

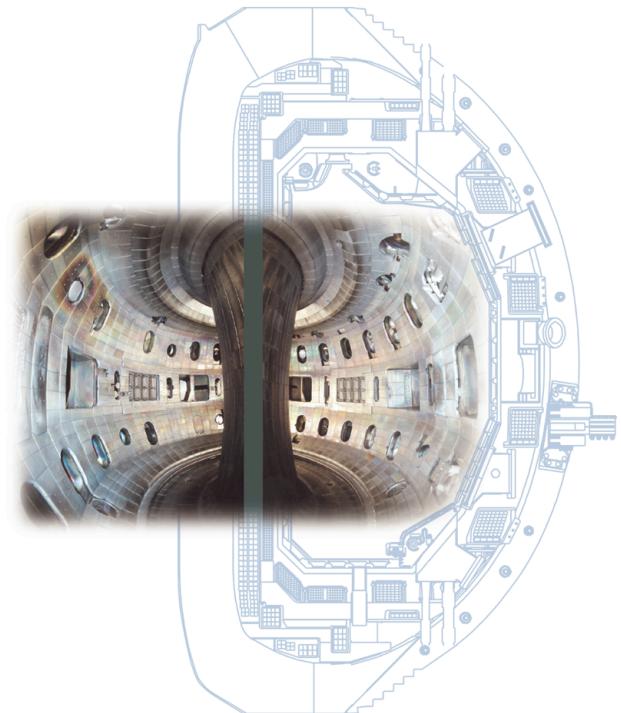
# **Poloidal Velocity of Impurity Ions in Neoclassical Theory**

**by**

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## Background

- Recent measurement of C<sup>+6</sup> poloidal velocity disagrees with NCLASS in magnitude and direction
- Toroidal velocity of C<sup>+6</sup> is close to its thermal velocity, violating the assumption of NCLASS
- Theoretical uncertainty can arise from different calculations in neoclassical theory

## Goals

- Calculate analytically poloidal velocities in a two-ion species plasma **with large toroidal flows** in the banana regime, with boundary layer correction
- Implement the moment approach of Hirshman-Sigmar for a two-ion species plasma
- Compare analytic theory, Hinton-Moore's numerical work, and the moment approach
- Compare with measurements in DIII-D

# Large Flow Equilibrium

- Circular, large aspect ratio flux surfaces ( $\delta = r/R \ll 1$ )  $B_\theta/B \ll 1$
- To leading order in gyro-radius/scale length expansion, ions share common toroidal (parallel) flow, rigid on each flux surface, related to radial electric field  $U = E_r/B_\theta$
- Temperatures are flux functions. Centrifugal force leads to poloidal variations of electric potential and densities:

$$\frac{e\tilde{\phi}_1}{T_e} = \delta X_e \cos\theta \quad \frac{\tilde{n}_a}{n_a} = \delta X_a \cos\theta \quad X_e = \frac{\sum_a Z_a m_a n_a U^2}{n_e T + \sum_a Z_a^2 n_a T_e} \quad X_a = \frac{m_a U^2}{T} - \frac{Z_a T_e}{T} X_e$$

- Perpendicular flow is sum of ExB and diamagnetic flows:

$$u_{a\perp} = -\frac{E_r}{B_\zeta} + \frac{T}{Z_a e B_\zeta} \frac{p'_a}{p_a}$$

# Linearized Drift Kinetic Equation

- First order parallel flow is obtained from LDKE
- Written in frame rotating with a flux surface
- Guiding center drifts:  $E \times B$ ,  $\text{grad}B/\text{curvature}$ , inertial forces
- Total energy: kinetic, electrostatic, and centrifugal
- Two classes of particles:

**Slow:**

$$\xi = v_{\parallel} / v \sim \sqrt{\delta}$$

**Freely circulating:**

$$\xi \sim 1$$

# Localization Approximation

- Introduce shifted distribution function where  $u_{\parallel}$  is common to all ions

$$f_{a1} = \frac{m_a v_{\parallel} u_{\parallel}}{T} f_{a0} + \frac{Z_a e \phi_1}{T} f_{a0} + f'_{a1}$$

- Assume:

freely circulating ions:  $f'_{a1} \sim \sqrt{\delta}$  slow ions:

$$\frac{\partial f'_{a1}}{\partial \xi} \sim 1 \quad \frac{\partial^2 f'_{a1}}{\partial \xi^2} \sim \frac{1}{\sqrt{\delta}}$$

- LDKE for slow ions is simplified:

G.C. drifts:  $\mathbf{E} \times \mathbf{B}$ , grad  $B$ , centrifugal force

Conservation of total energy  $\varepsilon_a$  leads to  $\xi^2 = 1 - \mu B_0 / \varepsilon_a + \delta_a \cos \theta$

where  $\delta_a = \delta \left( 1 + \frac{2TX_a}{m_a v^2} \right)$

is effective trapping factor

- Fokker-Planck operator can be replaced by  $\frac{v_a}{2} \frac{\partial^2 f'_{a1}}{\partial \xi^2}$  LDKE is

$$v_{\parallel} \frac{\Theta}{r} \left( \frac{\partial f'_{a1}}{\partial \theta} \right)_{\varepsilon_a, \mu} - \frac{v_a}{2} \left( \frac{\partial^2 f'_{a1}}{\partial \xi^2} \right)_v = \delta_a \sin \theta \frac{m_a v^2}{2T} \left[ u_{\parallel} \Theta + \frac{T}{Z_a e B_{\xi}} \left( \frac{n'_a}{n_a} + \frac{\overline{m_a v^2}}{2T} - \frac{3}{2} \frac{T'}{T} \right) \right] f_{a0}$$

# Banana Regime

- Introduce scaled variables  $\xi_* = \xi / \sqrt{\delta_a}$  and scaled distribution function  $g_a$

$$f'_a = \sqrt{\delta_a} g_a \frac{m_a v}{T} \left[ u_{\parallel} + \text{sgn}(B_{\xi}) \frac{T}{Z_a e B_{\theta}} \left( \frac{n'_a}{n_a} + \frac{\overline{m_a v^2}}{2T} - \frac{3}{2} \frac{T'}{T} \right) \right] f_{a0}$$

It follows:  $\xi_* \frac{\partial g_a}{\partial \theta} - \frac{\sin \theta}{2} \frac{\partial g_a}{\partial \xi_*} - \frac{v_{a*}}{2} \frac{\partial^2 g_a}{\partial \xi_*^2} = \frac{\sin \theta}{2}$  where  $v_{a*} = v_a (\Theta v / r)^{-1} \delta_a^{-3/2}$

- Solution in banana regime has asymptotic behavior

$$g_a \approx \mp 0.98 \left( 1 - 0.92 \sqrt{|v_{a*}|} \right) \quad \xi_* \rightarrow \pm \infty$$

- Particle flux can be calculated by flux-friction relation

$$Z_a e B_{\theta} \Gamma_a = \text{sgn}(B_{\xi}) \int \frac{d\theta}{2\pi} \int d^3 v m_a v_{\parallel} C_a(f_1)$$

- Integral is dominated by slow ions and can be evaluated using the asymptotic behavior

# Ambipolarity and Common Parallel Flow

- The main ion flux is (similarly for impurity ions)

$$-Z_i e B_\theta \Gamma_i = 2.94 \sqrt{\delta} \frac{m_i^{3/4} m_I^{1/2} n_i}{\tau_{il}} \left\{ k_{i0} \left[ \operatorname{sgn}(B_\xi) u_\parallel + \frac{T}{Z_a e B_\theta} \left( \frac{n'_a}{n_a} - \frac{3}{2} \frac{T'}{T} \right) \right] + k_{i1} \frac{T}{Z_a e B_\theta} \frac{T'}{T} \right\}$$

$$k_{in} = \frac{1}{\alpha \sqrt{\rho}} \int_0^\infty dx \frac{e^{-x^2} x^{2n+1} [G(x) + \alpha G'(\rho x)] (1 + X_i/x^2)^{1/2}}{1 + 0.89 \sqrt{v_{*_i}} \left\{ [G(x) + \alpha G'(\rho x)] / \left[ x^4 (1 + X_i/x^2)^{3/2} \right] \right\}^{1/2}}$$

$$G'(x) = (1 - 0.5/x^2) (2/\sqrt{\pi}) \int_0^x e^{-y^2} dy + e^{-x^2}/\sqrt{\pi} x \quad \rho = \sqrt{m_I/m_i} \quad \alpha = Z_I^2 n_I / Z_i^2 n_i$$

- The common flow  $u_\parallel$  is obtained from ambipolarity, with the result

$$u_\parallel = -\frac{T}{e B_\theta} \frac{\operatorname{sgn}(B_\xi)}{k_{i0} + k_{I0}} \left[ \frac{k_{i0}}{Z_i} \left( \frac{n'_i}{n_i} - \frac{3}{2} \frac{T'}{T} \right) + \frac{k_{I0}}{Z_I} \left( \frac{n'_I}{n_I} - \frac{3}{2} \frac{T'}{T} \right) + \left( \frac{k_{i1}}{Z_i} + \frac{k_{I1}}{Z_I} \right) \frac{T'}{T} \right]$$

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# Impurity Ion Poloidal Velocity

- Combining parallel and perpendicular flows yields poloidal velocity of impurity ions:

$$u_{I\theta} = \frac{T}{eB_\xi} \left[ c_1 \left( \frac{1}{Z_i} \frac{n'_i}{n_i} - \frac{1}{Z_I} \frac{n'_I}{n_I} \right) + \left( \frac{c_2}{Z_i} + \frac{c_3}{Z_I} \right) \frac{T'}{T} \right]$$

$$c_1 = -k_{i0}/(k_{i0} + k_{I0}) \quad c_2 = -(k_{i1} - 3k_{i0}/2)/(k_{i0} + k_{I0}) \quad c_3 = 1 - (k_{I1} - 3k_{I0}/2)/(k_{i0} + k_{I0})$$

- Hinton-Moore's results (weak toroidal rotation) take the same form except  $k_{ai}$  are replaced by

$$k_{i0}^{HM} = \frac{1}{2\alpha\sqrt{\rho}} \frac{F_{11}(1) + \alpha F_{11}(\rho)}{1 + 1.26\bar{v}_{i^*}[F_{11}(1) + \alpha F_{11}(\rho)]} \quad k_{i1}^{HM} = \frac{1}{2\alpha\sqrt{\rho}} \frac{F_{12}(1) + \alpha F_{12}(\rho)}{1 + 0.37\bar{v}_{i^*}[F_{12}(1) + \alpha F_{12}(\rho)]}$$

$$F_{11}(\rho) = \frac{\sqrt{1+\rho^2}}{\rho} - \frac{1}{\rho^2} \ln\left(\rho + \sqrt{1+\rho^2}\right)$$

$$F_{12}(\rho) = \frac{\rho}{\sqrt{1+\rho^2}}$$

# The Moment Approach

- **The basic equations**  $\langle \vec{B} \cdot \nabla \vec{\Pi}_a \rangle = \langle BF_{a0} \rangle$   $\langle \vec{B} \cdot \nabla \vec{Q}_a \rangle = \langle BF_{a1} \rangle$   
are the same as flux-friction relations when  $\delta$  is small:

$$Z_a e B_\theta \Gamma_a = \text{sgn}(B_\xi) \int \frac{d\theta}{2\pi} \int d^3 v m_a v_\parallel C_a(f_1) \quad -Z_a e B_\theta Q_a / T = \text{sgn}(B_\xi) \int \frac{d\theta}{2\pi} \int d^3 v m_a v_\parallel (m_a v^2 / 2T - 5/2) C_a(f_1)$$

- LDKE implies relations between poloidal and parallel flows:

$$u_{a\theta} = u_{a\parallel} \Theta - \frac{E_r}{B_\xi} + \frac{T}{Z_a e B_\xi} \frac{p'_a}{p_a} \quad \frac{2q_{a\theta}}{5p_a} = \frac{2q_{a\parallel}}{5p_a} \Theta + \frac{T}{Z_a e B_\xi} \frac{T'}{T}$$

- First assumption: friction integrals can be calculated using

$$f_{a1} = \left( m_a v_\parallel / T \right) \left[ u_{a\parallel} + \left( m_a v^2 / 2T - 5/2 \right) \left( 2q_{a\parallel} / 5p_a \right) \right] f_{a0}$$

- Second assumption: radial fluxes are related to poloidal flows:

$$-Z_i e B_\theta \Gamma_i = 2f_t \frac{m_i^{3/4} m_I^{1/2} n_i}{\tau_{il} \Theta} \left[ k_{i0}^{HS} u_{i\theta} + \left( k_{il}^{HS} - \frac{5}{2} k_{i0}^{HS} \right) \frac{2q_{i\theta}}{5p_i} \right]$$

$$-Z_i e B_\theta Q_i / T = 2f_t \frac{m_i^{3/4} m_I^{1/2} n_i}{\tau_{il} \Theta} \left[ \left( k_{il}^{HS} - \frac{5}{2} k_{i0}^{HS} \right) u_{i\theta} + \left( k_{i2}^{HS} - 5k_{il}^{HS} + \frac{25}{4} k_{i0}^{HS} \right) \frac{2q_{i\theta}}{5p_i} \right]$$

## The Moment Approach (Continued)

- The “viscosity coefficients”  $k^{HS}$  are obtained by examining the manner of solution of the LDKE

$$k_{in}^{HS} = \frac{1}{\sqrt{\alpha\rho}} \int_0^{\infty} dx \frac{e^{-x^2} x^{2n+1} [G'(x) + \alpha G'(\rho x)]}{D_1 D_2}$$

$$D_1 = 1 + 2.33 \bar{V}_{i^*} \frac{G'(x) + \alpha G'(\rho x)}{x^4} \quad D_2 = 1 + 1.85 \frac{qR}{\sqrt{T/m_i \tau_{ii}}} \frac{H(1, x) + \alpha H(\rho, x)}{x^4}$$

$$H(\rho, x) = \left[ 3 + \frac{2}{\rho^2} - \frac{3}{2(\rho x)^2} \right] \frac{2}{\sqrt{\pi}} \int_0^x e^{-y^2} dy + \left[ \frac{3}{\rho x} - 4 \left( 1 + \frac{1}{\rho^2} \right) \rho x \right] \frac{e^{-\rho^2 x^2}}{\sqrt{\pi}}$$

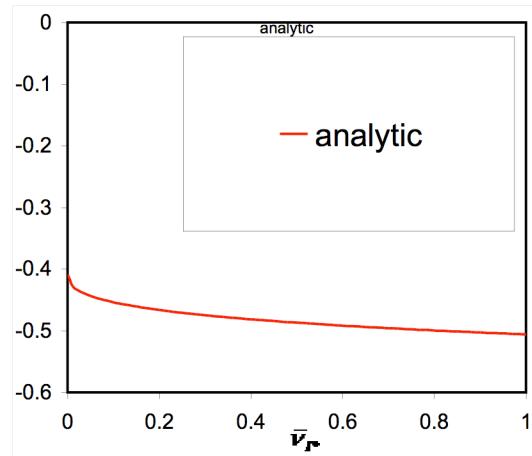
- Solve four linear equations for  $u_{i\parallel}$ ,  $2q_{i\parallel}/5p_i$ ,  $u_{I\parallel}$ ,  $2q_{I\parallel}/5p_I$

from which  $c_1$   $c_2$   $c_3$  can be found

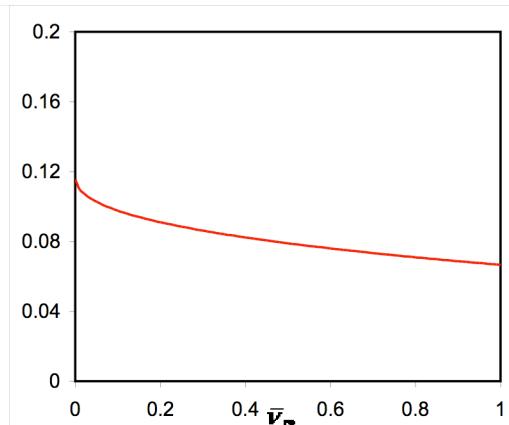
# Comparing Calculations (Weak Rotation)

- **Parameters chosen:**  $Z_I^2 n_I / Z_i^2 n_i = 1$     $m_I / m_i = 6$     $\bar{v}_{i^*} = 0$
- **Significant differences exist**
- **Moment approach depends on**  $\delta$

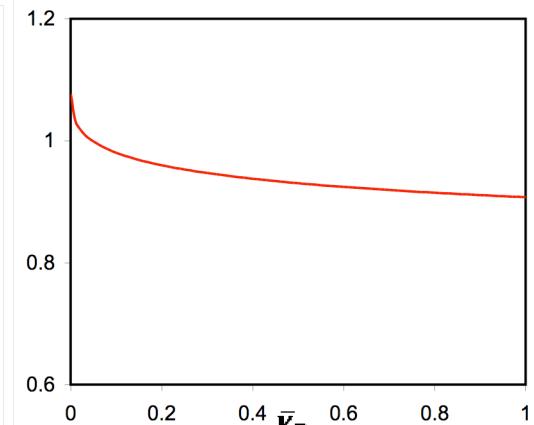
**C<sub>1</sub>**



**C<sub>2</sub>**



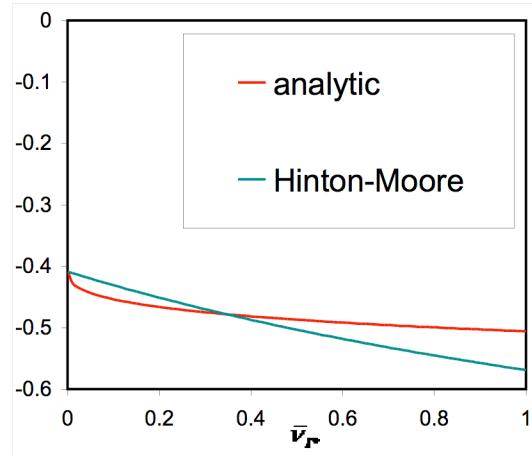
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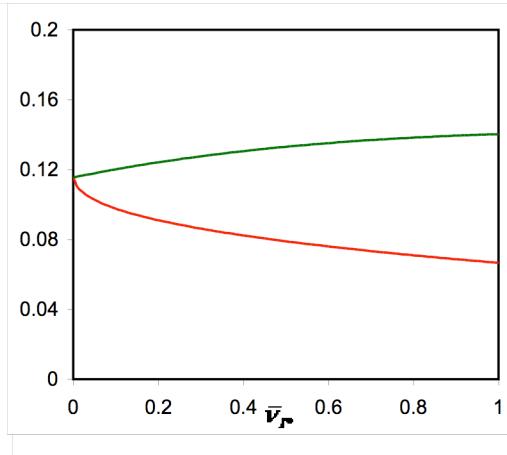
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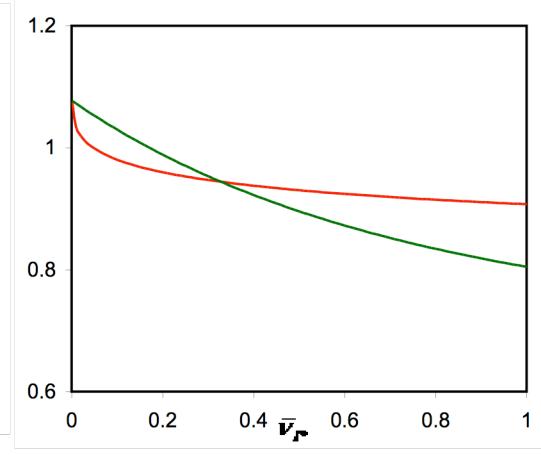
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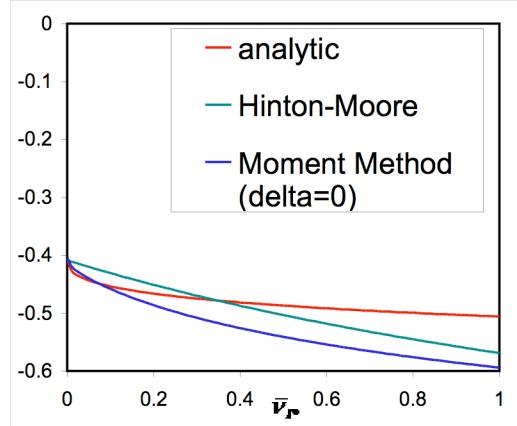
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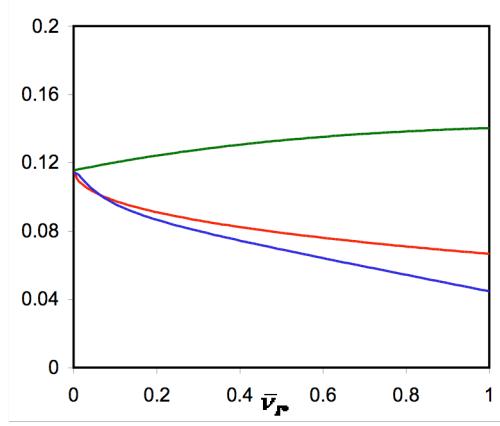
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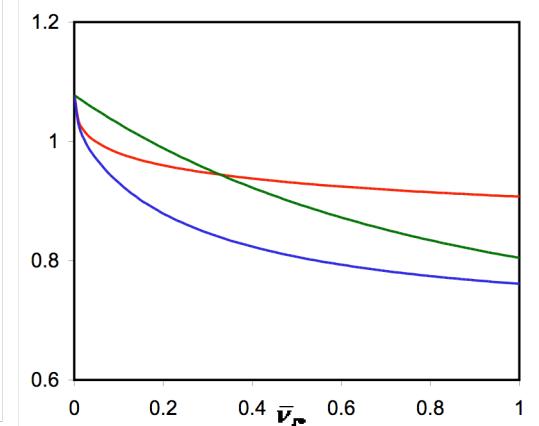
**C<sub>1</sub>**



**C<sub>2</sub>**

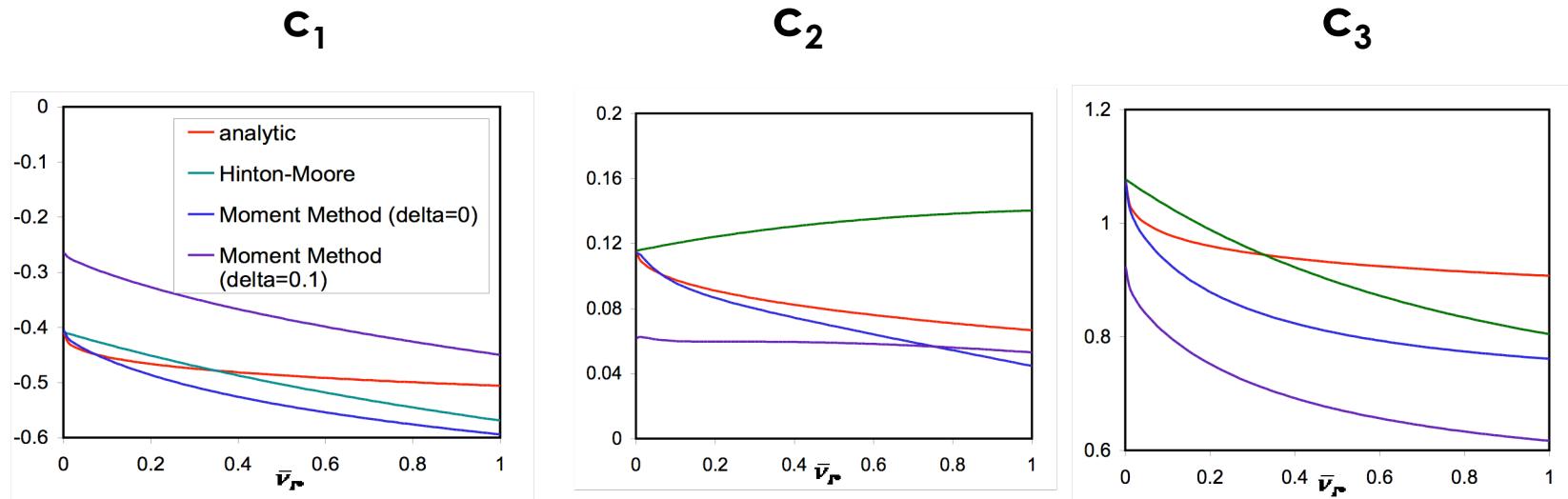


**C<sub>3</sub>**



# Comparing Calculations (Weak Rotation)

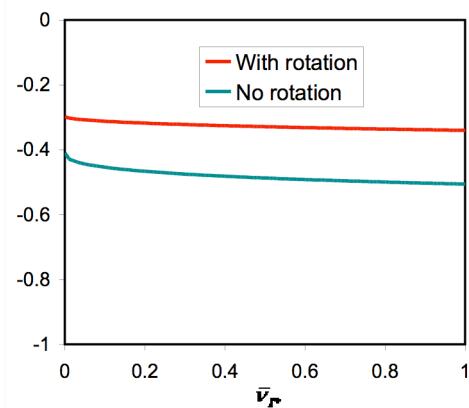
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- **Significant differences exist**
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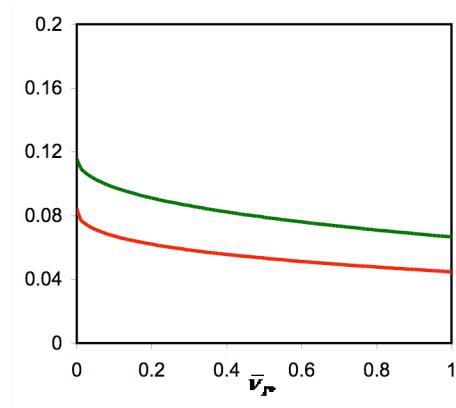
# Effect of Toroidal Rotation

\*Increase in coefficients drives poloidal velocity in the direction of ion diamagnetic flow

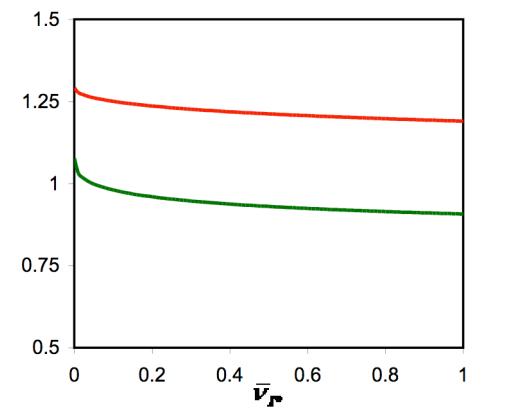
**C<sub>1</sub>**



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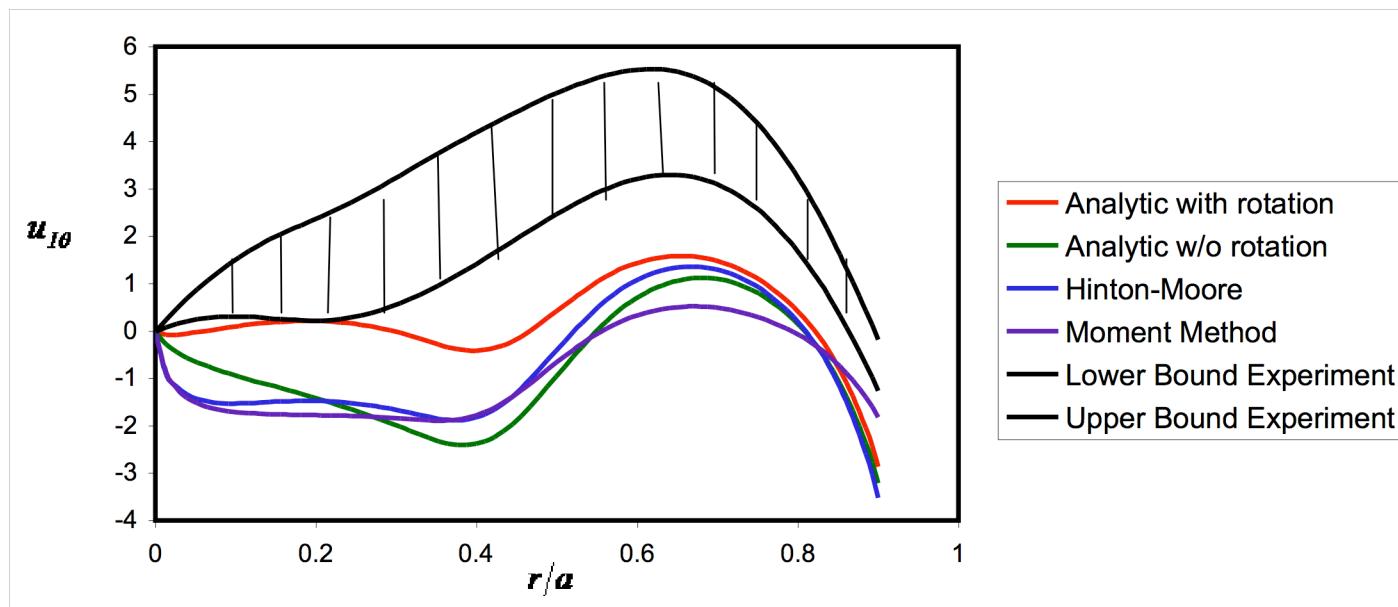
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# Comparison with DIII-D Experiment

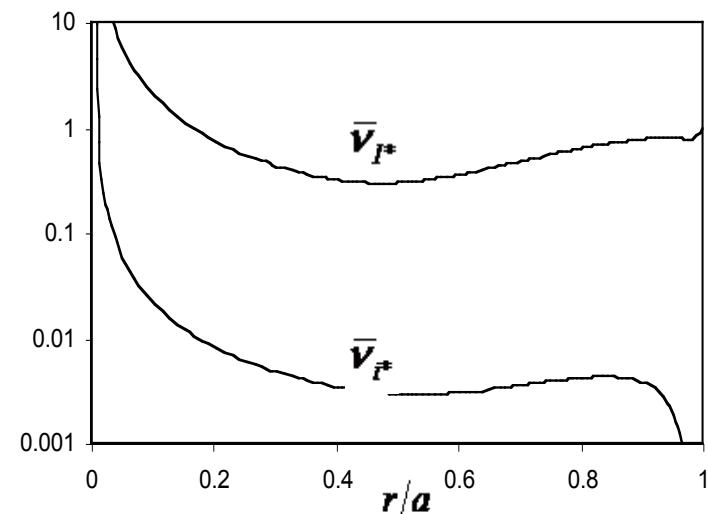
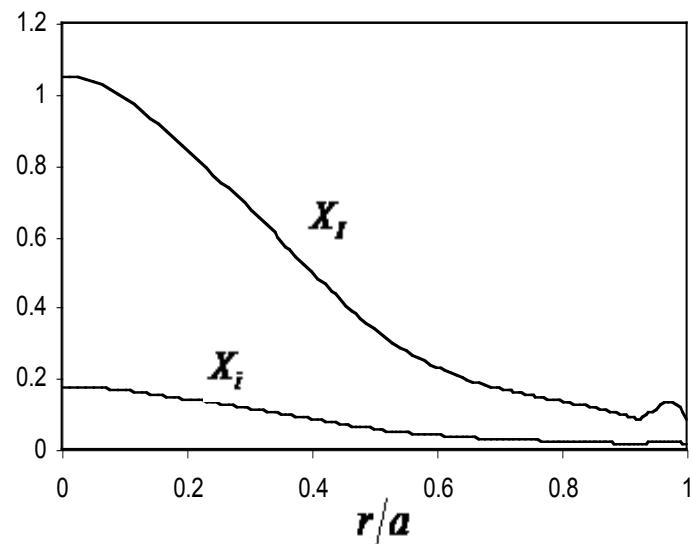
- Taking toroidal rotation into account alleviates discrepancy with experiment

## $C^{+6}$ Poloidal Velocity Profile



# Rotation Parameter and Collisionality

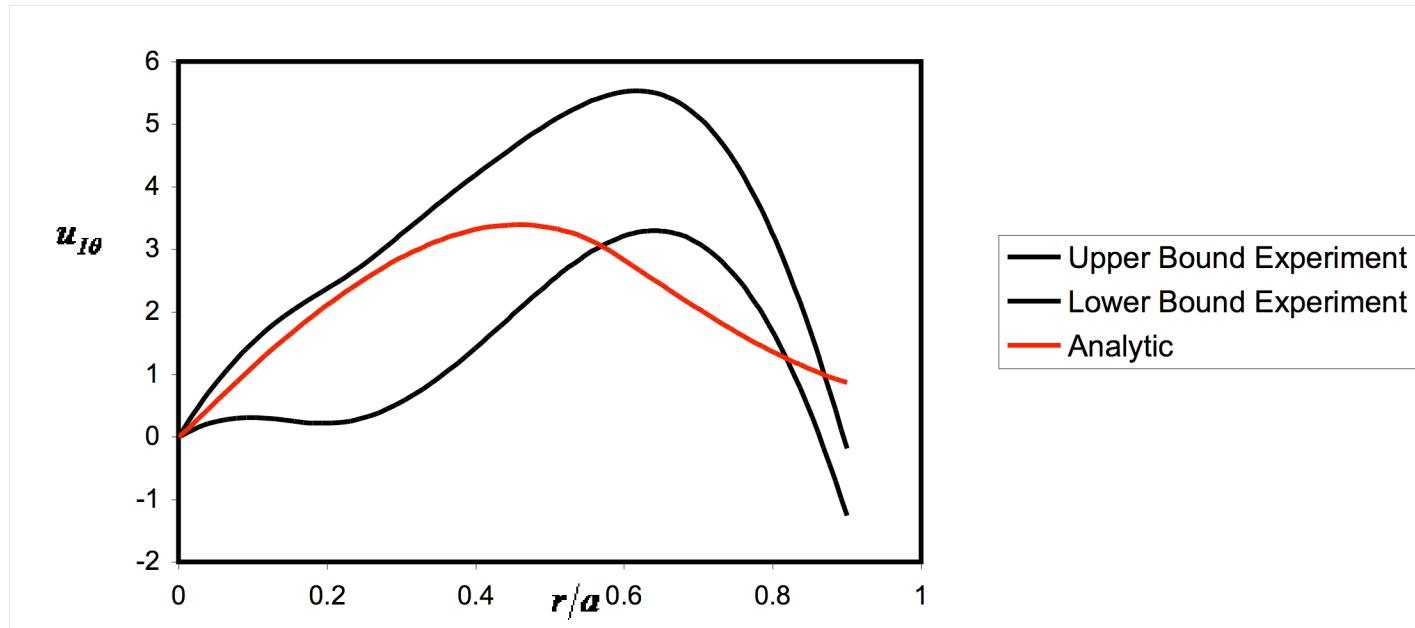
- Toroidal rotation is important in central region
- Analytic theory is marginal at best with regard to collisionality



# If Steady State with no ion Sources is Assumed

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- then  $\Gamma_I = \Gamma_i = 0$
- which leads to  $u_{I\theta} = \left( \frac{5}{2} - \frac{k_{I1}}{k_{I0}} \right) \frac{1}{Z_I e B_\xi} \frac{\partial T}{\partial r}$
- All calculations predict reasonable agreements with experiment



# Conclusions

- Taking toroidal rotation into account alleviates discrepancy with experiments
- Significant differences exist among different neoclassical calculations
- More accurate numerical work needed for experimentally relevant collisionality and magnetic geometry