

PROGRESS IN MFE SCIENCE – TOKAMAK RESEARCH

by
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American Physical Society
Division of Plasma Physics Meeting
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MFE-Tokamak

RESEARCH RESULTS FROM

Alcator C-mod	JET	TCV
ASDEX Upgrade	JFT-2M	TdeV
Compass-D	JT 60U	TEXTOR
DIII-D	MAST	TEXT
ET	NSTX	TFTR
FTU	PBX-M	TORE-SUPRA
HBT-EP	PLT	TRIAM-1M
HIT	START	T-10

SPECIAL THANKS FOR DIRECT CONTRIBUTIONS

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S. Bernabei	I. Hutchinson	T. Luce	S. Seitz	S. Wolfe
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E. Doyle	J. Kinsey	H. Ninomiya	E. Synakowski	
E. Frederickson	A. Kitsunezaki	W. Park	T. Taylor	
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C. Greenfield	L. Lao	R. Pinsker	R. Waltz	
M. Greenwald	G.S Lee	P. Politzer	M. Watkins	
R. Hawryluk	F. Leuterer	M. Porkolab	R. Weynants	
J. Hosea	B. Lipschultz	R. Prater		

MAIN POINTS

- We have learned a tremendous amount about magnetically confined plasmas
 - Measurements and theory
 - Calculations
- Exciting new directions are opening
 - Advanced Tokamak research
- We are technically ready for next steps

OUTLINE

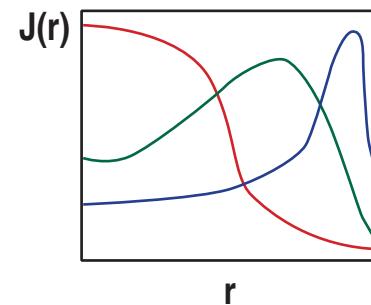
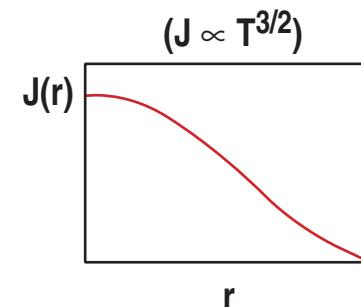
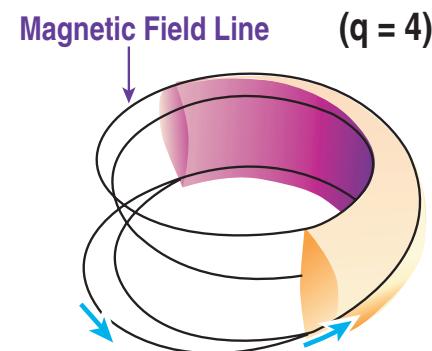
- The tokamak equilibrium
- Heating and current drive
- Stability
- Confinement
- Power and particle control
- Burning plasma physics
- Next steps
- Conclusions

WHAT IS A TOKAMAK?

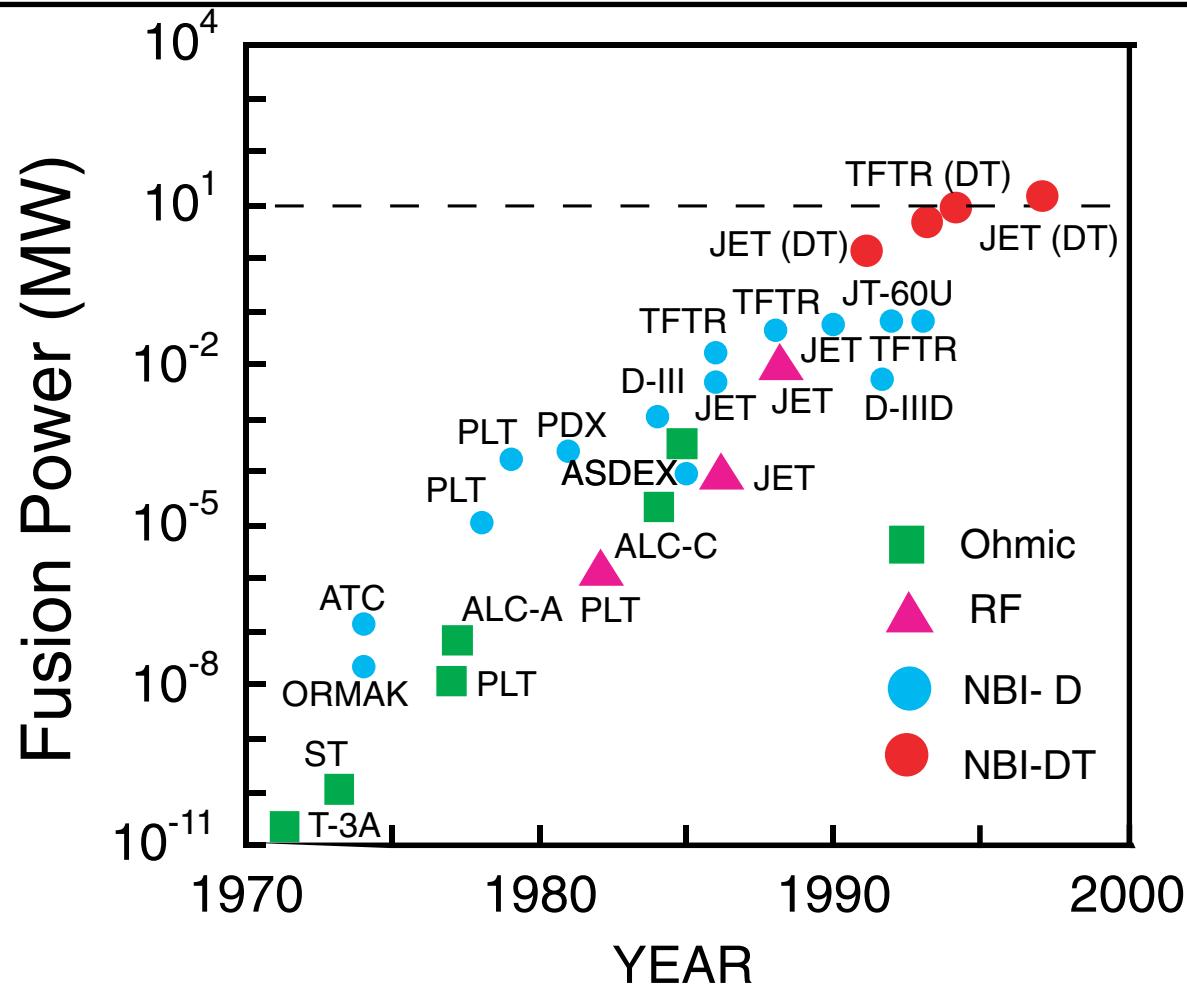
- An axisymmetric toroidal confinement configuration with a strong toroidal plasma current and an applied toroidal magnetic field strong enough to make the edge winding factor > 2
- Not part of the basic definition but certainly part of the opportunity for variation and innovation within the concept are:

- Shape (elongation, triangularity)
- Aspect ratio
- Divertor or limiter boundary
- Toroidal field strength
- Current profile
- Pressure profile
- Rotation profile
- Radial electric field profile
- Wall stabilization

} Advanced Tokamak



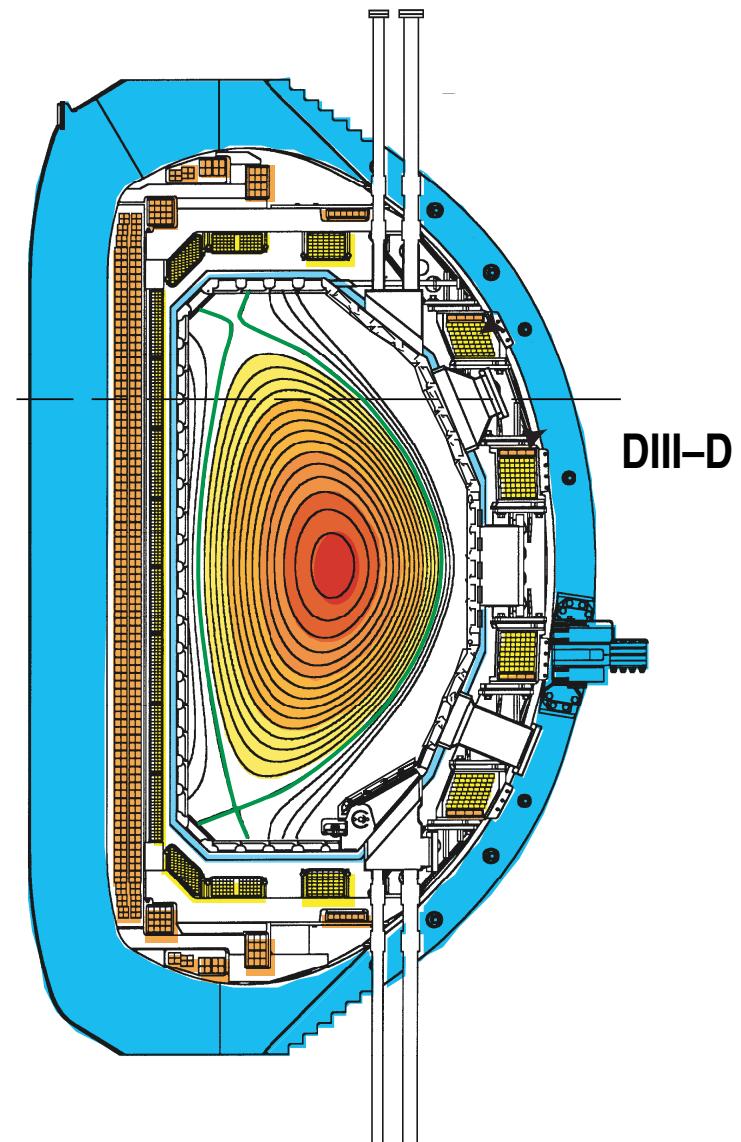
TOKAMAKS HAVE MADE EXCELLENT PROGRESS IN FUSION POWER



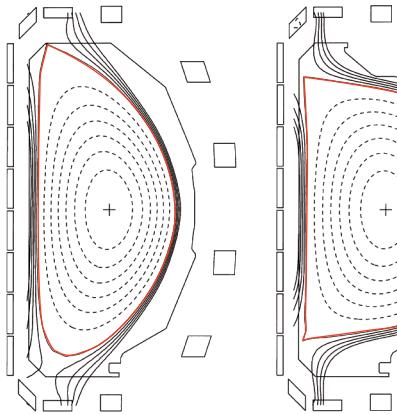
PLASMA EQUILIBRIUM THEORY IS WELL UNDERSTOOD AND EXTENSIVELY USED

- Ampere's Law and the force balance equation $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$ and $\vec{\nabla}P = \vec{J} \times \vec{B}$ lead to the Grad-Shafranov equation for the poloidal flux function.

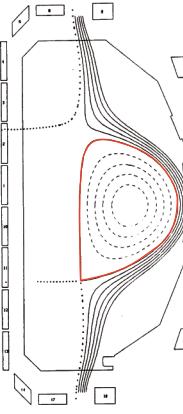
Equilibrium codes solve this equation for the closed flux contours that give the tokamak its good confinement.
- Such codes are used extensively in
 - Experiment design, control of complex shapes is precise
 - On-line data analysis $W(t)$, $\beta(t)$, $\tau_E(t)$
 - Providing the geometry for transport analysis



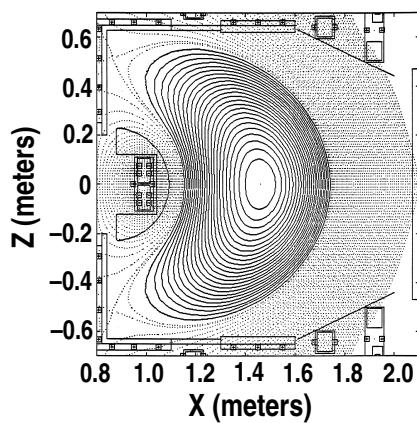
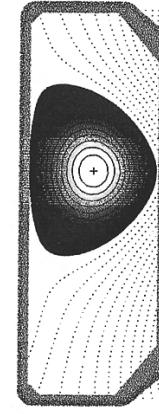
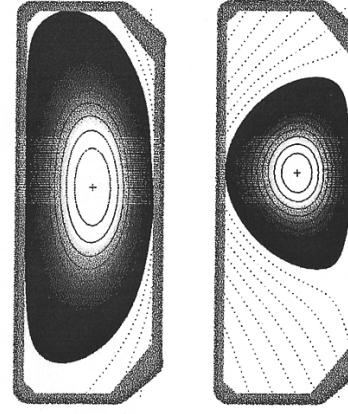
PLASMA EQUILIBRIUM SHAPE CONTROL IS A HIGHLY DEVELOPED SCIENCE



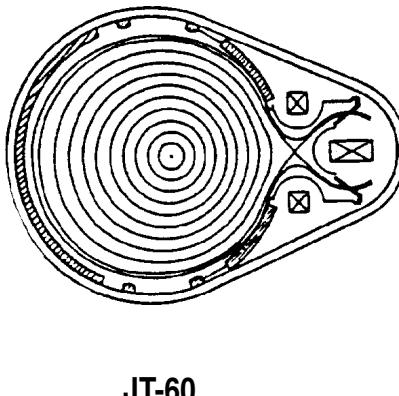
DIII-D



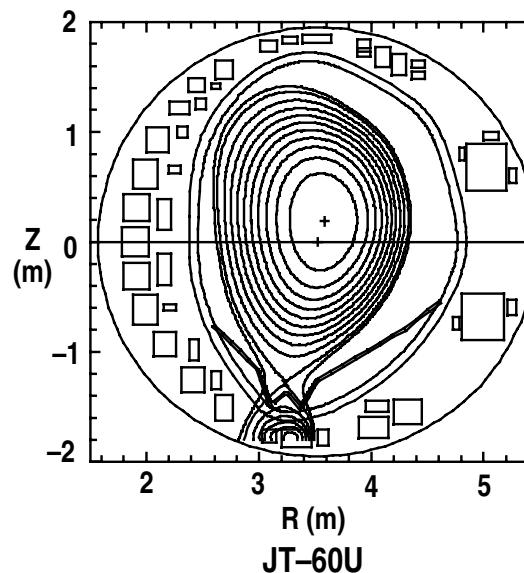
TCV



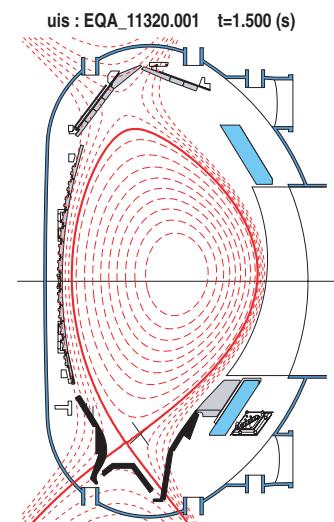
PBX-M



JT-60



JT-60U



ASDEX UPGRADE

MFE—Tokamak

SUCCESSFUL METHODS OF HEATING AND CURRENT DRIVE FOR STEADY-STATE HAVE BEEN DEVELOPED

70's

80's

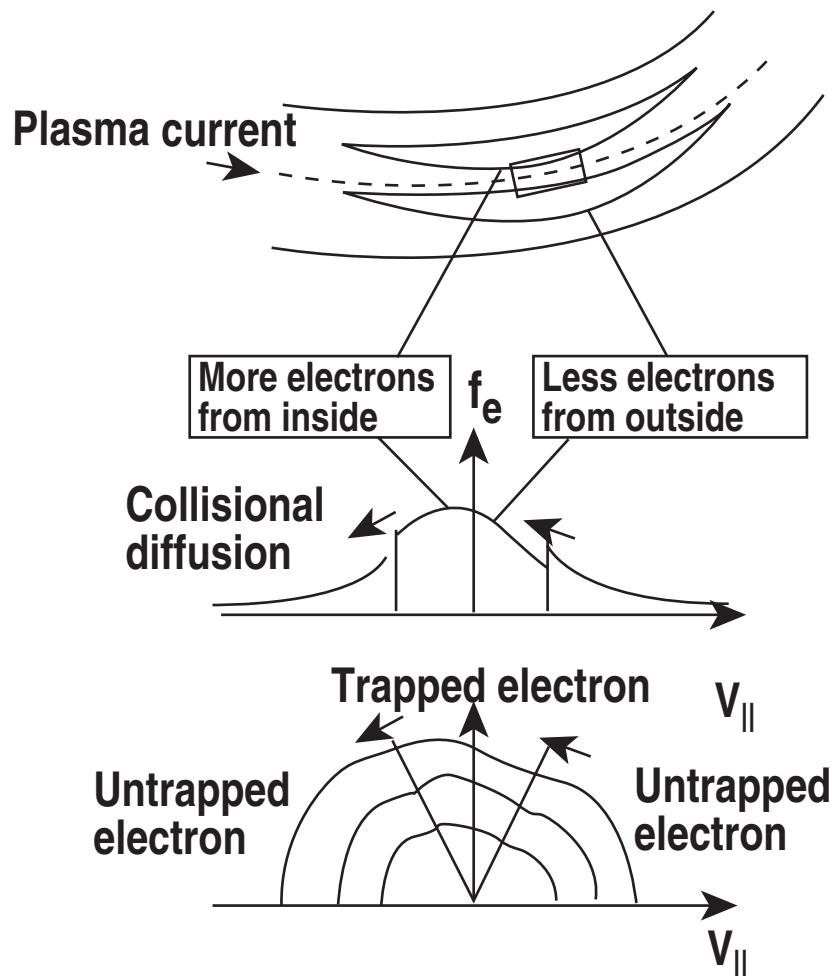
90's

Explored heating methods
Wave coupling
Fast ion orbits
NBI deposition

Multi-MW heating
Current drive
Heating to H-mode
Global rotation
Measured bootstrap current
Ray tracing codes
Fokker-Planck codes

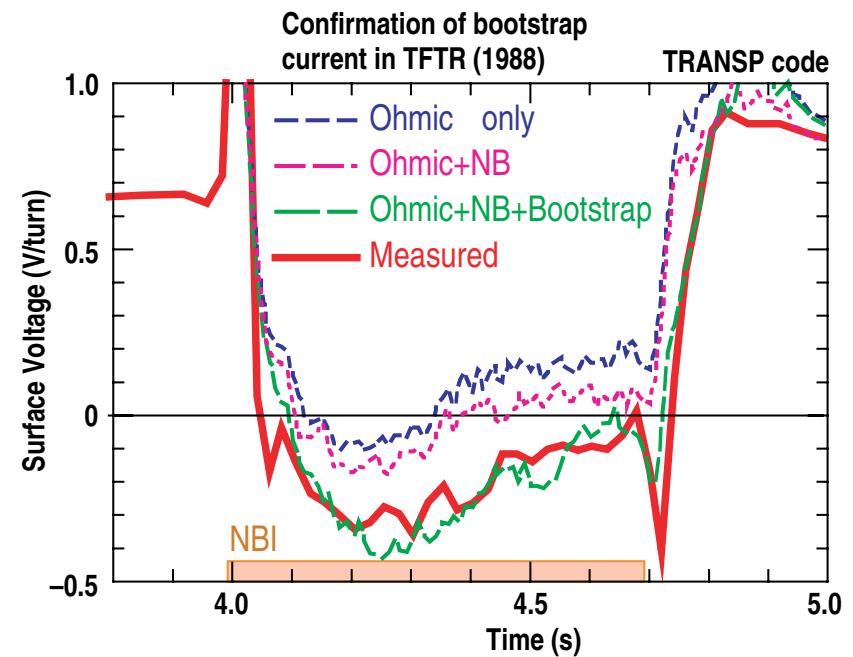
Control of current profile
Control of MHD activity
High bootstrap fraction
Full wave codes

THE PLASMA'S SELF-GENERATED BOOTSTRAP CURRENT IS THE BASIS FOR MODERN APPROACHES TO STEADY-STATE OPERATION



(Kikuchi, PPCF 37 (1995))

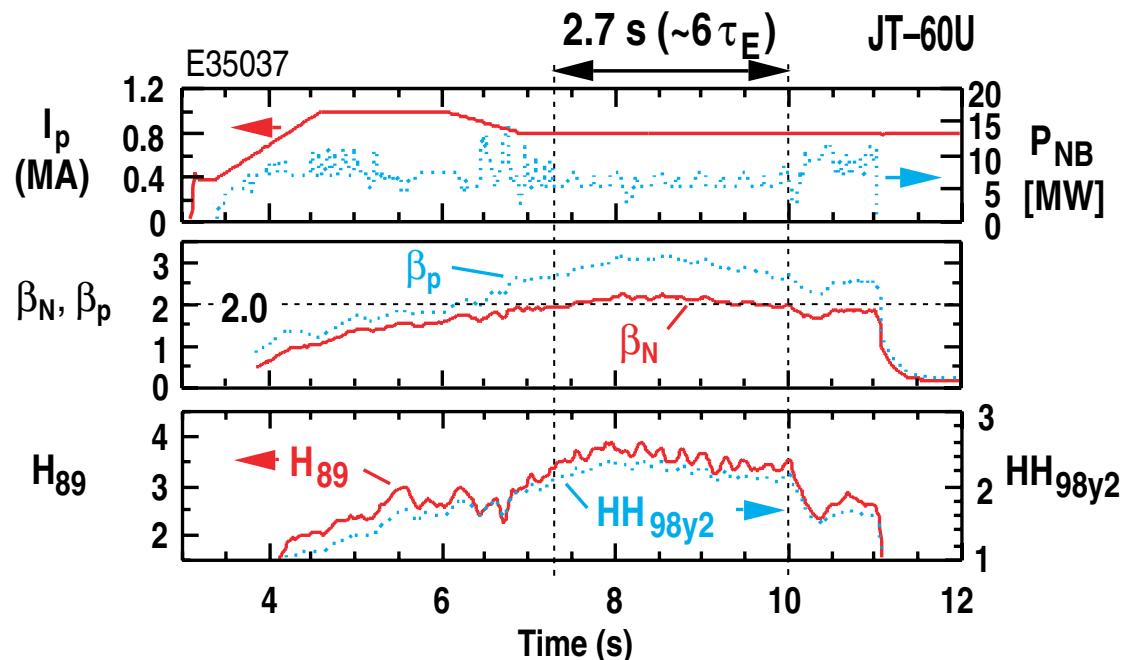
- An element of neoclassical transport theory
- $J_{bs} \propto$ local pressure gradient



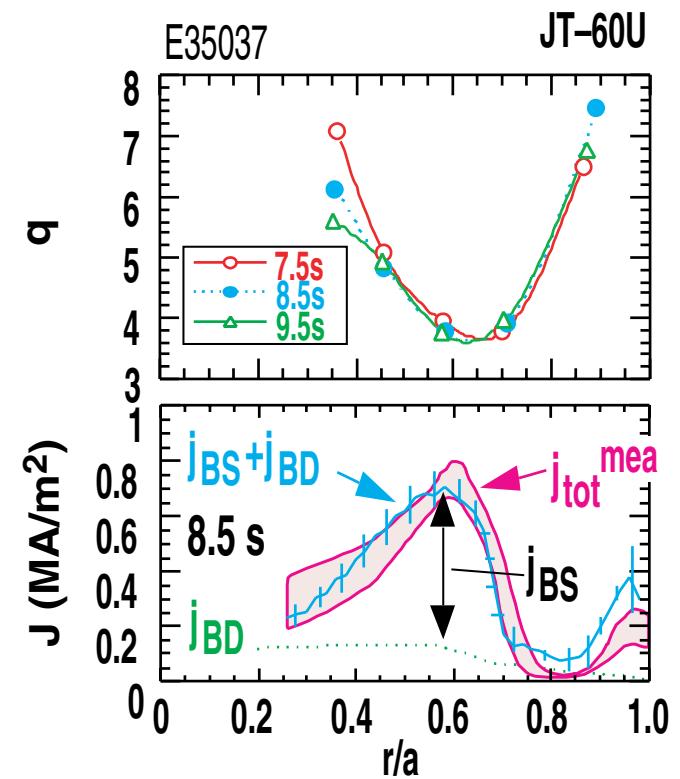
MFE—Tokamak

A HIGH PERFORMANCE PLASMA WITH FULL NON-INDUCTIVE CURRENT DRIVE AND 80% BOOTSTRAP FRACTION IN JT-60U

- $H_{89} \sim 3.5$, $HH_{98y2} \sim 2.2$, $\beta_N \sim 2$, $\beta_p \sim 2.9$, $f_{BS} \sim 80\%$ for $6\tau_E$ with full non-inductive CD
- Current profile was largely determined by the bootstrap current, and was nearly stationary



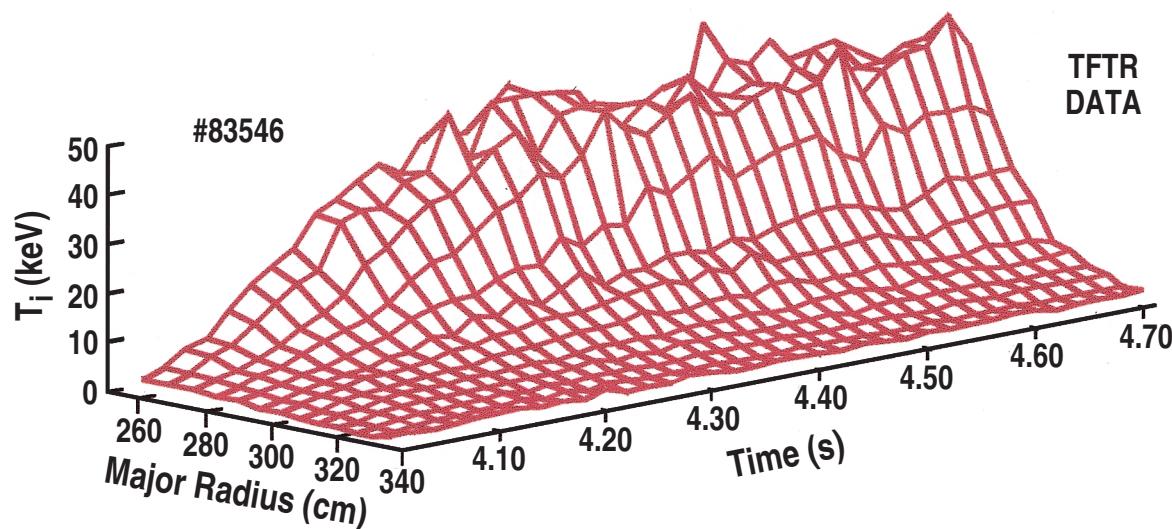
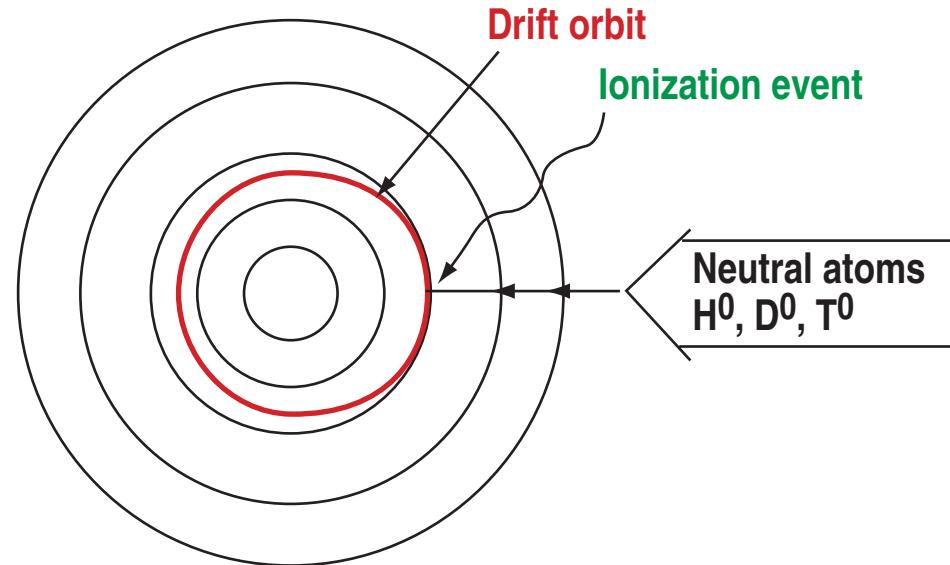
JT 60 also 80% bootstrap fraction



NEUTRAL BEAM HEATING AND CURRENT DRIVE

- Workhorse for high temperature and β studies
- Can drive current

Ion Sources E_b
Positive ions ≤ 150 keV
Negative ions ≤ 1 MeV

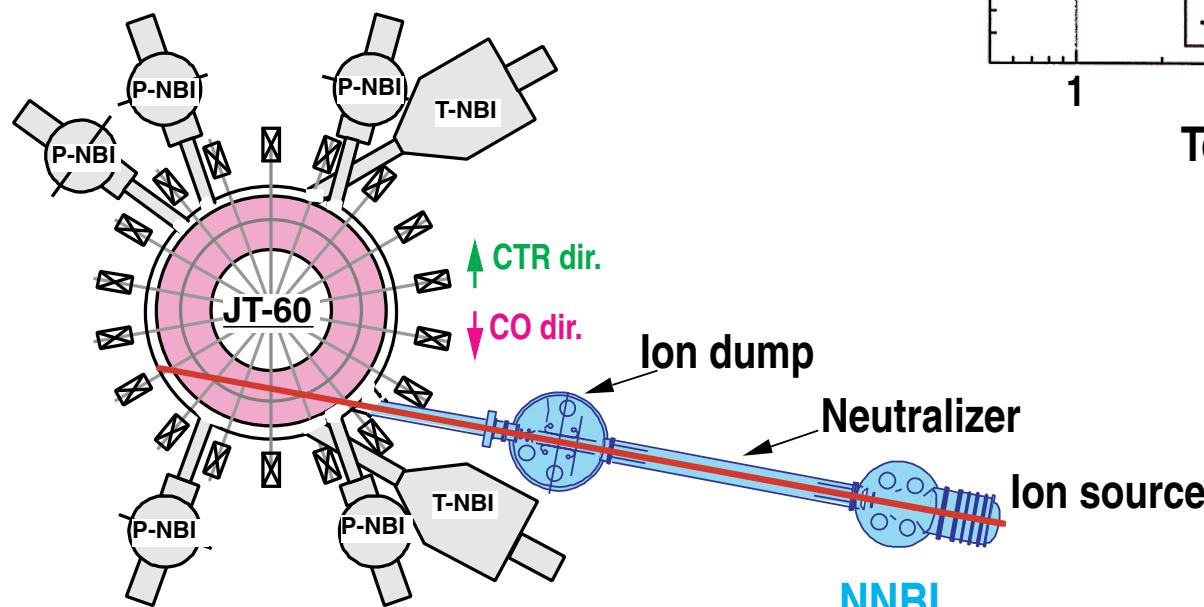


NEUTRAL BEAM CURRENT DRIVE IN ACCORD WITH THEORY

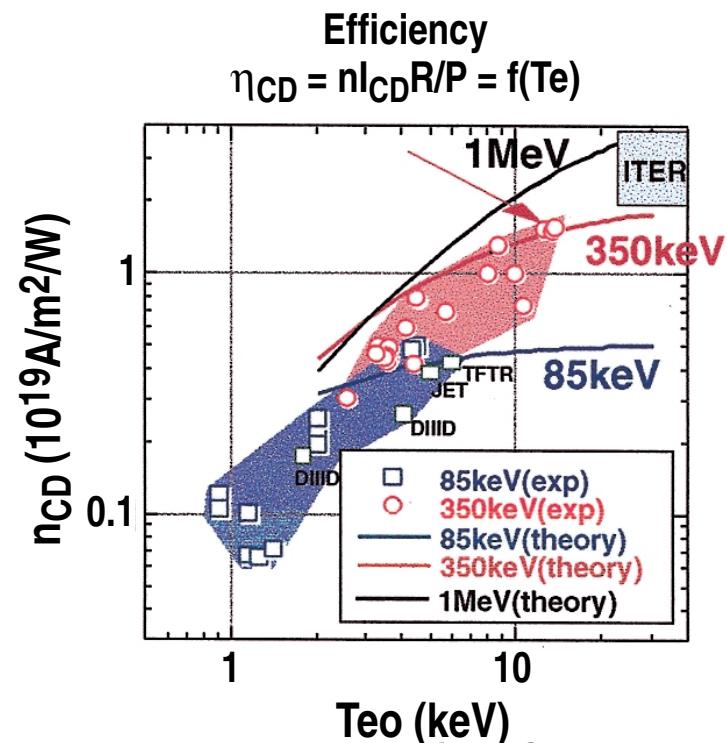
Full current drive case in JT-60U (1.3 s)

$$\begin{array}{ll} I_p = 1.5 \text{ MA} & B_T = 3.7 \text{ T} \\ \text{HH} = 1.3-1.4 & \beta_N = 2.4-2.5 \end{array}$$

	I_{CD}	E	P
NNBCD	0.6 MA	360 keV,	4 MW
PNBCD	0.3 MA	85 keV	10-18 MW
BOOTSTRAP	0.8 MA		
ECH	—	—	1.6 MW
			1.7 MA



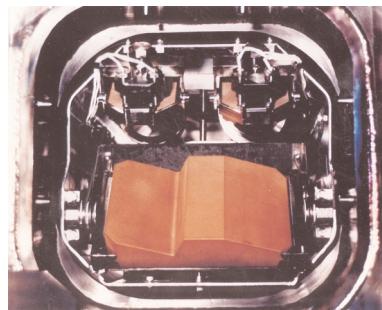
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MFE—Tokamak

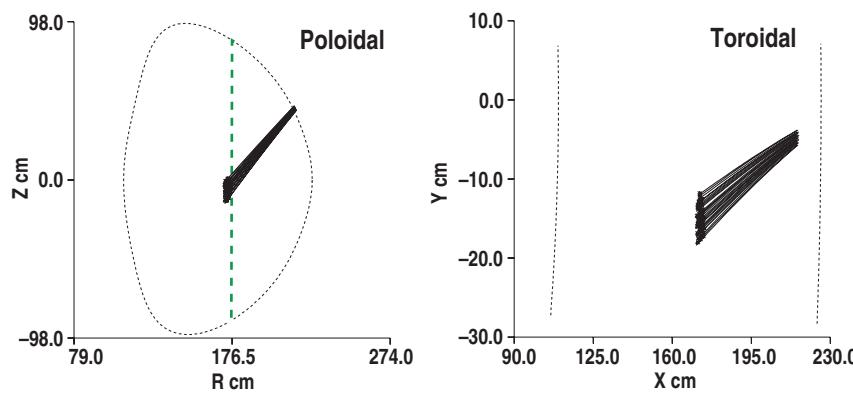
ELECTRON CYCLOTRON HEATING AND CURRENT DRIVE ($\omega = n\omega_{ce}$)

- Waves propagate in vacuum, so antenna can be far from the plasma

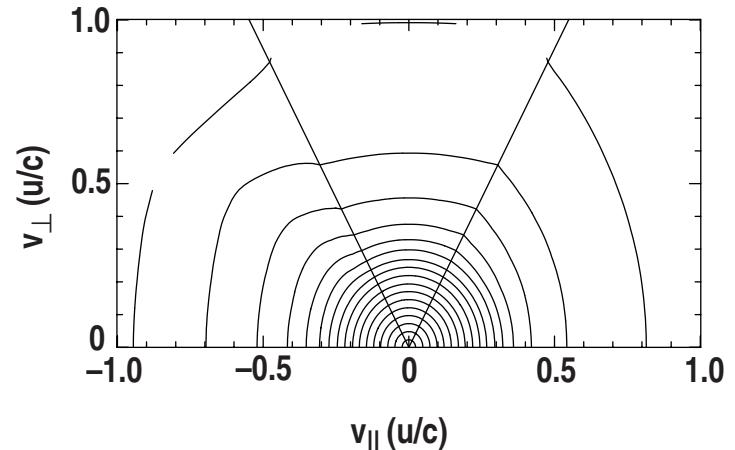


DIII-D

- Inside the plasma the waves propagate up to a critical density (related to the plasma frequency) and are absorbed near the cyclotron resonance or its harmonics

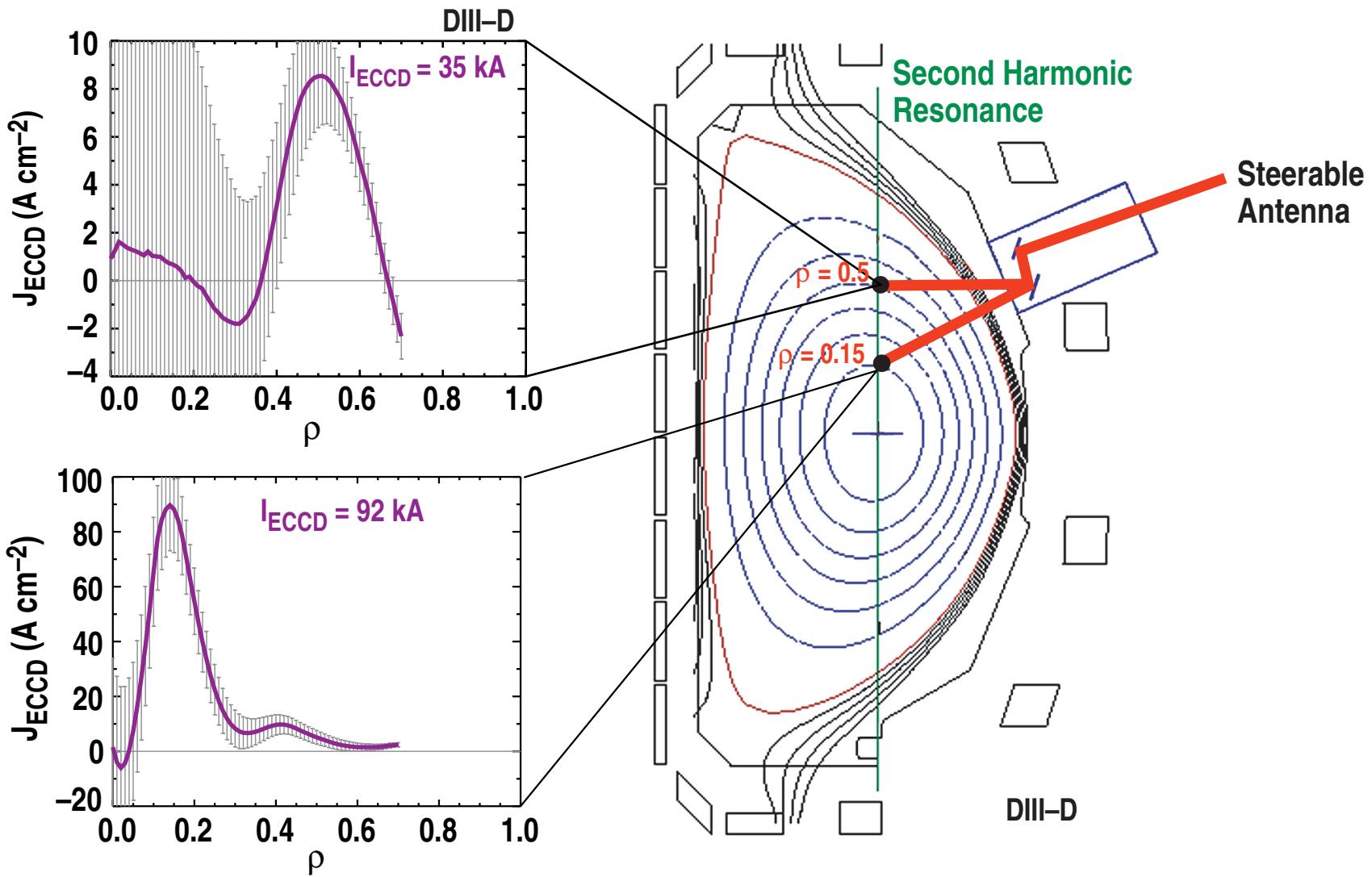


- Damping of EC waves causes diffusion in V_{\perp} direction. Collisional relaxation on ions generates current through generation of an asymmetric $V_{||}$ distribution



- Calculational tools include ray tracing codes (TORAY, GENRAY, BANDIT-3D) and Fokker-Planck codes (CQL3D, BANDIT-3D, Giruzzi, RELAX, Krivenski, Fukuyama)

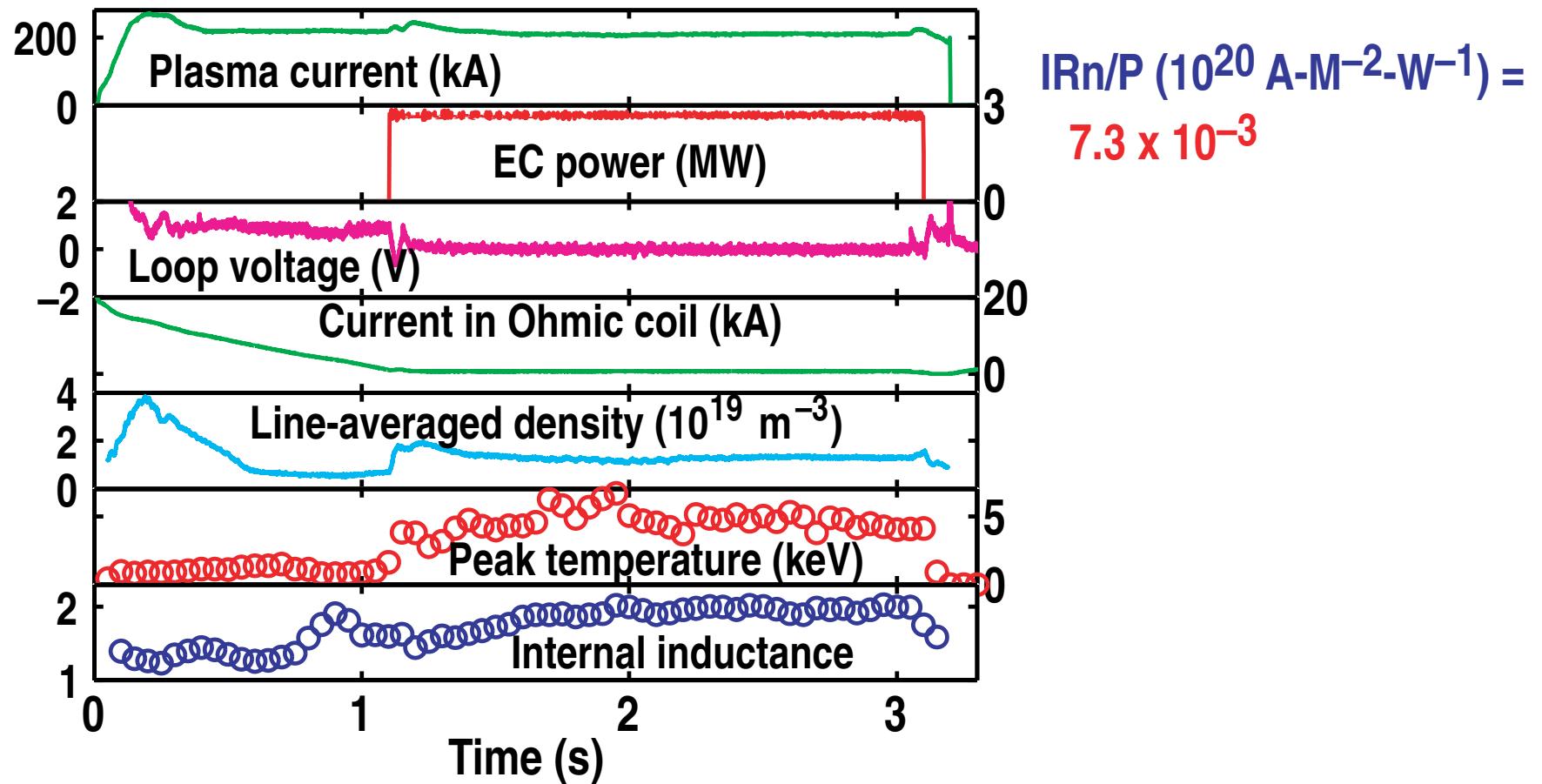
MICROWAVE ELECTRON CYCLOTRON HEATING PROVIDES LOCALIZED CURRENT DRIVE



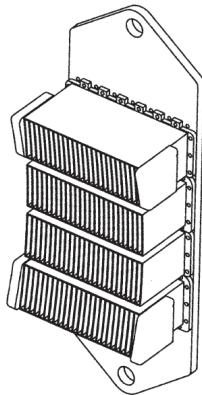


Fully non-inductive discharges

210 kA sustained in steady state by 2.7 MW co-ECCD



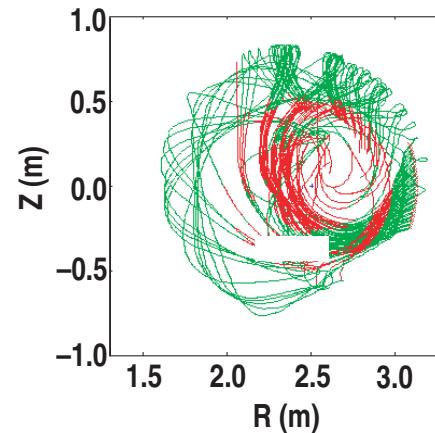
LOWER HYBRID HEATING AND CURRENT DRIVE ($\omega_{ci} < \omega < \omega_{ce}$)



Lower Hybrid **coupling**

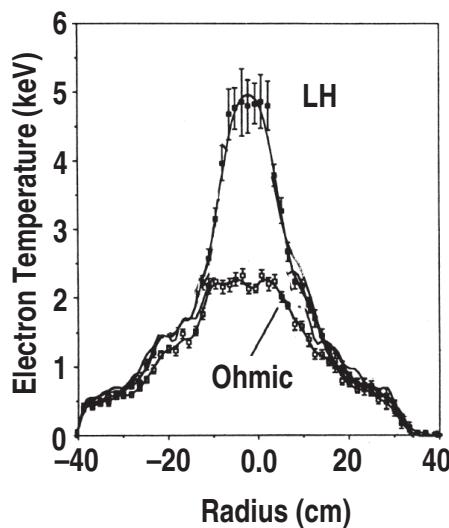
requires $n_{||} > 1$
(Brambilla, SWAN)

Phased array
or waveguides

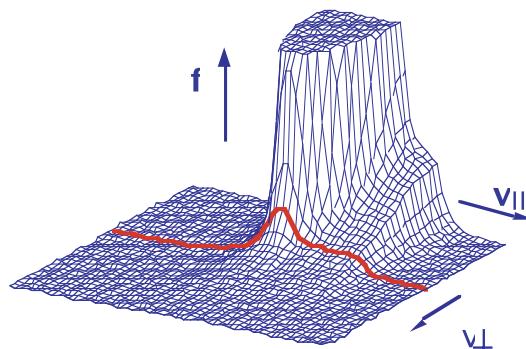


Ray tracing: the accessible waves cross the plasma and can undergo several reflections at the edge before being absorbed.

Codes by: *Cardinali, Bonoli, Ignat, Valeo, Harvey, Takase*
(Figures from Giruzzi)



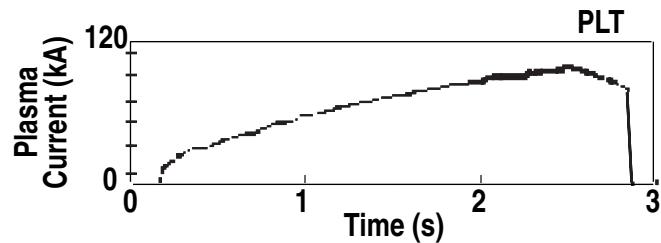
Electrons
heated by
LH (PLT)



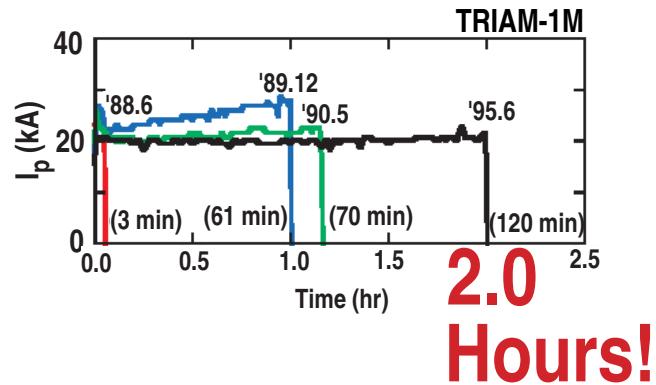
Damping of LH waves forms a parallel energetic electron tail in the distribution function via **Electron Landau Damping**. This asymmetry constitutes the non-inductive current (Fisch, Karney)

LHCD SUCCESSFUL IN MANY APPLICATIONS

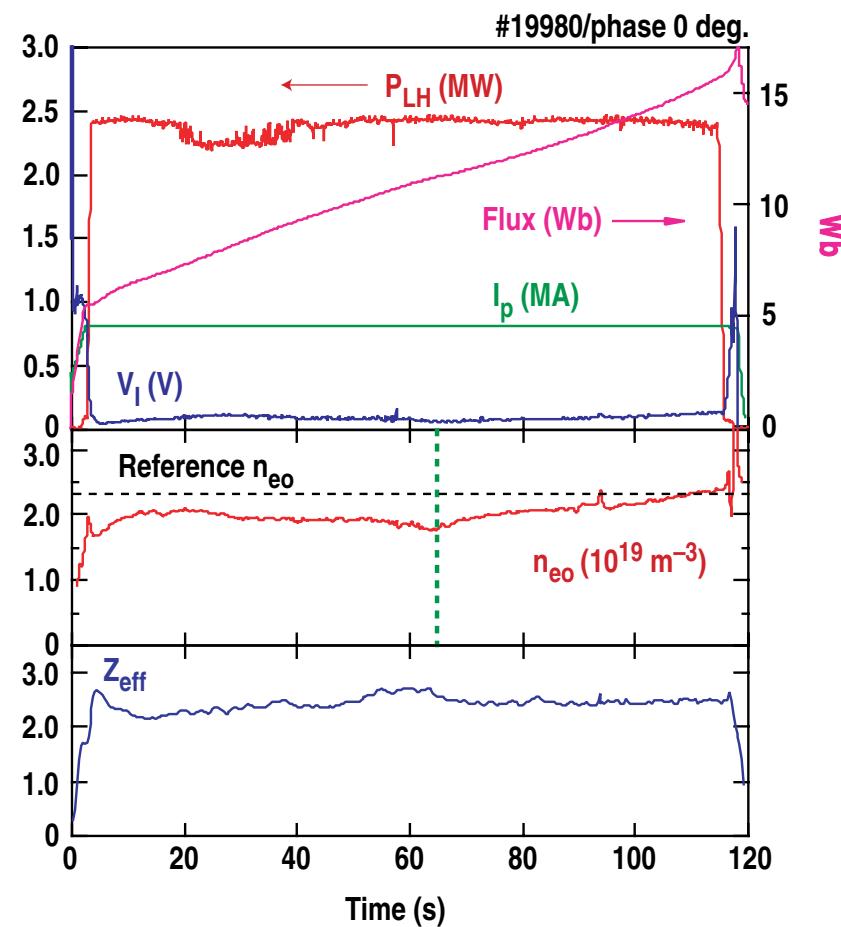
- Plasma current initiated and ramped up by LHCD



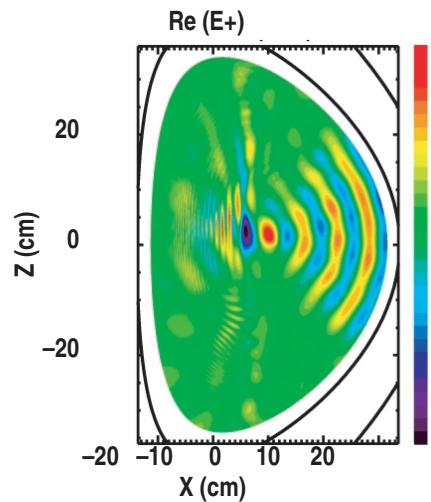
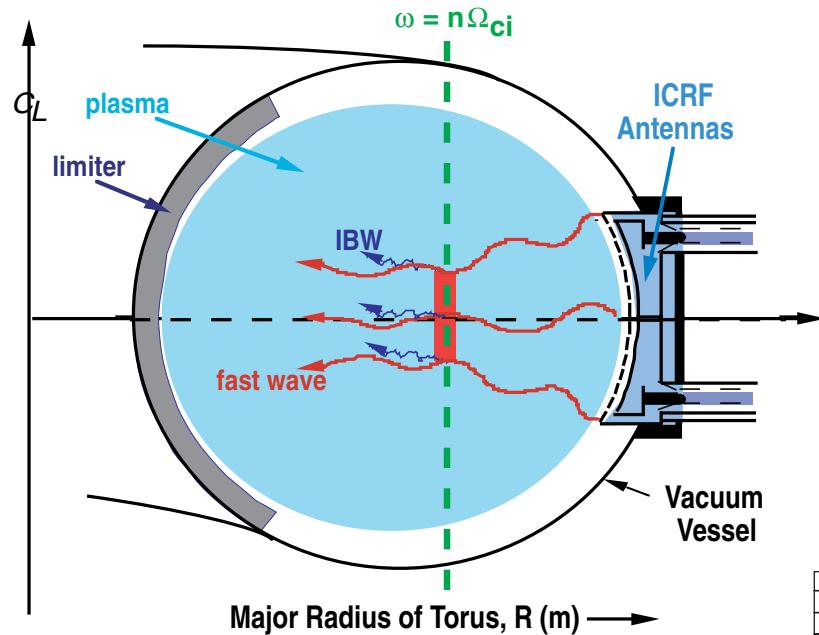
- Plasma current maintained in steady state:
 - JET; 3 MA, 4 s
 - TRIAM-1M; 20 kA, 2 hr



- 2-minute-long discharge at $I_p = 0.8$ MA
- Injected energy = 290 MJ

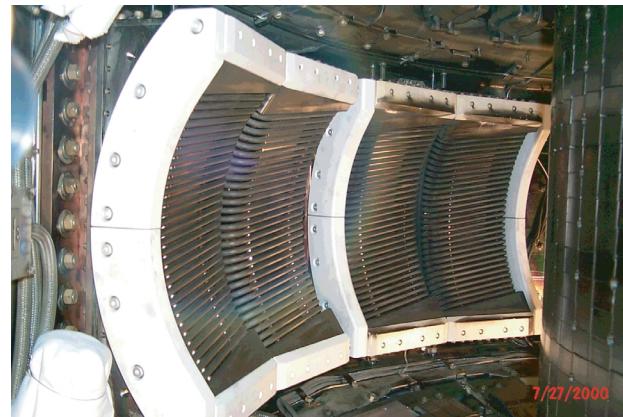


ICRF HEATING AND CURRENT DRIVE ($\omega = n\Omega_{ci}$) INVOLVES WAVE EXCITATION, PROPAGATION, ABSORPTION AND MODE CONVERSION



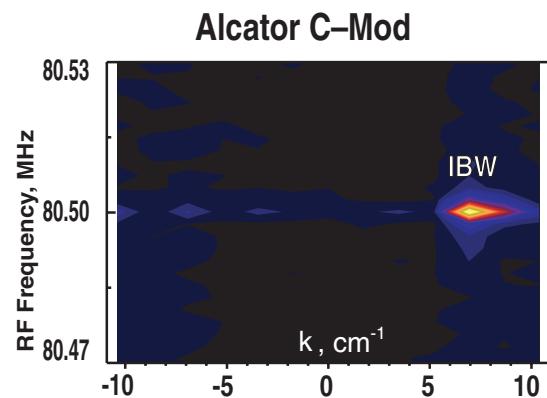
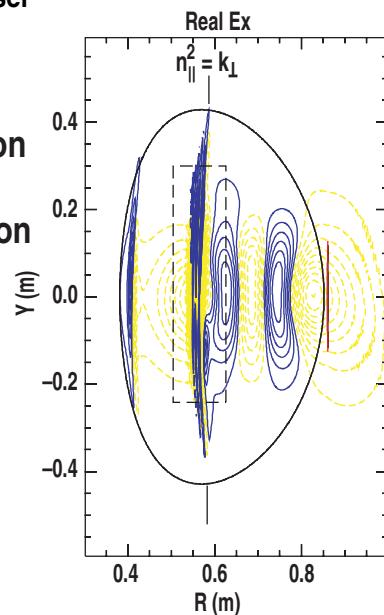
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Wave Propagation
(TORIC, PICES)



Absorption
Mode
Conversion

AORSA
PICES
TORIC
METS

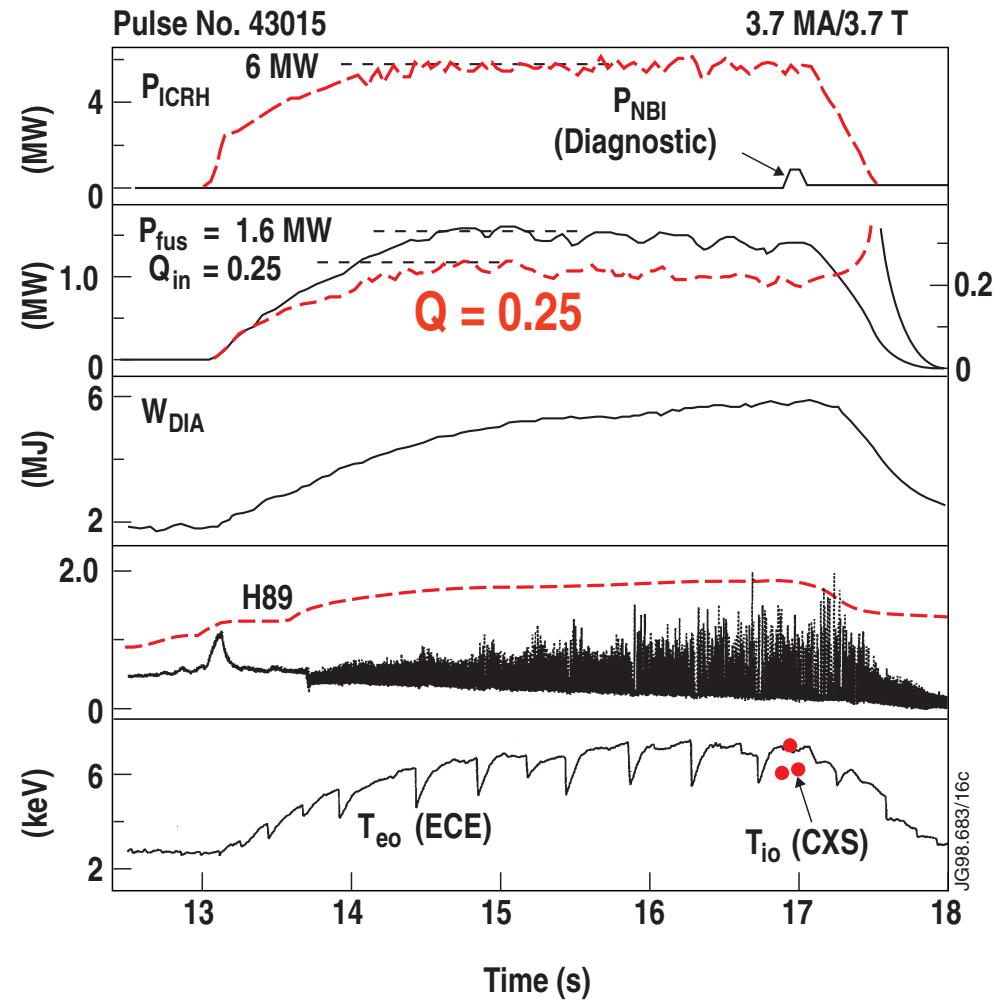
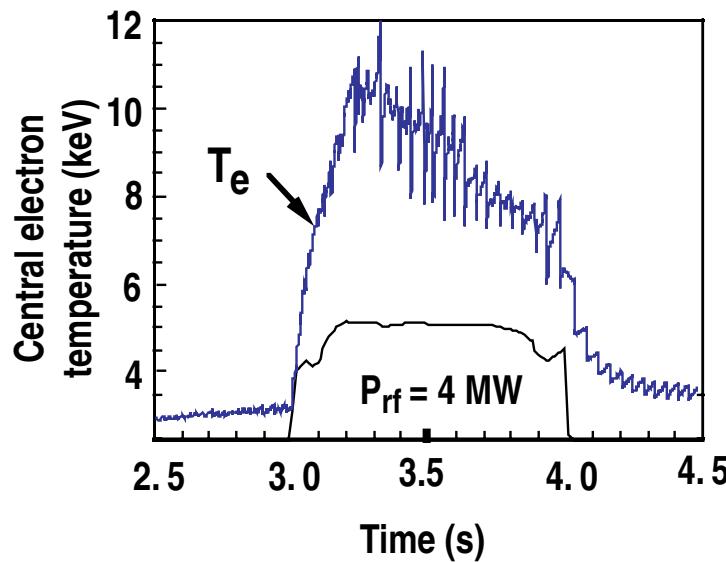


IBW Measured
PCI Diagnostic

MFE—Tokamak

BASIC ICRF SCHEMES (MINORITY D AND ^3He , $2\omega_{\text{CT}}$) FOR A DT REACTOR HAVE BEEN VERIFIED

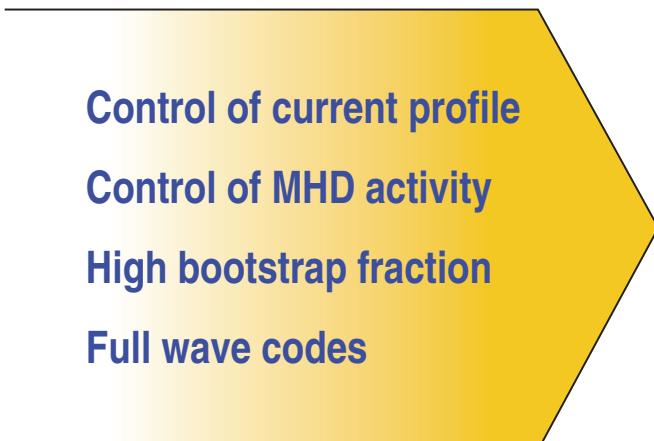
- Mode conversion experiments in D – ^3He produced the highest electron heating efficiency in TFTR
- JET: 6 MW ICRF → 1.66 MW fusion power



HEATING AND CURRENT DRIVE CHALLENGES FOR THE NEXT DECADE

90s

2000 – 2010

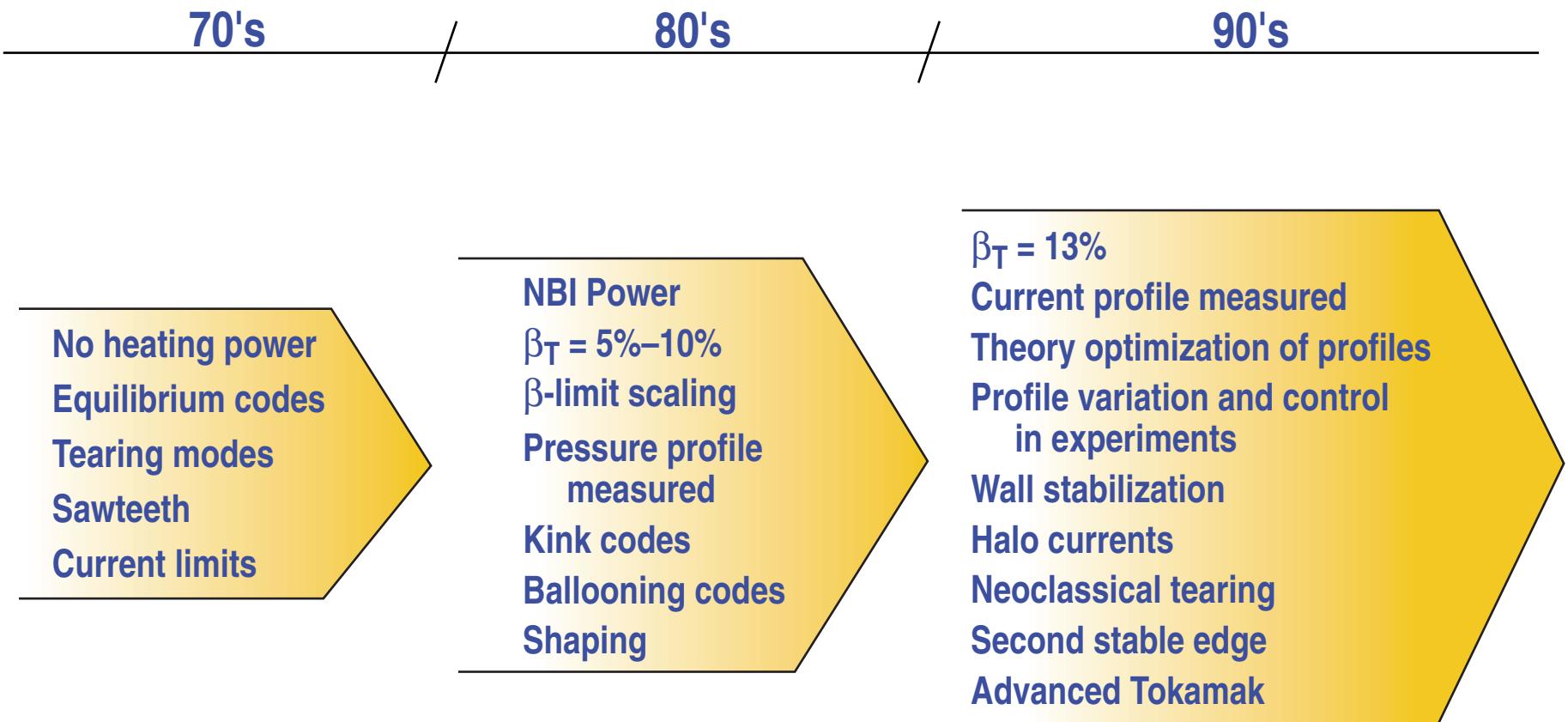


- Control of current profile
- Control of MHD activity
- High bootstrap fraction
- Full wave codes



- Current profile control
- Transport barrier control
- Coupling of Fokker-Planck, transport, and stability codes
- Helicity injection
- Strong alpha heating

MHD STABILITY PHYSICS MATURED IN THE 80's AND MOVED TO PROFILE OPTIMIZATION IN THE 90's



THE EFFECTS OF PLASMA INSTABILITIES RANGE FROM LOSS OF THE CONFIGURATION TO LOCAL TRANSPORT

Spatial Scale of the Mode	Mode Description	Principal Consequence
$\sim a$	Global kink modes Ideal MHD (low n)	Disruptions β and I_p limits
$\sim \frac{1}{5}a$	Tearing modes Resistive MHD Ideal Ballooning ($n \rightarrow \infty$)	Macroscopic Transport Profile Modification
$\sim \frac{1}{10}a$	Edge Localized Modes	Periodic bursts at the edge
ρ_i	Ion Temperature Gradient Modes Drift Waves	Ion Transport
ρ_e	Electron Temperature Gradient Modes Drift Waves	Electron Transport

IDEAL MHD INSTABILITIES LIMIT THE MAXIMUM BETA

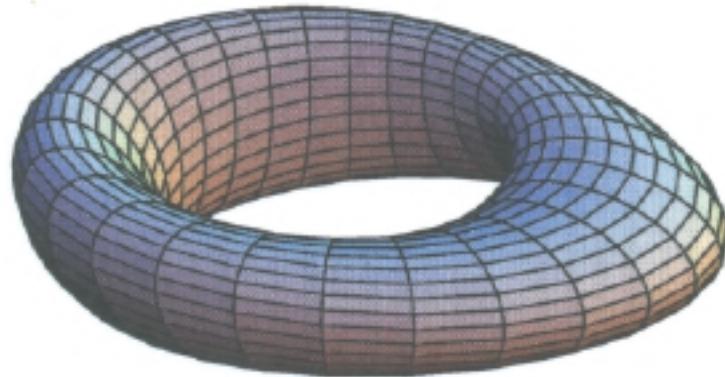
Change in potential energy for a small displacement ξ :

$$\delta W = \frac{1}{2} \int d\mathbf{r}^3 \left\{ \frac{|\delta \mathbf{B}|^2}{\mu_0} + \frac{\mathbf{B}^2}{\mu_0} |\nabla \cdot \xi_{\perp} + 2\xi_{\perp} \cdot \kappa|^2 + \gamma p |\nabla \cdot \xi|^2 - J_{||} (\xi_{\perp} \times \mathbf{b}) \cdot \delta \mathbf{B} - 2(\xi_{\perp} \cdot \nabla p) (\kappa \cdot \xi_{\perp}) \right\}$$

STABILIZING

DESTABILIZING

Kink Mode: low n, global

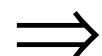
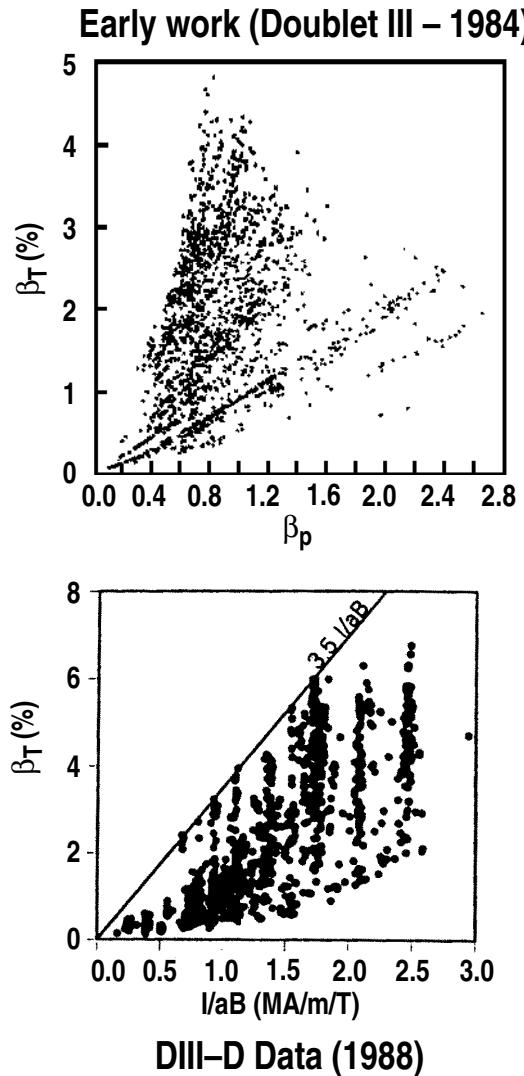


Ballooning Mode: High n , localized in bad curvature region



Pressure-driven Kink (Kink-ballooning) Mode

BETA LIMIT SCALINGS WERE DERIVED THAT FIT WELL EXPERIMENTAL RESULTS



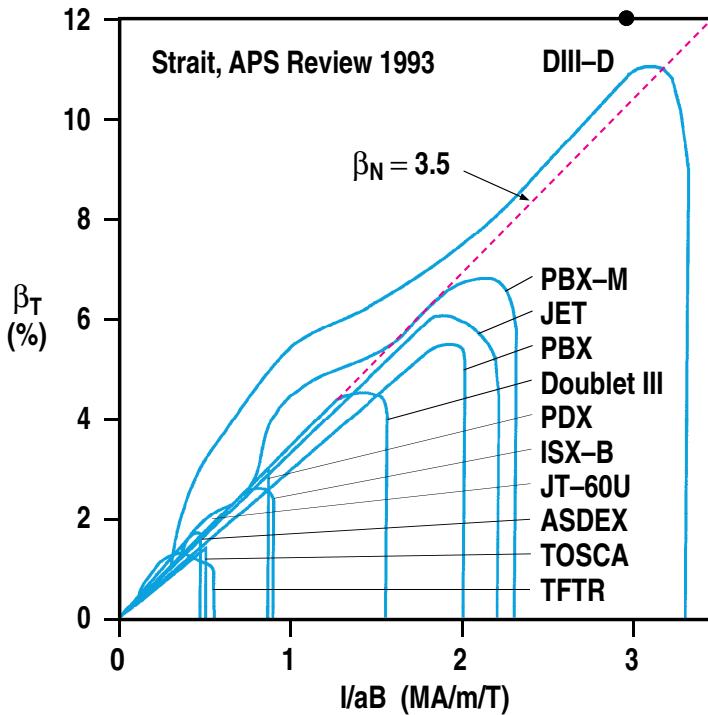
Theory calculations (1982–1984), Troyon scaling

$$\beta_T (\%) \leq 2.8 \frac{I (\text{MA})}{a(\text{m}) B_T (\text{T})}, \text{ Define } \beta_N = \beta_T / (I/aB)$$

$$\beta_p \beta_T = 25 \left(\frac{I + \kappa^2}{2} \right) \left(\frac{\beta_N}{100} \right)^2$$

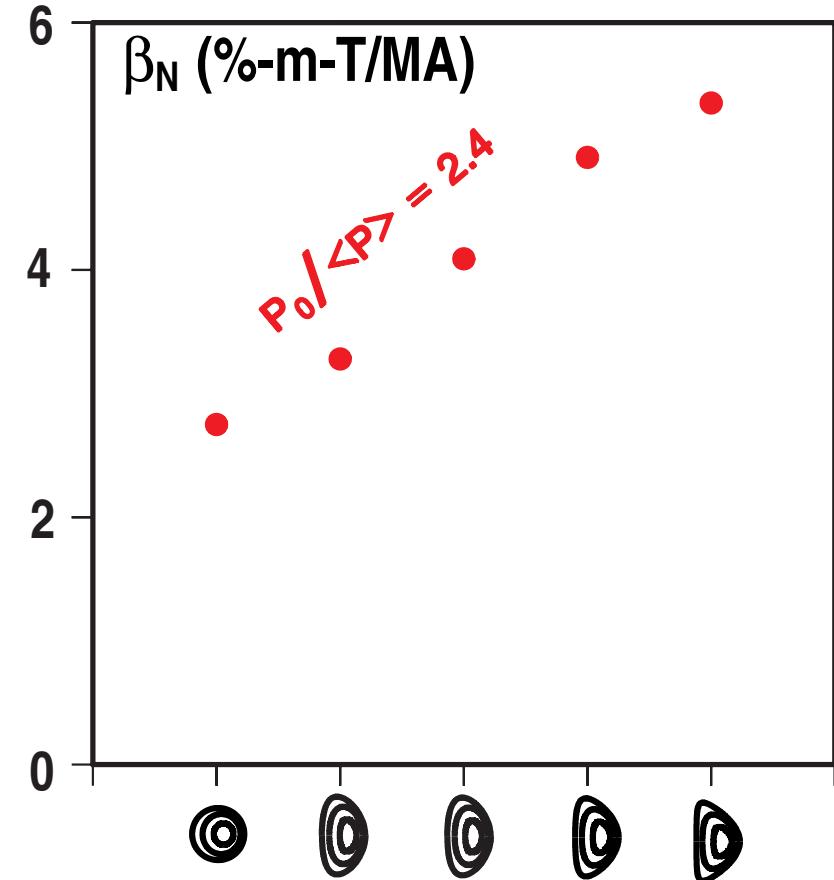
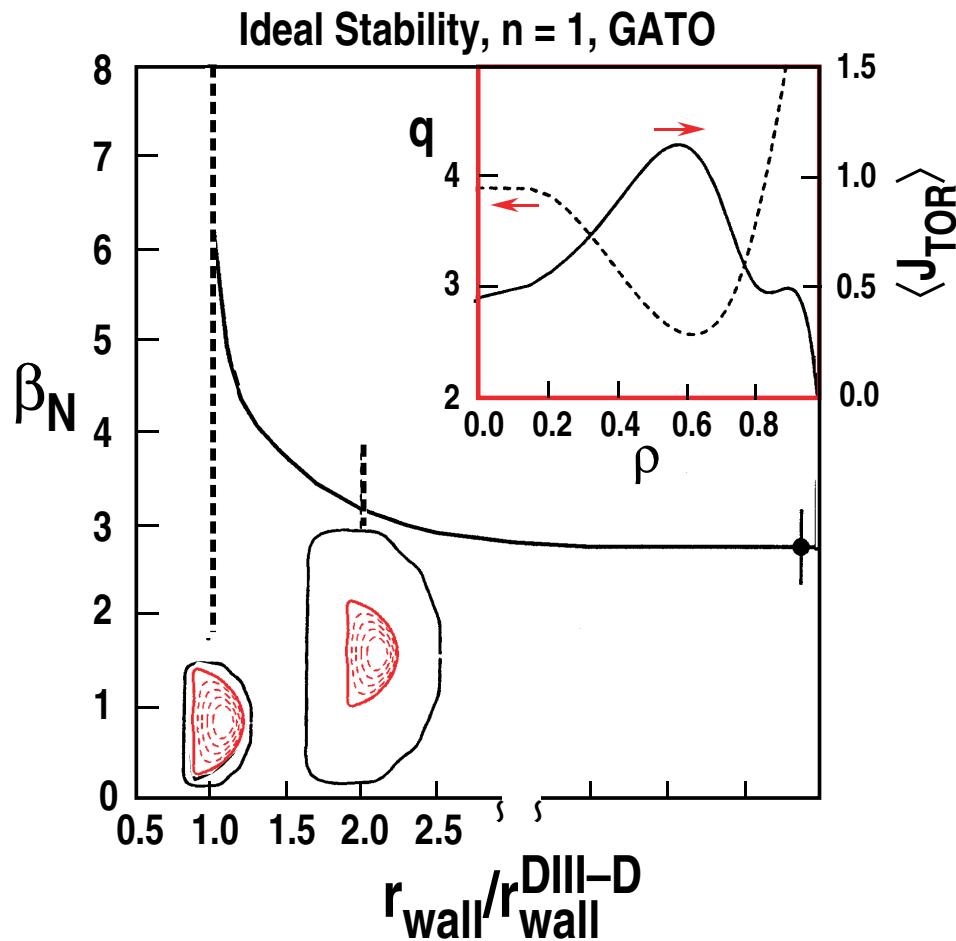
Fusion power $\beta_T^2 B^4$

Bootstrap fraction $c \epsilon^{1/2} \beta_p$

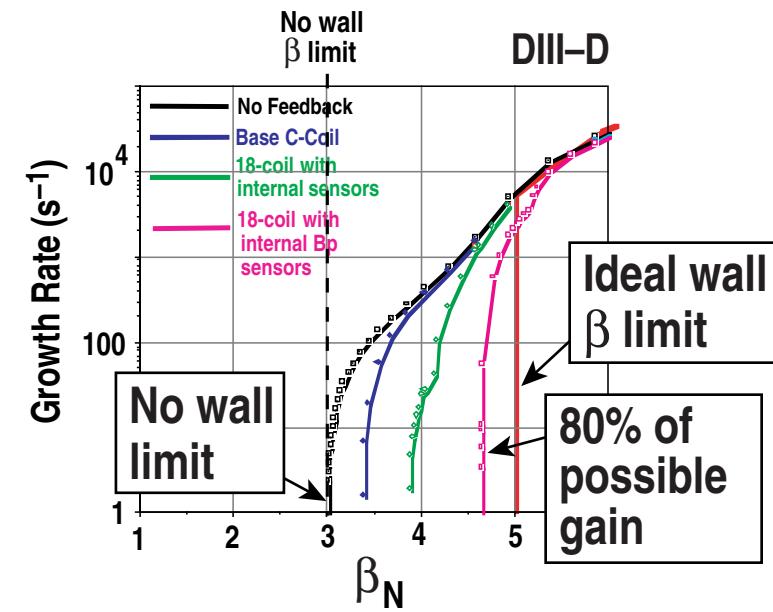
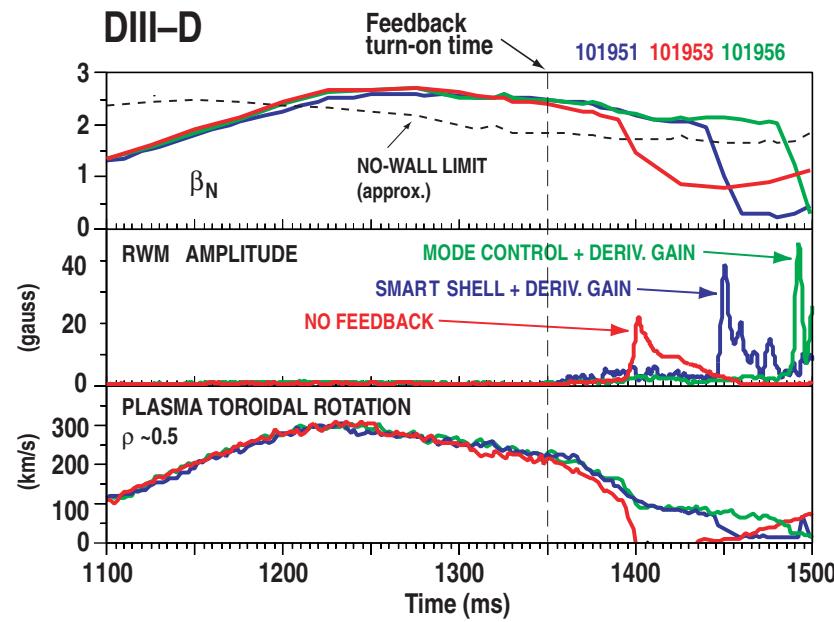
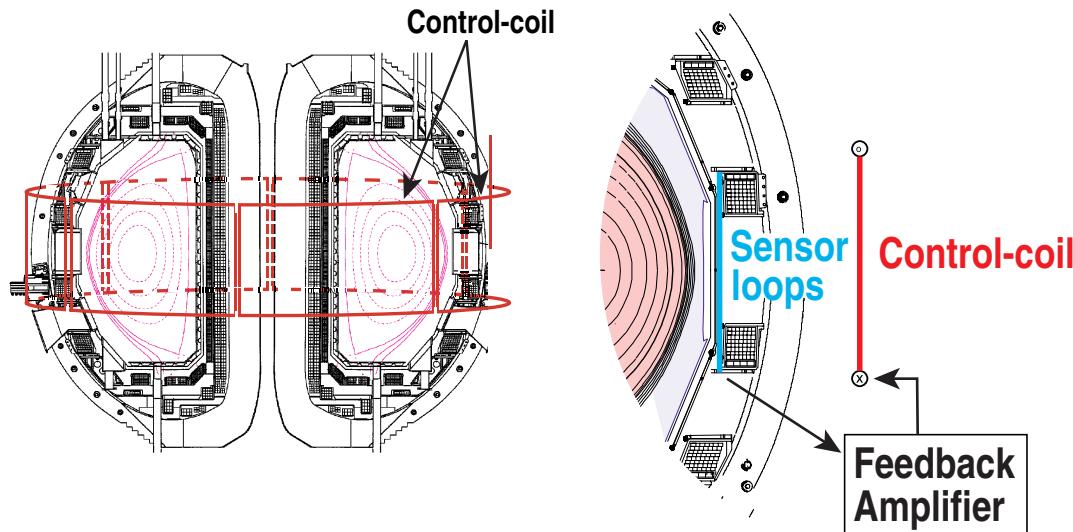


MFE—Tokamak

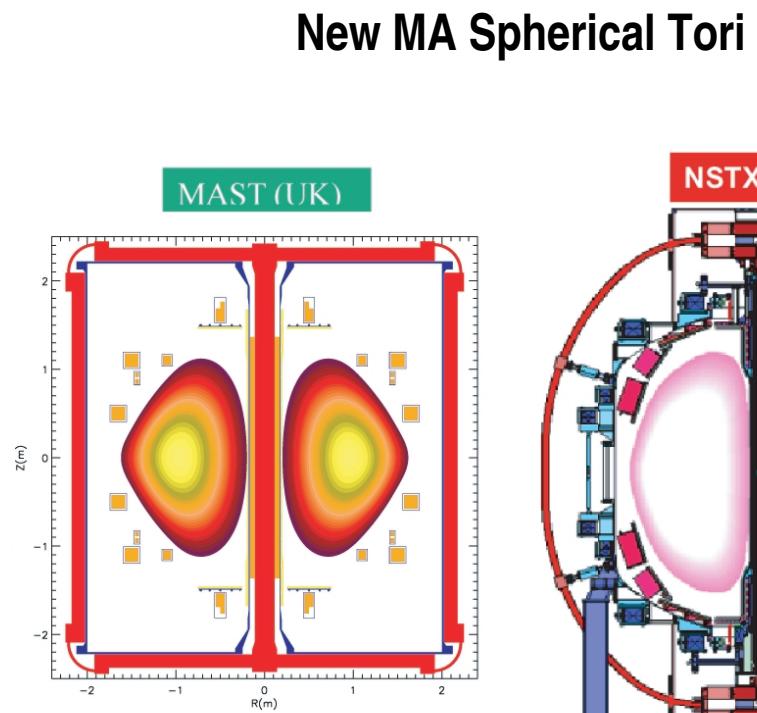
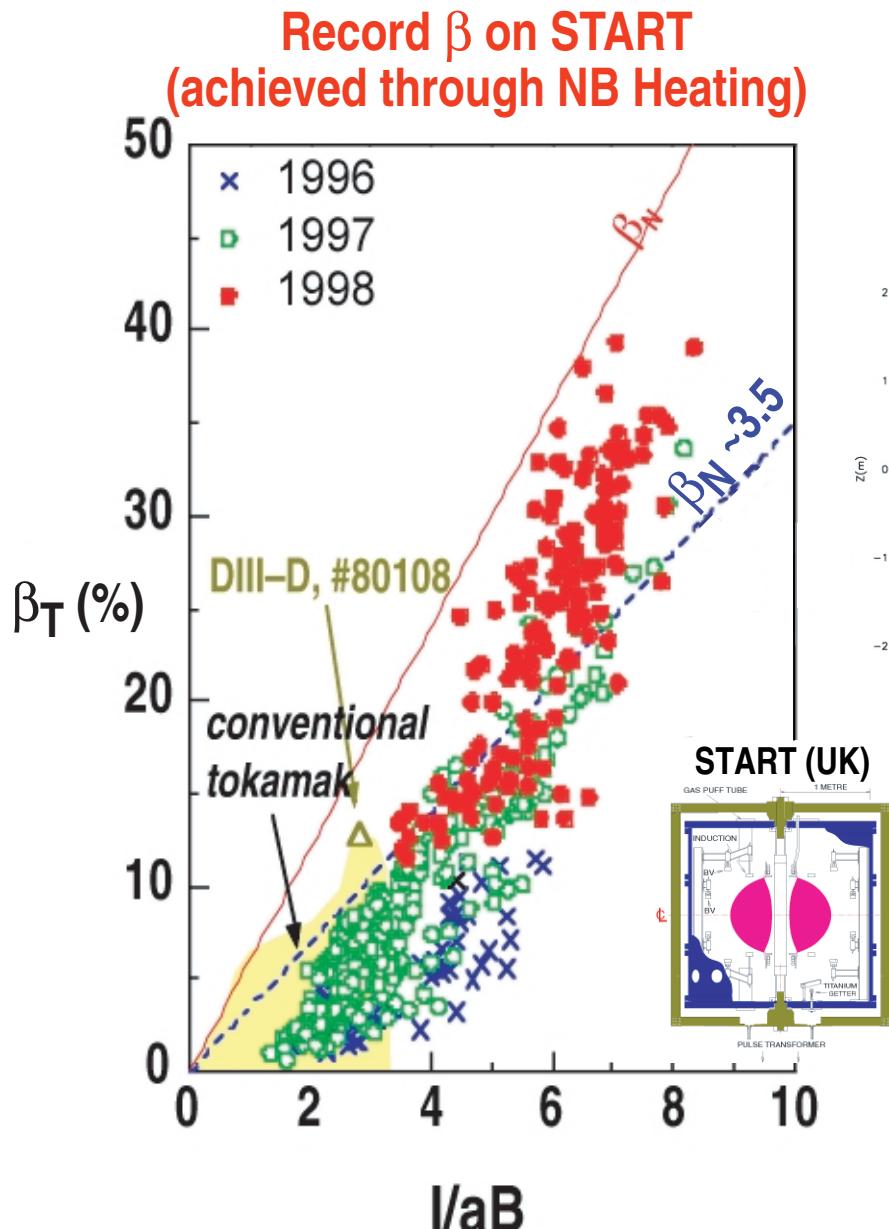
WALL STABILIZATION, PLASMA SHAPING, AND OPTIMAL PRESSURE AND CURRENT PROFILE MAY DOUBLE THE STABLE OPERATING SPACE OF THE TOKAMAK



IDEAL KINK MODE GROWTH IS SLOWED BY A RESISTIVE WALL AND RESPONDS TO FEEDBACK STABILIZATION



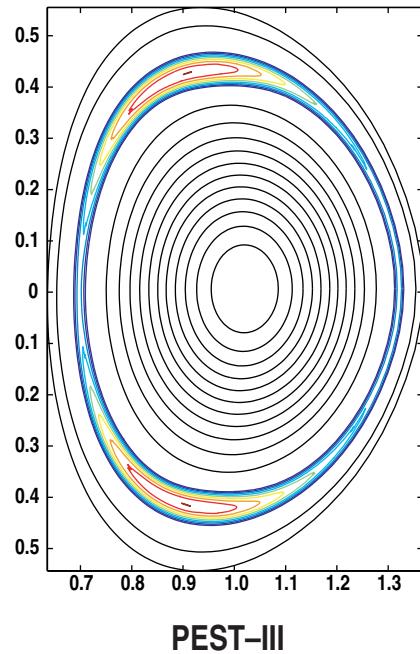
LOW ASPECT RATIO RAISES β_N and β_T



TEARING MODES

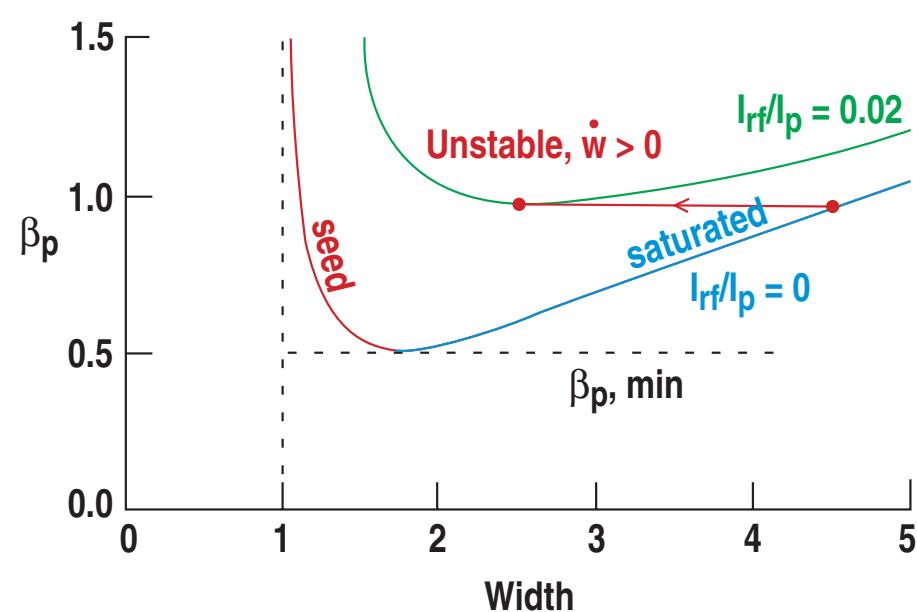
Classical

- Finite resistivity
- Current can diffuse and form clumps — magnetic islands — on rational q flux surfaces
- Driven by ∇J
- Growth time 10s of milliseconds



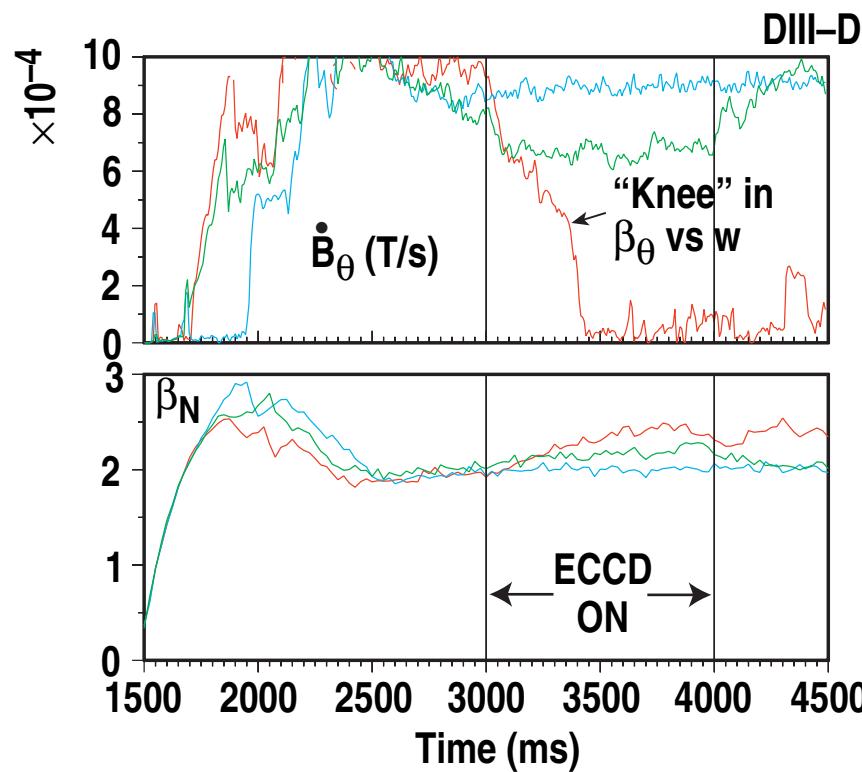
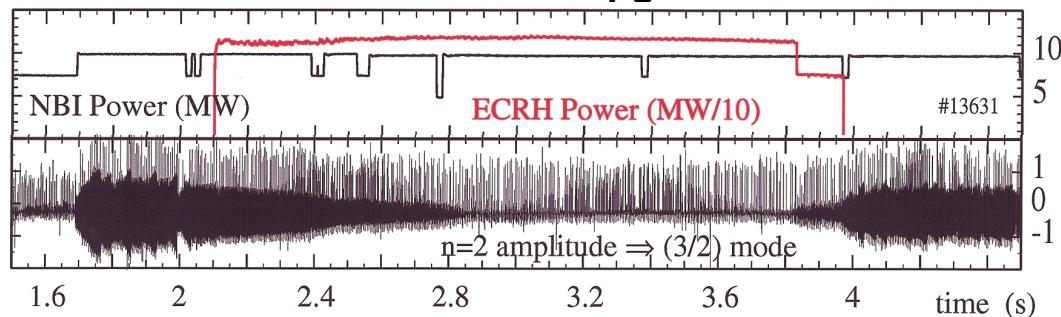
Neoclassical

- $\nabla P=0$ in island removes equilibrium bootstrap current
 - Helical current perturbation amplifies seed island
- Providing auxiliary current drive predicted to stabilize NTM



STABILIZATION OF NTMs BY ECCD

ASDEX-Upgrade

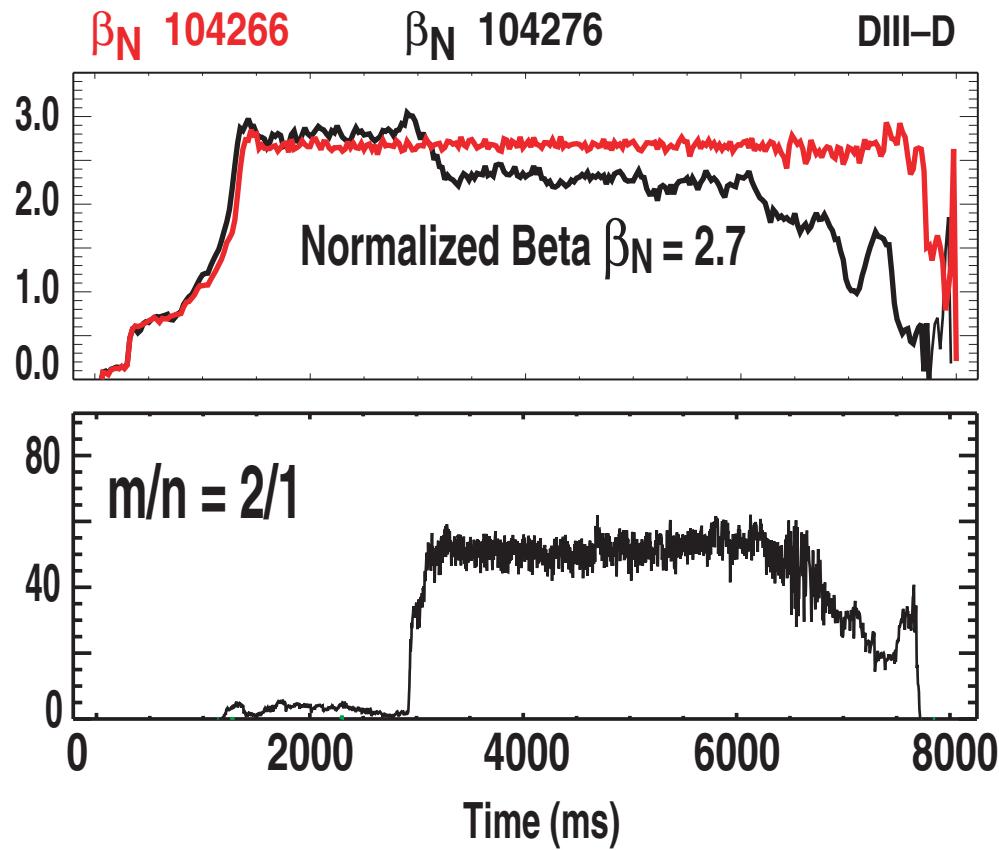


ECCD in DIII-D

Similar results from JT-60U

MFE—Tokamak

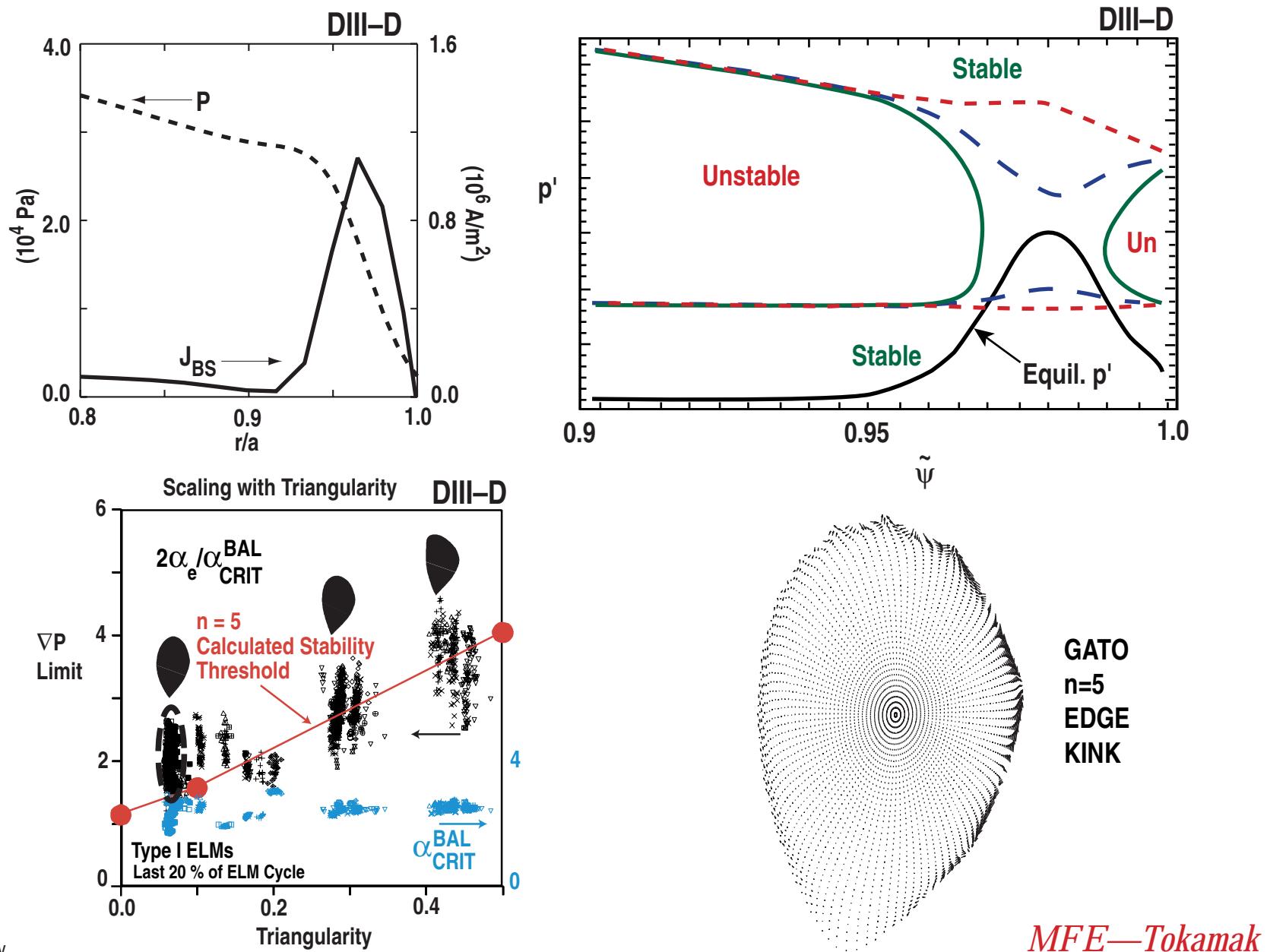
PRECISE CONTROL NEAR THE β -LIMIT IS THE KEY TO AVOIDING DISRUPTIONS



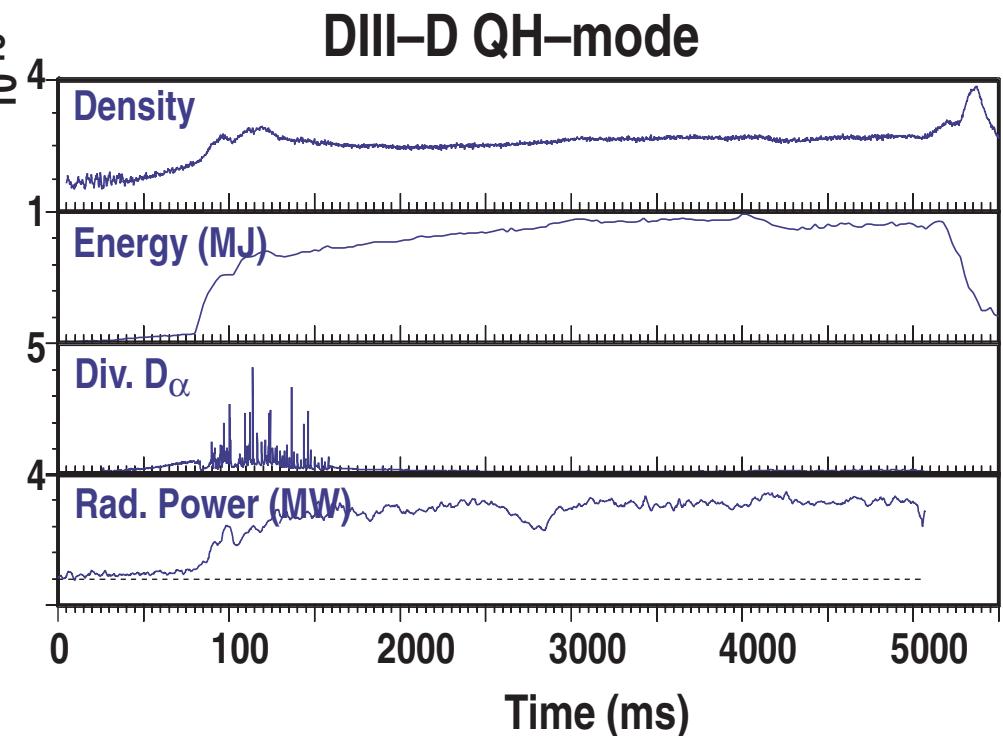
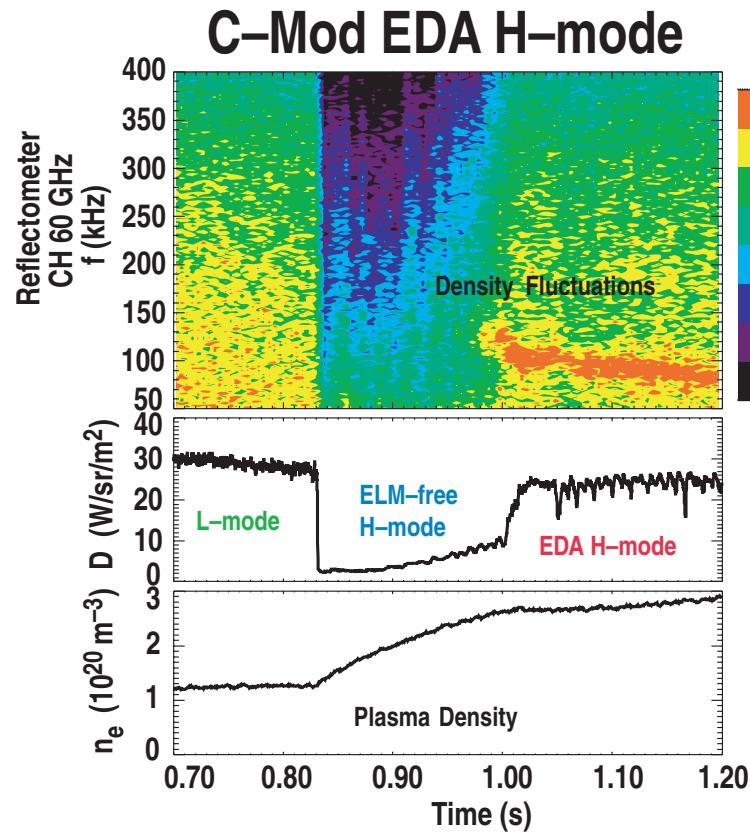
1. Need to operate close to stability limits
 - Good control
 - Knowledge of limits

High performance DIII-D discharge regulated 5% below 2/1 tearing limit for $35 \tau_E$ (6.3 seconds)
2. Mitigation of disruption consequences massive gas puff or pellets
 - No runaway electrons
 - Reduced halo currents and forces on structural components
 - Reduced heat pulses to the divertor surfaces

EDGE LOCALIZED MODES (ELMS) ARE NOW UNDERSTOOD TO BE INTERMEDIATE n KINKS

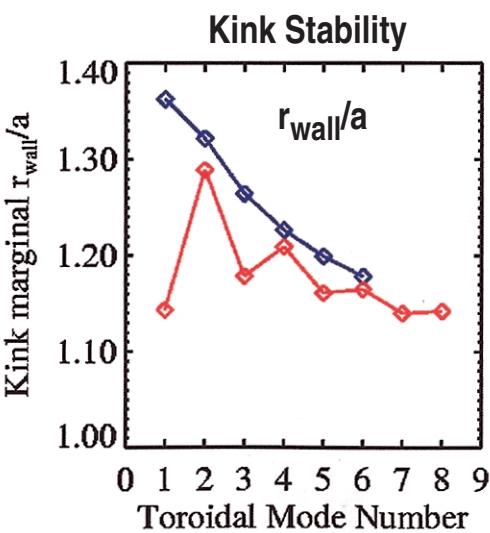
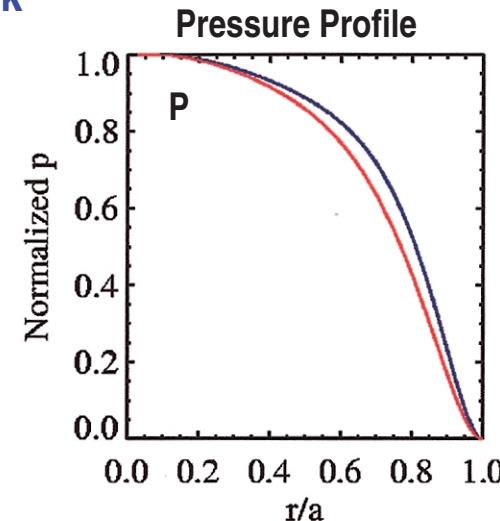
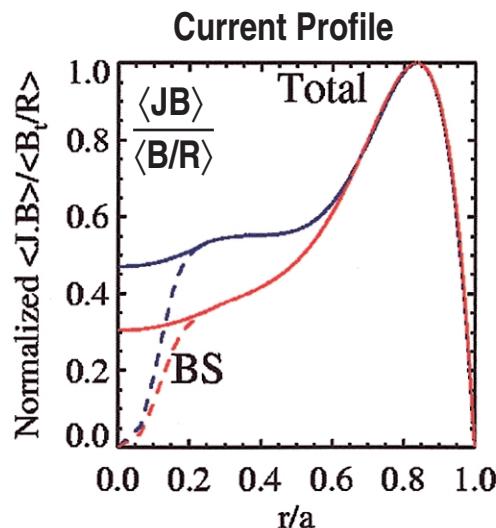
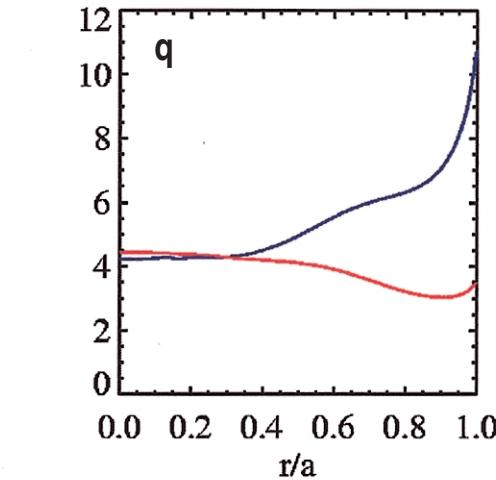


BOTH ALCATOR C-MOD AND DIII-D HAVE FOUND ELM-FREE REGIMES WITHOUT DENSITY OR IMPURITY ACCUMULATION



THE FUTURE

- Advanced Tokamak stability theory points to states with very broad pressure profiles and hollow current profiles and nearly 100% bootstrap current as perhaps the ultimate potential of the Tokamak



ARIES—AT

A=3.3
 $\kappa=2.5$
 $\delta=0.6$
 $\beta=14\%$
 $\beta_N=6$

ARIES—ST

A=1.6
 $\kappa=3.6$
 $\delta=0.64$
 $\beta=56\%$
 $\beta_N=8.2$

(J. Menard, S. Jardin, J. Manickam)

MFE—Tokamak

STABILITY CHALLENGES FOR THE NEXT DECADE

90's

2000–2010

$\beta_T = 13\%$

Current profile measured

Theory optimization of profiles

Profile variation and control
in experiments

Wall stabilization

Halo currents

Neoclassical tearing

Second stable edge

Advanced Tokamak

Wall stabilized β -limit

Bootstrap fraction $\rightarrow 100\%$

Pressure and current profile control

Very hollow $J(r)$

Broad pressure profiles

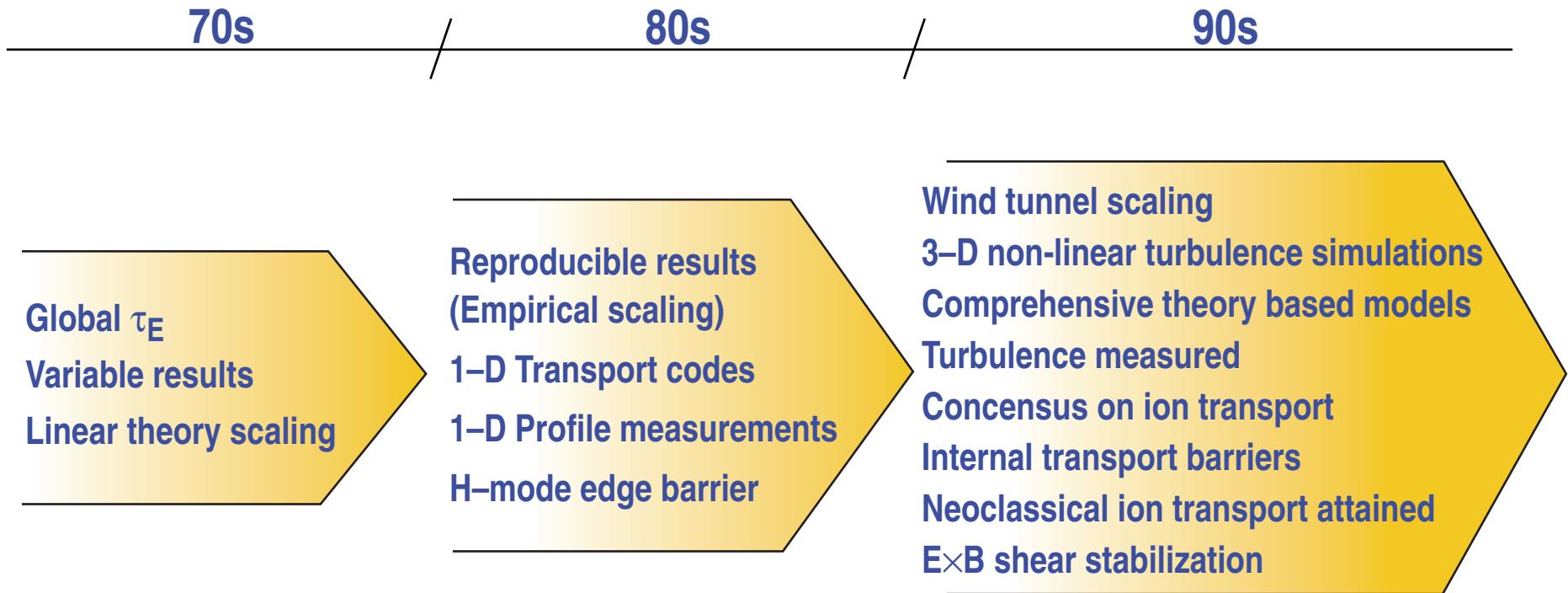
Optimum edge stability

Feedback stabilization or avoidance
of neoclassical tearing

Disruption mitigation

3-D MHD, understand disruptions
away from β -limit

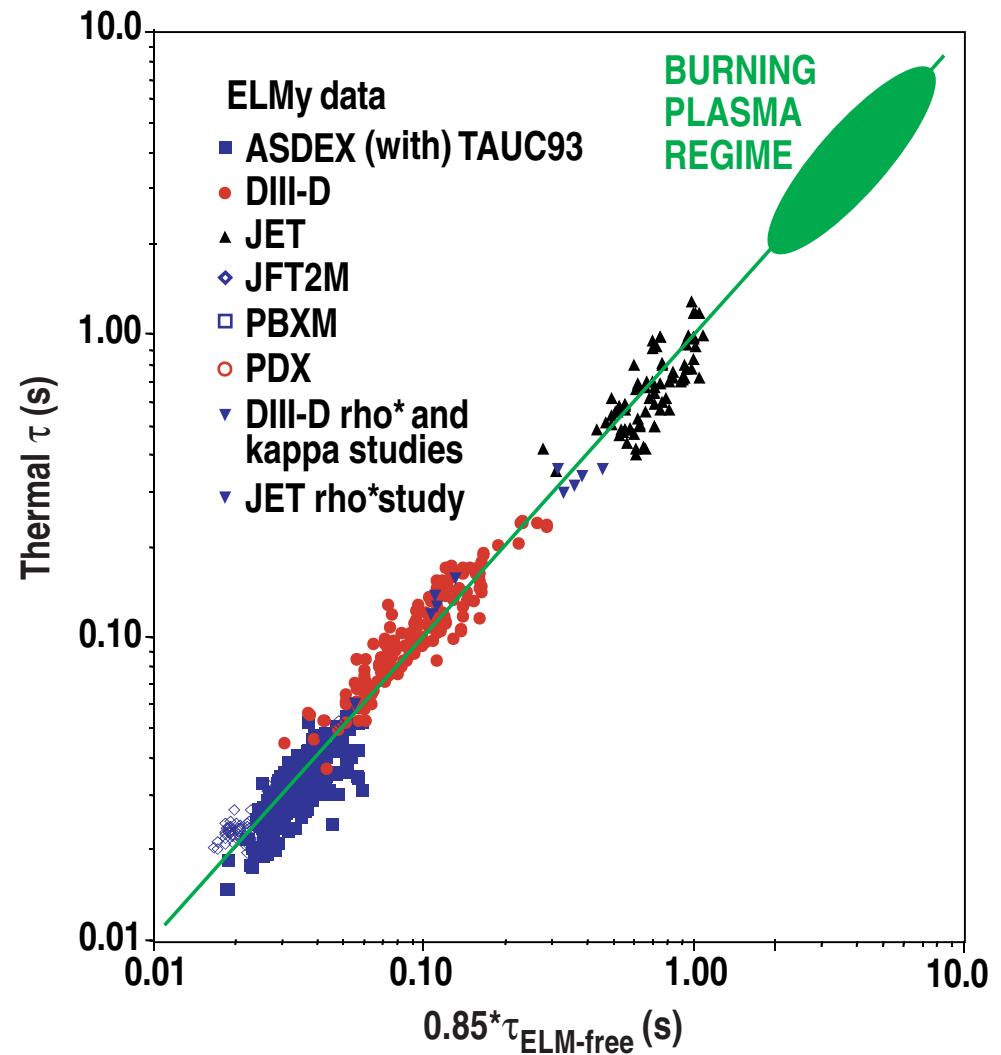
THE 90's HAVE SEEN EXCITING ADVANCES IN CONFINEMENT SCIENCE



TOKAMAK CONFINEMENT PROVED (EMPIRICALLY) PREDICTABLE

- In the 80's consistent scaling behavior was seen across many tokamaks implying
 - A common underlying transport physics was discoverable
 - Multi-machine confinement scaling relations could be constructed, e.g.

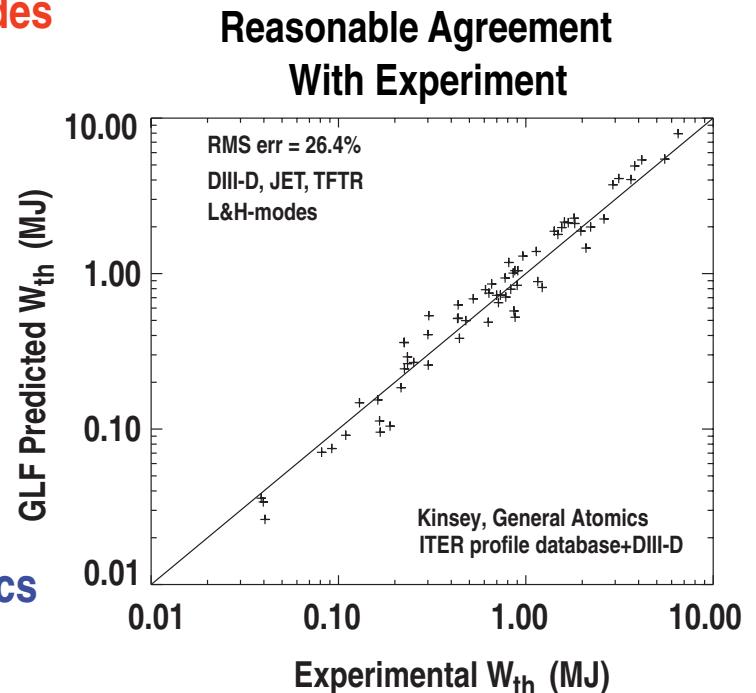
$$\begin{aligned}\tau_{E, \text{th, ELM}} &= 0.85 \tau_{E, \text{th, ELM-free}} \\ &= 0.031 I_p^{1.06} B^{0.32} \\ &\quad P^{-0.67} M^{0.41} R^{1.79} n_e^{0.17} \epsilon^{-0.11} \kappa^{-0.6}\end{aligned}$$



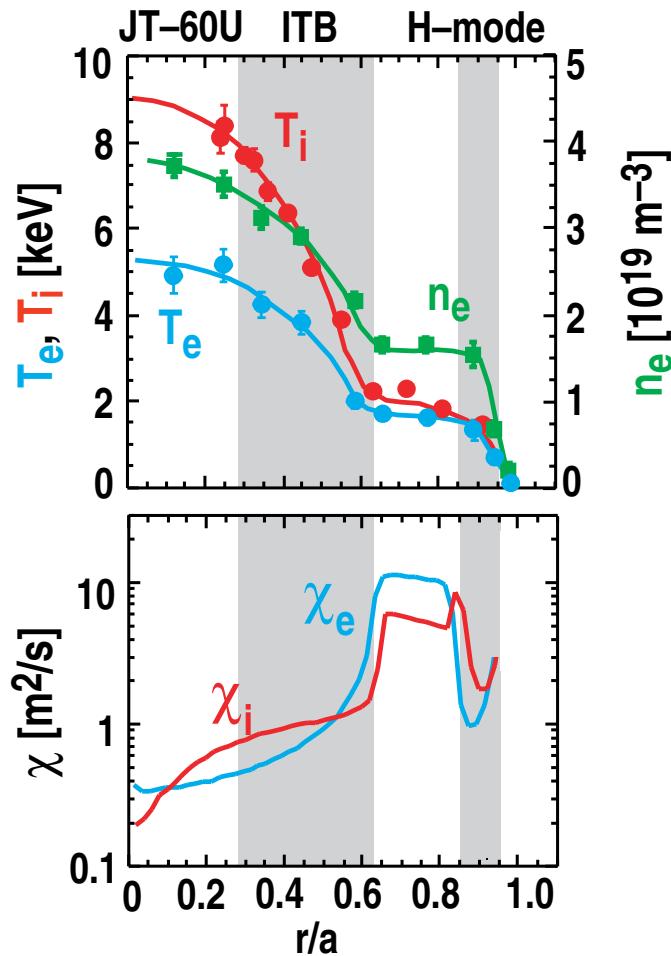
- Dimensionless wind tunnel scaling is providing a more fundamental physics basis

STRATEGY TO CALCULATE TRANSPORT

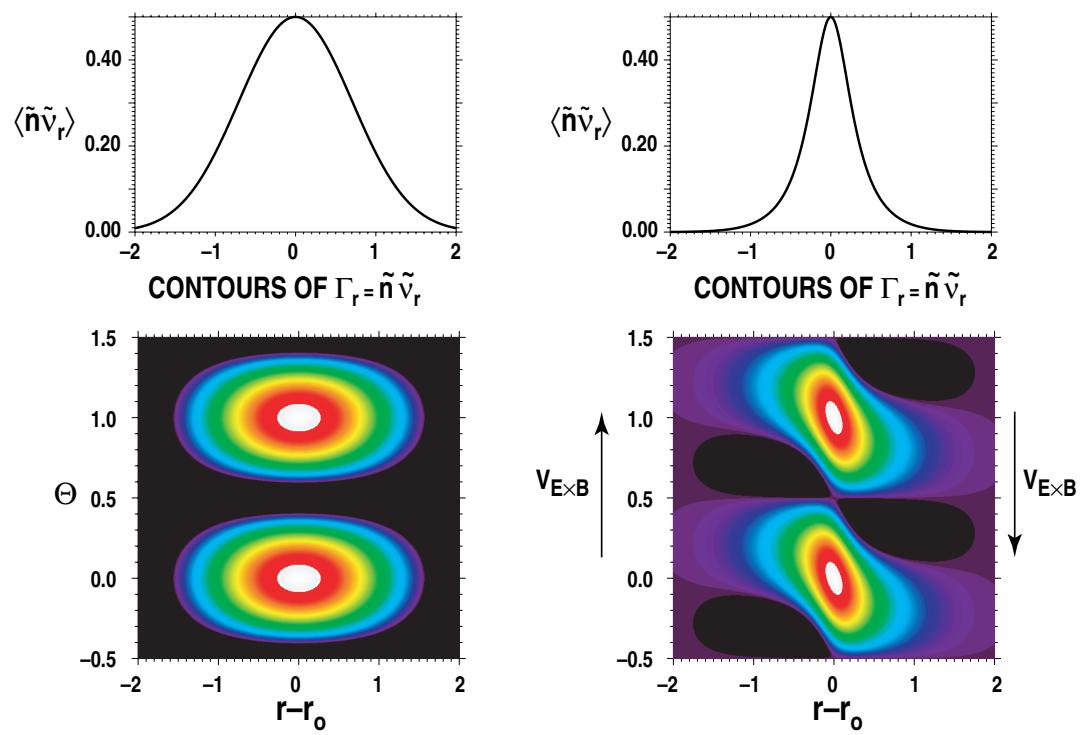
- Theory-based 3D nonlinear simulations being used to benchmark theoretical transport models which are then compared to experiment
- Linear gyrokinetic codes describe local ballooning mode instabilities
 - Long wavelength — ion temperature gradient (ITG) and trapped electron driven
 - Short wavelength — electron temperature gradient (ETG) driven
- Nonlinear flux tube and approximate gyrofluid codes
 - $\rho_i/a \rightarrow 0$
 - Only local ballooning
- Nonlinear codes spanning several hundred gyroradii
 - Finite ρ_i/a
 - More time consuming
- ITG/trapped electron flux tube simulations have been used to benchmark gyrofluid local transport code models with comprehensive physics
- International profile data base after 1995 allows systematic and comparative statistical tests of transport code models



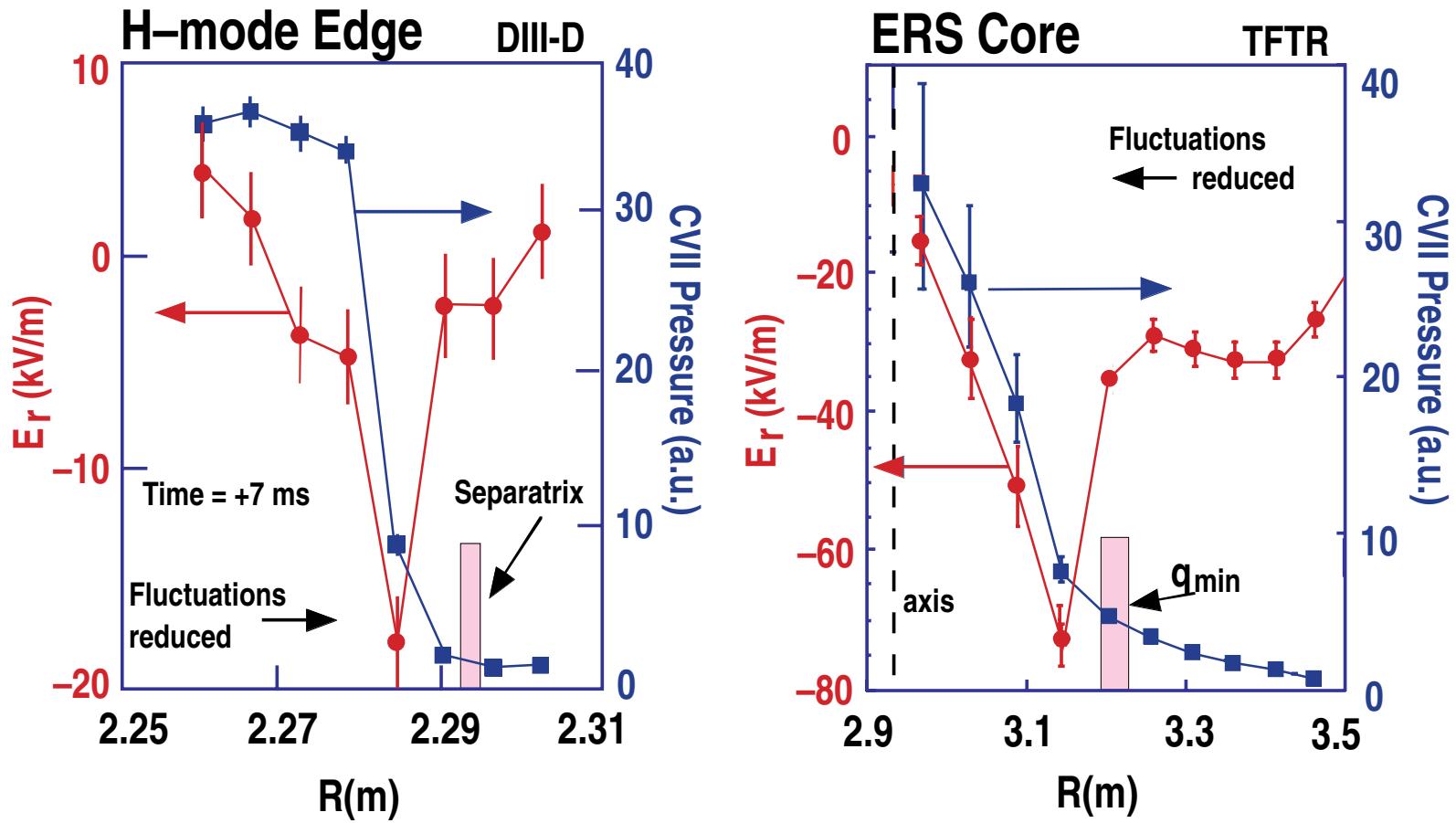
RECENT EXCITEMENT TRANSPORT BARRIERS FORMED BY SHEARED E \times B FLOW



Basic Idea: Sheared E \times B flow compresses turbulent eddies in the radial direction



SHEARED E×B FLOW SUPPRESSION OF TURBULENCE UNDERLIES BOTH EDGE AND CORE TRANSPORT BARRIERS

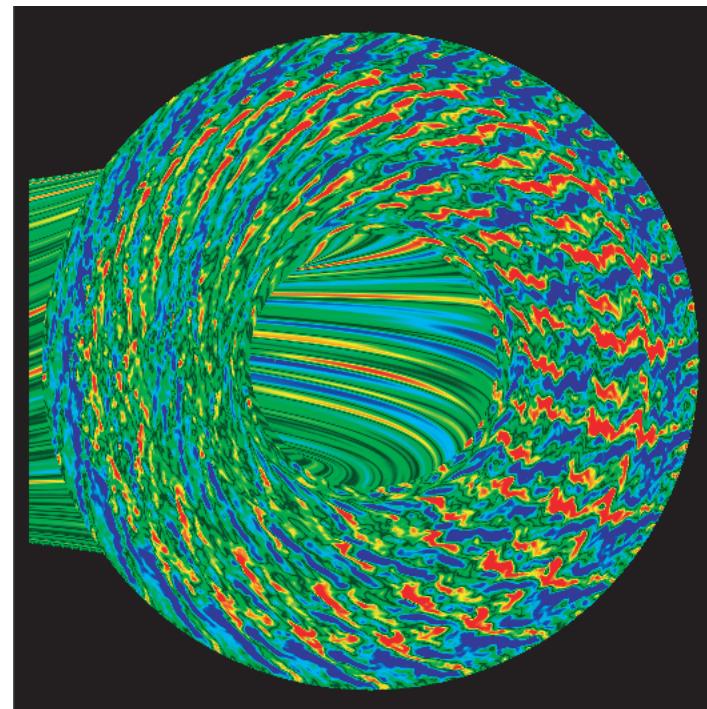
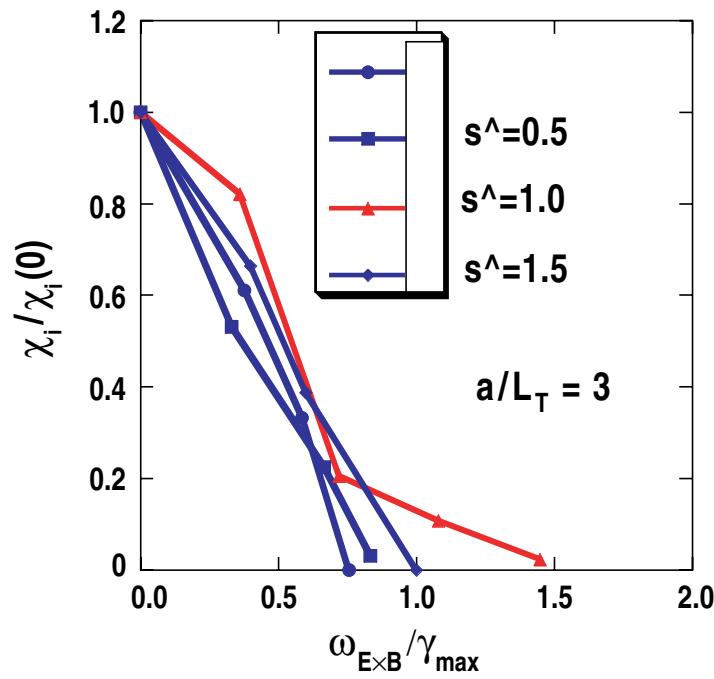


$$E_r = (Z_i e n_i)^{-1} \nabla P_i - v_{\theta i} B_\phi + v_{\phi i} B_\theta, \quad \text{The } E \times B \text{ shearing rate } \omega_{E \times B} = \left| \frac{(RB_\theta)^2}{B} \frac{\delta}{\delta \psi} \left(\frac{E_r}{RB_\theta} \right) \right|$$

[Hahm and Burrell, Phys. Plasmas 2, 1648]

EQUILIBRIUM SCALE SHEARED E \times B FLOWS CAN QUENCH ITG TRANSPORT IF THE SHEARING RATE EXCEEDS THE MAXIMUM LINEAR GROWTH RATE OF THE TURBULENCE

- ITG simulation of local annulus $160 \rho_s$ wide [R.E. Waltz, et al., Phys. Plasmas 1, 2229 (1994)]
- Application of E \times B shear $\omega_{E\times B} \sim \gamma_{\max}$ breaks up eddies and considerably reduces transport

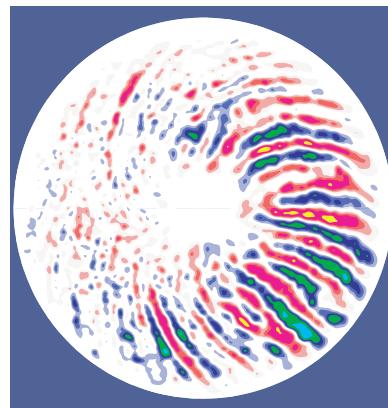


No E \times B flow

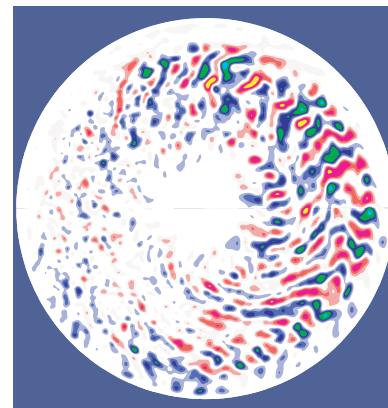
PLASMA TURBULENCE SIMULATION CODES USE FULL TOROIDAL GEOMETRY TO CALCULATE TRANSPORT RATES

- Recent advance: Small scale sheared poloidal flows can shear apart radial eddies, reducing their radial step size and the transport by an order of magnitude

Without
sheared
flows

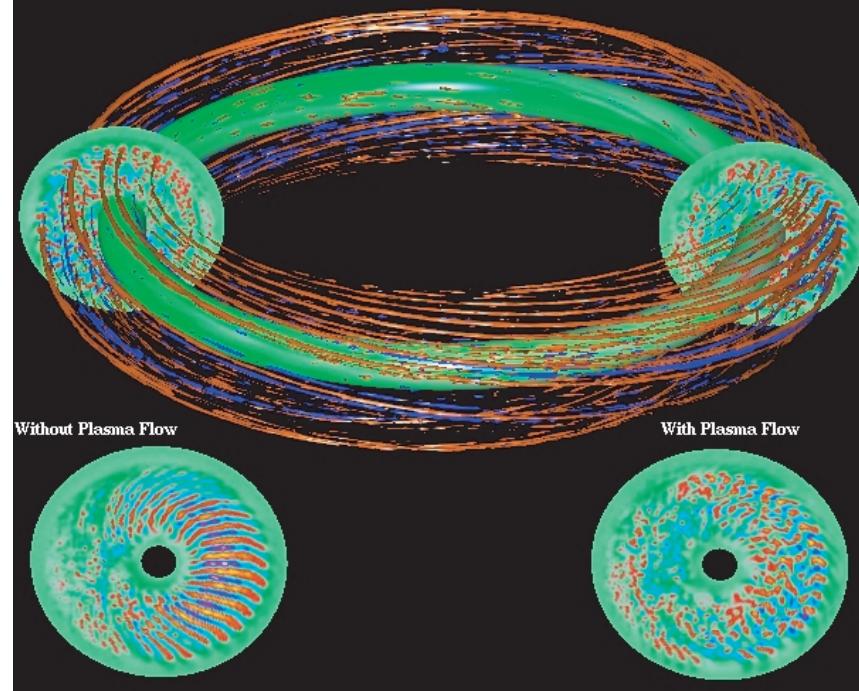


With
sheared
flows



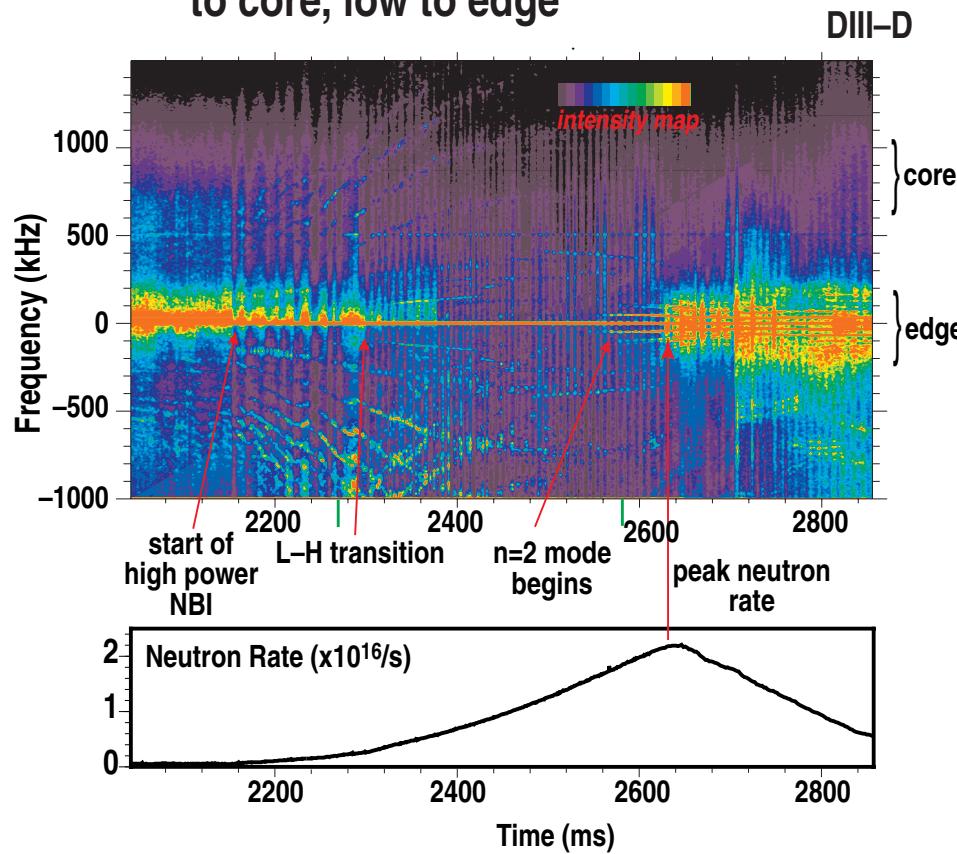
Gyrokinetic particle simulation of plasma microturbulence

[Z. Lin et al, Science 1998]

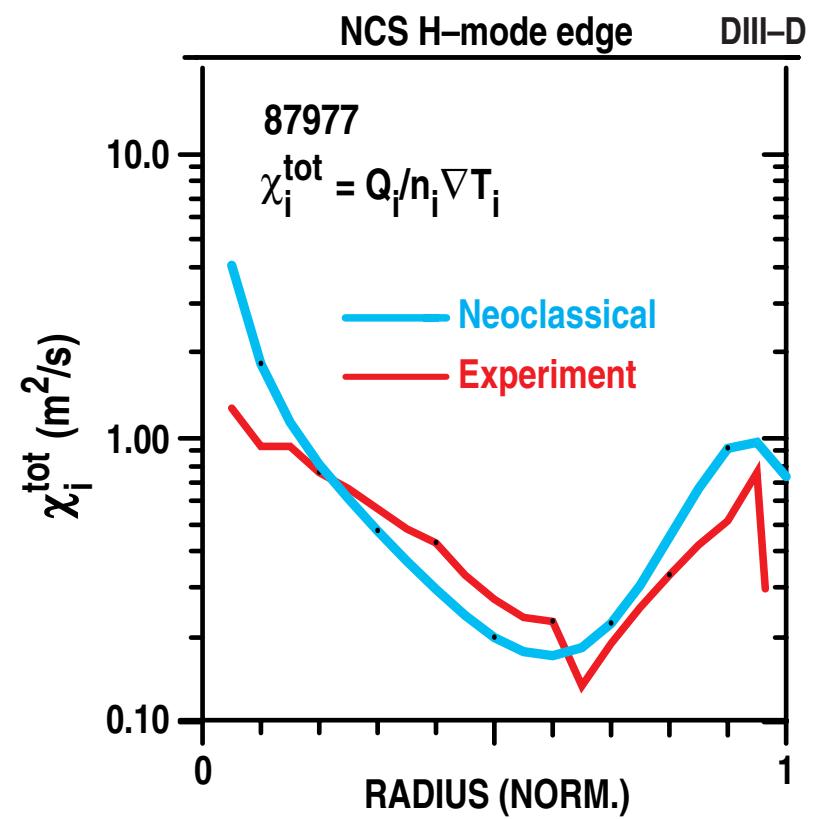


ION-NEOCLASSICAL TRANSPORT WITHOUT TURBULENCE, ACROSS ENTIRE PLASMA RADIUS

- Color contour map of fluctuation intensity as function of time from FIR scattering data
 - Higher frequencies correspond to core, low to edge



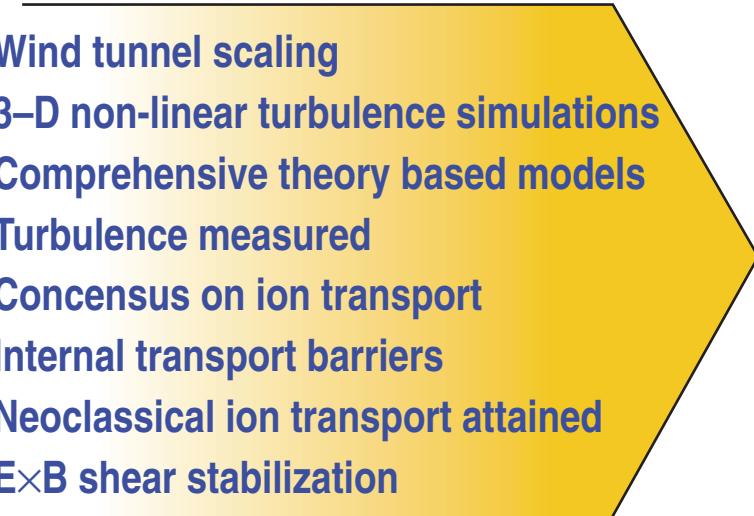
- Total ion thermal diffusivity at time of peak performance
 - $H = 4.5 \quad W = 4.2 \text{ MJ}$
 - $\beta = 6.7\% \quad \beta_N = 4.0$

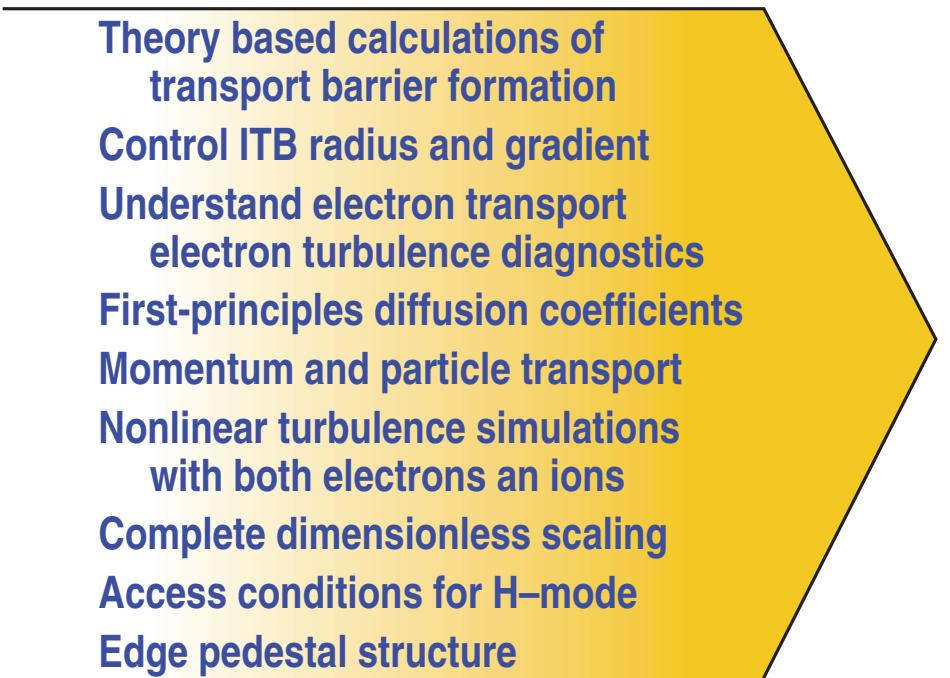


CONFINEMENT CHALLENGES FOR THE NEXT DECADE

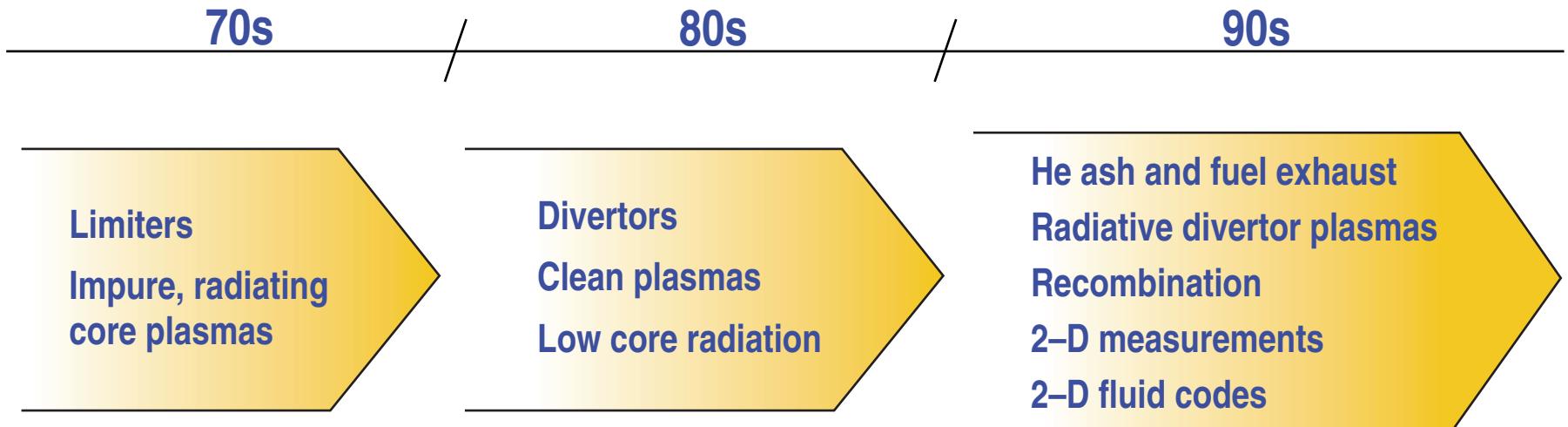
90s

2000 – 2010

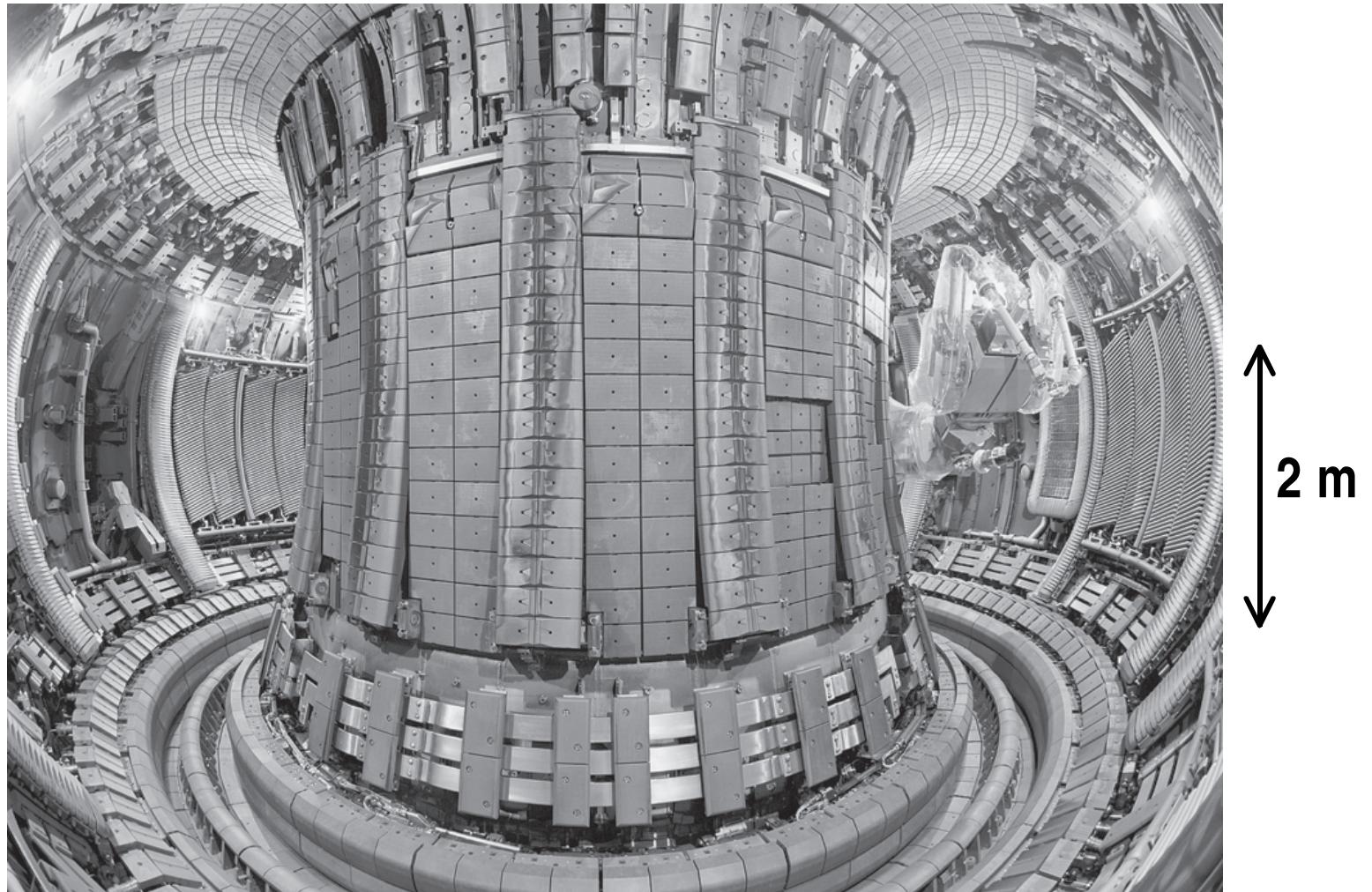
- 
- Wind tunnel scaling
 - 3-D non-linear turbulence simulations
 - Comprehensive theory based models
 - Turbulence measured
 - Concensus on ion transport
 - Internal transport barriers
 - Neoclassical ion transport attained
 - E×B shear stabilization

- 
- Theory based calculations of transport barrier formation
 - Control ITB radius and gradient
 - Understand electron transport electron turbulence diagnostics
 - First-principles diffusion coefficients
 - Momentum and particle transport
 - Nonlinear turbulence simulations with both electrons and ions
 - Complete dimensionless scaling
 - Access conditions for H-mode
 - Edge pedestal structure

THE SCIENCE OF POWER AND PARTICLE EXHAUST LEAPED FORWARD IN THE 90's



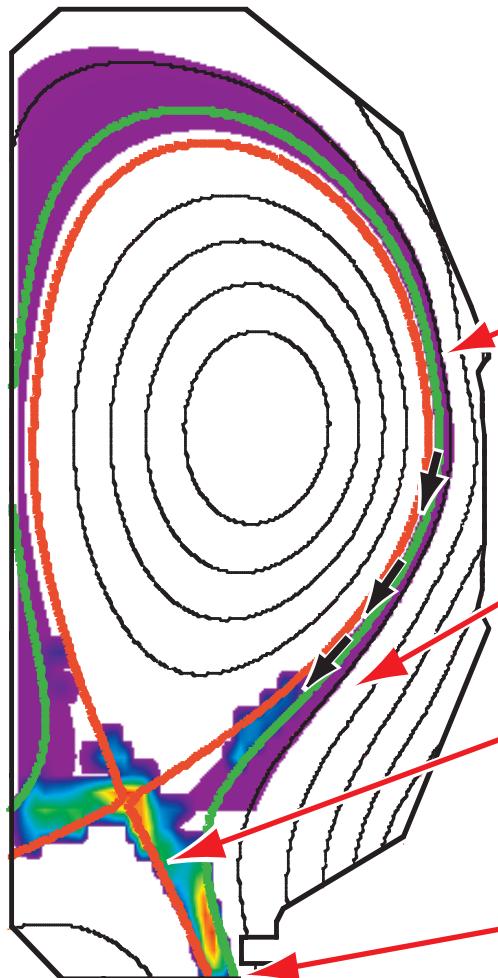
THE JET DIVERTOR IS TYPICAL OF TOKAMAKS TODAY



Axisymmetric lower single null with graphite tiles to handle high heat flux

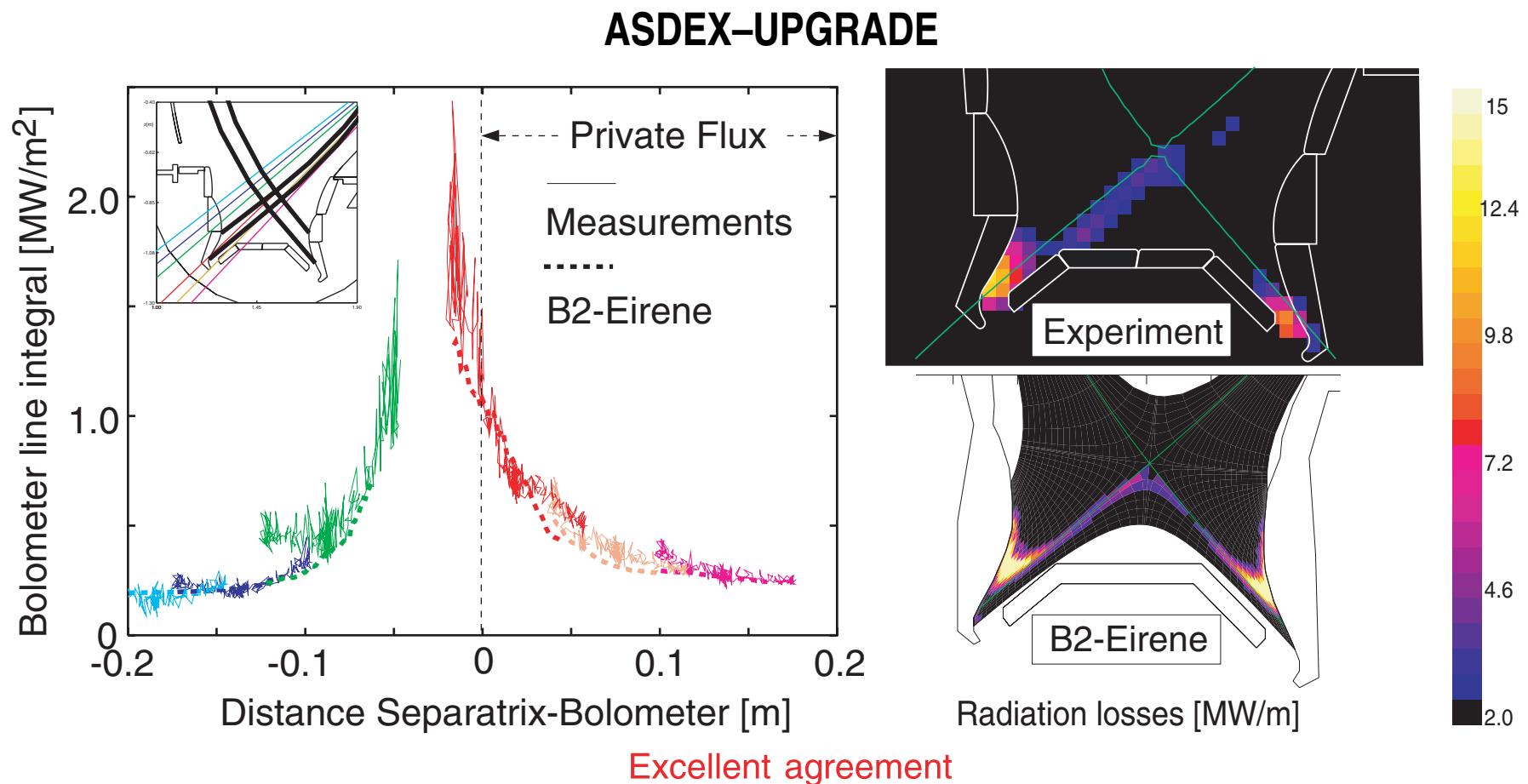
MFE—Tokamak

THE PHYSICS ELEMENTS THAT ARE DOMINANT IN THE DIVERTOR PROBLEM ARE NOW INCORPORATED IN 2-D CODES

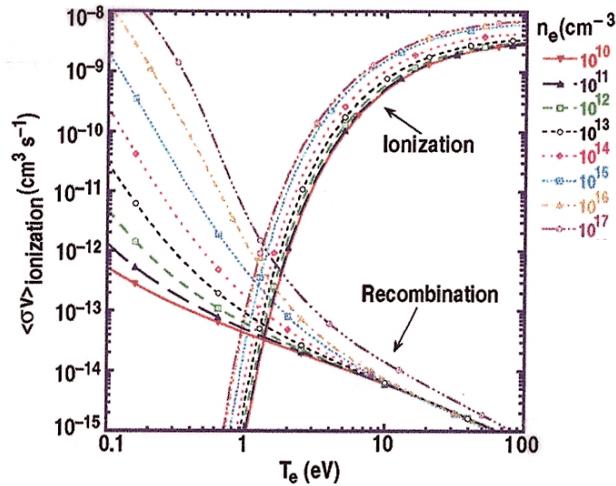


- Strong parallel transport
Fluid drifts
Actual flux surface geometry
- Non-equilibrium radiation rates
2-D flow patterns
- Neutral recycling
Recombination
Detailed divertor structures
- Erosion of surfaces
Ablation during intense heat pulses

AN EXAMPLE OF EXCELLENT AGREEMENT BETWEEN B2-E IRENE CALCULATED AND MEASURED RADIATION DISTRIBUTIONS



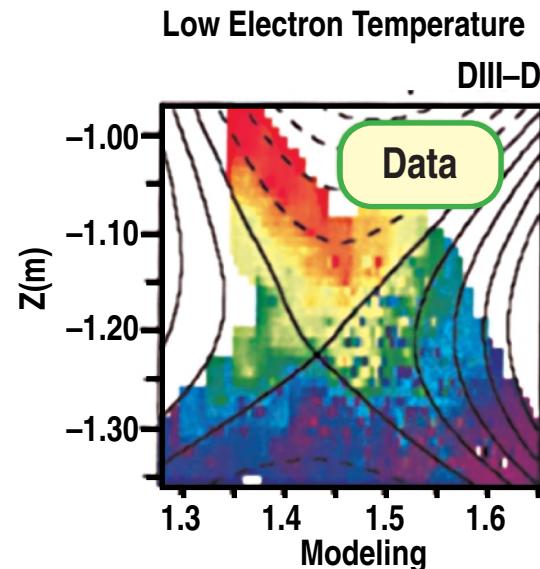
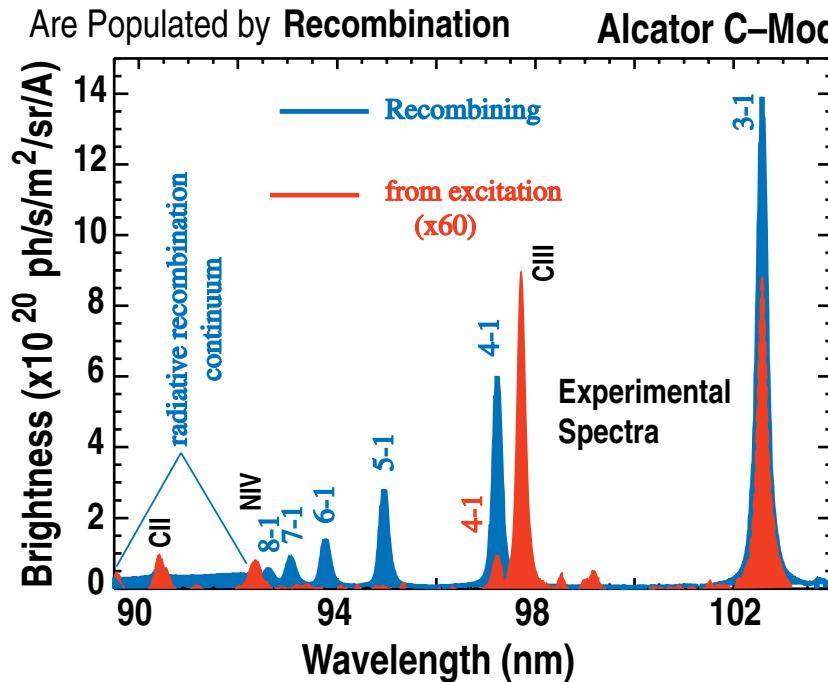
RECOMBINING DIVERTOR PLASMAS DISCOVERED



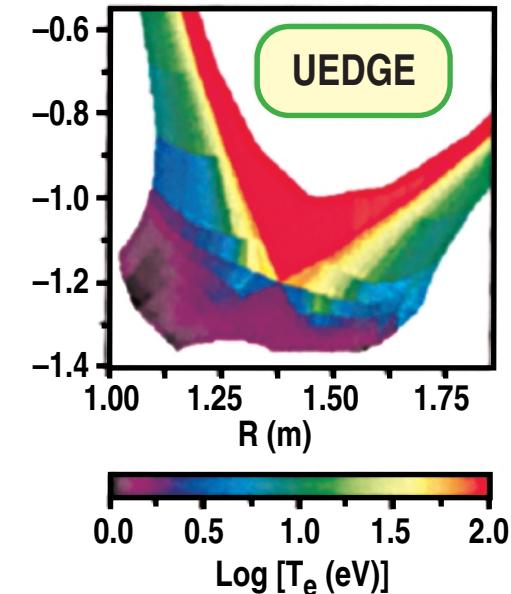
Alcator C-Mod

- $T_e \sim 1 \text{ eV}$ at divertor plate (probes)
- T_e 0.4-0.6 eV in divertor plasma (spect.)

Scaling of Lyman Series Line Intensities
Shows When the Upper Levels of the Lines
Are Populated by Recombination

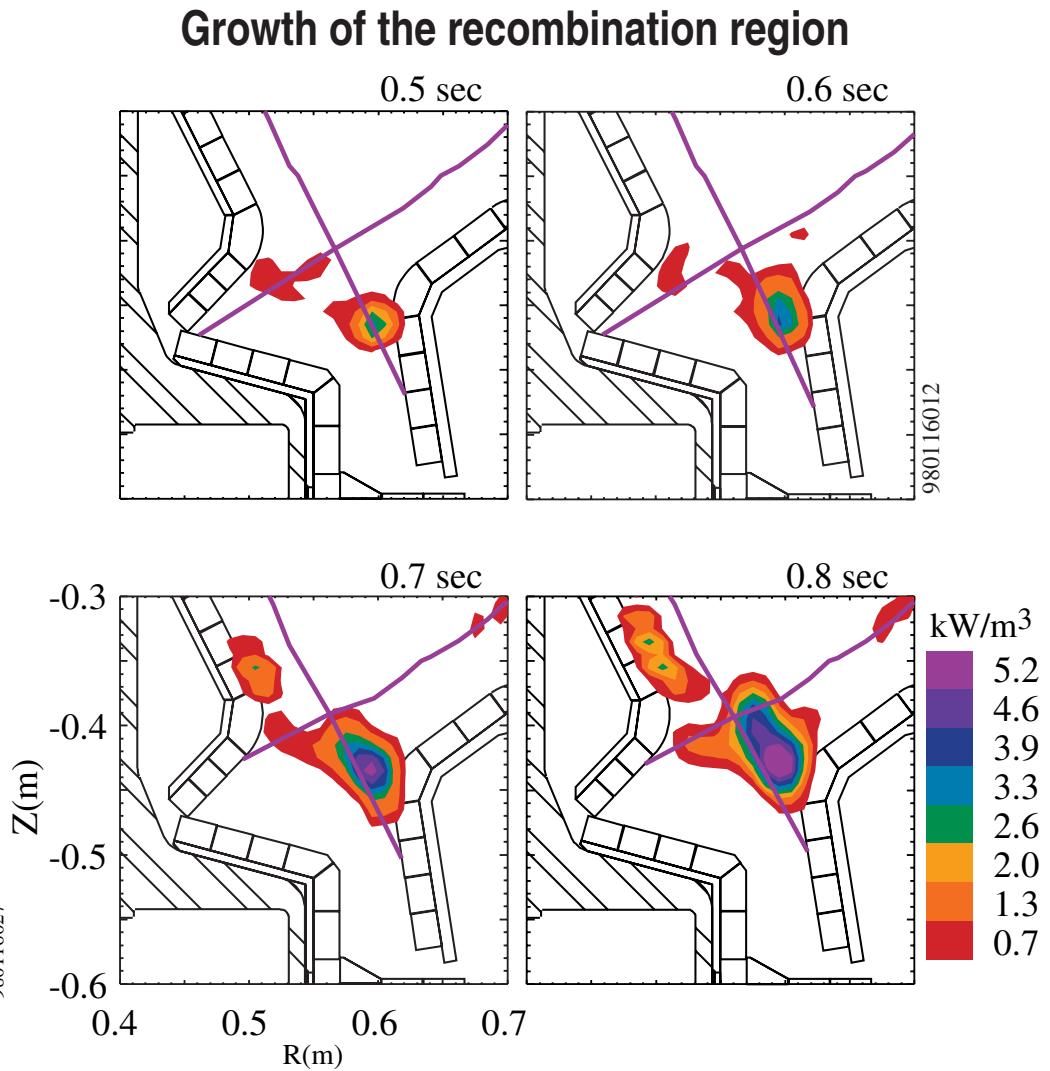
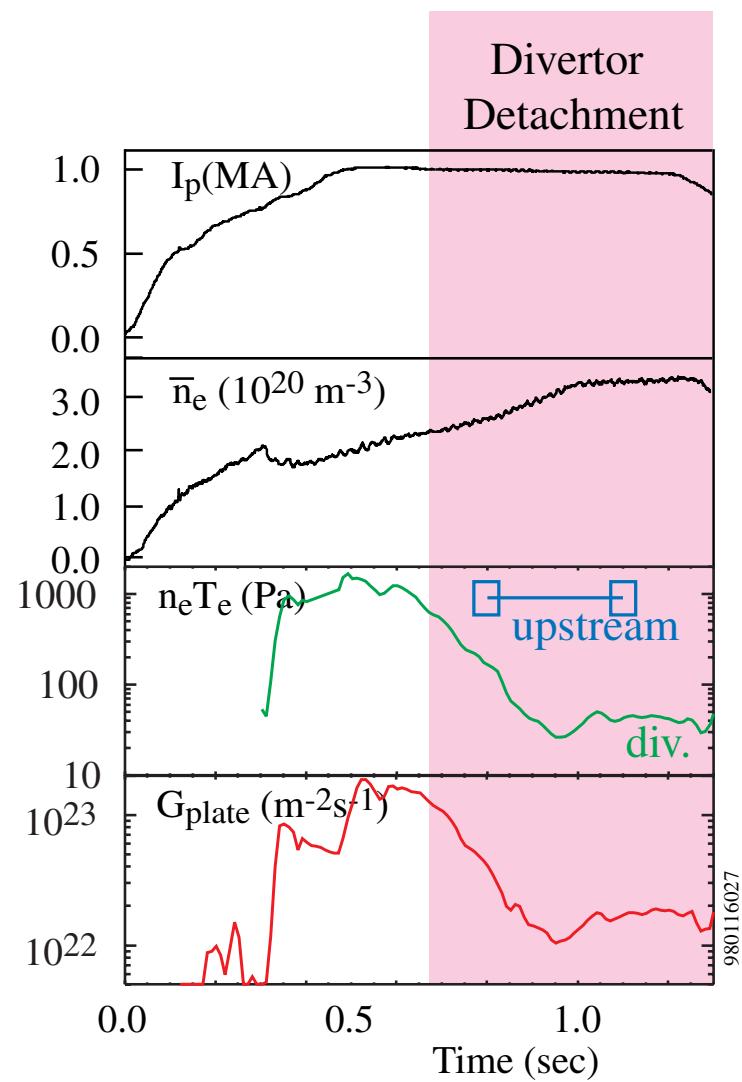


Alcator C-Mod

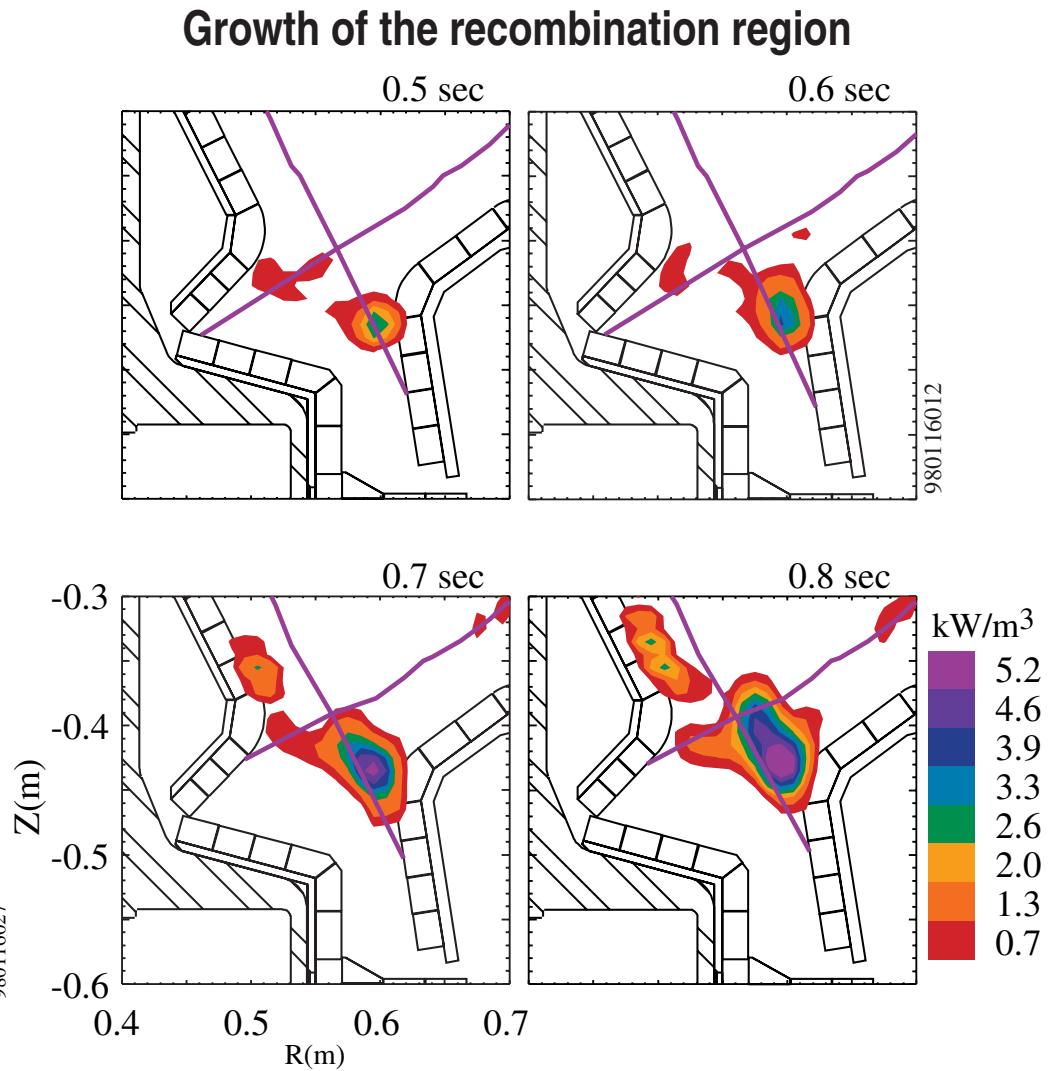
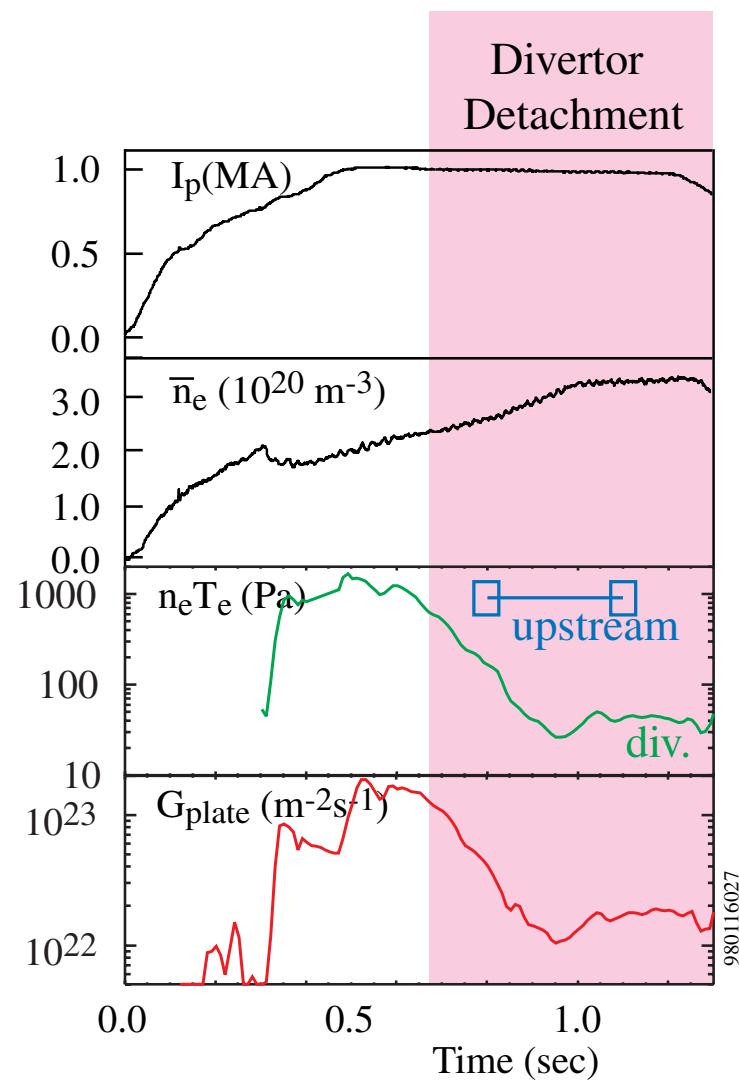


MFE—Tokamak

DIVERTOR DETACHMENT IN ALCATOR C-MOD

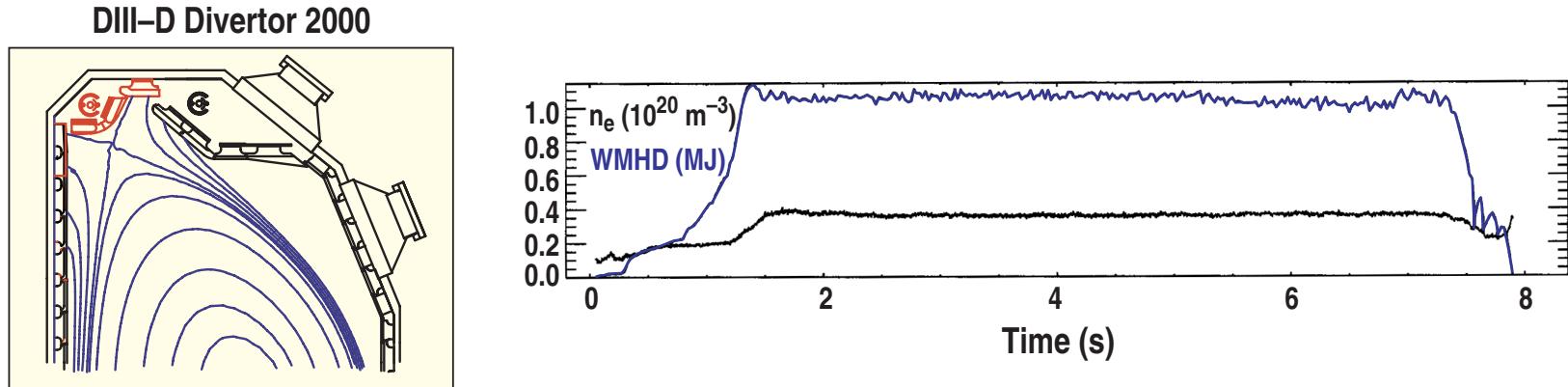


DIVERTOR DETACHMENT IN ALCATOR C-MOD

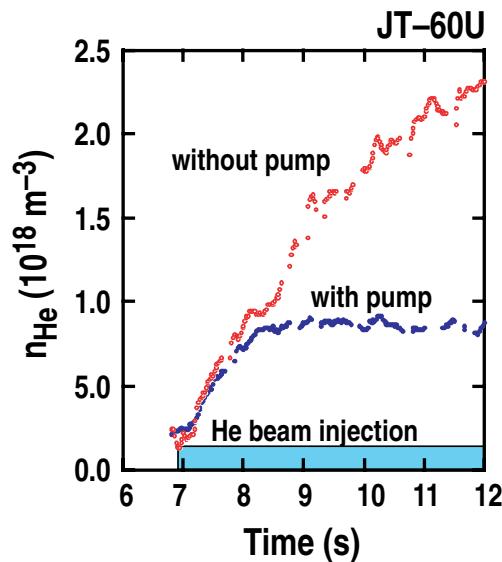


EXHAUST OF FUEL AND HELIUM ASH DEMONSTRATED

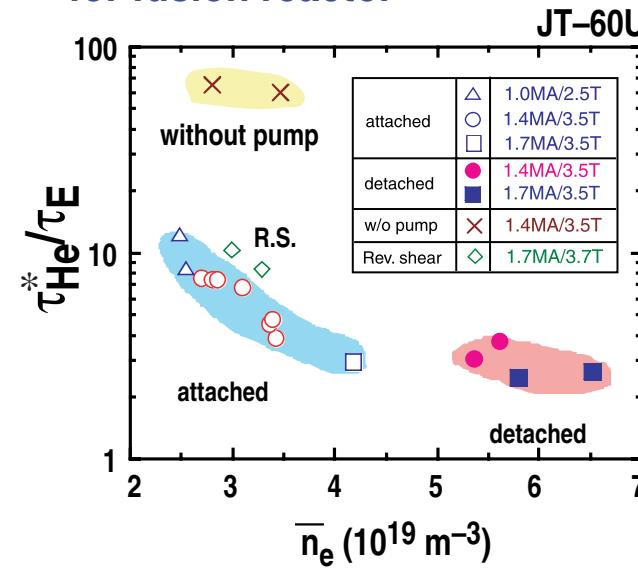
- Plasma density regulated constant by gas fueling and divertor pumping



- Divertor pumping prevents accumulation of helium ash (injected by neutral beams)

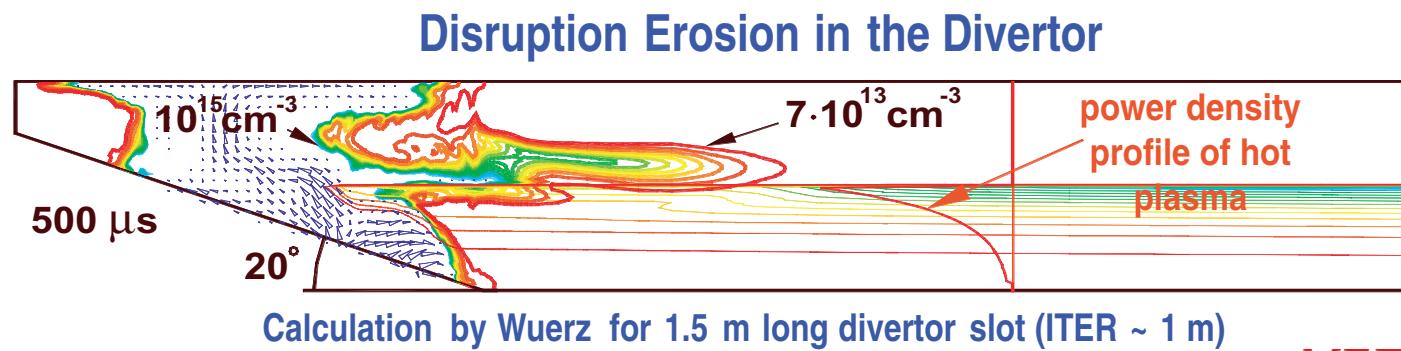
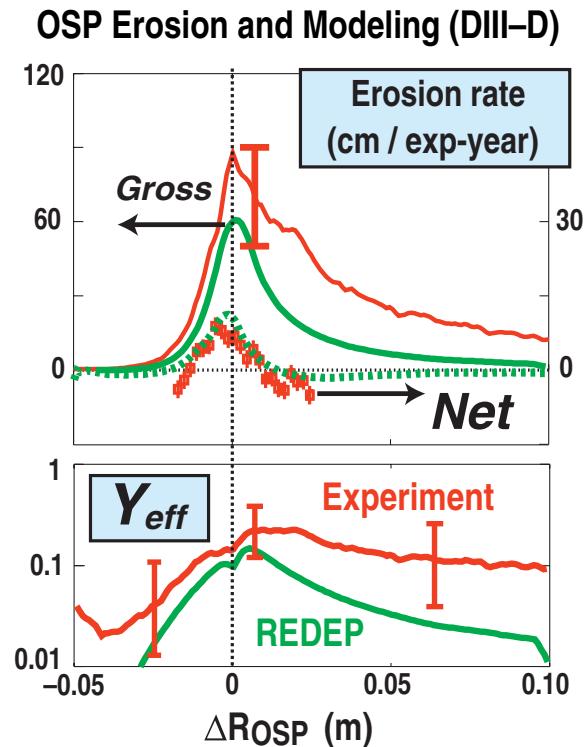


- Pumpout rate of helium adequate for fusion reactor



CODES TO CALCULATE THE EROSION OF DIVERTOR SURFACES ARE BEING TESTED AGAINST EXPERIMENTAL DATA

- Erosion during normal operation
 - REDEP matches DIII-D data for carbon
 - Treats physical and chemical sputtering and 2-D material transport
 - Codes: REDEP, WBC, ERO, DIVIMP, MCI, IMPMC
- Erosion during ablative heat pulses
 - 2-D codes treat vaporization melting vapor shield formation, radiation transport
 - Tested against plasma gas experiments
 - Codes: WURZ, LANGYEL, HASSANEIN



MFE—Tokamak

POWER AND PARTICLE EXHAUST CHALLENGES FOR THE NEXT DECADE

90s

2000 – 2010

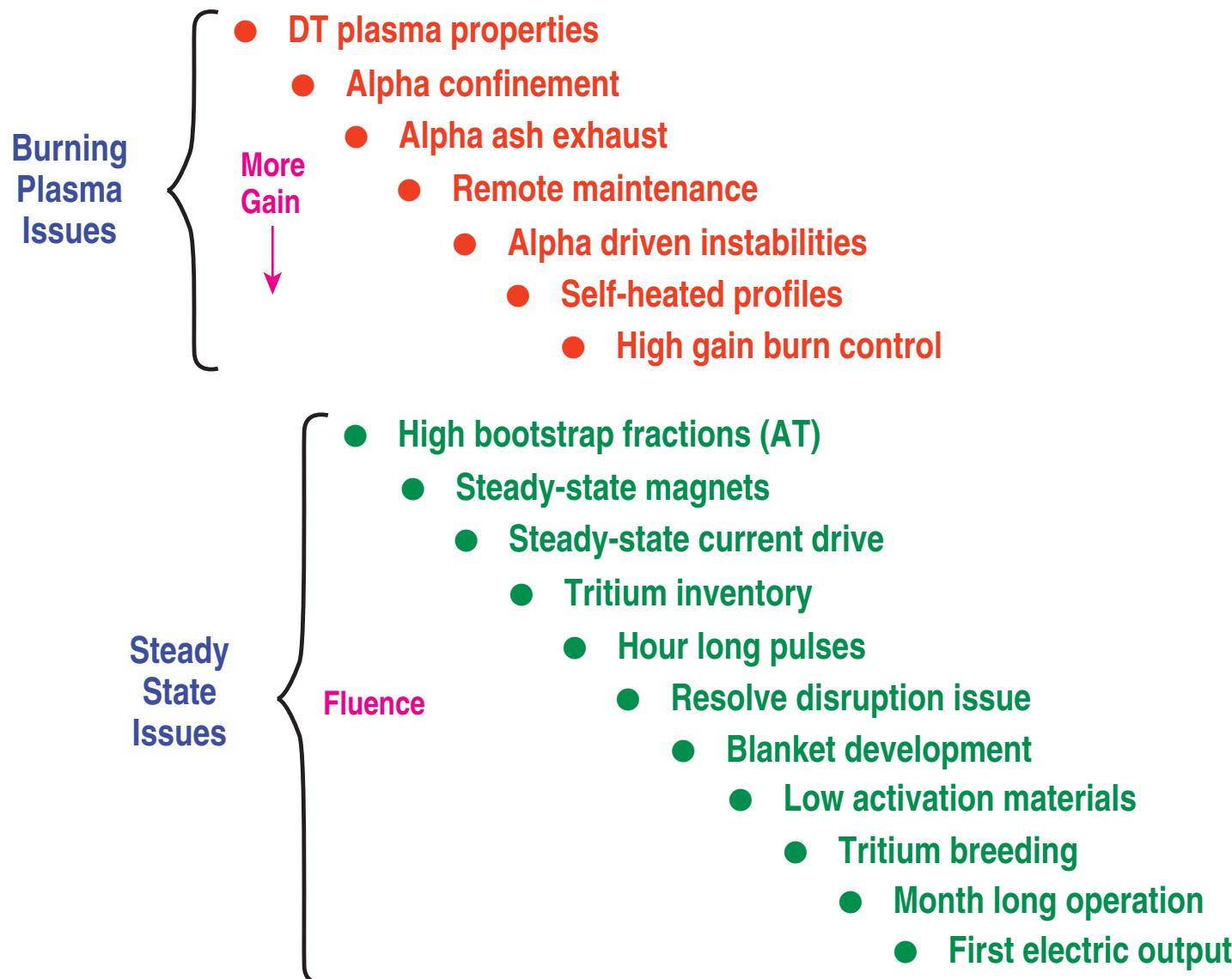
Helium ash and fuel exhaust
Radiative divertor plasmas
Recombination
2-D measurements
2-D fluid codes

Optimal plasma edge shape
2-D SOL/divertor flows
Helium and fuel exhaust in AT regimes
Use of copious core radiation
Understanding erosion and redeposition (T inventory)
Modeling and mitigating disruption erosion

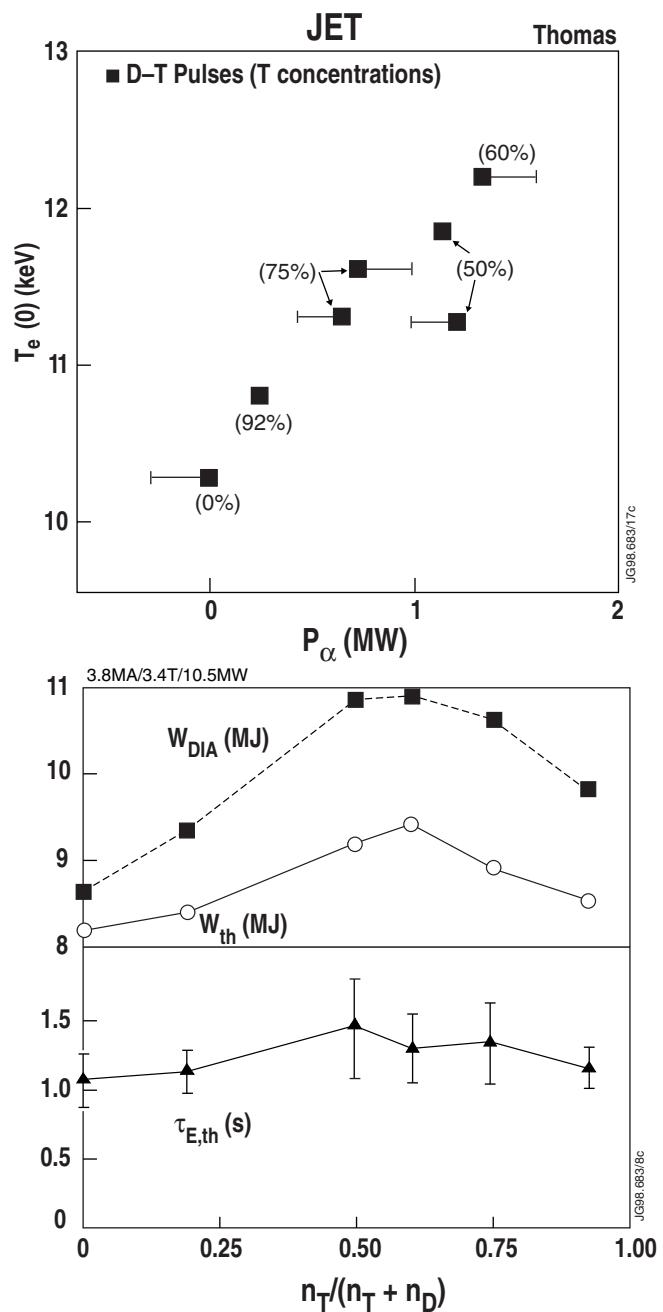
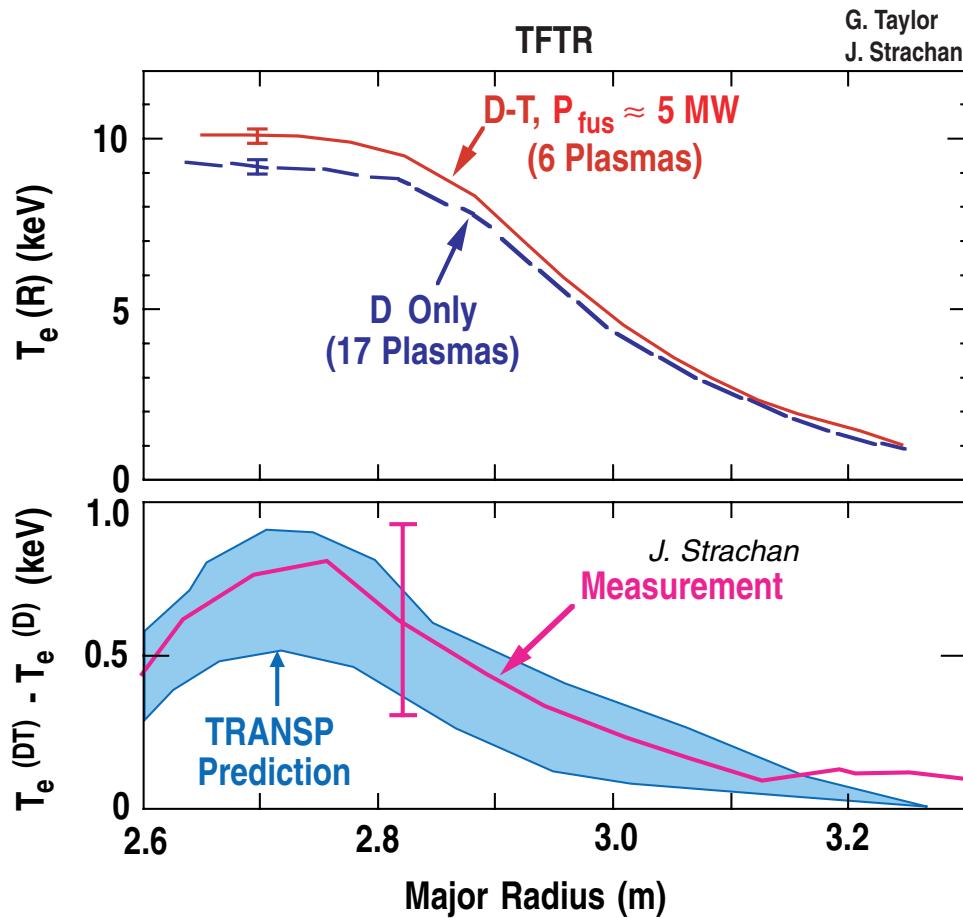
SCIENTIFIC BASIS — DEEP, EXTENSIVE, FULL OF PROMISE

Area	Status	Advanced Tokamak Challenge	Promise
Heating	Understood, technology developed	Pressure profile control, alpha heating	Burning plasmas
Current drive	Physics understood	High bootstrap fraction, local profile control	Steady-state bootstrap fraction → 100%
Stability	Operating space understood, predictable	Wall stabilization	Double the stable operating space
Confinement	Closing in on ability to calculate	Transport barrier control	Near neoclassical ion confinement
Power and particle control	Major physics elements calculable	Low density divertors compatible with current drive	Steady-state with low surface erosion

WE ARE READY TO TAKE UP BURNING PLASMA AND STEADY-STATE ISSUES

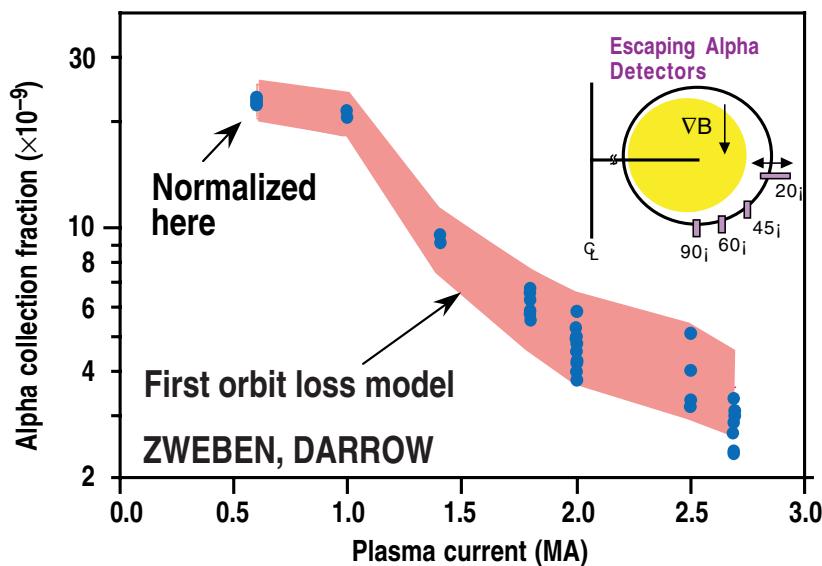


ALPHA HEATING OBSERVED

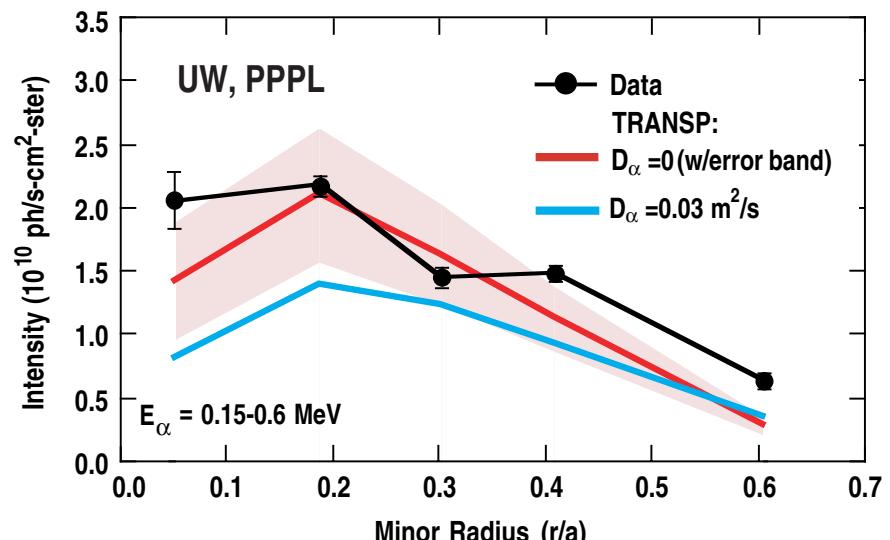


CLASSICAL ALPHA CONFINEMENT VERIFIED (TFTR)

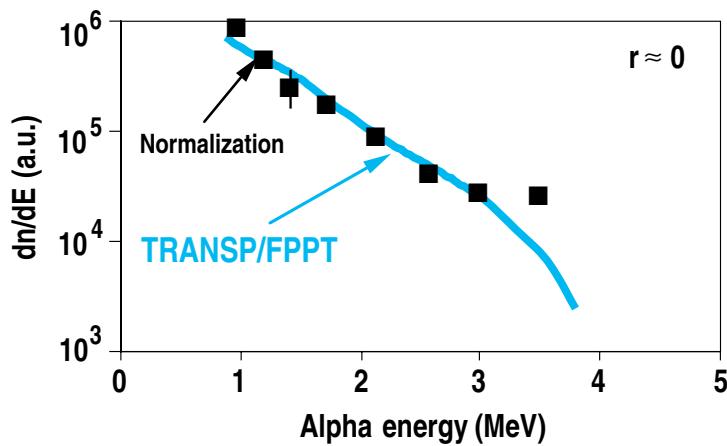
First orbit loss (3% at 2.5 MA)



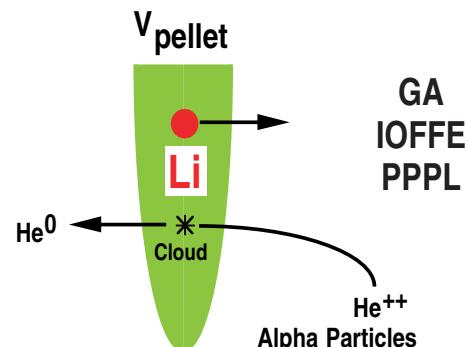
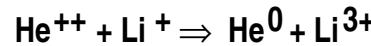
Radial transport



Slowing down spectrum



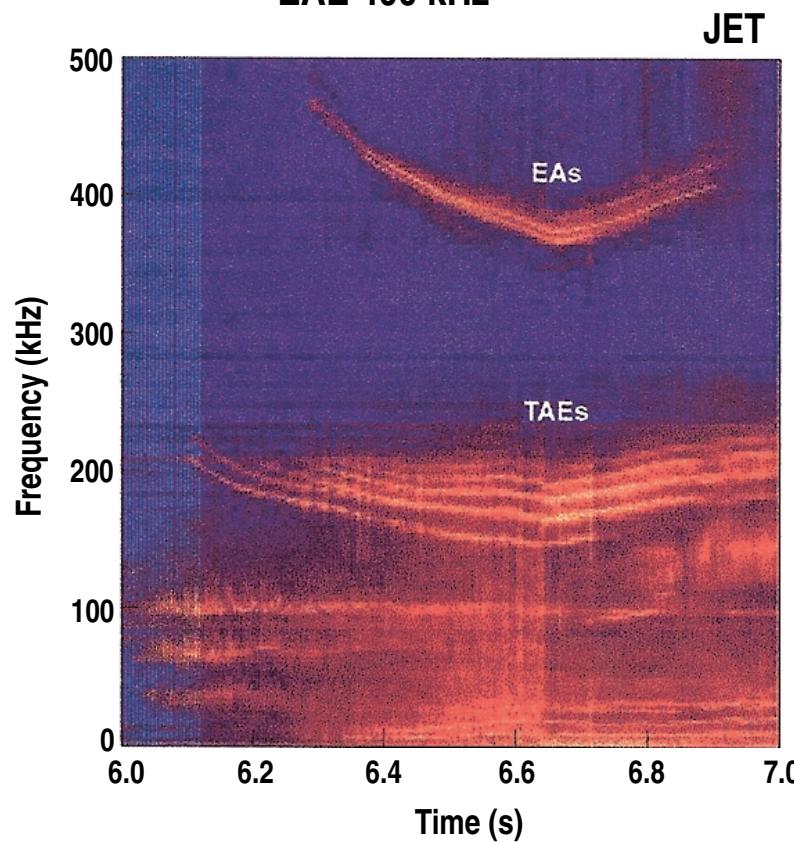
Double Charge Exchange Technique



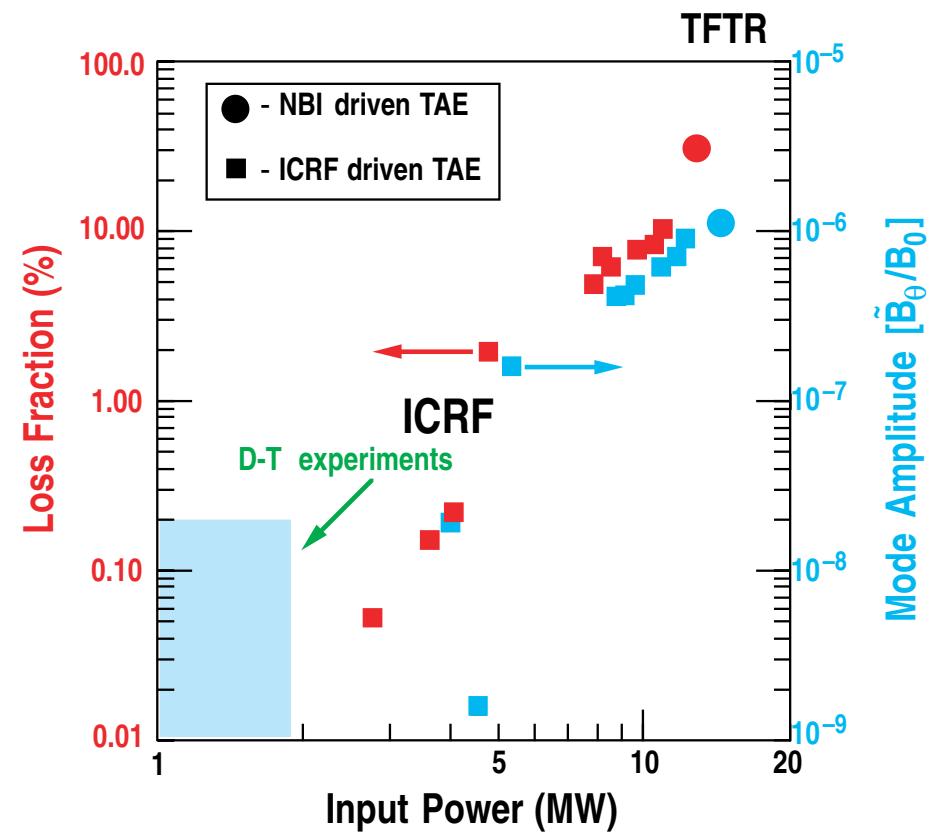
MFE—Tokamak

THEORETICALLY PREDICTED ALFVÉN EIGENMODES WERE OBSERVED

AE Modes excited in
JET by ICRH minority ions
TAE 200 kHz
EAE 400 kHz



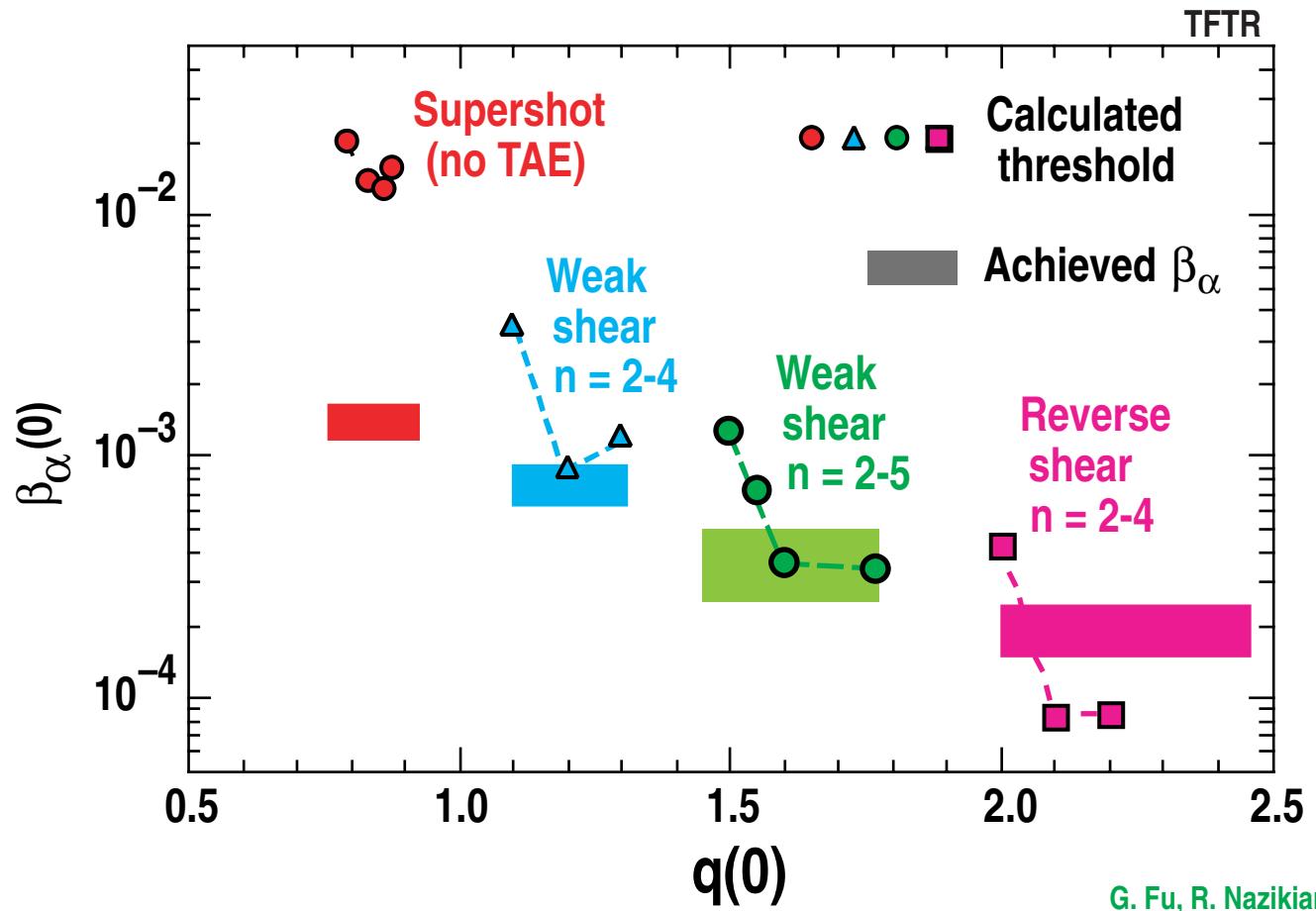
Substantial fast ion losses in TFTR
from TAE modes driven by neutral
beam or ICRF tail ions



- AE Modes absent in highest fusion power cases

MFE—Tokamak

OBSERVED α -DRIVEN TAES CONSISTENT WITH FULL LINEAR THEORY

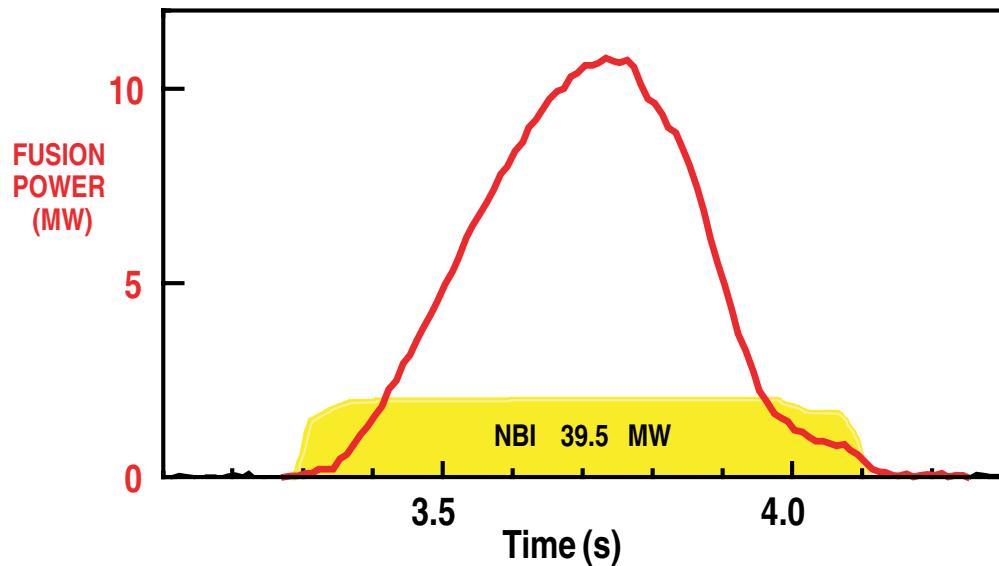


- Calculations with NOVA-K code
- Weak shear and high $q(0)$ are destabilizing
- Weak or reverse shear plasmas in a reactor may be unstable to high- n TAEs

COPIOUS FUSION POWER HAS BEEN PRODUCED

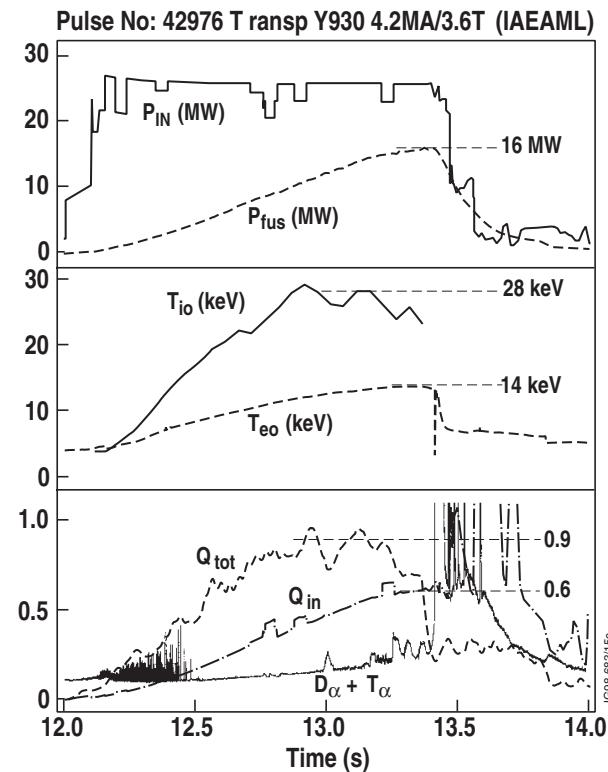
TFTR D-T Campaign

- 10.7 MW
- $P_{\text{FUSION}}/P_{\text{HEAT}} = 0.27$
- 1.55 GJ fusion energy



JET D-T Campaign

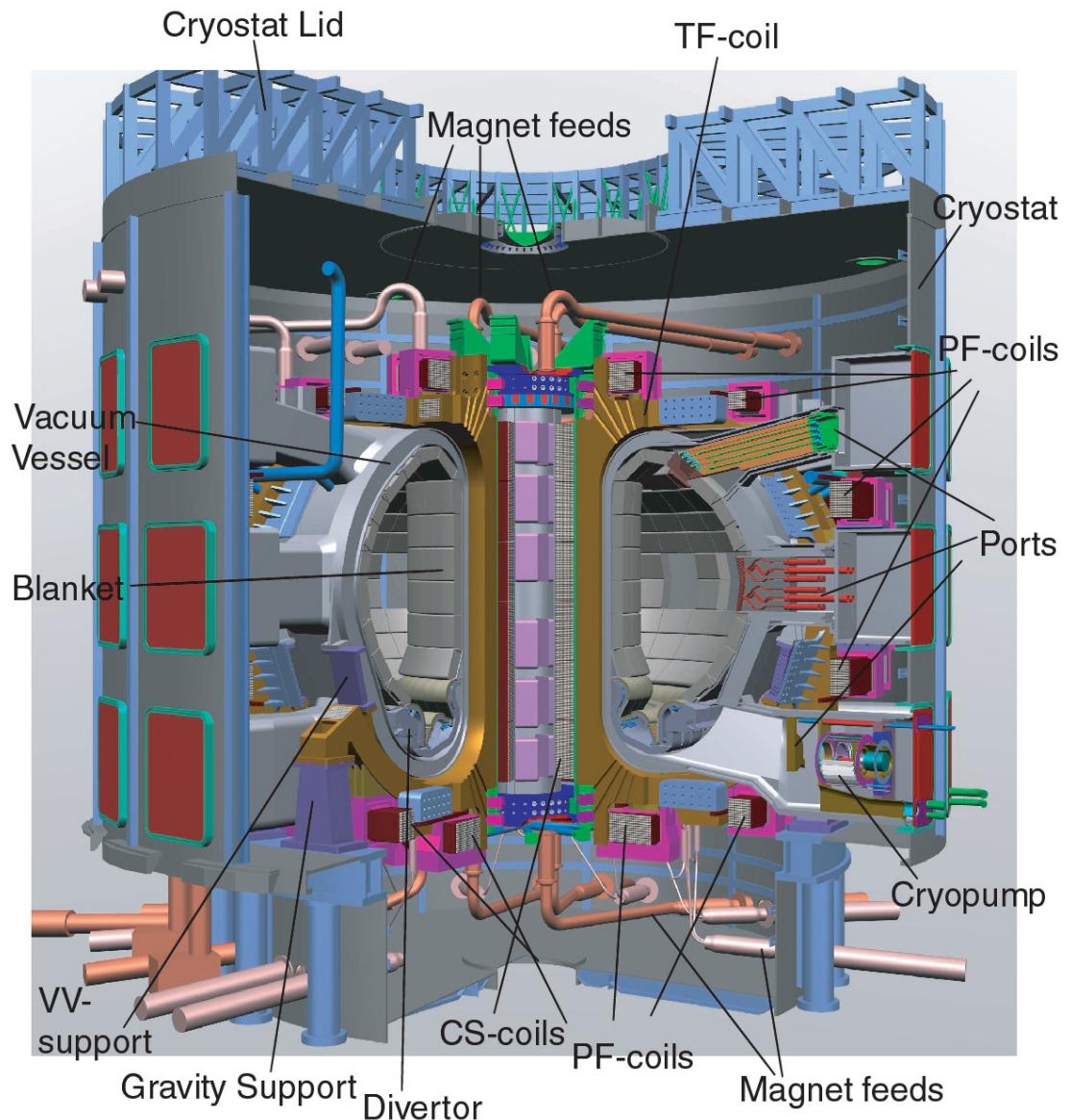
- 16 MW
- $P_{\text{FUSION}}/P_{\text{HEAT}} = 0.6$
- 0.68 GJ fusion energy





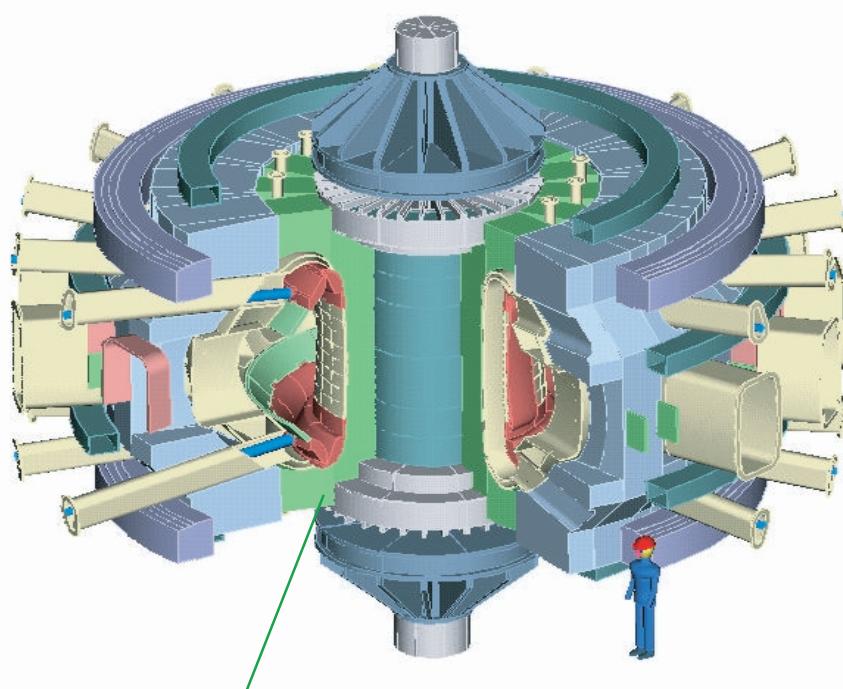
THE ITER-FEAT MACHINE

- Cut through cryostat, TF and PF coils, Vacuum Vessel, Blanket and Divertor



Fusion Ignition Research Experiment (FIRE)

<http://fire.pppl.gov>



LN BeCu ("HTS")

Design Goals

- $R = 2.0 \text{ m}$, $a = 0.525 \text{ m}$
- $B = 10 \text{ T}$, (12T) *
- $W_{\text{mag}} = 3.8 \text{ GJ}$, (5.5T) *
- $I_p = 6.5 \text{ MA}$, (7.7 MA) *
- $P_{\alpha} > P_{\text{aux}}$, $P_{\text{fusion}} < 200 \text{ MW}$
- Burn Time $\approx 18.5 \text{ s}$ ($\approx 12 \text{ s}$) *
- Tokamak Cost $\leq \$ 0.3\text{B}$
Base Project Cost $\leq \$ 1\text{B}$

* Higher Field Mode

Attain, explore, understand and optimize fusion- dominated plasmas that will provide knowledge for attractive MFE systems

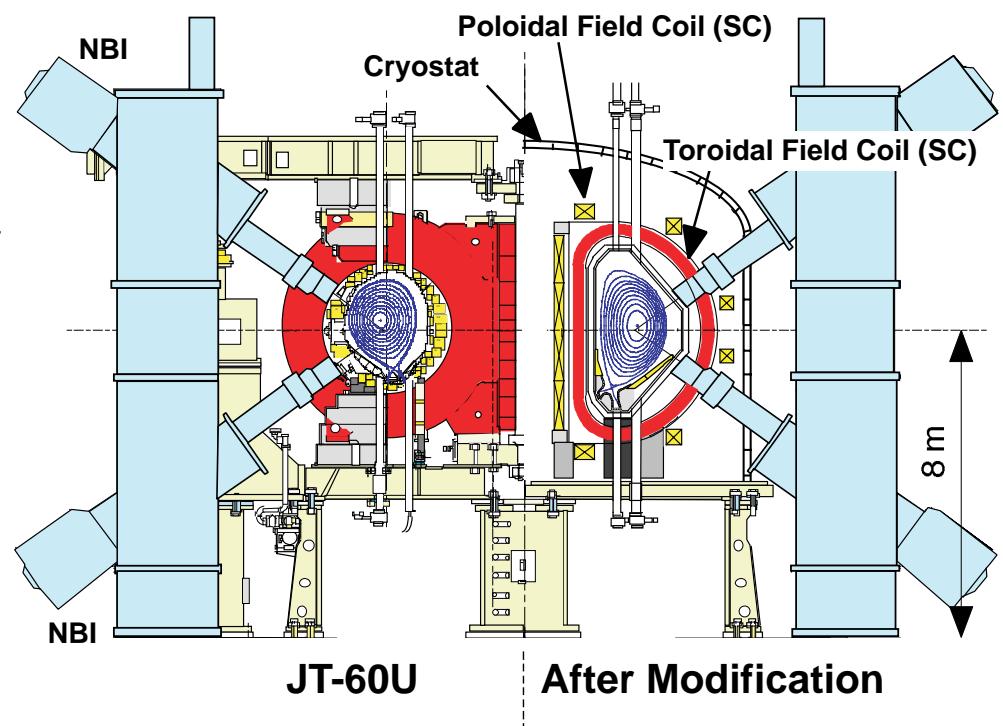
A Proposal of JT-60 Modification

JAERI

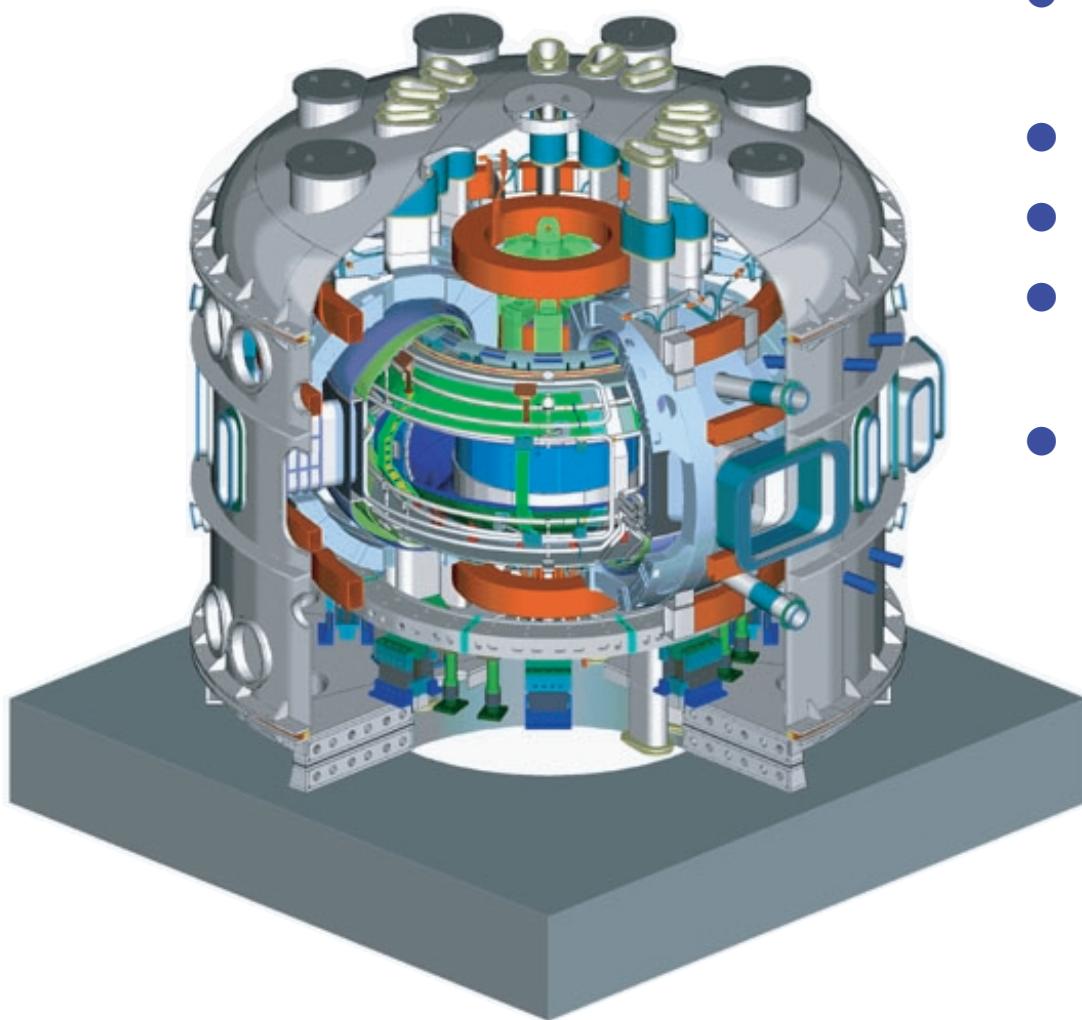
- ¥ To conduct researches on steady state operation of tokamaks
- ¥ To contribute to the ITER operation
- ¥ Under discussions at the Fusion Council

Parameter	Main Parameter		Compact ITER	
	JT-60U	JT-60 (After Modification)	Pulse	Steady-state
Pulse Length	15 s	100 s	400 s	Steady
Maximum Input Power	40 MW (10 s)	40 MW (10 s) ≥10MW (100 s)	73 MW	73MW
Plasma Current I_p	3-5 MA	4 MA	15 MA	7.8 MA
Toroidal Field B_t	4 T (at 3.4 m)	3.8 T (at 2.8 m)	5.3 T	4.98 T
Major Radius R_p	3.4 m	2.8 - 3 m (2.8 m*)	6.2 m	6.6 m
Minor Radius a_p	0.9 m	0.7-0.9 m (0.85 m*)	2.0 m	1.6 m
Elongation κ_{95}	1.8 ($\delta_{95}=0.06$)	≤1.9 (1.7*)	1.7	2.0
Triangularity δ_{95}	0.4 ($\kappa_{95}=1.33$)	≤0.45 (0.35*)	0.35	0.35
Working Gas	DD	DD	DT	DT

* Nominal Design Value



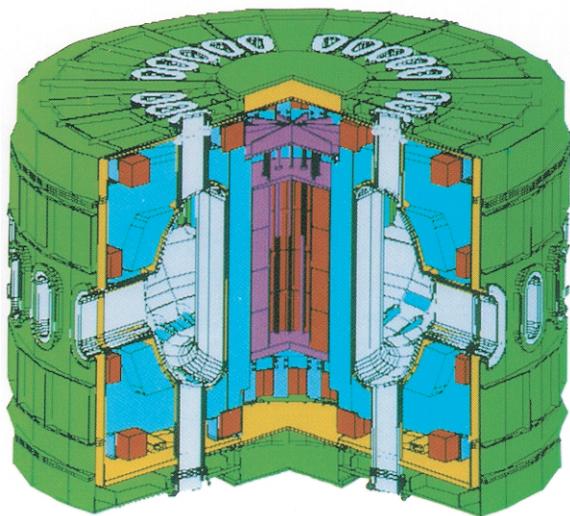
EXTENDING THE ADVANCED TOKAMAK: KSTAR



- 20–300 s pulse length (S/C technology)
- $B = 3.5 \text{ T}$, $I = 2 \text{ MA}$
- $R = 1.8 \text{ m}$, $a = 0.5 \text{ m}$
- Double-null divertor, $\kappa = 2$, $\delta = 0.8$
- 16-27 MW profile control: (neutral beam, ion cyclotron, lower hybrid)

HT-7U ADVANCED TOKAMAK – HAFEI CHINA INSTITUTE OF PLASMA PHYSICS ACADEMIA SINICA

HT-7U



Construction: Approved
Completion: mid 2003

$R/a = 1.7/0.4$ m
 $B = 3.5$ T
 $I = 1$ MA
 $\kappa = 1.6\text{--}2.0$
 $\delta = 0.4\text{--}0.8$

ASIPP



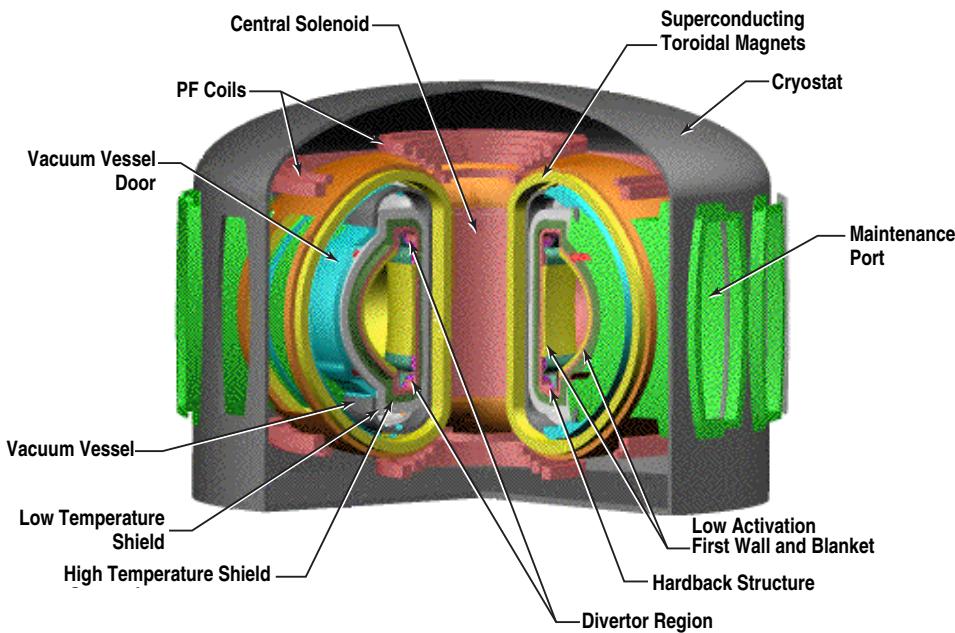
HT-7



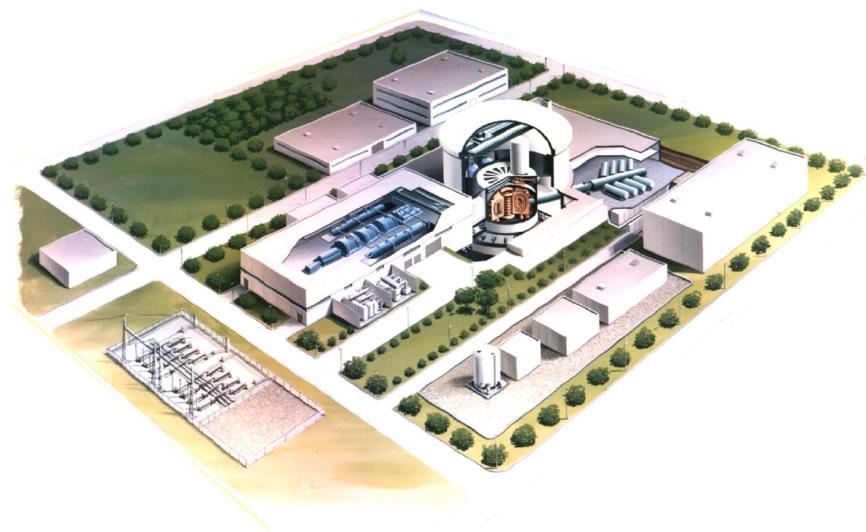
MFE—Tokamak

THE ADVANCED TOKAMAK LEADS TO AN ATTRACTIVE FUSION POWER PLANT

● The U.S. ARIES — RS system study



● The Japanese SSTR system study



● Attractive features

- Competitive cost-of-electricity
- Steady-state operation
- Maintainability
- Low-level waste
- Public and worker safety

	Conventional	AT
Size, major radius (m)	8	5
COE ¢/kWhr	~13	~7
Power cycle	Pulsed	Steady state

MFE-Tokamaks

SUMMARY

- Research in the tokamak has greatly advanced fusion energy science
- Tokamak research has shown fusion energy is feasible in the laboratory
- The tokamak is scientifically and technically ready to proceed to burning plasma and/or steady-state next steps
- Advanced Tokamak research seeks to find the ultimate potential of the tokamak as a magnetic confinement configuration
 - Anticipated results point to practical and attractive fusion energy