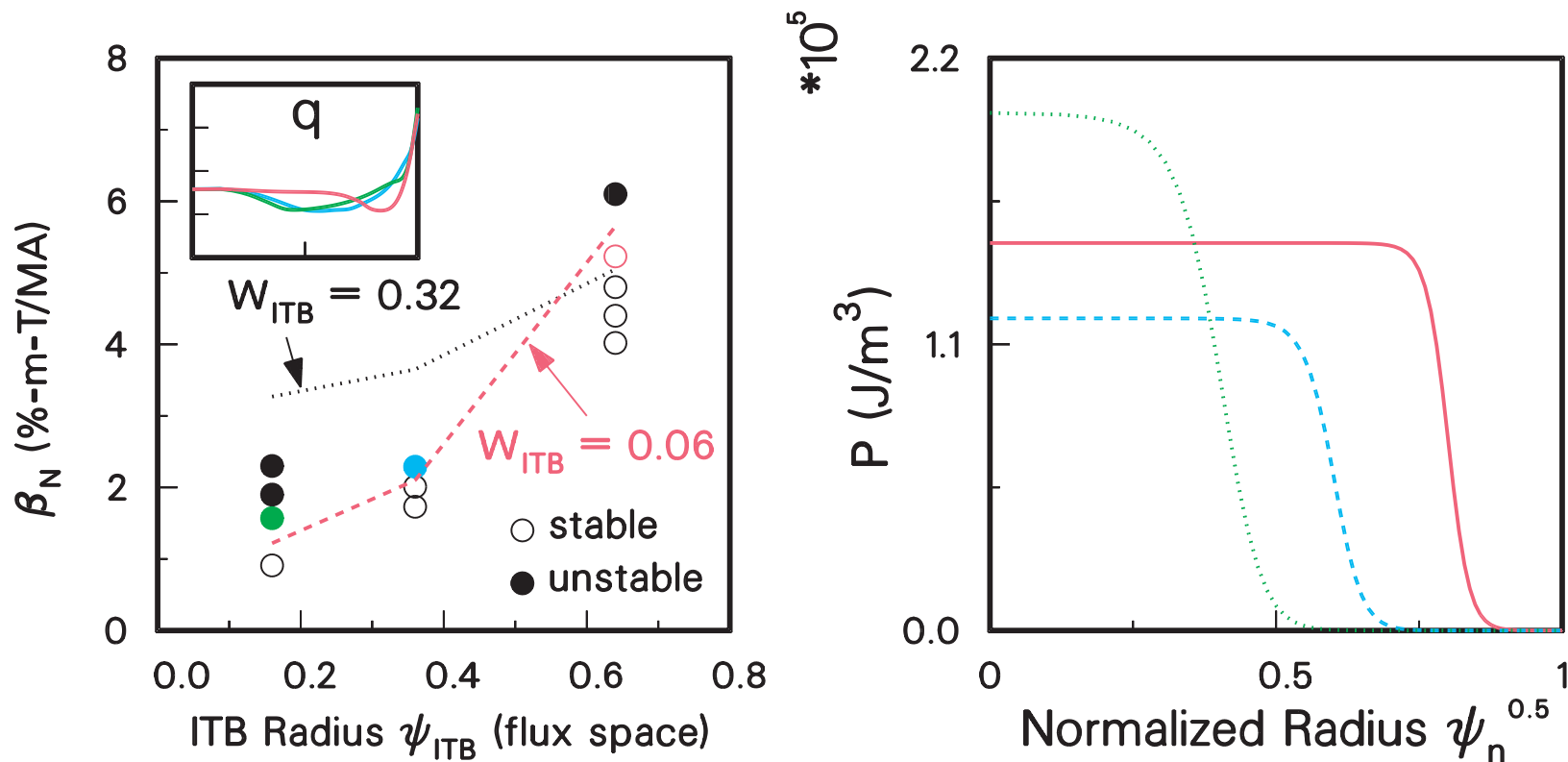
# STABILITY LIMIT IMPROVES WITH INTERNAL TRANSPORT BARRIER RADIUS

- fixed shape DND,  $q_{95} = 5.1$ ,  $q(0) = 3.2$ ,  $q_{\min} = 2.2$
- ideal  $n = 1$  with wall at  $1.5a$ ,  $\psi_{q_{\min}}^{0.5} - \psi_{\text{ITB}}^{0.5} = 0.05$
- stability improves mainly due to geometric effects



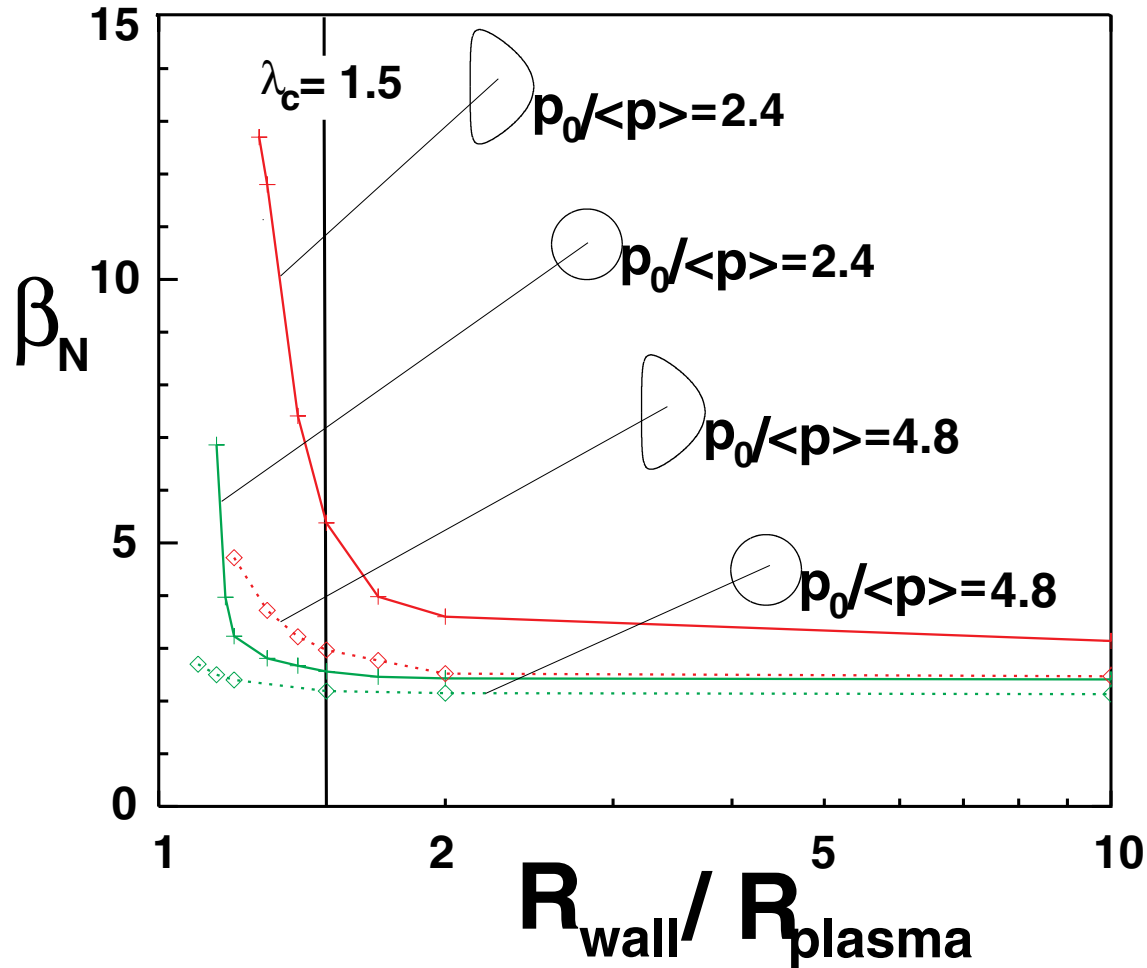
# STABILITY LIMIT IMPROVES WITH INTERNAL TRANSPORT BARRIER RADIUS

- fixed shape DND,  $q_{95} = 5.1$ ,  $q(0) = 3.2$ ,  $q_{\min} = 2.2$
- ideal  $n = 1$  with wall at  $1.5a$ ,  $\psi_{q_{\min}}^{0.5} - \psi_{ITB}^{0.5} = 0.05$
- stability improves due to geometric effect, closer to wall, and stronger shear





# PREVIOUS STABILITY STUDY SHOWS THAT WALL STABILIZATION IS CRUCIAL

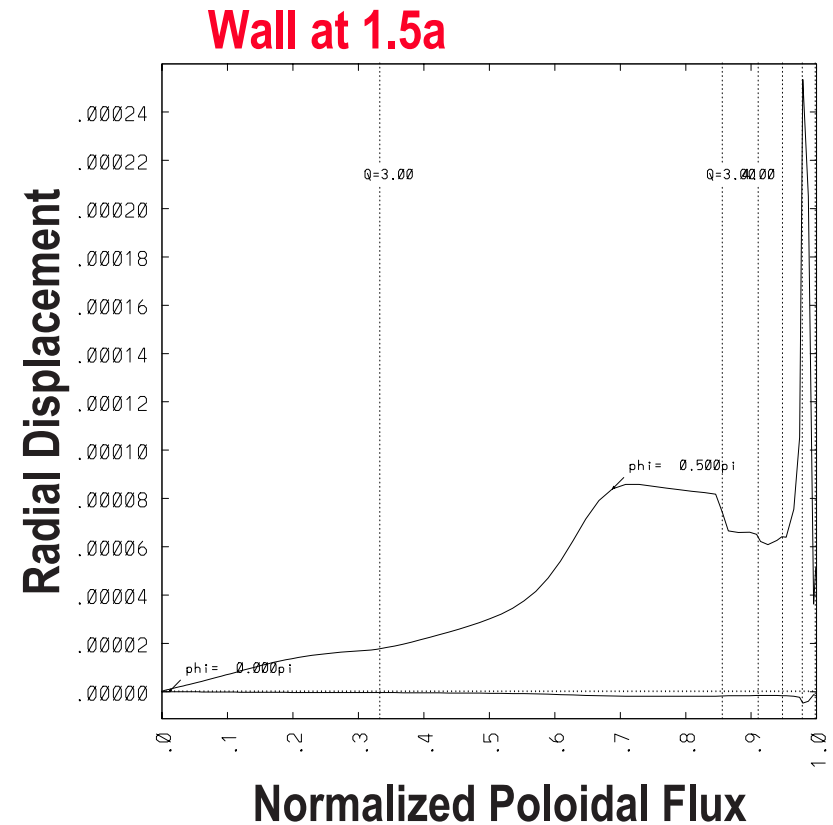
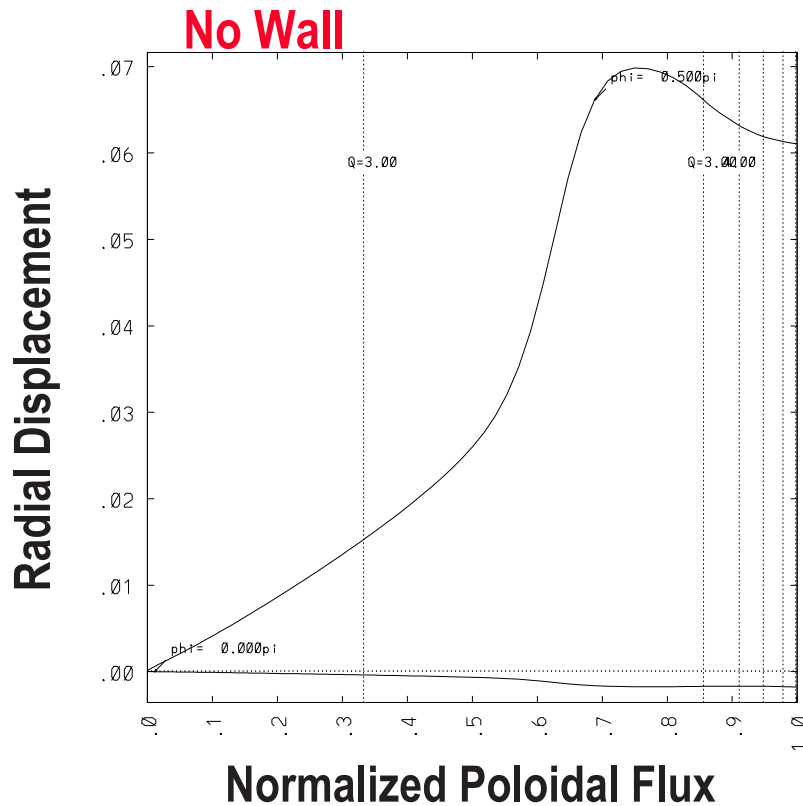


- With a close wall  $\beta_N$  is substantially increased

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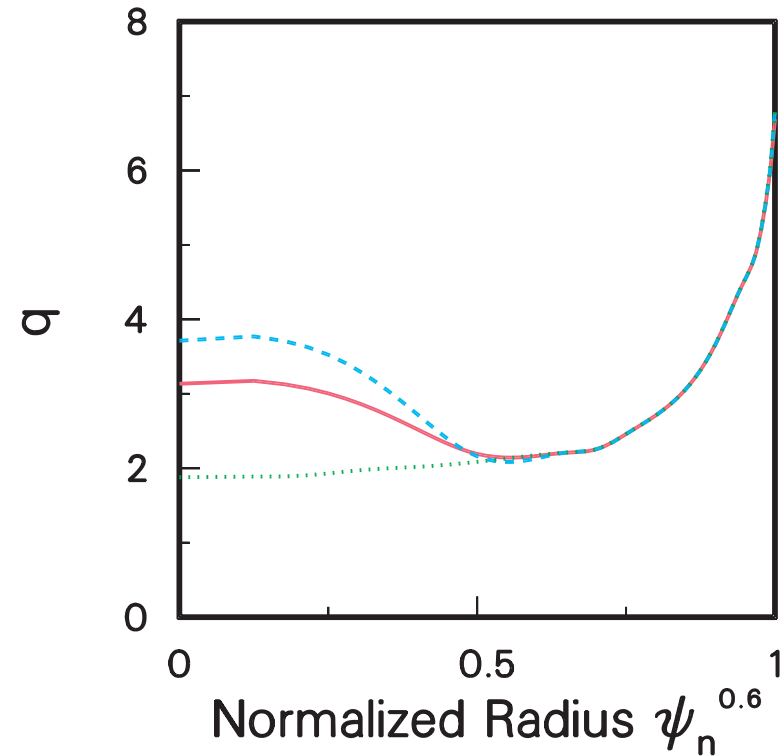
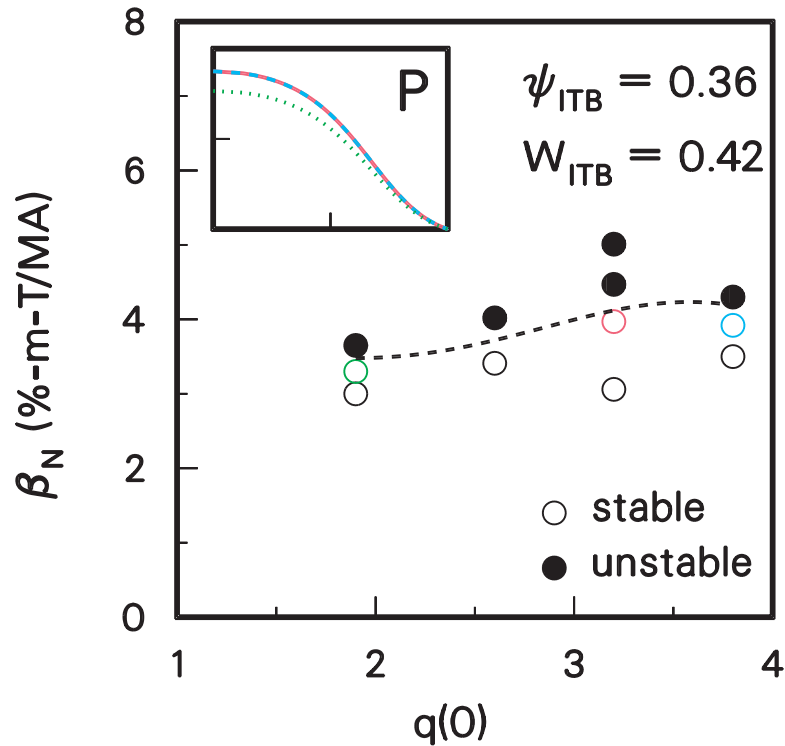
# WALL STABILIZATION IS CRUCIAL FOR STABILITY

- $\beta_N = 5.2$ ,  $W_{ITB} = 0.06$ ,  $\psi_{ITB} = 0.36$ ,  $q(0) = 3.2$ ,  $q_{min} = 2.2$ ,  $q_{95} = 5.1$
- Computed using GATO with a conducting wall at 1.5a



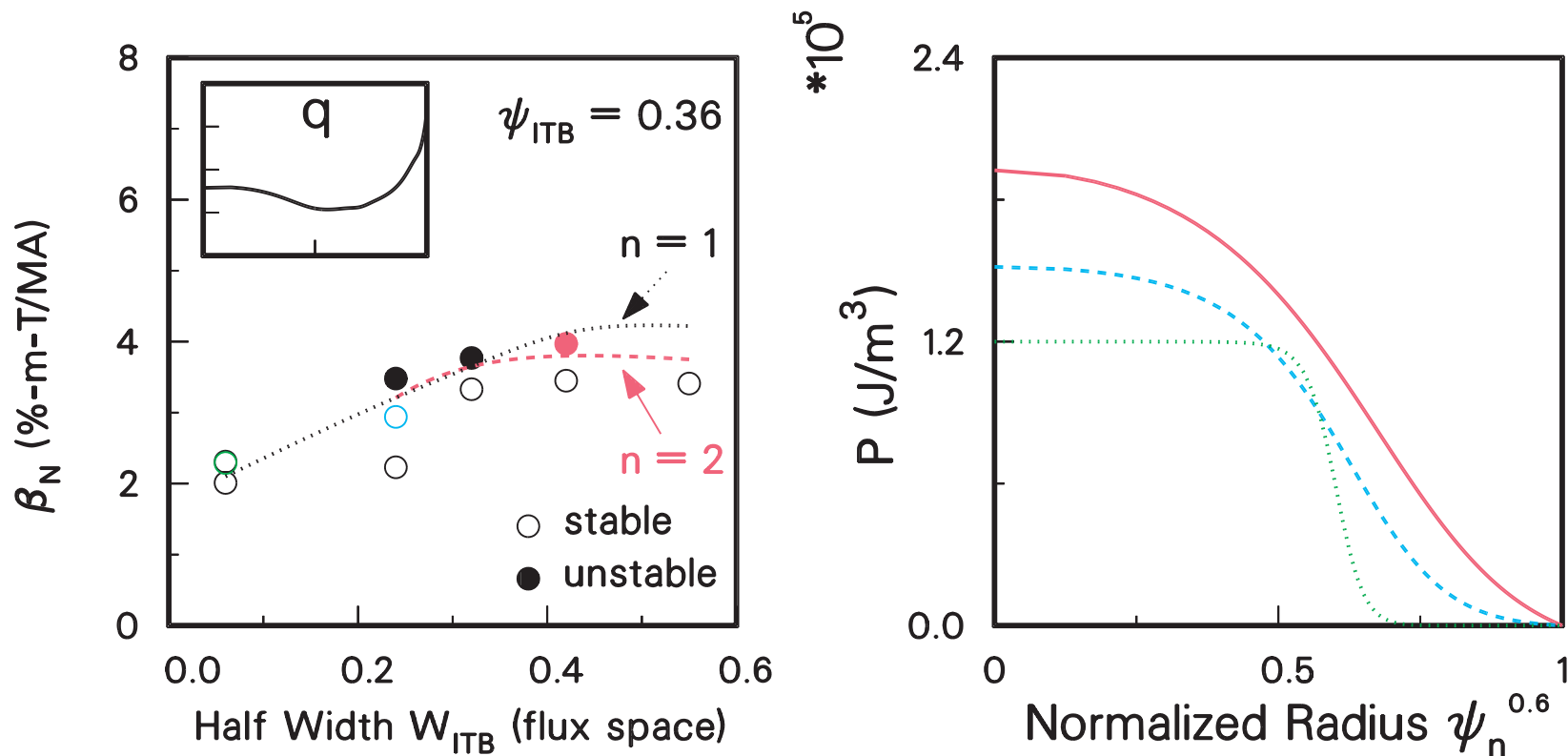
# STABILITY LIMIT VARIES WEAKLY WITH $q(0)$

- fixed shape DND,  $q_{95} = 5.1$ ,  $q_{\min} = 2.2$
- hyperbolic tangent pressure representation
- ideal  $n = 1$ , wall at  $1.5a$



## $n = 2$ MODES ARE MORE UNSTABLE IN ITB WITH LARGE WIDTH

- fixed shape DND,  $q_{95} = 5.1$ ,  $q(0) = 3.2$ ,  $q_{\min} = 2.2$
- ideal  $n = 2$ , wall at  $1.5a$
- wall stabilization is less effective against  $n = 2$  modes



# SUMMARY

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- **Hyperbolic tangent function provides an useful representation to systematic study the effects of Internal transport barrier (ITB) width and radius on MHD stability**
- **Stability limit improves with transport barrier width and radius**
- **Wall stabilization is crucial for ITB with large radius**
- **Stability limit varies weakly with  $q(0)$**
- **$n=2$  modes are more unstable in ITB with large radius and width**
- **Future work**
  - **More sophisticated pressure models, hyperbolic tangent + linear**
  - **Higher  $n$  modes, edge stability**
  - **Shaping, squareness, outboard bump**