Feedback stabilization of current-driven resistive-wall-modes (RWMs) at q_{95} ~4 in DIII-D

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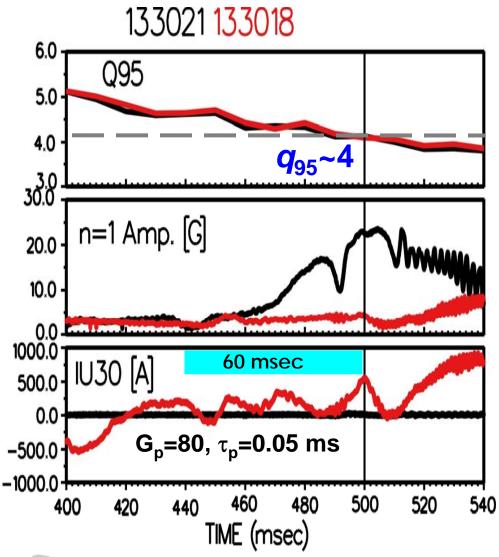


Reproducible current-driven RWM enables us to explore the RWM feedback process

- Due to the irreproducibility of pressure-driven RWMs, the RWM feedback process has not been evaluated thoroughly.
- The RWM feedback control can be assessed using a reproducible RWM target at $q_{95} \sim 4$.
- The experimental results help us evaluate various RWM feedback performance, as well as the RWM feedback process.



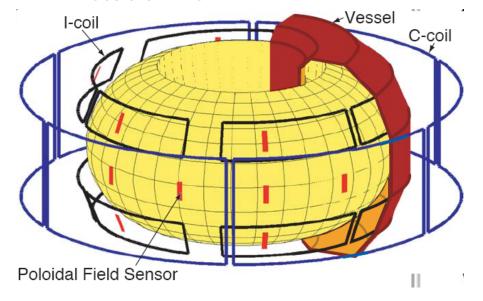
Complete feedback stabilization of current-driven RWM at q_{95} ~4 has been achieved in DIII-D



 Ohmic discharge with high current ramp-up rate

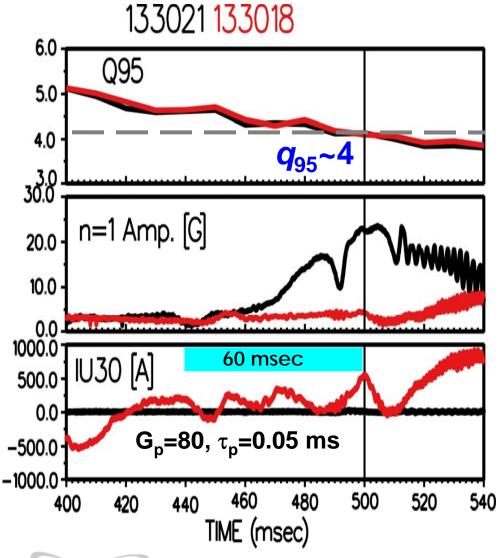
Tools

- Internal coils ("I-coils"):
 Direct Feedback + Dynamic error field correction (EFC)
- External coils ("C-coils"):Static EFC





Complete feedback stabilization of current-driven RWM at q_{95} ~4 has been achieved in DIII-D



- Ohmic discharge with high current ramp-up rate
- Feedback loop ($\tau_p << \tau_w$)

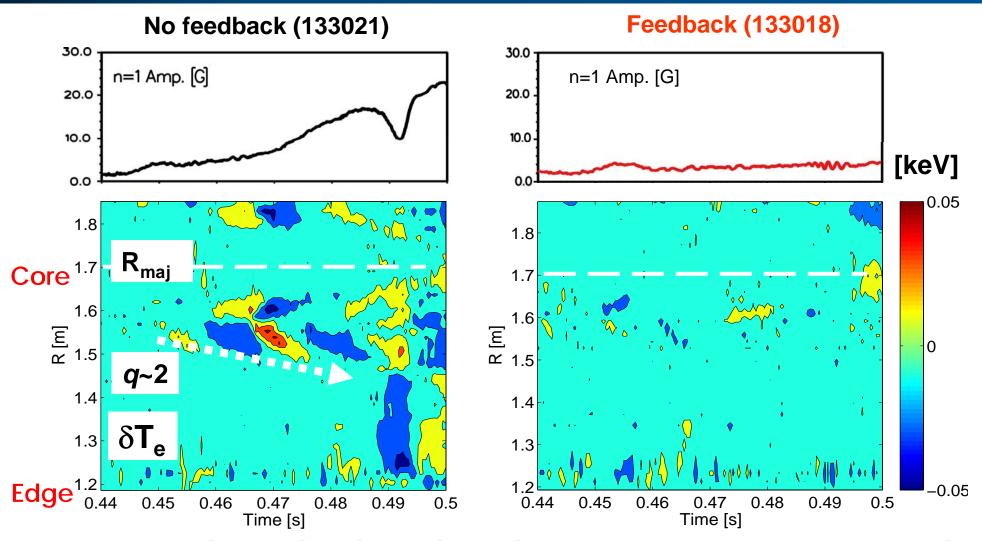
$$V_{FB}^{n=1} \qquad (\tau_{W}, \tau_{L/R}, \delta I_{FB}^{n=1})$$
Power Supply Plant (DIII-D/RWM)
$$\delta B^{n=1} \qquad \delta B^{n=1} \qquad (\delta B^{n=1}, \delta B^{n=1})$$

Controller
$$K(s) = \frac{1}{1 + s\tau_p} \left[G_p + \frac{G_d s\tau_d}{1 + s\tau_d} \right]$$

 $G_{p,d}$: Gain $\tau_{p,d}$: time constant where p - proportional, and d - derivative



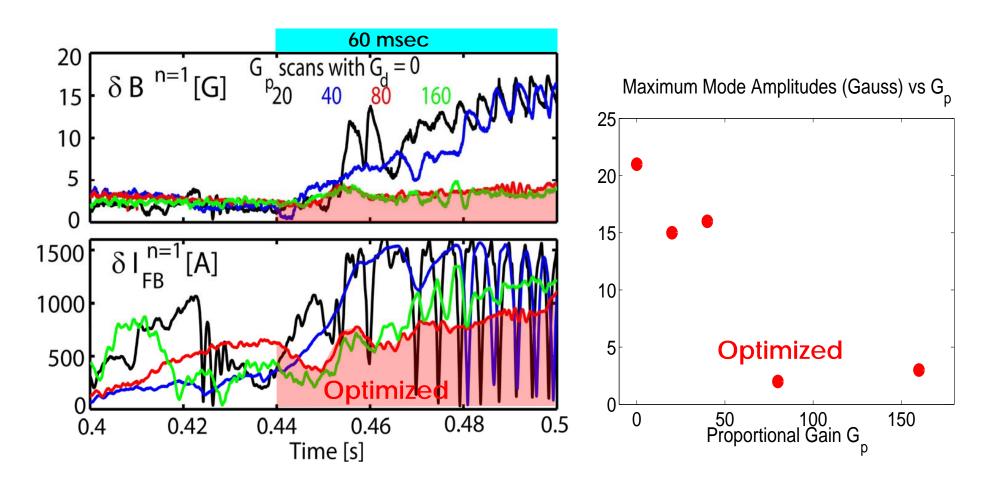
The RWM-associated internal structures are eliminated by RWM feedback control



RWM-induced edge disturbance is also suppressed.



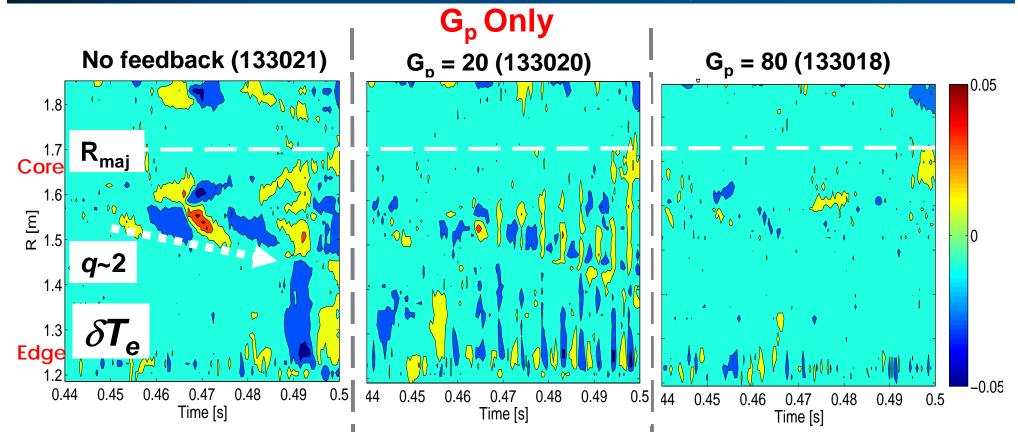
The optimized gain ($G_p=80$) has been found with G_p only



 As the gain approaches the optimal level, the mode growth rate decreases as expected.



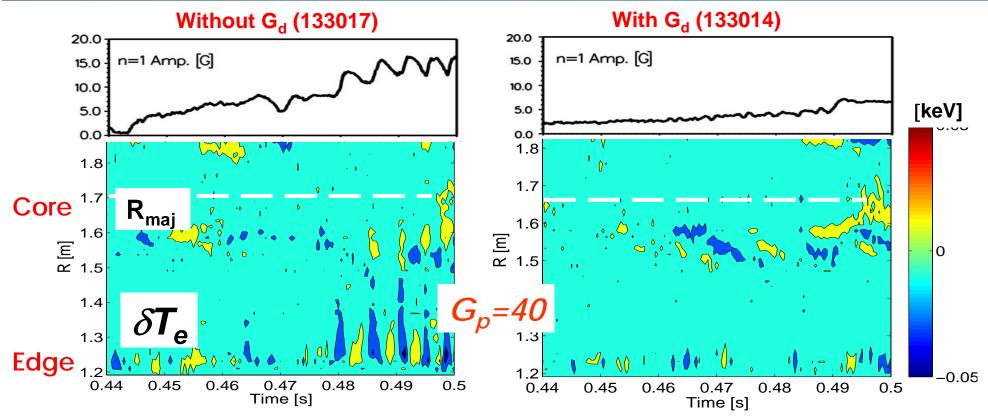
Sub-optimal gain is not only less effective in suppressing the RWM but also disturbs the plasma edge



 Meanwhile, the edge disturbances are not observed at the over-optimal gain (e.g. G_p = 160).



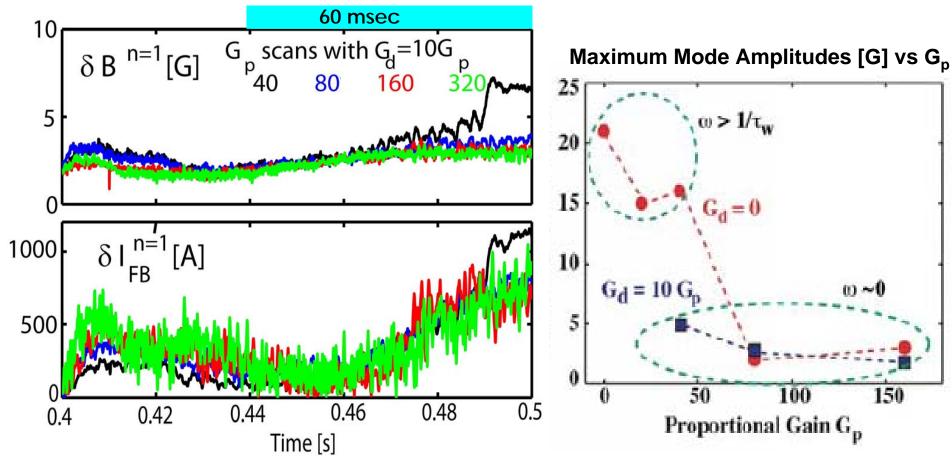
The use of derivative gain broadened the effective gain range for RWM feedback stabilization at q_{95} ~4



- A value of G_d = 10G_p is chosen to use voltage controller 'effectively' as current controller, based on τ_d and τ_{L/R} of the feedback system.
- The addition of G_d minimizes the phase lag in time between RWM and the applied field.

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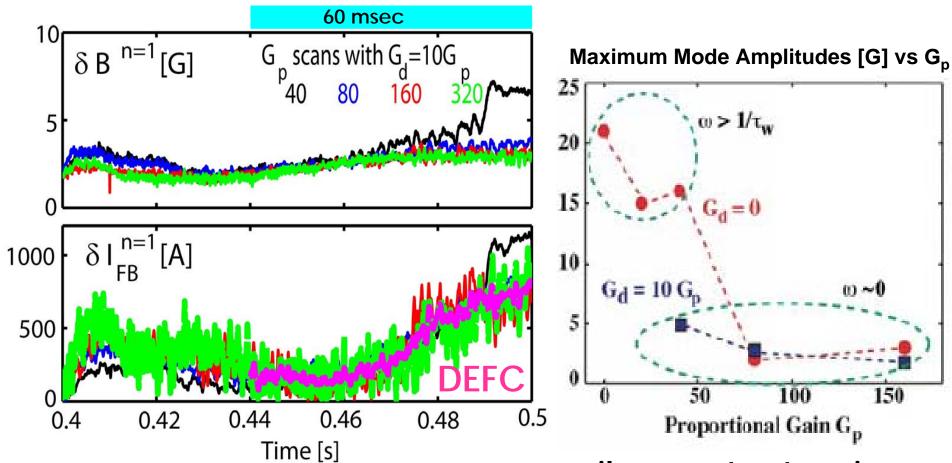
Direct RWM control is the dominant stabilization process, while good error field correction is prerequisite



 Similarly finite amplitude of the coil currents at various G_p values indicate the EFC portion necessary for effective stabilization.

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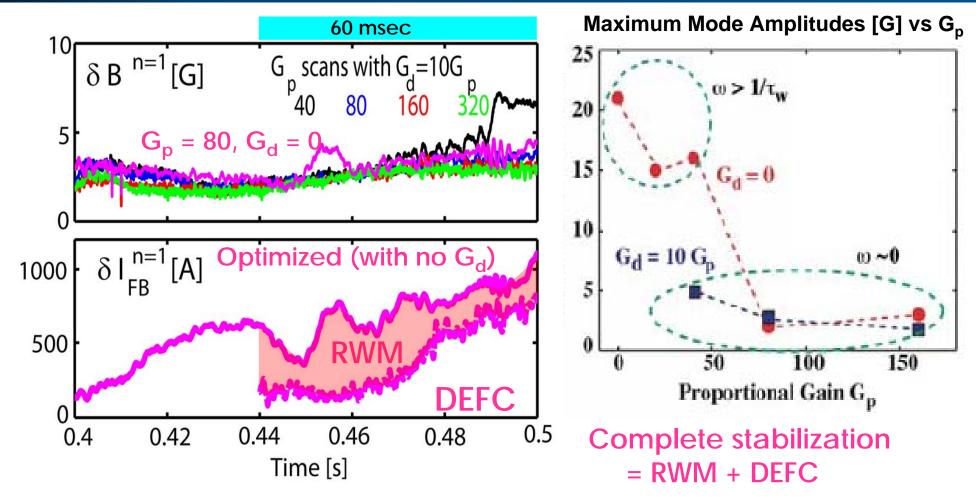
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Direct RWM control is the dominant stabilization process, while good error field correction is prerequisite



 From the known DEFC, the portion of the coil current necessary for the direct RWM control can be extracted.



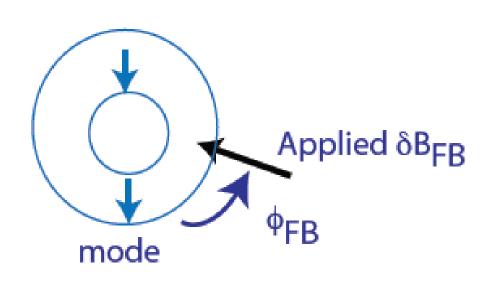
Conclusions

- Current-driven RWM at q_{95} ~ 4 was completely stabilized by the RWM feedback control.
 - An optimized proportional gain (G_p=80) has been found without using derivative gain.
 - The use of derivative gains ($G_d=10G_p$) expanded the stable range of proportional gains.
 - Reducing a phase lag in time avoids any mismatch between RWM and applied field.
- The success of stabilization of the current-driven RWM at q_{95} ~ 4 is primarily due to the direct RWM control, while a good error field correction is overlaid.
- Similar feedback performance is expected even for the pressure-driven RWM in high- β plasmas, as long as the difference of the plasma responses between low and high- β plasmas is properly addressed.





A phase-shifted n=1 field in the direction of $co-l_p$ rotation is more effective than in the opposite direction.



 A range of preferred toroidal phase shifts ahead of the RWM exists for effective feedback

