

# Density Control Using the New Divertor Pumping Configuration in DIII-D

by  
T.W. Petrie

for

P.M. Anderson, M.A. Mahdavi, N.H. Brooks,  
R.J. Colchin,\* J.R. Ferron, C.M. Greenfield,  
A.W. Hyatt, C.J. Lasnier,<sup>†</sup> T.C. Luce, C.J. Murphy,  
C.C. Petty, M.J. Schaffer, M.R. Wade, W.P. West,  
and J.G. Watkins<sup>‡</sup>

\*Oak Ridge National Laboratory, Oak Ridge, Tennessee.

<sup>†</sup>Lawrence Livermore National Laboratory, Livermore, California.

<sup>‡</sup>Sandia National Laboratories, Albuquerque, New Mexico.

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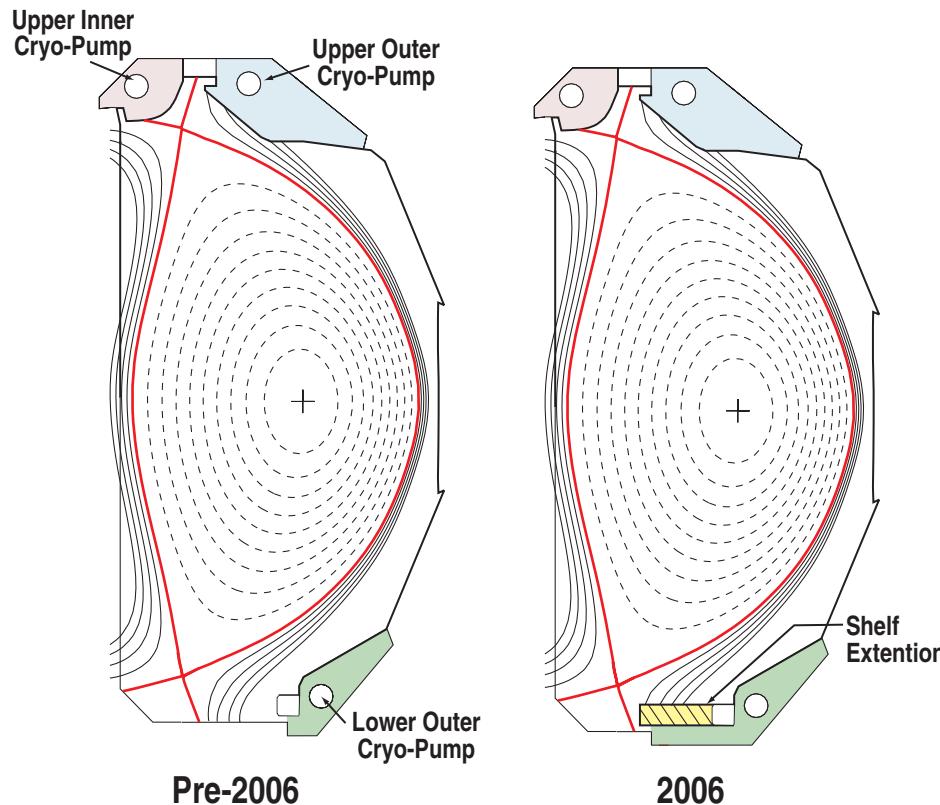


# The Changes to the Pumping Configuration Were Driven by the DIII-D Advanced Tokamak Program

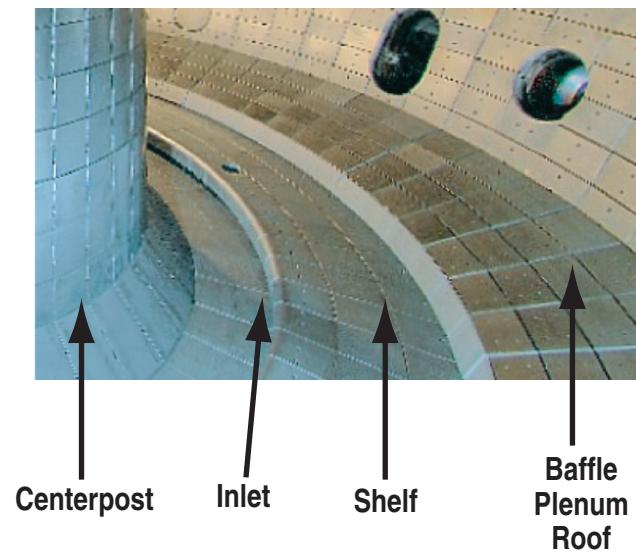
- **High performance “AT” plasmas benefit from:**
  - High triangularity ( $\delta$ ), double-null (DN) shaping → higher  $f_{bs}$  and  $\beta_N$
  - Application of ECCD ( $\propto 1/n_e$ )
    - Shape/maintain favorable current density profiles
    - Achieve 100% non-inductive current
- **Density control in a high- $\delta$  DN shape is difficult to maintain if active particle exhaust is limited to only one divertor (pre-2006)**
  - Solution: Modify hardware for pumping high  $\delta$ , DNs from both divertors
- **Changes to the lower divertor pumping configuration were made during the 2005-2006 vent to implement this solution**
- **The new pumping configuration has improved density control in DN and near-DN shapes**

# Recent Modifications to the Lower Divertor Makes it Possible to Pump High- $\delta$ DN Plasmas from Both Divertors

- Prior to 2006, the lower divertor cryopump was poorly situated for removing recycled neutral particles from high  $\delta$ , symmetric DNs
- A shelf extension was installed in 2006 to serve as a conduit for neutrals between the lower outer divertor target and the pumping plenum

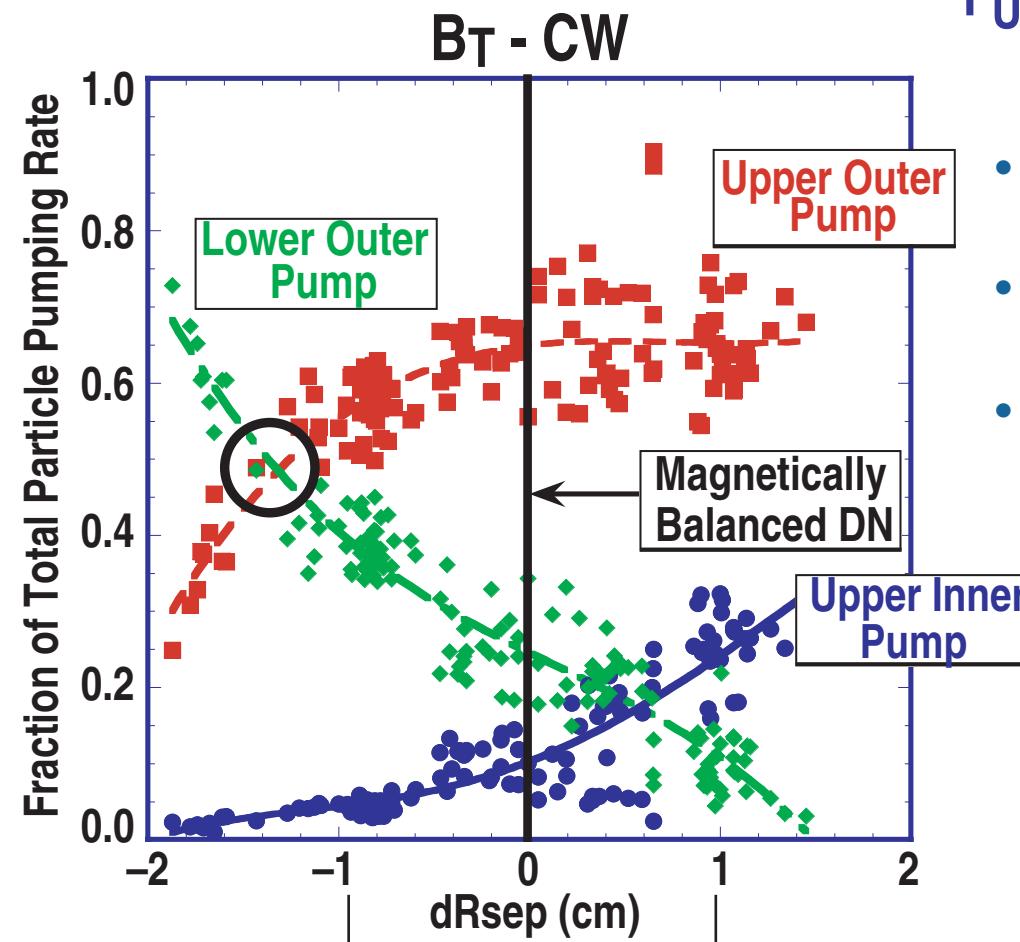
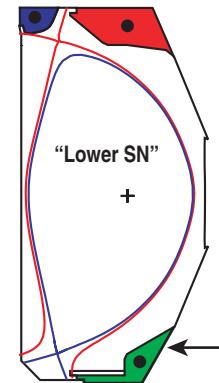
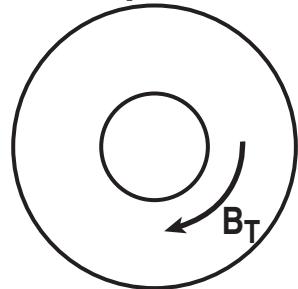


Lower Divertor (2006)



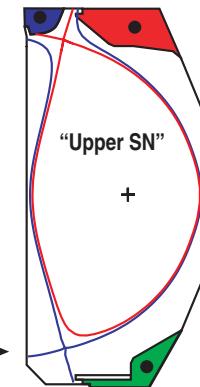
# The Fractional Contribution of Each Cryopump to the Total Particle Exhaust Rate Depends on the Magnetic Balance

Top View

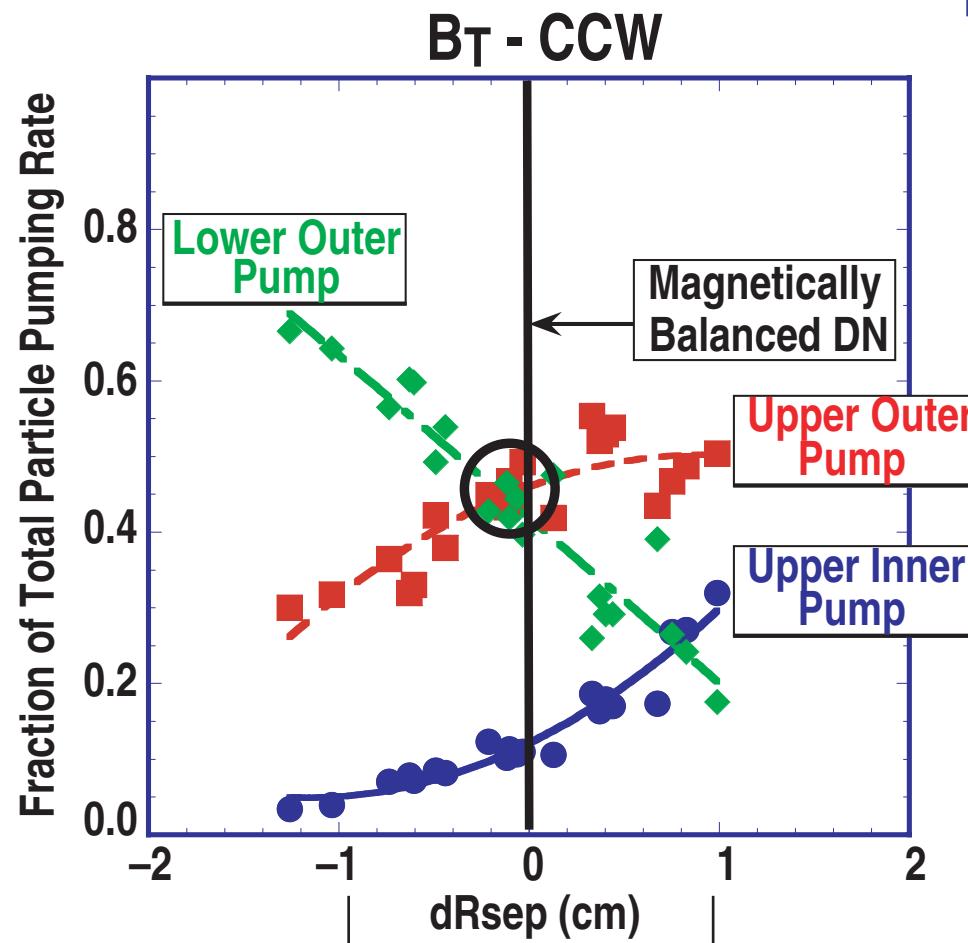
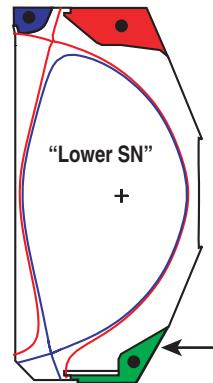
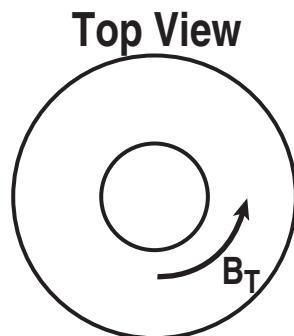


$$F_{UP-IN} + F_{UP-OUT} + F_{LO-OUT} = 1$$

- DN:  $F_{UP-OUT} > F_{UP-IN}$  &  $F_{LO-OUT}$
- DN:  $\frac{F_{UP-OUT}}{F_{LO-OUT}} \approx 2.5$
- DN:  $F_{UP-IN}$  removes  $\approx 10\%$  of total pumped particles

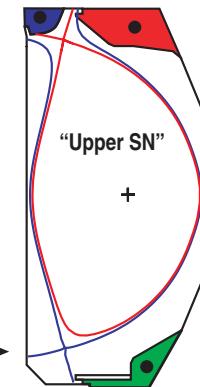


# Reversing the Direction of $B_T$ Significantly Affects the Fractional Contributions of the Two Outer Pumps

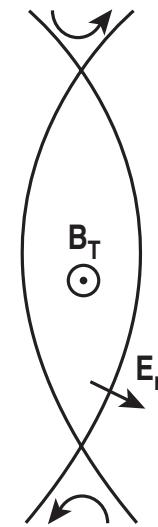
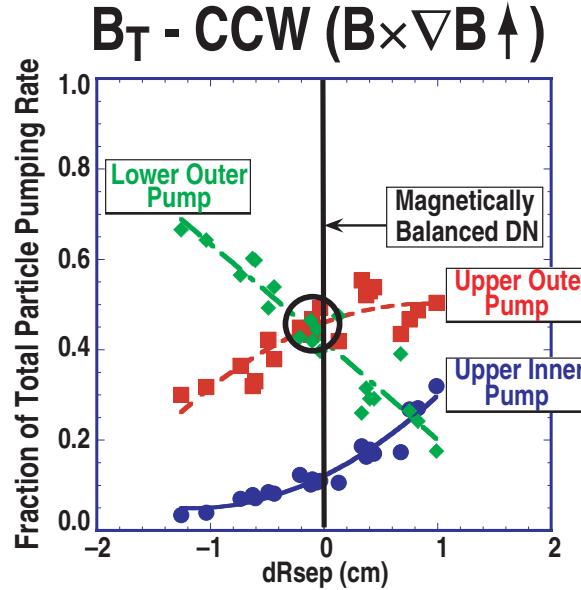
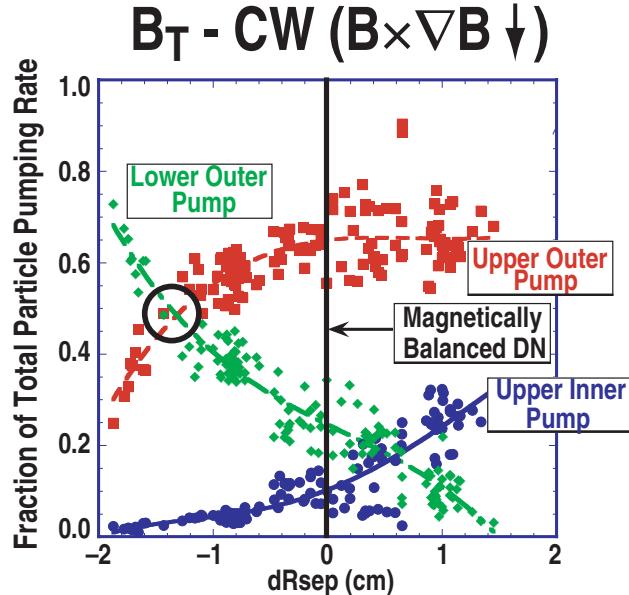


$$F_{UP-IN} + F_{UP-OUT} + F_{LO-OUT} = 1$$

- DN:  $F_{UP-OUT} \approx F_{LO-OUT}$  near DN
- DN:  $F_{UP-IN}$  is still  $\approx 10\%$



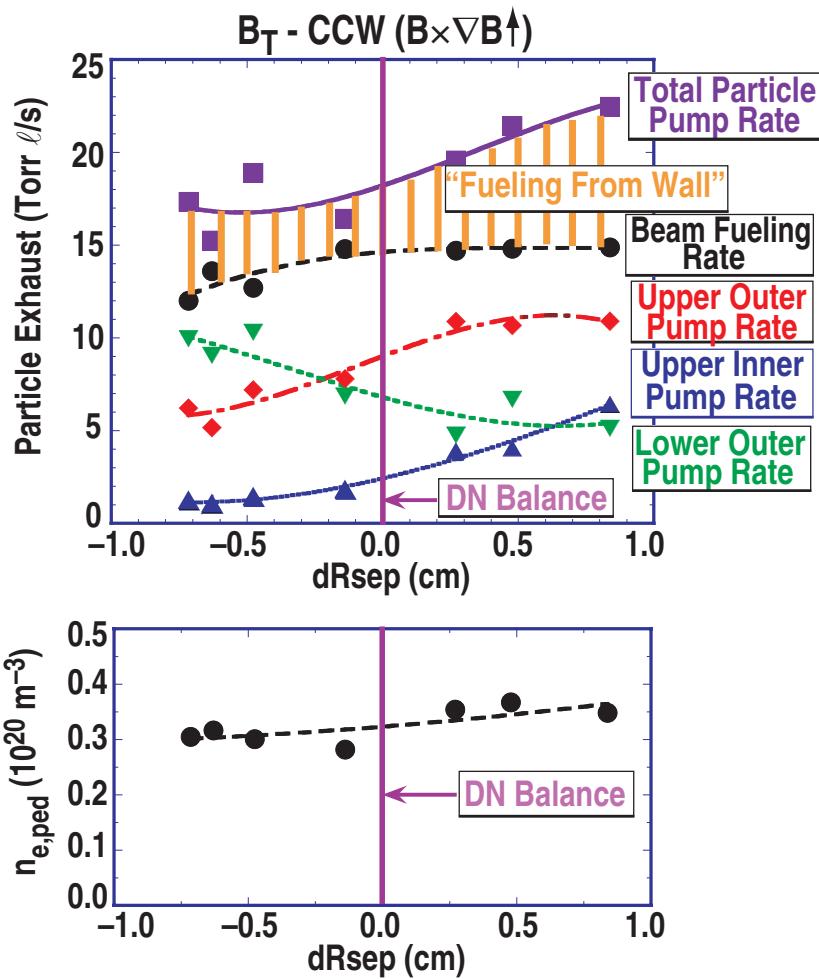
# Both Particle Drifts and Divertor Geometry Appear to be Important Factors in Pumping Behavior



- The difference in pumping “crossover” locations in the CW and CCW cases is qualitatively consistent with the roles of particle drifts in the SOL and divertor\*
  - $B_T - CW \rightarrow B \times \nabla B \downarrow, B_T - CCW \rightarrow B \times \nabla B \uparrow$
- But still not symmetric around  $dRsep=0$ : May be due to differences in geometry between upper and lower divertors (e.g., neutral particle trapping)

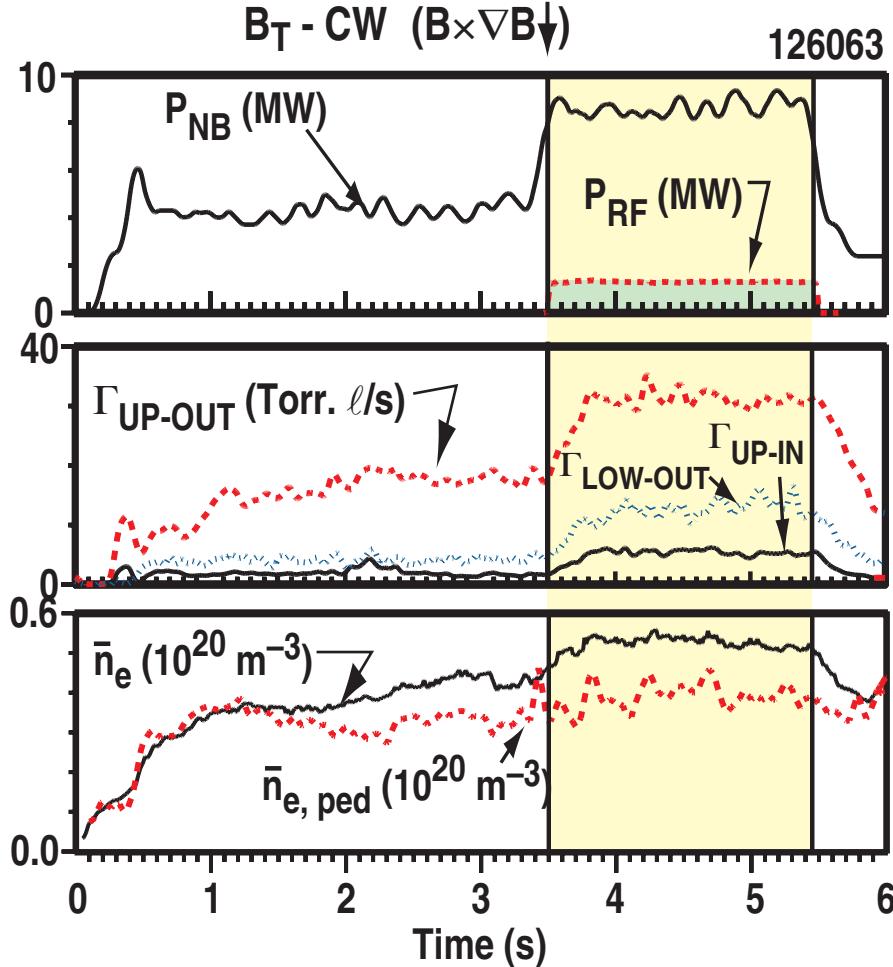
\*T.W. Petrie, et al., Nucl. Fusion 46 (2006) 57

# Particle Pumping and Low Plasma Density Can Be Maintained in Both Upwardly Biased and Downwardly-Biased DN Shapes



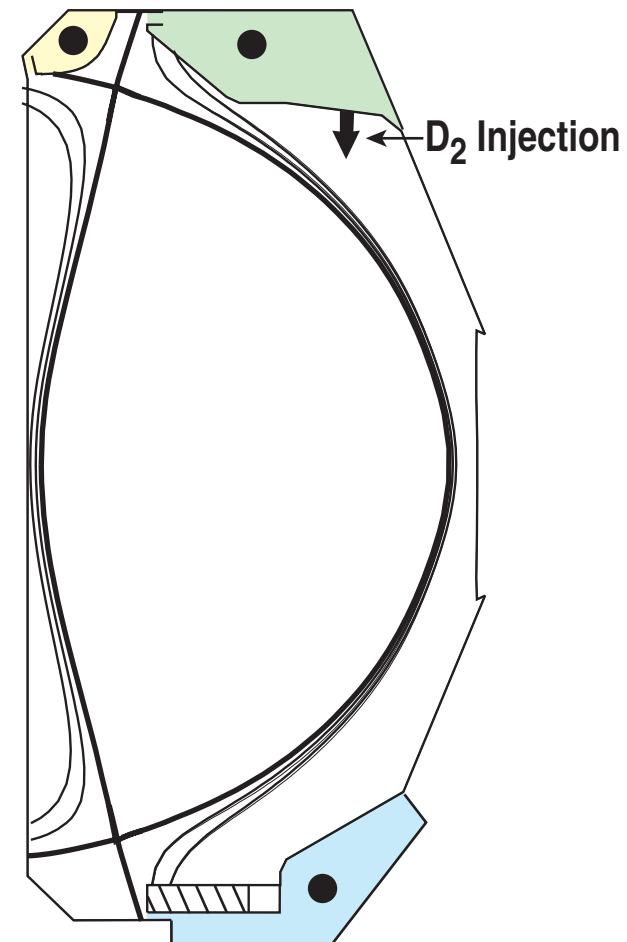
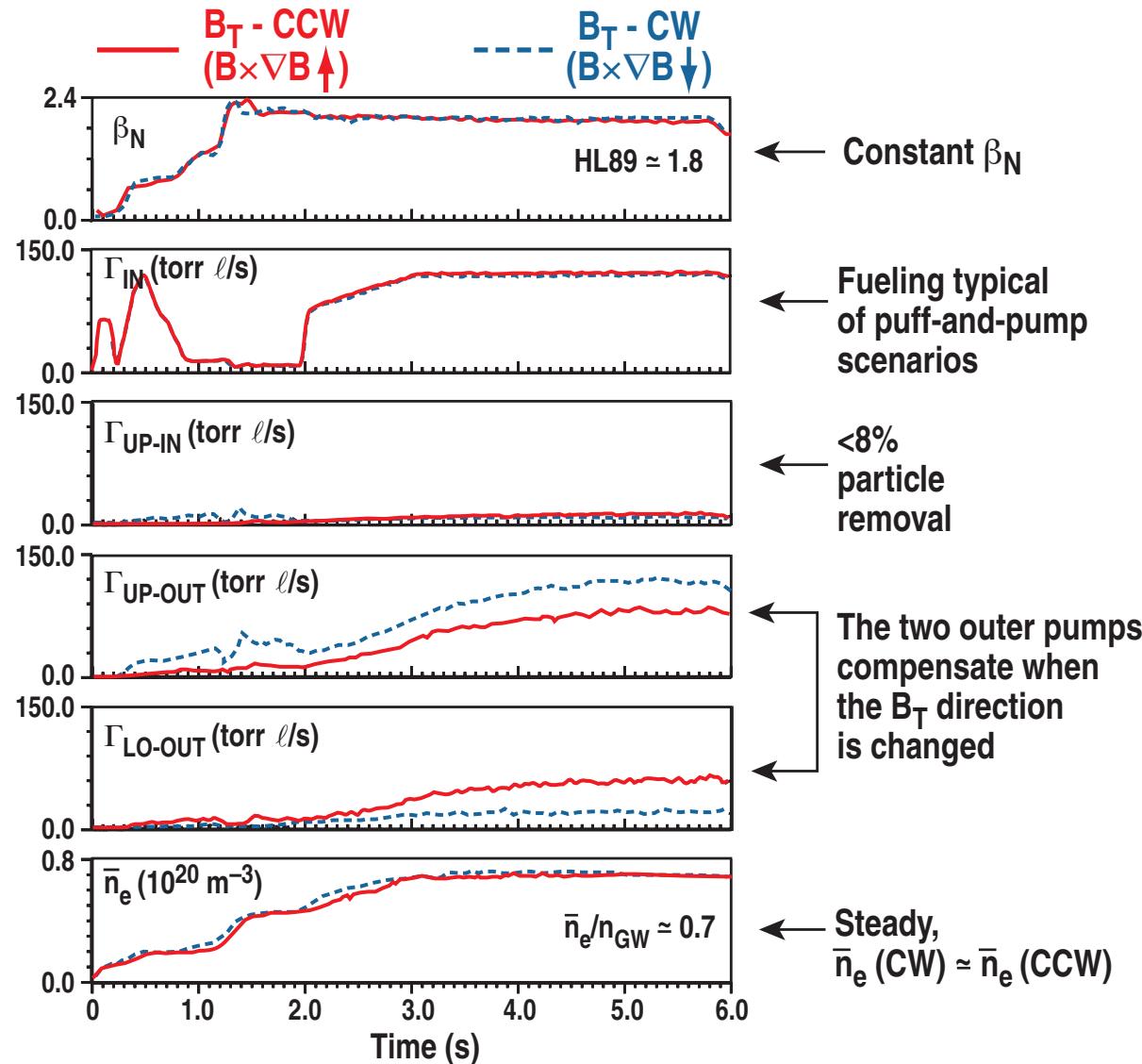
- The total particle pumping rate was greater than the particle fueling rate from the beams  
⇒ The “wall” was a source of particles at the time of measurement
- The combined particle exhaust of the two outer pumps remained nearly constant as  $dR_{sep}$  was changed near DN
- The pedestal density was fairly insensitive to changes in magnetic balance

# Initial Results at Controlling Density in DN AT Plasmas are Encouraging



- $\rightarrow \beta_N \approx 3.6$ , HL89 = 2.6 during the high power phase
- Lower outer pump makes an important ( $\approx 30\%$ ) contribution to particle control
- $\bar{n}_e$  and  $n_{e,ped}$  are steady, and they are  $\approx 20\%$  lower than previous DN densities with upper pumps only

# The Modified Pumping Configuration Makes it Possible to do Experiments involving High Gas Throughput in High- $\delta$ DN Plasmas for Both $B_T$ Directions

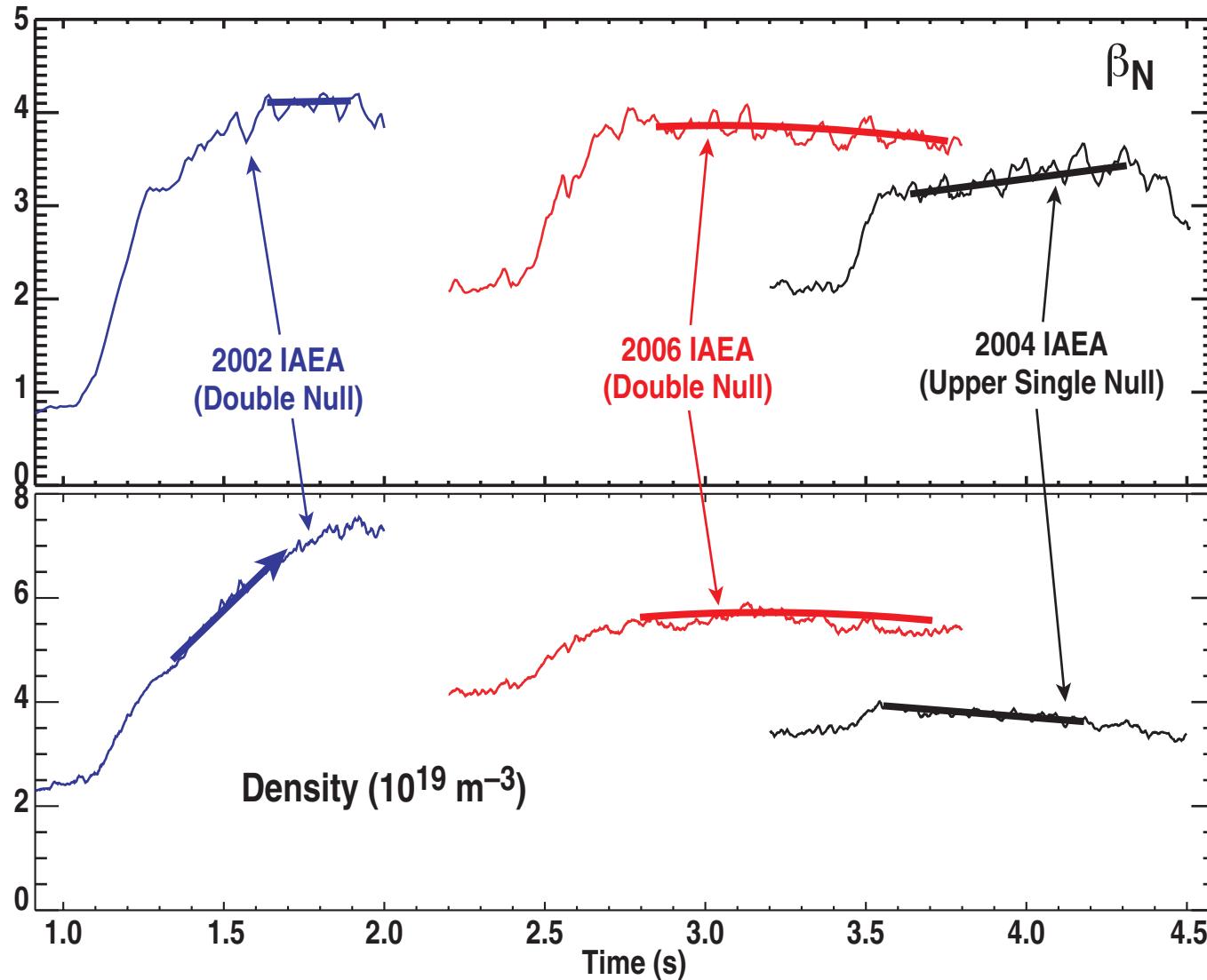


# Summary and Conclusion

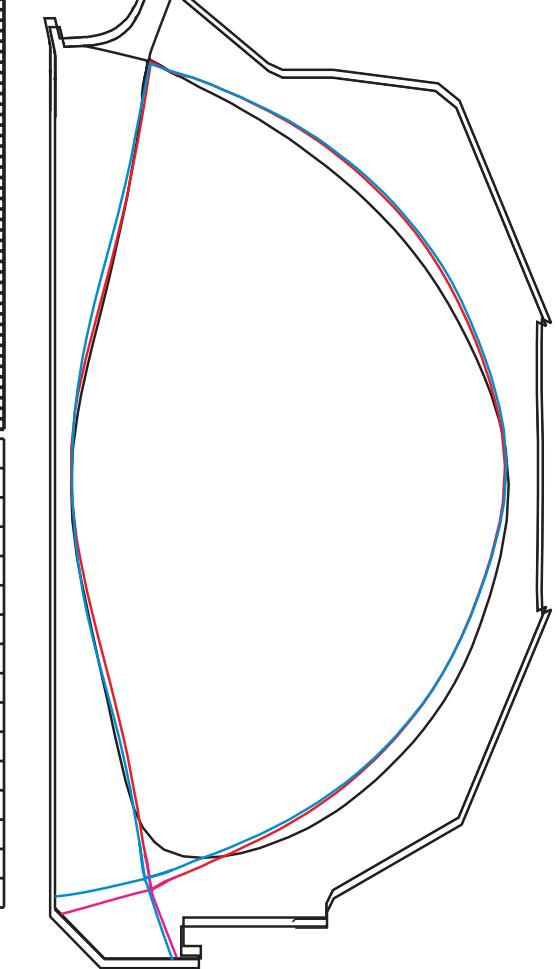
- **Simultaneous particle pumping from both upper and lower divertors of high triangularity, DN plasmas is now possible in DIII-D**
  - Characterized pumping WRT two key parameters: dRsep and  $B_T$  - direction
  - Demonstrated density control in high performance AT plasmas
- **In addition to its value to the AT program, the new pumping capability is able to handle high gas throughput scenarios in DN and near-DN shapes, e.g., Puff and Pump in DN\***

\*T.W. Petrie, IAEA FEC 2006

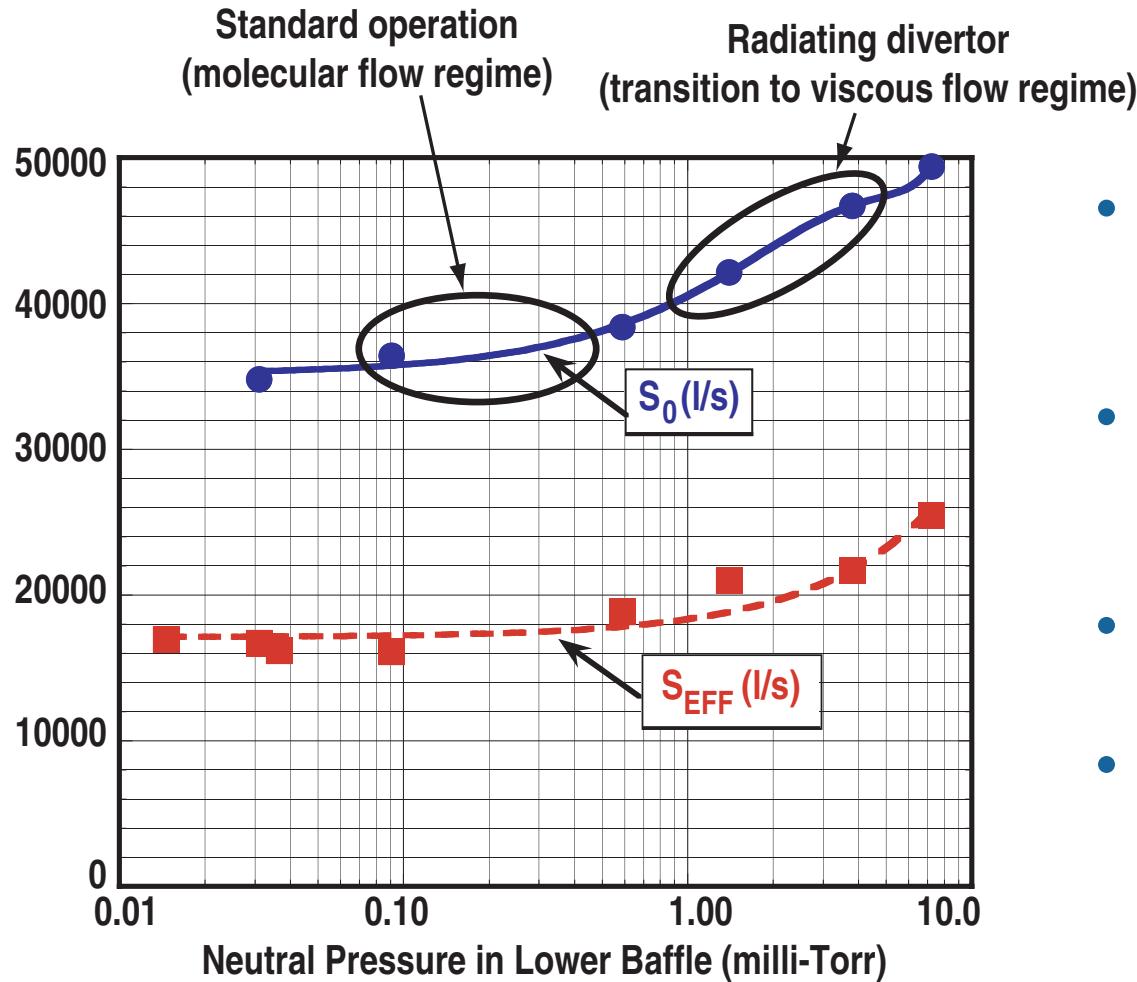
# New Lower Divertor Has Enabled Improved Density Control in High $\beta$ , Double Null Plasmas



2002 IAEA (106745)  
2004 IAEA (120096)  
2006 (126067)



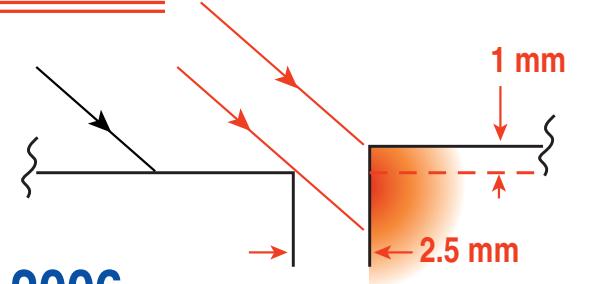
# DIII-D Plasma Operation Produces a Wide Range in Neutral Pressure Inside the Lower Divertor Baffle



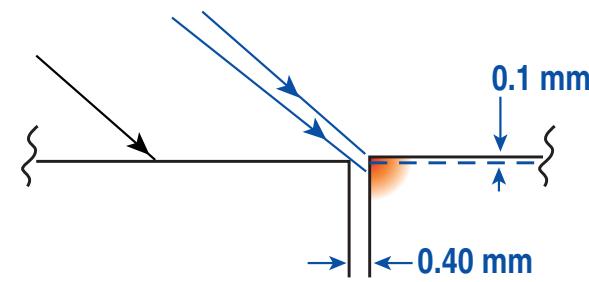
- $S_o \Rightarrow$  pumping speed of pump
- $S_{EFF} \Rightarrow$  effective pumping speed
- $S_{EFF} \approx 0.5 \times S_o$
- Conductance is matched to  $S_o$

# Divertor Tile Heating is Much More Uniform in the New Lower Divertor

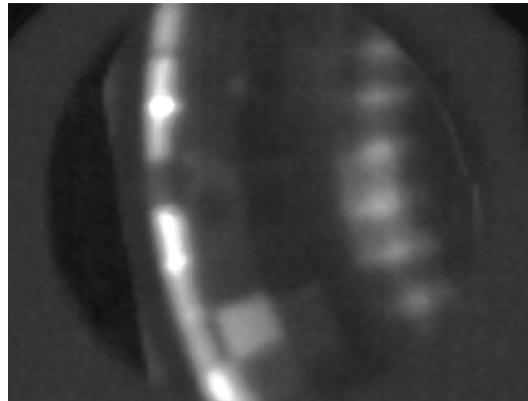
Pre-2006



2006

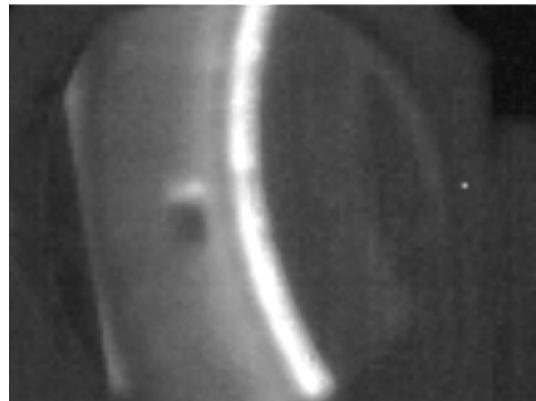


Infrared Light



2005

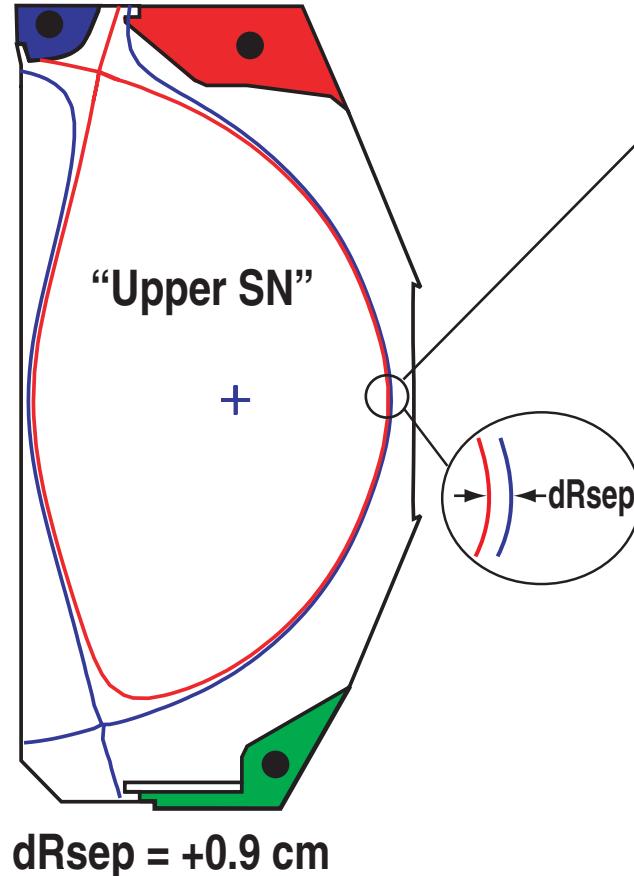
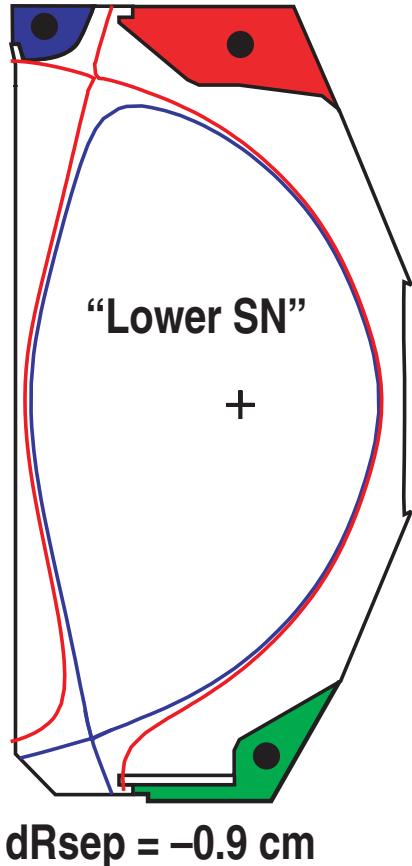
Outer Strike Point   Inner Strike Point



2006

- Reduced tile gaps to  $\approx 0.4$  mm
- Alignment of tiles to  $\lesssim 0.1$  mm height differential

# Definition of Magnetic Balance



$$dR_{sep} = R_{LOW} - R_{UP}$$

$R_{LOW}$  = major radius of the lower divertor separatrix flux surface at the outer midplane

$R_{UP}$  = major radius of the upper divertor separatrix flux surface at the outer midplane