

ELM STUDIES ON DIII-D

Presented by T. Osborne

General Atomics

in collaboration with

K.H. Burrell, T.N. Carlstrom, M.S. Chu, E.J. Doyle¹, J. Ferron, P.Gohil, C.M. Greenfield, R.J. Groebner, A. Hyatt, G.L. Jackson, R.J. LaHaye, L. Lao, C. Lasnier², E. Lazarus³, A.W. Leonard, M.A. Mahdavi, T.W. Petrie, C. Rettig¹, R.D. Stambaugh, G.M. Staebler, E.J. Strait, T.S. Taylor, A.D. Turnbull, H. Zohm⁴, and the DIII-D Team.

¹University of California at Los Angeles,

²Lawrence Livermore National Laboratory,

³Oak Ridge National Laboratory,

⁴MPI f. Plasmaphysik, Garching, Germany, EURATOM Association

Presented at the
Meeting of the American Physical Society,
Division of Plasma Physics,
Denver Colorado, USA
November 11-15, 1996.

ELM Issues Important for ITER

ITER requires H-mode E for ignition and to maintain high P_F during burn, $H_{\text{ITER93-H}} > 0.8$.

Since steady state ELM free discharges have not been demonstrated ITER must be prepared to operate with ELMs

The current ITER divertor design can tolerate $1\text{MJ}/\text{m}^2/\text{ELM}$ or $10\text{MJ}/\text{ELM}$ (1% at ignition) assuming all the ELM energy loss arrives in the divertor with the same spacial distribution as the steady state heat flux.

With these experiments we wish to answer the question:
Is high E ELMy H-mode with low ELM heat flux to the divertor possible for ITER ?

Discharges Studied

ITER cross sectional shape and R/a ($L_{\text{DIII-D}} / L_{\text{ITER}} = 0.2$).

$$3 < q_{95} < 6, (q_{\text{ITER}} = 3).$$

$$0.75 < I(\text{MA}) < 1.5, (I_{\text{ITER}} = 2.2)$$

$$1 < B(\text{T}) < 2, (B_{\text{ITER}} = 5.7).$$

$$0.06 < P_{\text{IN}}/S \text{ (MW/m}^2\text{)} < 0.3, (0.17_{\text{IGNITION}} < P/S_{\text{ITER}} < 1.25_{\text{BURN}}).$$

$$0.2 < n_{\text{GREENWALD}} < 0.7, (n_{\text{ITER}} = 1.0).$$

Gas Puff Fueled.

Open Divertor.

No Divertor Pumping.

B Drift Toward the X-point.

ELM Classification

Type 1

$$dfreq_{ELM}/dP_{IN} > 0$$

No Precursors

$$p'_{EDGE} \quad p'_{BALLOONING}$$

$$\text{Large } W_{ELM}/W \quad 6 \%$$

$$\text{High } H_{ITER93-H} > 0.9$$

Type 3

$$dfreq_{ELM}/dP_{IN} < 0$$

Coherent precursors

$$p'_{EDGE} \quad p'_{BALLOONING}$$

$$\text{Small } W_{ELM}/W \quad 1 \%$$

$$\text{Low } H_{ITER93-H} < 0.9$$

Two Regimes

- Low n_e
- Low T_e

Pedestal Heights for Different ELM Classes

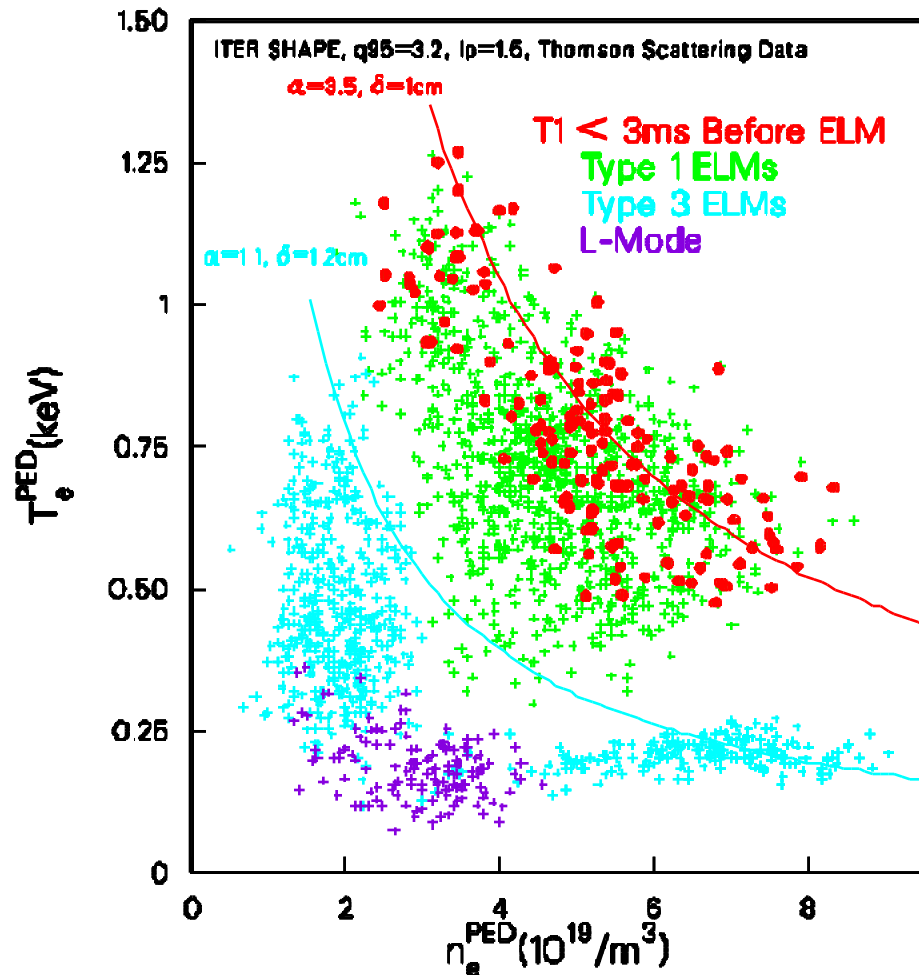
Different classes of ELMs appear in distinct regions of electron density and temperature pedestal heights.

Pressure gradient, α , at **Type 1** ELMs is near ideal ballooning limit.

Type 3 ELMs appear in two regions.

Low n_e Type 3 ELMs have $\alpha < \alpha_{\text{CRIT}}$.

Low T_e Type 3 ELMs have $T_e < T_{\text{CRIT}}$. In ASDEX-U these ELMS have been produced with $\alpha = \alpha_{\text{TYPE-1}}$ at high n_e . In DIII-D, n_e was limited by marfing and return to L-mode.



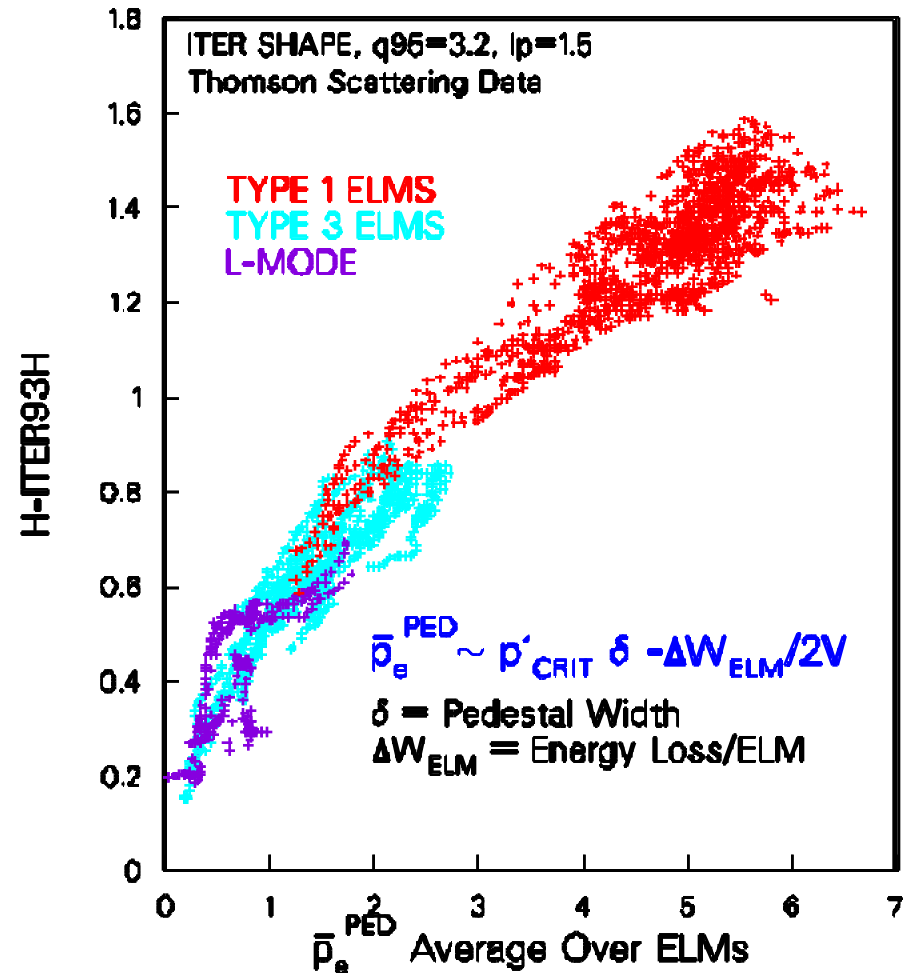
H-Mode Pedestal and Energy Confinement

Discharges with large H-mode pedestals have high energy confinement enhancement, **H**.

Type 1 ELM discharges have large pedestals due to high edge pressure gradient.

Low n_e Type 3 ELM discharges have limited α and therefore poor **H**.

Low T_e Type 3 ELM discharges may reach higher **H** if α increases at high n_e as in ASDEX-U.

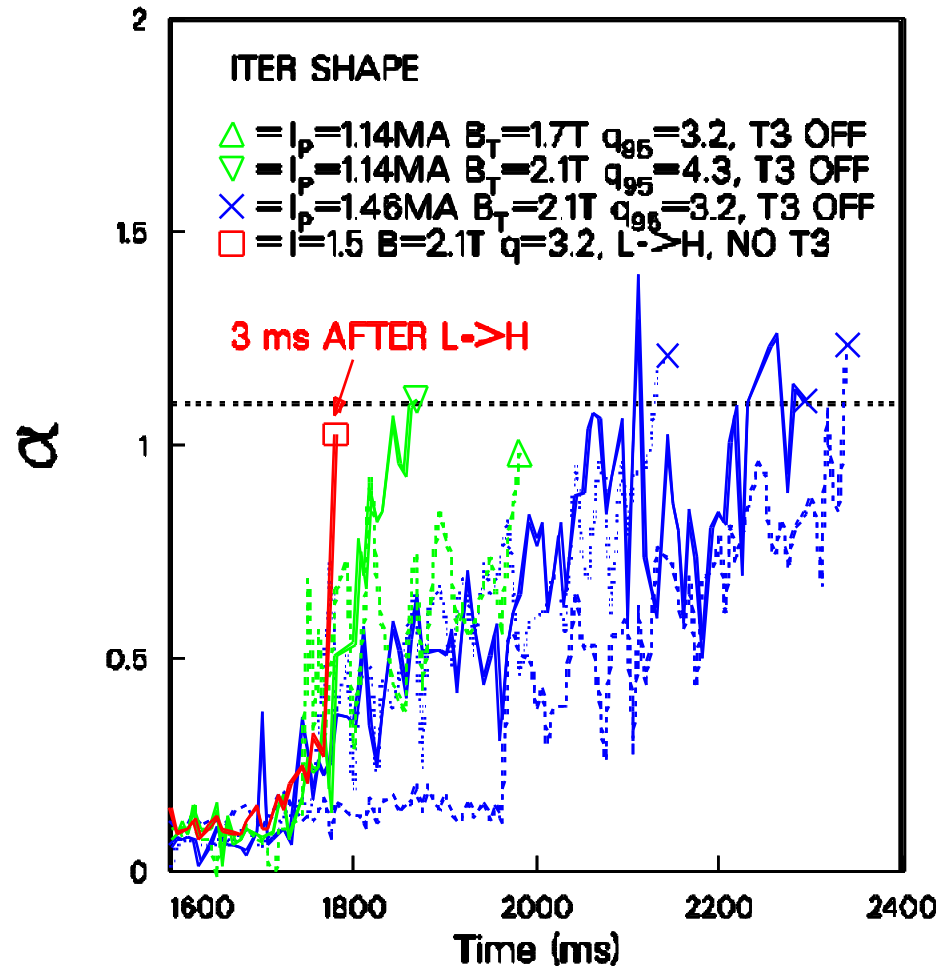


Critical Pressure Gradient for Low Density Type 3 ELMS

Low n_e Type 3 ELMS shut off at approximately the same edge pressure gradient, α .

Discharges at high density which do not have Low n_e Type 3 ELMS reach the critical α shortly after the L->H transition.

Rapid build up of α may be due to a large neutral influx following the L->H transition in this case.

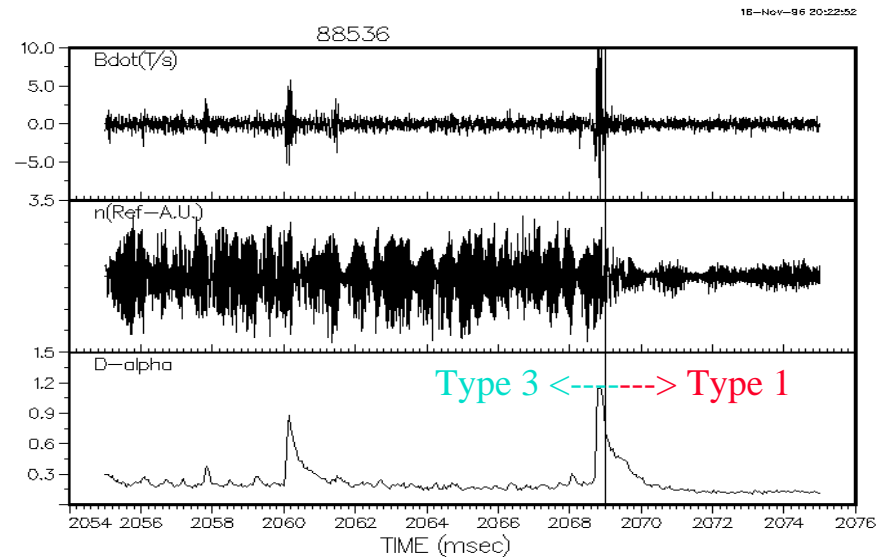
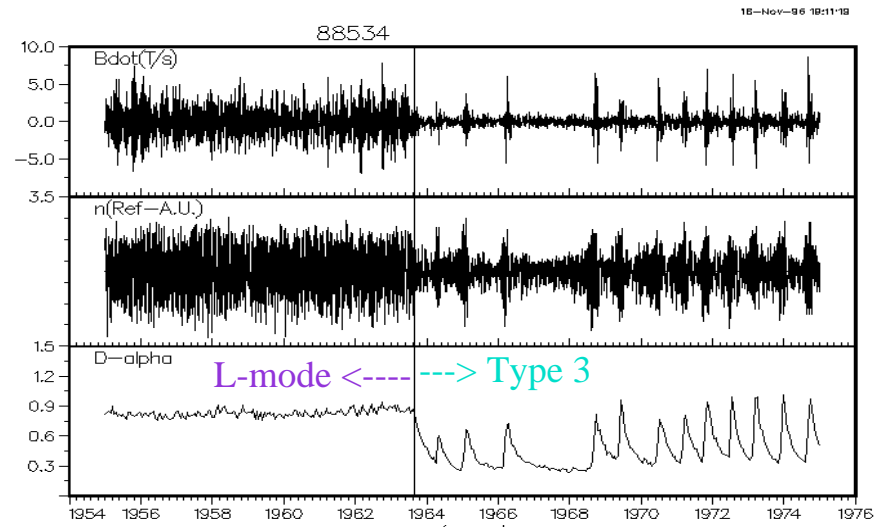


Low Density Type 3 ELM Regime

The end of the low density type 3 ELM phase has the characteristics of a secondary transition.

Density fluctuations are reduced both at the L->T and T3->T1 transitions.

A sudden reduction in the width of the H-mode pedestal, δ_{PED} , is also observed at the T3->T1 transition.



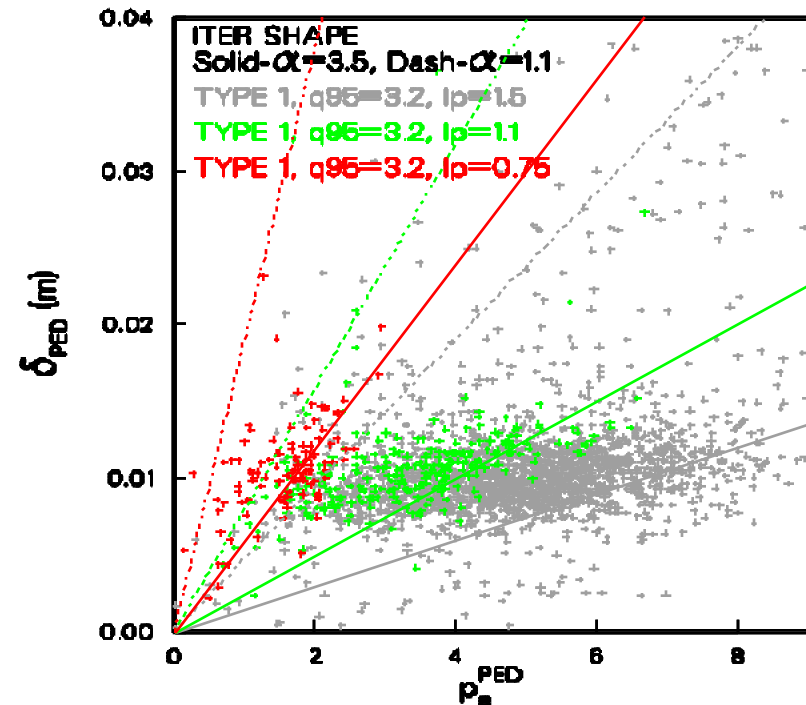
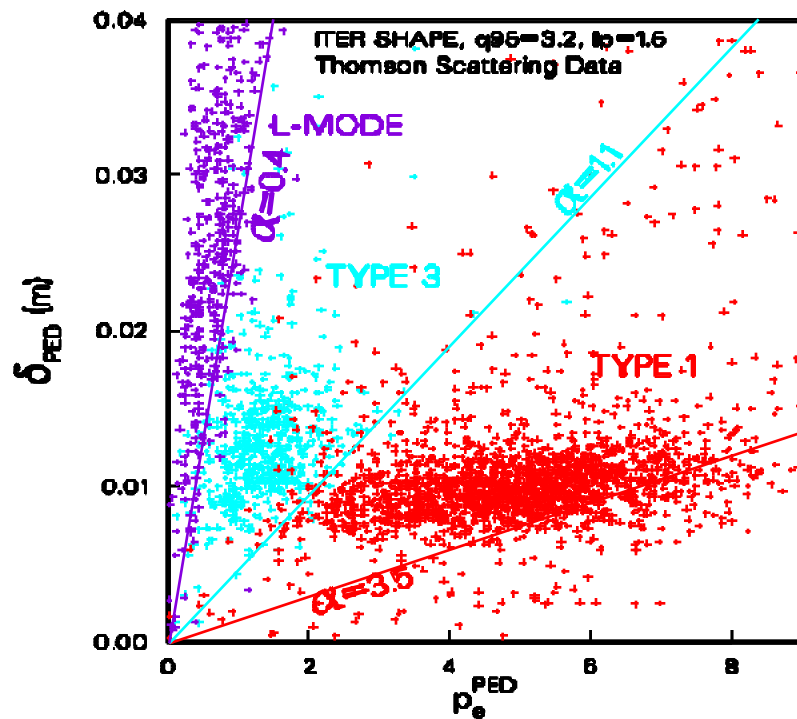
H-Mode Pedestal Characteristics

The width of the steep gradient region is relatively constant and similar for **Type 1** and **Type 3** ELMs.

The width is independent of I_p at fixed q for **Type 1**.

The range of pressure gradient, $\Delta\alpha$, spanned in **Type 1** ELMs is constant at fixed q .

The lower bound in α for **Type 1** is roughly the upper bound for **Type 3**.



Estimate of **Type 1** ELM Energy Loss for ITER

The DIII-D data for ITER shape discharges suggest that:

The range in edge pressure gradient, $\Delta\alpha$, spanned in Type 1 ELMs remains constant at fixed \mathbf{q} .

- The same $\Delta\alpha$ might be expected in ITER since the magnetic shear is independent of size.

The width of the steep gradient region, δ_{PED} , is fixed through most of the ELM cycle and is fixed at fixed \mathbf{q} .

Assuming the type 1 ELM energy loss represents a change in the H-mode pedestal height: $W_{\text{ELM}} = \delta_{\text{PED}} p'_{\text{PED}} V$.

Assuming $p_{\text{PED}} \propto L^{1-g}$ where L is the length scale gives for

$g=0$, $W_{\text{ITER}} = 32 \text{ MJ}$ (suggested by $\delta_{\text{PED}} = \text{const}$ at fixed \mathbf{q})

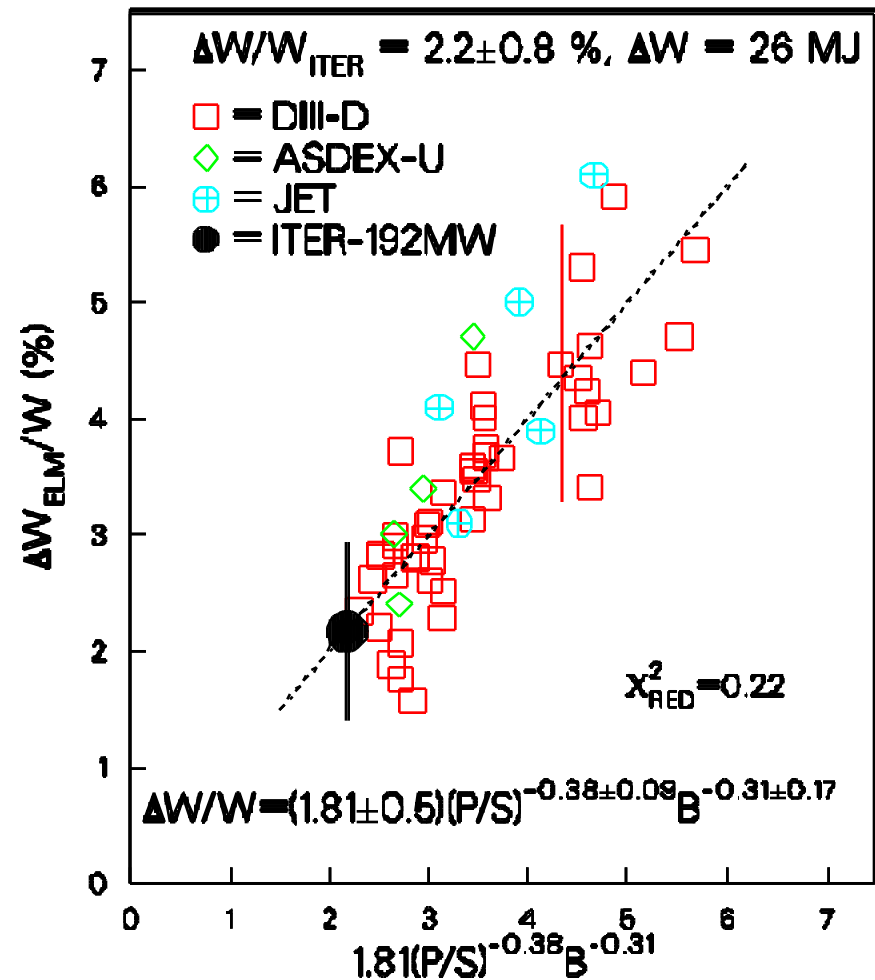
$g=0.5$, $W_{\text{ITER}} = 11 \text{ MJ}$, $g=1$, $W_{\text{ITER}} = 1 \text{ MJ}$

$\propto T_{\text{PED}}^{1/2} (\text{JET})$, $W_{\text{ITER}} = 7 \text{ MJ}$

Scaling of **Type 1** ELM Energy Loss

A scaling of the energy loss per **Type 1** ELM with global parameters gives **26 MJ** for ITER.

Using ITER93-H scaling for energy confinement time implies W_{ELM} depends strongly only on plasma current and geometry.



Type 1 ELM Effects in the Divertor

For ITER shaped plasmas with $q_{95} = 3.2$ most of the ELM energy loss reaches the divertor with the majority to the inner leg (which is typically detached in DIII-D).

$$\begin{aligned}W_{\text{DIV}} &= (0.75 \pm 0.25) W_{\text{ELM}} \\W_{\text{INNER}} &= (0.50 \pm 0.16) W_{\text{ELM}} \\W_{\text{OUTER}} &= (0.23 \pm 0.11) W_{\text{ELM}}\end{aligned}$$

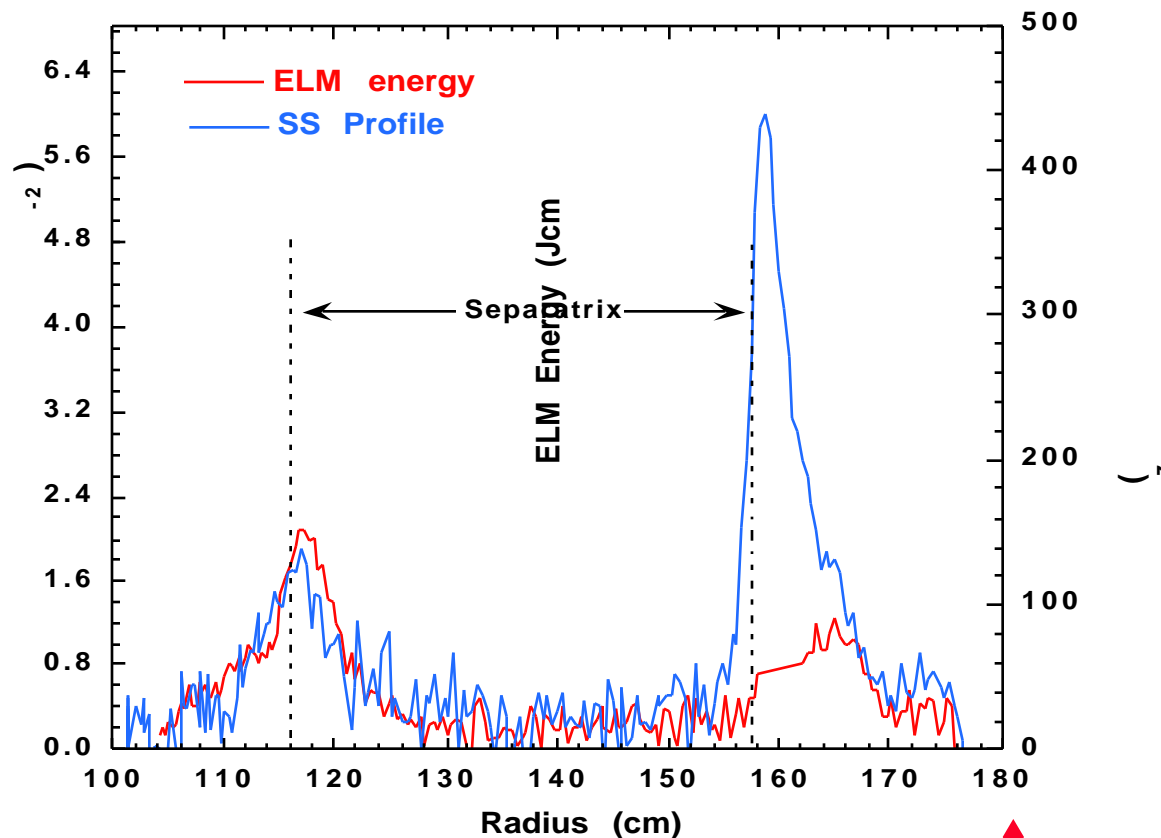
The ELM heat flux is distributed over about a factor of two larger area than the time averaged heat flux.

The ELM energy loss arrives in the divertor on a millisecond time scale.

Divertor Heat Flux During Type 1 ELM

The ELM heat flux dominates the inboard heat flux since the inboard leg is typically detached.

The ELM profile is broader at the outboard strike point than the steady state.



Conclusions

Prospects for high energy confinement ELMy H-mode with low ELM heat flux to the divertor in ITER.

Although **Type 3 ELMs** have low ΔW they may not be compatible with high **H** factor.

- If the **low n_e regime** is limited to $\alpha < \alpha_{\text{TYPE-1}}$ and δ_{PED} are similar, then **H** will be reduced.
- In the **low T_e regime** **H** might reach Type 1 values at high n_e where possibly $\alpha_{\text{TYPE-3}} = \alpha_{\text{TYPE-1}}$ (Asdex-U).
 - ⑦ T_{PED} for ITER would be 6.4, 2.2, or 0.25 that of DIII-D for g of 0, 0.5, or 1.0. If the low T_e regime represents a resistive effect it might not occur in a higher T_{PED} ITER.

Conclusions, continued

Prospects for high energy confinement ELMy H-mode with low ELM heat flux to the divertor in ITER.

Estimates of **Type 1 ELM** energy loss and divertor effects for ITER are near the limit of what is acceptable.

- Need to develop techniques for controlling either the ELM energy loss or the fraction which arrives in the divertor.

Conclusions, continued

The oscillation of the edge pressure gradient between two limits for Type 1 ELMs is suggestive of the recent CDBM theory of S. Itoh, et. al^[1] in which the plasma oscillates between M-Mode and H-mode.

[1] Sanae-I Itoh, Kimitaka Itoh, Atsushi Fukuyama, and Masatohi Yagi, *Plasma Phys. Control. Fusion*, **38** (1966) 527-549.