

IDEAL AND NON IDEAL MHD STABILITY IN HIGH PERFORMANCE DIII-D DISCHARGES

A.D. Turnbull, D. Brennan, M.S. Chu, L.L. Lao, J.R. Ferron

A.M. Garofalo,[†] P.B. Snyder, J. Bialek,[†] I.N. Bogatu,^{††} J.D. Callen,^{*}

M.S. Chance,^{**} K. Comer,^{*} D.H. Edgell,^{††} S.A. Galkin,^{†††} D.A. Humphreys,

J.S. Kim,^{††} R.J. La Haye, T.C. Luce, M. Okabayashi,^{**} B.W. Rice,[◇] E.J. Strait,

T.S. Taylor, H.R. Wilson^{***}

[†]Columbia University, ^{††}FA RTECH, ^{*}University of Wisconsin, Madison

^{**}Princeton Plasma Physics Laboratory, ^{†††}University of California, San Diego,

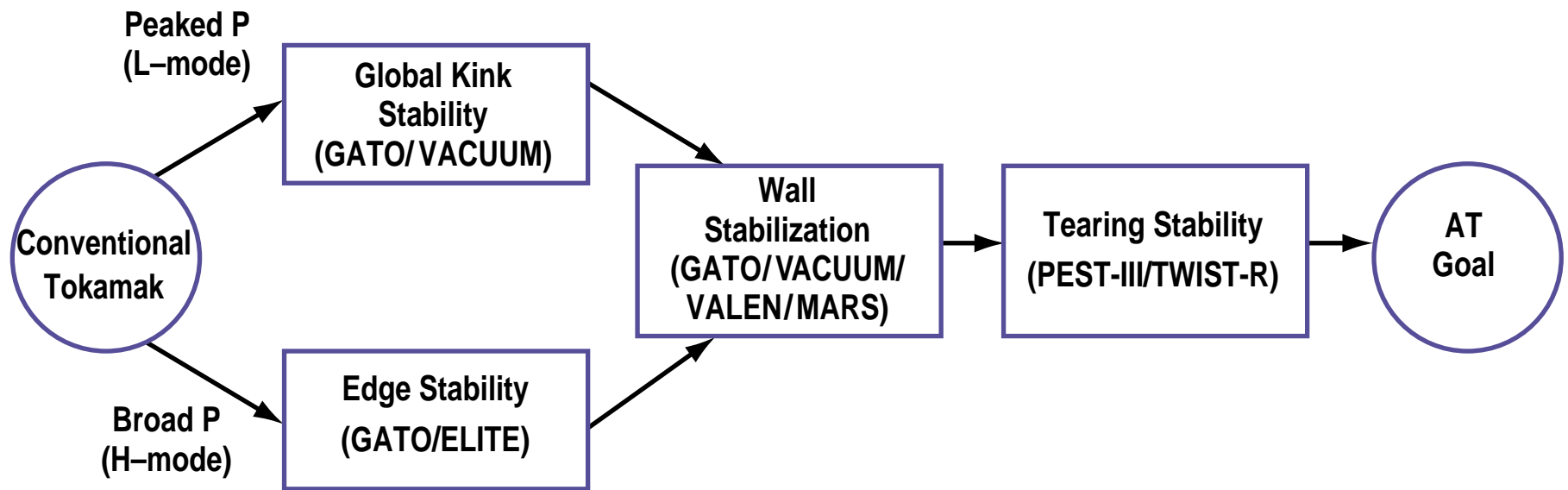
^{***}Culham Laboratory, United Kingdom, [◇]Xenogen

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HIGH PERFORMANCE OF TOKAMAK DISCHARGES IS LIMITED BY MHD INSTABILITY

- **Basic challenge: high confinement, and high β with steady-state**
⇒ Large pressure gradients and bootstrap currents ⇒ MHD instability
- **Route to high performance AT scenarios requires several stability issues to be resolved**
⇒ **Require accurate and realistic numerical tools**



- **In all cases accurate equilibrium reconstructions (using EFIT) are crucial**

PEAKED PRESSURE DISRUPTIONS DESCRIBED BY MODEL OF DISCHARGE DRIVEN THROUGH INSTABILITY BOUNDARY

- Discharges with highly peaked pressure invariably disrupt near $\beta_N \sim 2$ from $n = 1$ mode
- Time scale $\sim (200 \mu\text{s})$ slower than characteristic ideal time ($\tau \sim 10 \mu\text{s}$) but faster than resistive time ($\tau \gtrsim 10 \text{ms}$)
- Time scales can be explained by new model for instability driven through ideal limit

$$\xi \sim \exp((t/\tau)^{3/2})$$

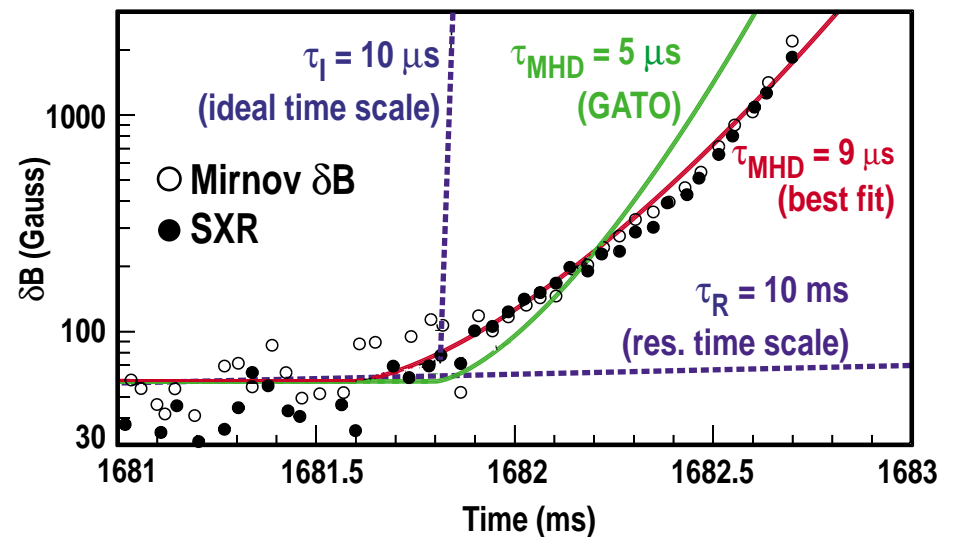
$$\tau = \left(\frac{3}{2}\right)^{2/3} \tau_D^{1/3} (\tau_{\text{MHD}})^{-2/3}$$

τ_D = Heating time scale

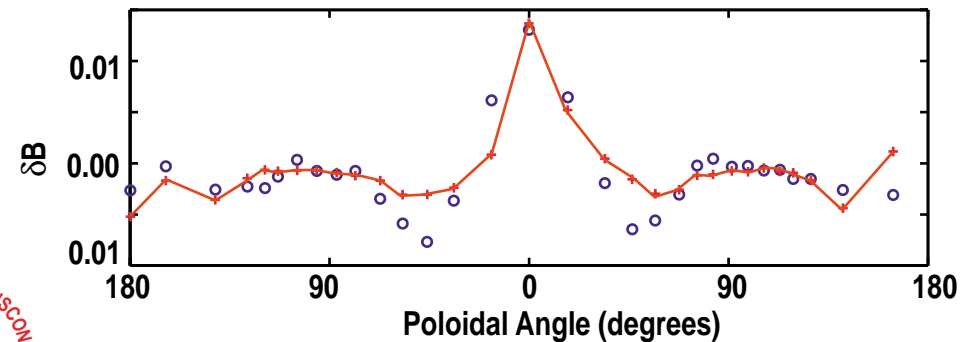
$$\tau_{\text{MHD}} \propto \frac{d}{d\beta} \gamma_{\text{MHD}}$$

[Callen et al Phys. Plasmas 6 2963 (1999)]

- Mode growth fits $\exp((t/\tau)^{3/2})$



- Measured and predicted poloidal Mirnov also agree

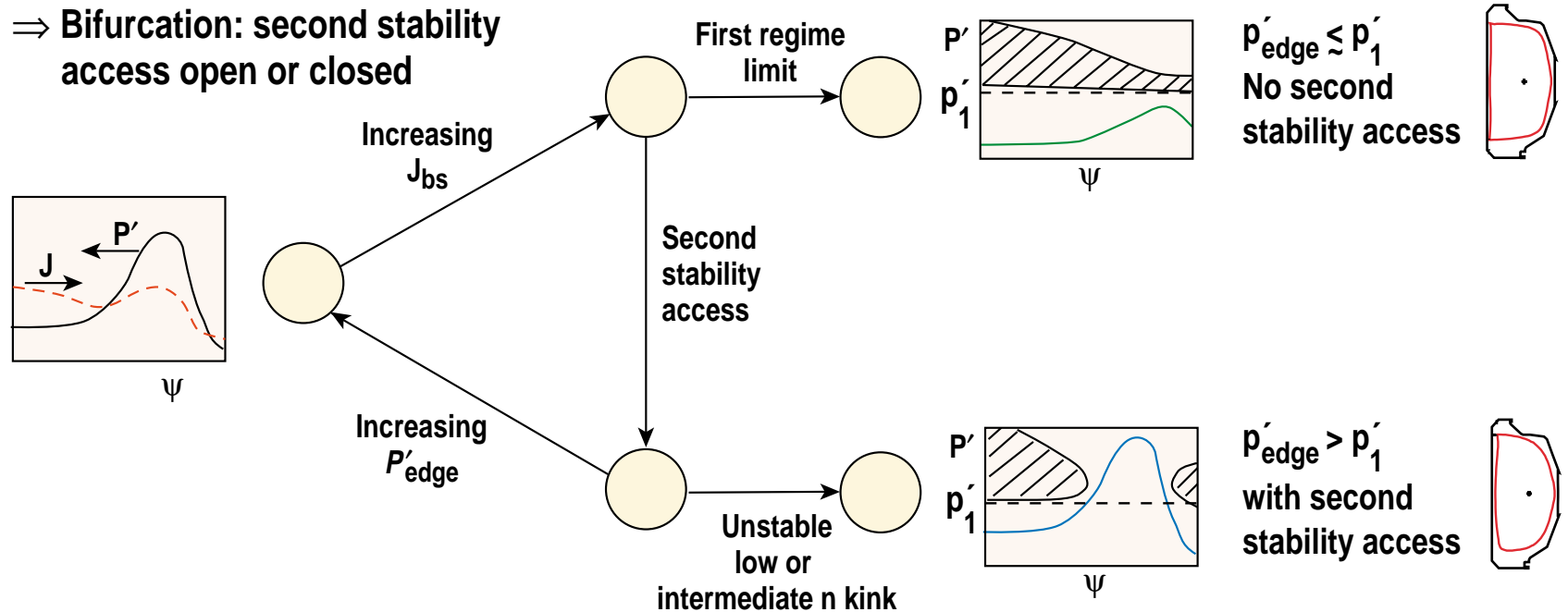


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NEW MODEL FOR EDGE INSTABILITY AS IDEAL EDGE INSTABILITIES DRIVEN BY EDGE PRESSURE GRADIENT AND BOOTSTRAP CURRENT

- ELMs in DIII-D range from small frequent benign through larger less frequent Type I ELMs to large X events that terminate high performance
- Key to new model: Increasing p'_{edge} drives increasing j_{BS} which facilitates second stability across

⇒ Bifurcation: second stability access open or closed



- Model predicts observed n as that which has lowest p'_{edge} limit with aligned J_{BS}
 - Verification requires quantitative stability calculations for full n range
- ELM size is determined by radial width of unstable mode

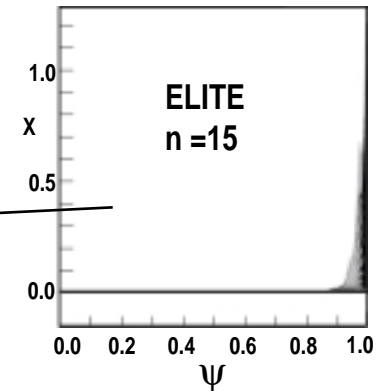
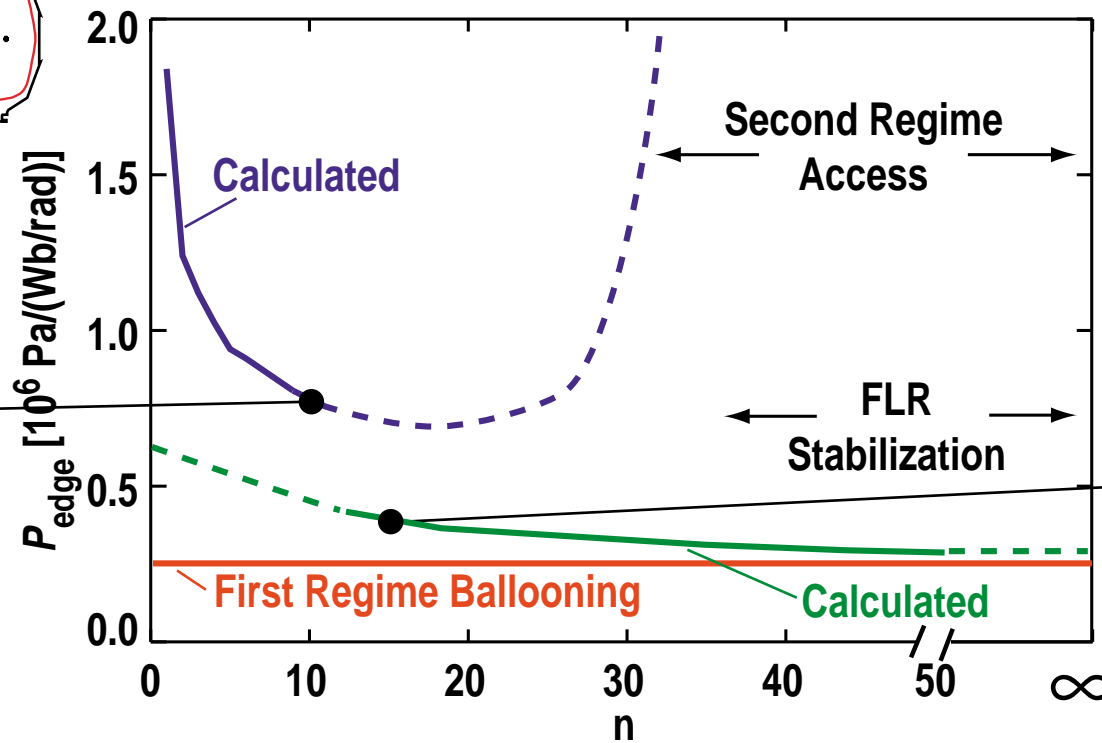
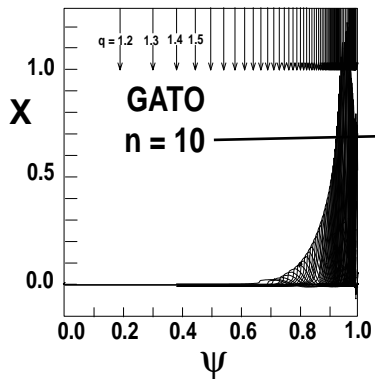
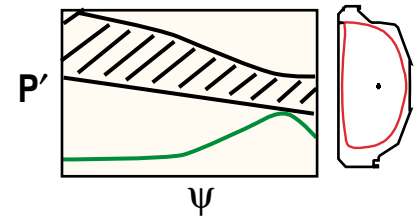
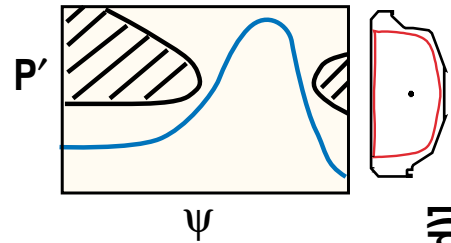
THEORY AND EXPERIMENTS SUPPORT A NEW MODEL FOR ELMS AS LOW TO INTERMEDIATE n IDEAL MODES

- Quantitative verification of model is obtained using stability calculations for full range of n

- Second regime access



- No second regime access



⇒ Large ELM

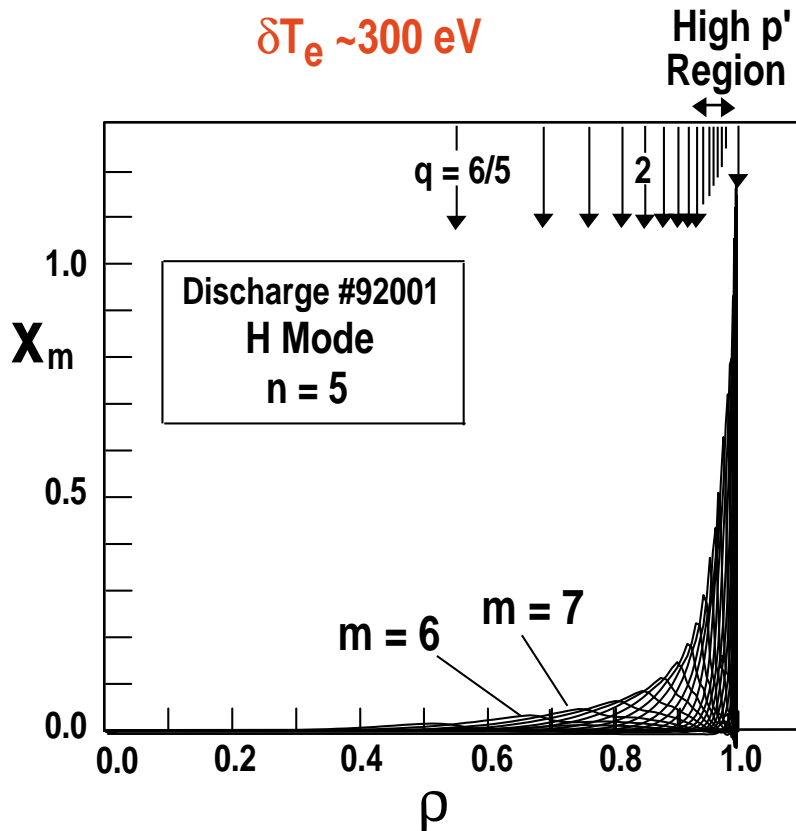
⇒ Small ELM

ELM SIZE CORRELATES WITH RADIAL WIDTH OF PREDICTED UNSTABLE INTERMEDIATE n KINK MODE

- Highly localized instability computed from GATO

⇒ Type I ELM has little effect

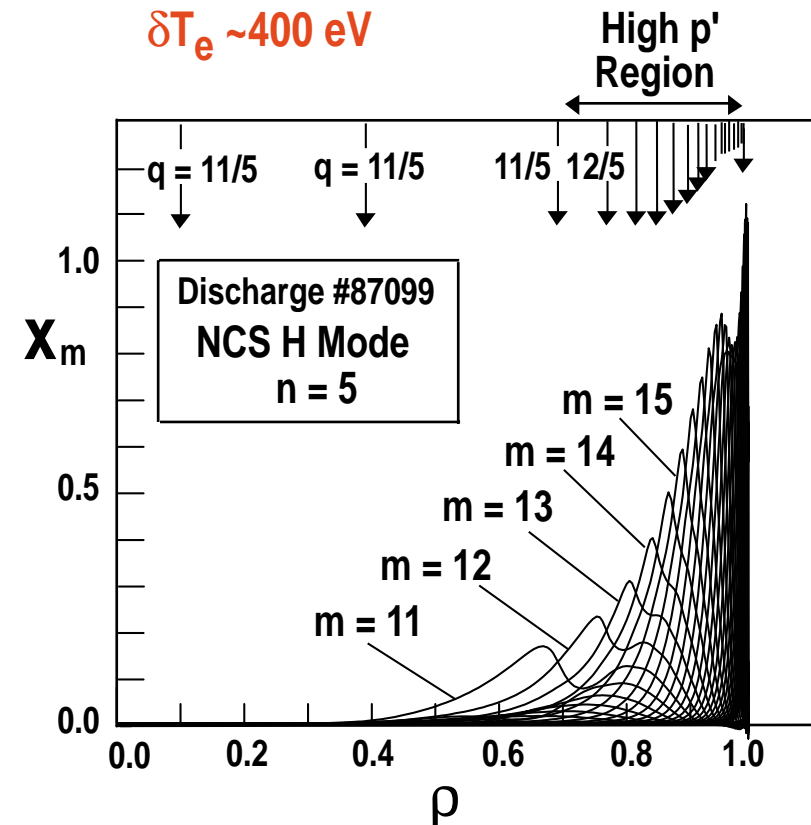
$\delta T_e \sim 300$ eV



- Predicted instability computed from GATO code penetrates into core

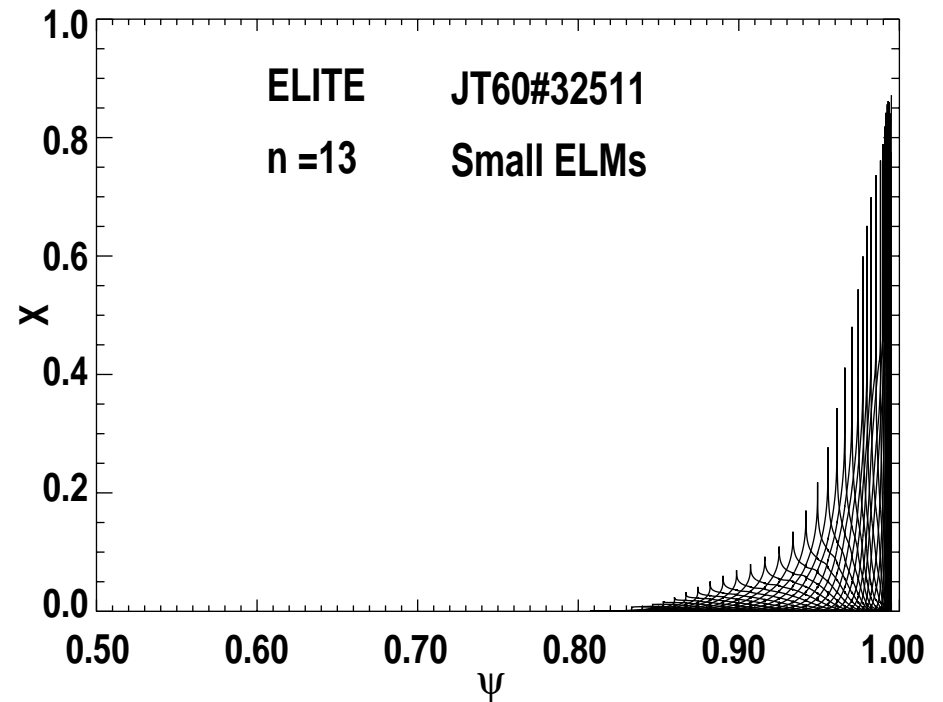
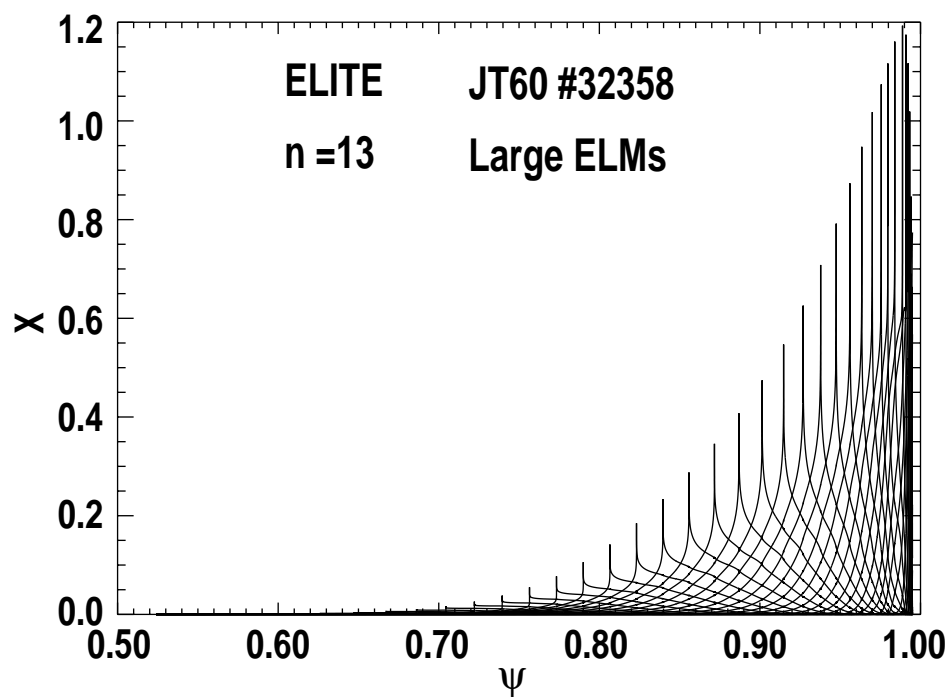
⇒ High performance is lost

$\delta T_e \sim 400$ eV



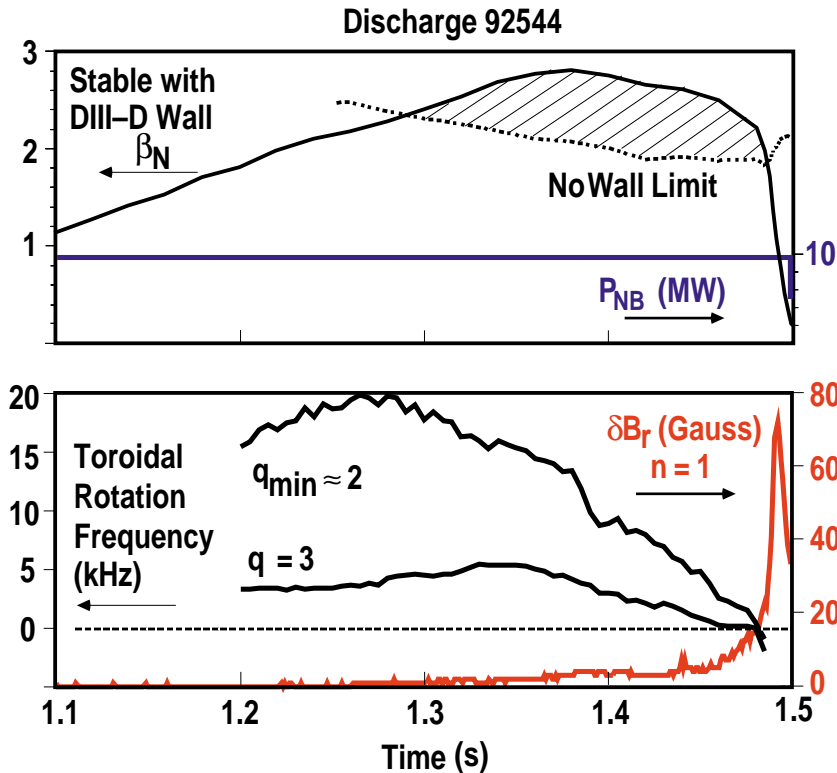
CALCULATIONS ALSO SHOW JT60 ELM BEHAVIOR FITS MODEL

- In JT-60 small “grassy” and Type I ELMs both have P'_{edge} at nominal first regime limit
- Calculated mode penetration (ELITE) is significantly larger in case with larger Type I ELMs

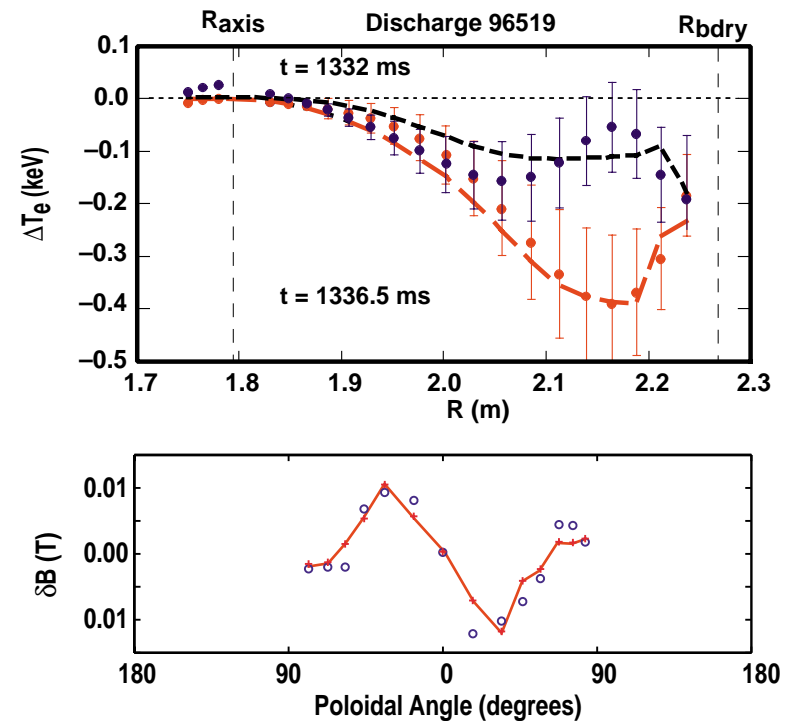


IDEAL STABILITY CALCULATIONS PROVIDE DEMONSTRATION OF RESISTIVE WALL MODE SUPPRESSION BY PLASMA ROTATION AND IDENTIFICATION OF RESISTIVE WALL MODE

- DIII-D discharges exceed predicted no-wall β limit by ~40% for ~70 wall times while plasma is rotating



- Predicted resistive wall mode radial and poloidal structure matches measured ECE and Mirnov fluctuations

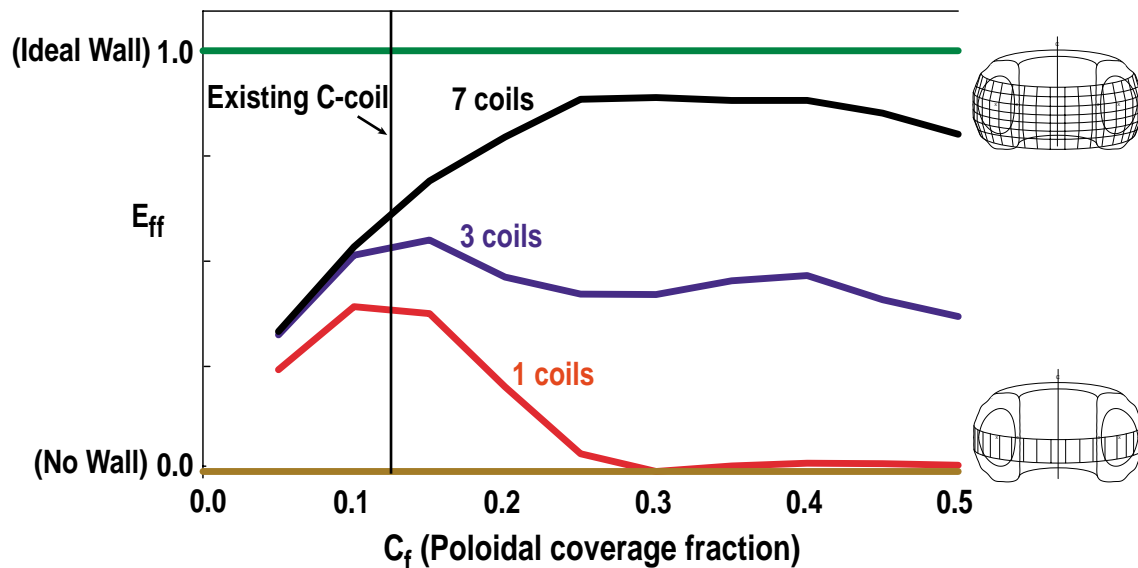


⇒ Ideal no wall eigenfunction from GATO is a good representation of the RWM

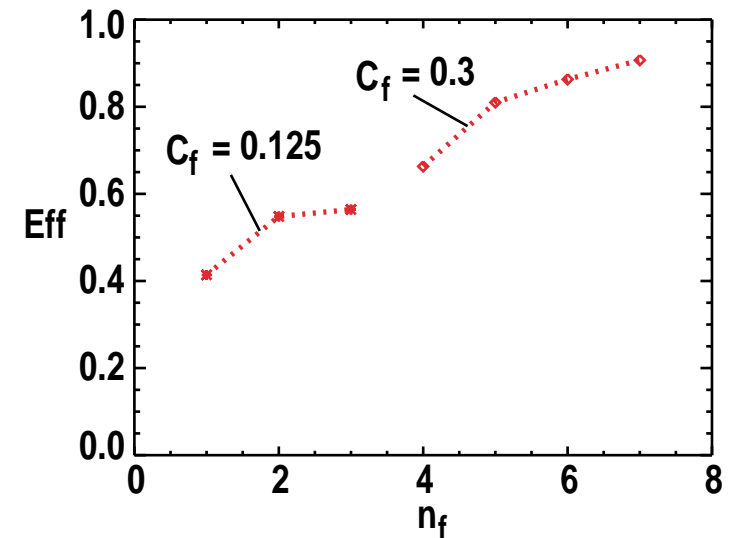
ACTIVE STABILIZATION MODELED USING GATO CODE COUPLED TO VACUUM CODE PREDICTS FEEDBACK EFFECTIVENESS

- Includes self consistent effect of feedback coils on instability
- Optimum effectiveness depends on poloidal coverage

$$E_{ff} = \frac{\partial W_F - \partial W_{\eta=\infty}}{\partial W_{\eta=0} - \partial W_{\eta=\infty}}$$



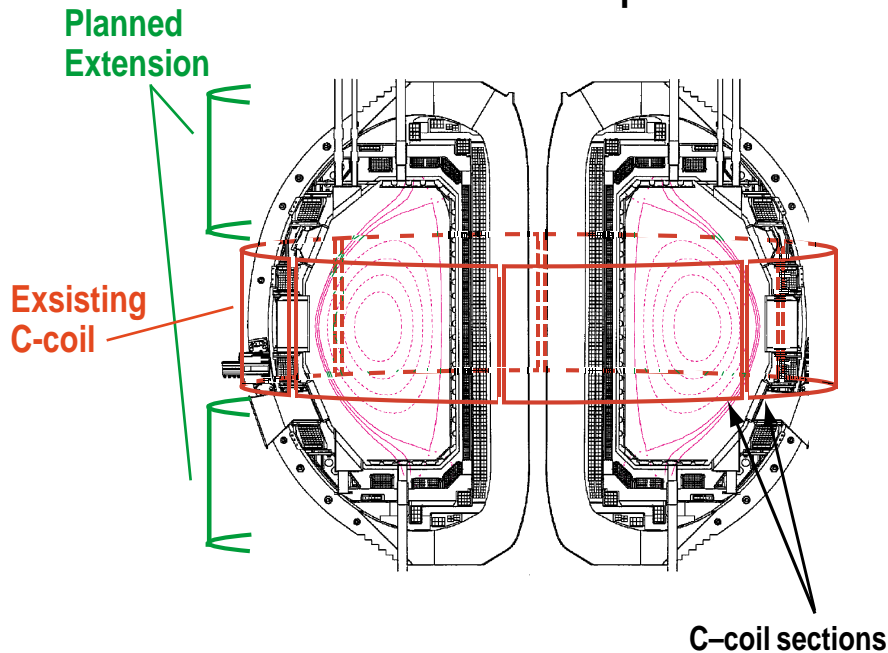
- Optimum effectiveness increases with number of individual coils



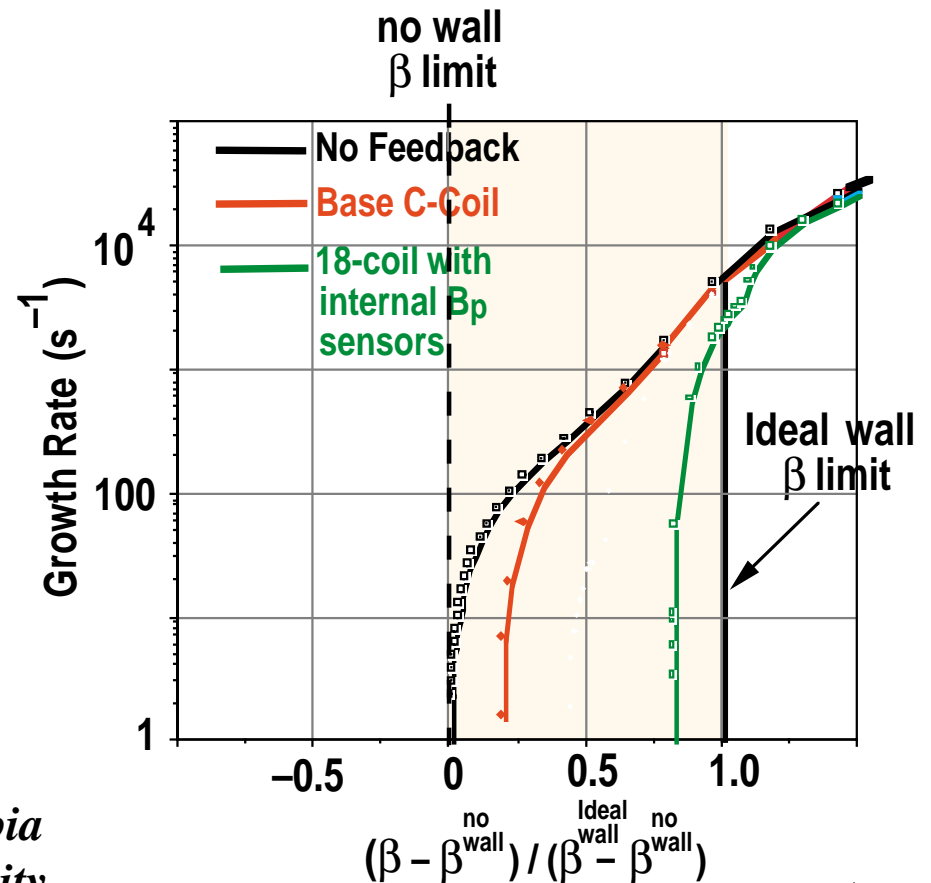
- Mode deformation found to be insignificant in present experimental situation

COUPLED GATO-VALEN CALCULATIONS PREDICT SIGNIFICANT GAIN IN DIII-D β LIMIT FOR EXTENDED C-COIL FEEDBACK SYSTEM

- DIII-D error field correction coils used in initial feedback experiments
 - 6 coil set at midplane

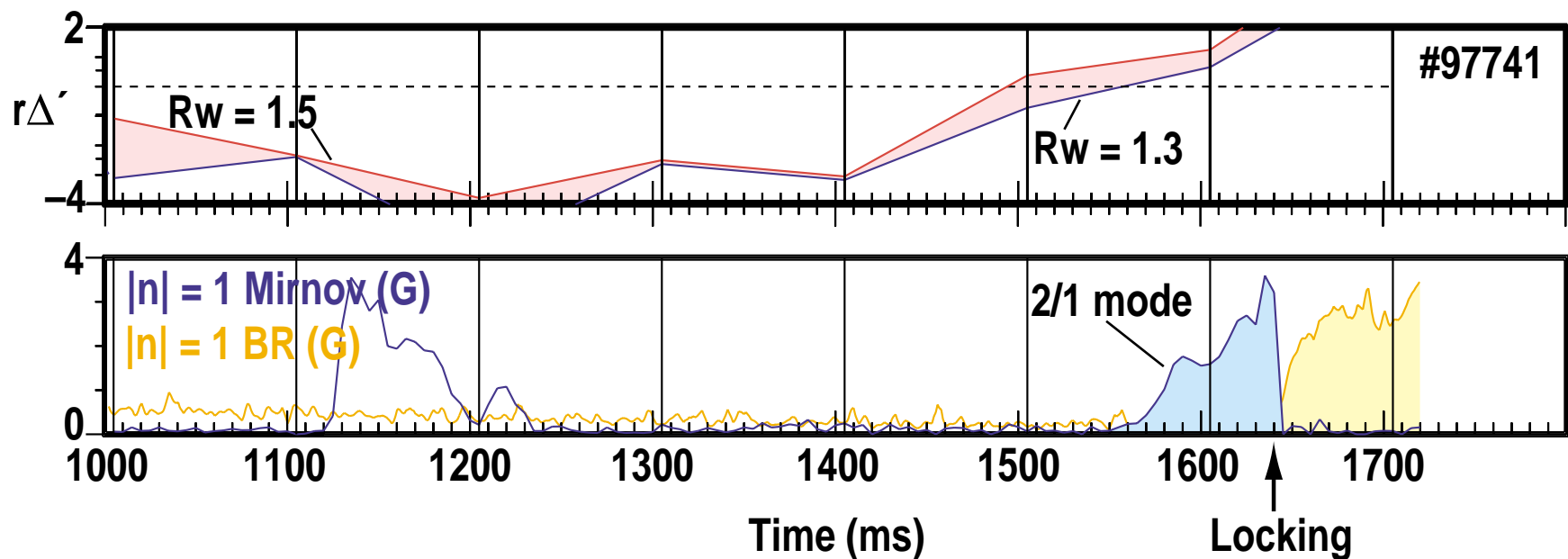


- Fixed ideal mode (GATO) input to VALEN used to optimize 3D coil and sensor loops
 - ⇒ Increasing present C coil set to 18 coils and using internal B_{pol} sensors can recover 80% of effectiveness of an ideal wall



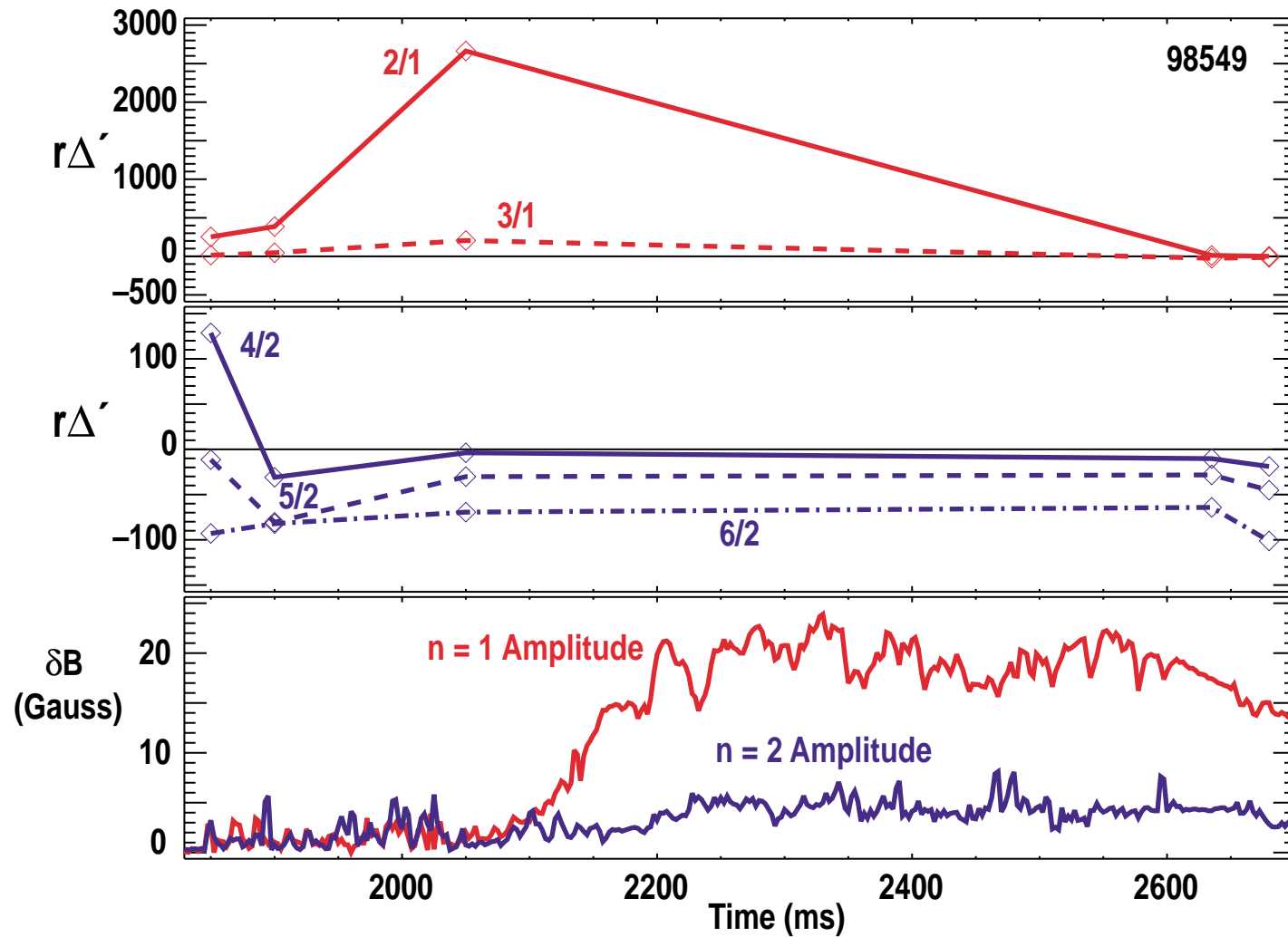
EQUILIBRIUM RECONSTRUCTIONS AND PEST-III CALCULATIONS PREDICT LINEARLY UNSTABLE TEARING MODE ONSET AT LOW β

- Calculations predict $\Delta' > 0$ at 1500–1550 ms for $m/n = 2/1$ mode
- Unstable $2/1$ mode observed at 1550 ms in agreement with predicted onset



- Correlation with observed stability obtained only with realistic 2D finite β stability calculation and using best fit equilibrium reconstruction

STABILITY OF HIGH PERFORMANCE LONG PULSE DISCHARGE IS CONSISTENT WITH PREDICTED LINEAR TEARING CALCULATION



SUMMARY

- MHD theory and calculations can make quantitative predictions of AT stability
 - Attention to details of profiles shape, walls etc. is crucial
 - Development of accurate and realistic computational tools is also essential
- Quantitative comparisons with observations are important for:
 - Identifying observed instabilities
 - Further progress

Peaked pressure global stability:	Correct time dependence and mode structure	➔	Avoidance by broadening pressure
Edge stability:	ELMs as intermediate n ideal modes	➔	Optimum edge pedestal and ELM control
Wall stabilization:	RWM identified and slowdown correlated with $\beta > \beta^{\text{no wall}}$	➔	Feedback stabilization
Tearing stability:	Linearly unstable and possible NTMs identified	➔	Tearing mode avoidance and Active stabilization with ECCD

STEADY STATE HIGH PERFORMANCE DISCHARGES CAN BE ACHIEVED USING UNDERSTANDING OF STABILITY LIMITS AND DISCHARGE CONTROL

- β controlled to remain ~20% below predicted RWM limit
- β also kept 5% below experimental 2/1 NTM β limit
- Discharge continued in steady state until beam termination

