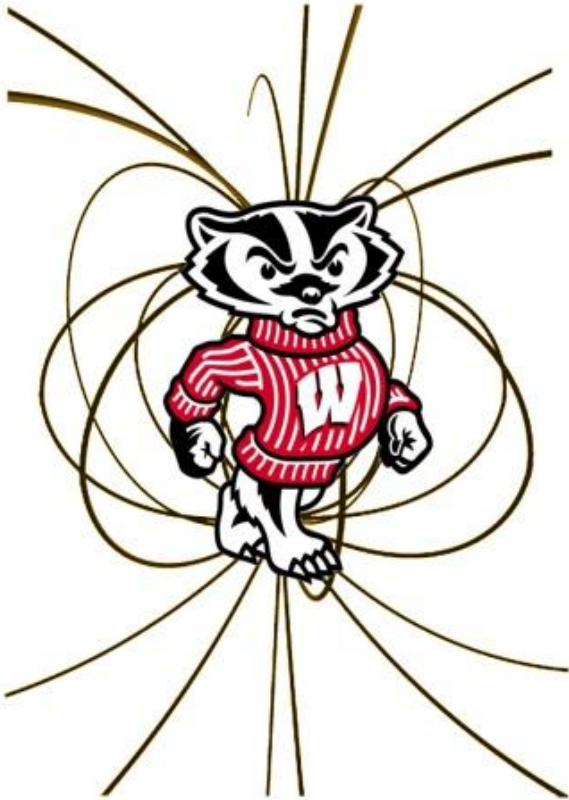


# Vertical Field Penetration and Mode-Locking of Global Modes with a Rotating Conducting Wall



**Carlos Paz-Soldan**

**M.I. Brookhart, C.C. Hegna,  
J.S. Sarff, C.B. Forest**

**University of Wisconsin-Madison**

**MHD Workshop Talk, Nov 21<sup>st</sup> 2011**

# Experiment overview



$$B_z \approx 0.1 \text{ T}$$

$$I_p \approx 7 \text{ kA}$$

$$L = 1.2 \text{ m}$$

$$R = 8 \text{ cm}$$

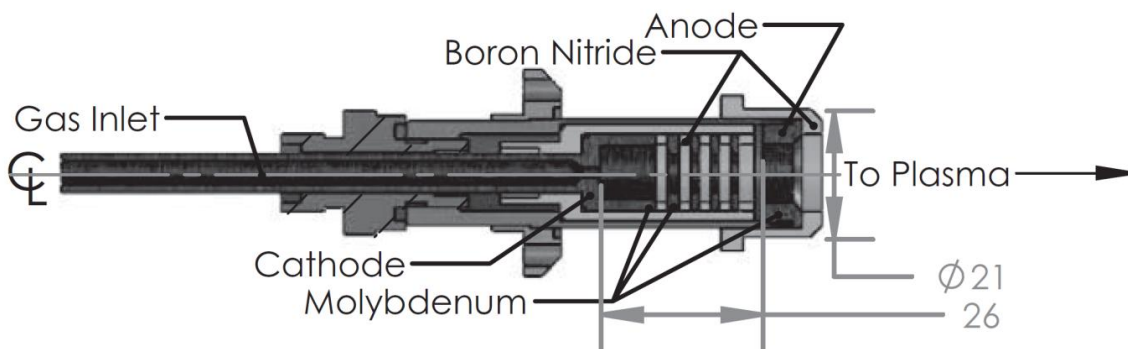
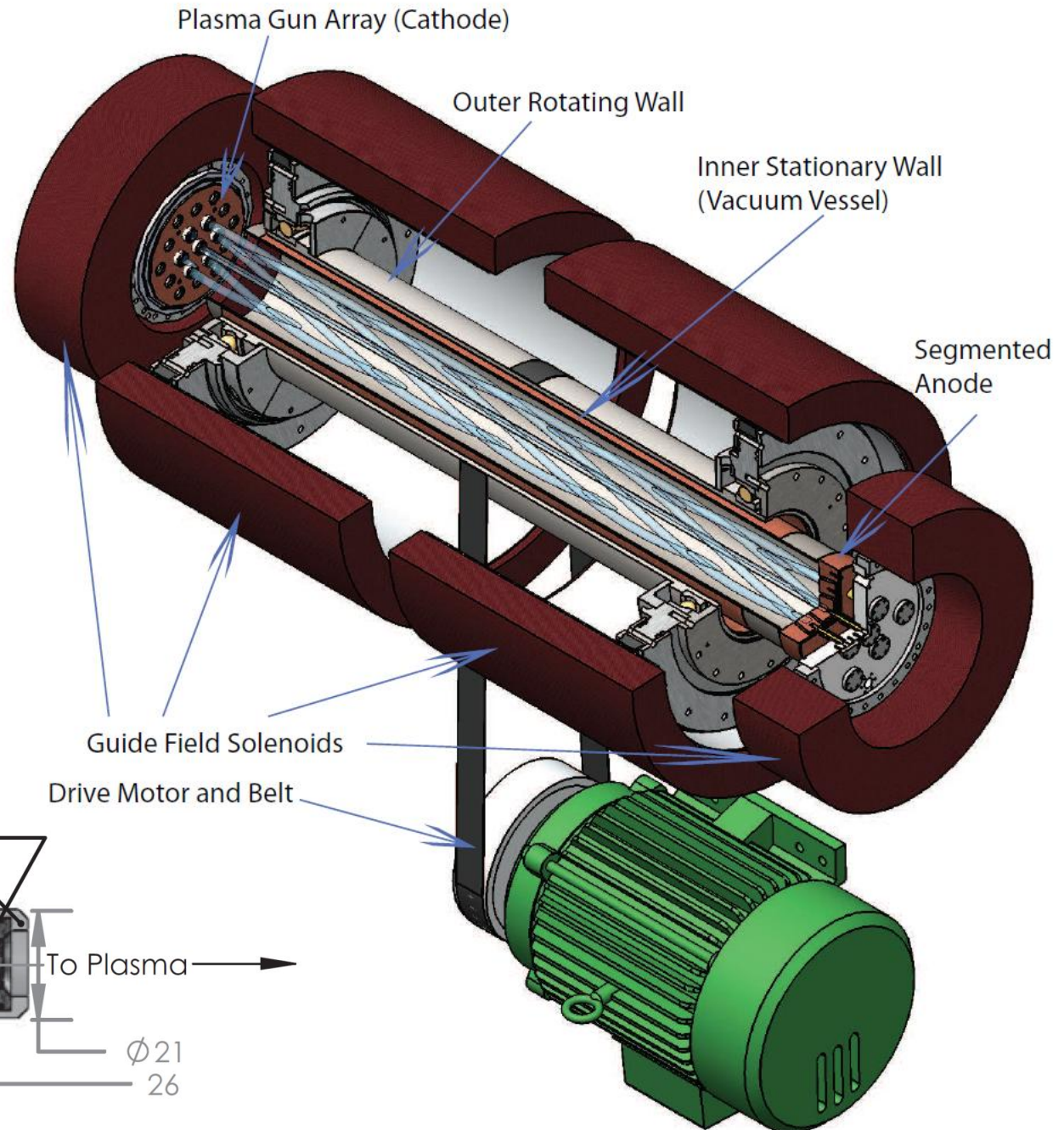
$$t \approx 20 \text{ ms}$$

$$\tau_w = 7 \text{ ms}$$

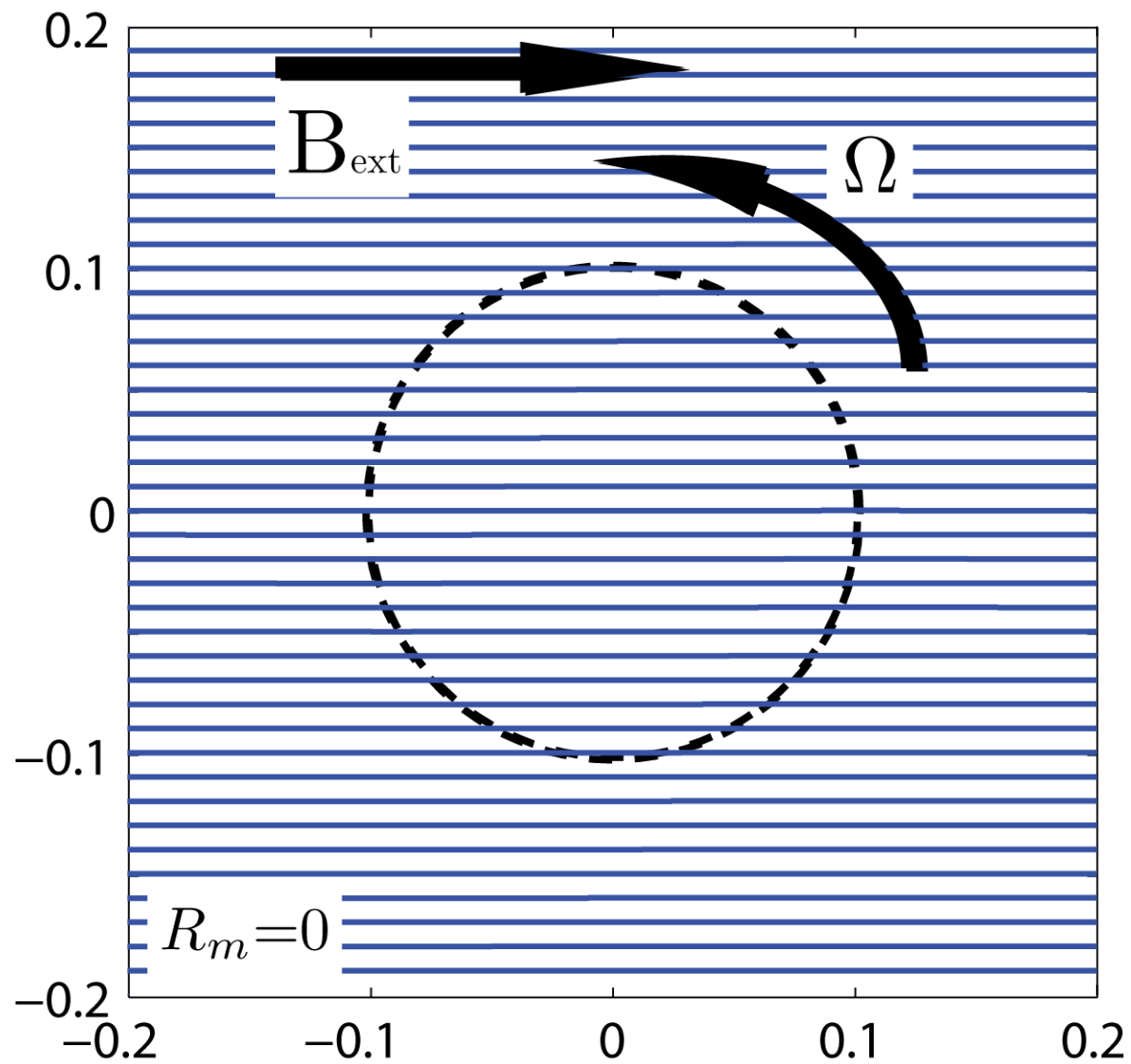
$$\tau_A \approx 2 \text{ } \mu\text{s}$$

$$T_e \approx 3.5 \text{ eV}$$

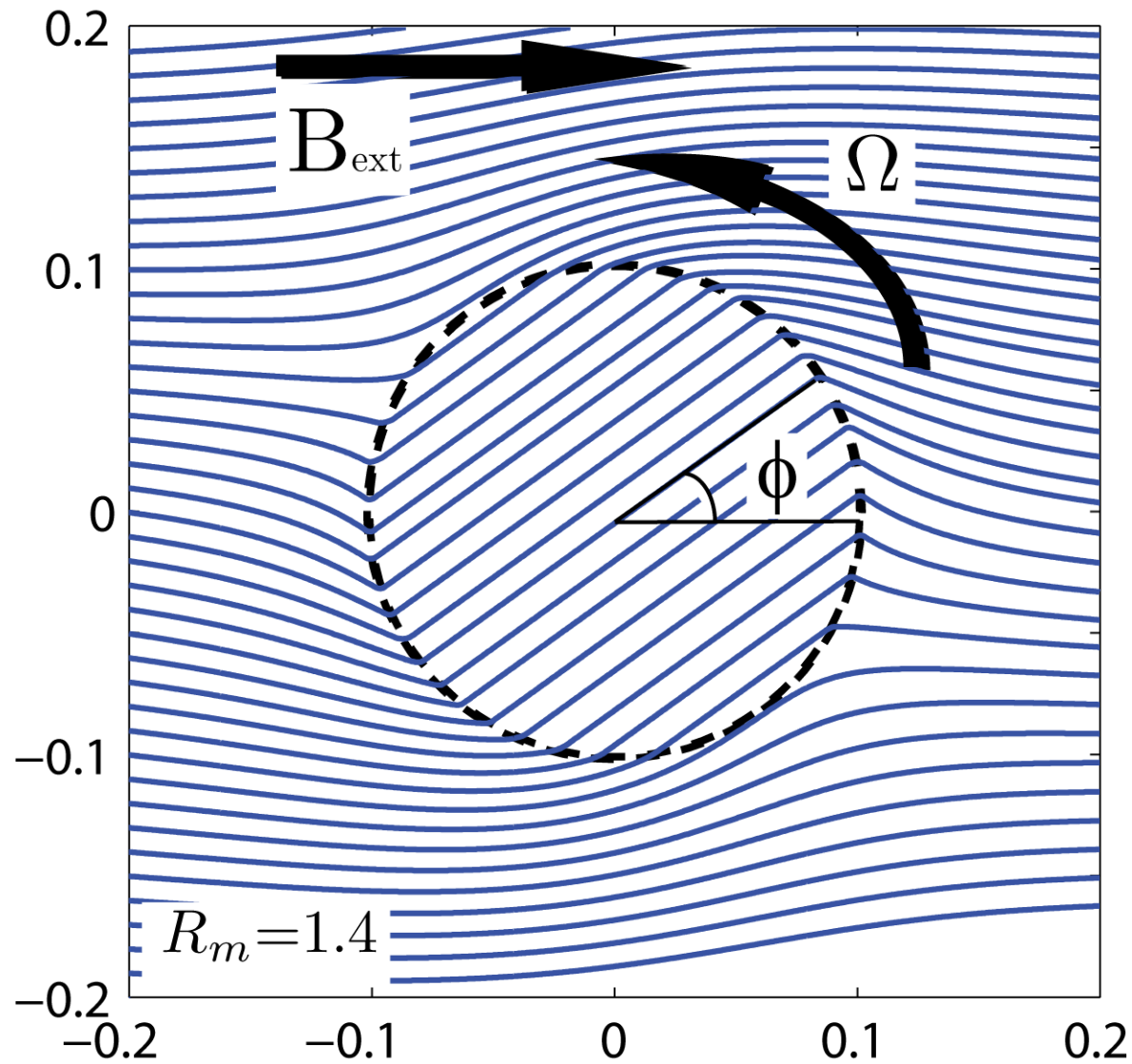
$$n_e \approx 10^{20} \text{ m}^{-3}$$



# Consider vertical field penetration

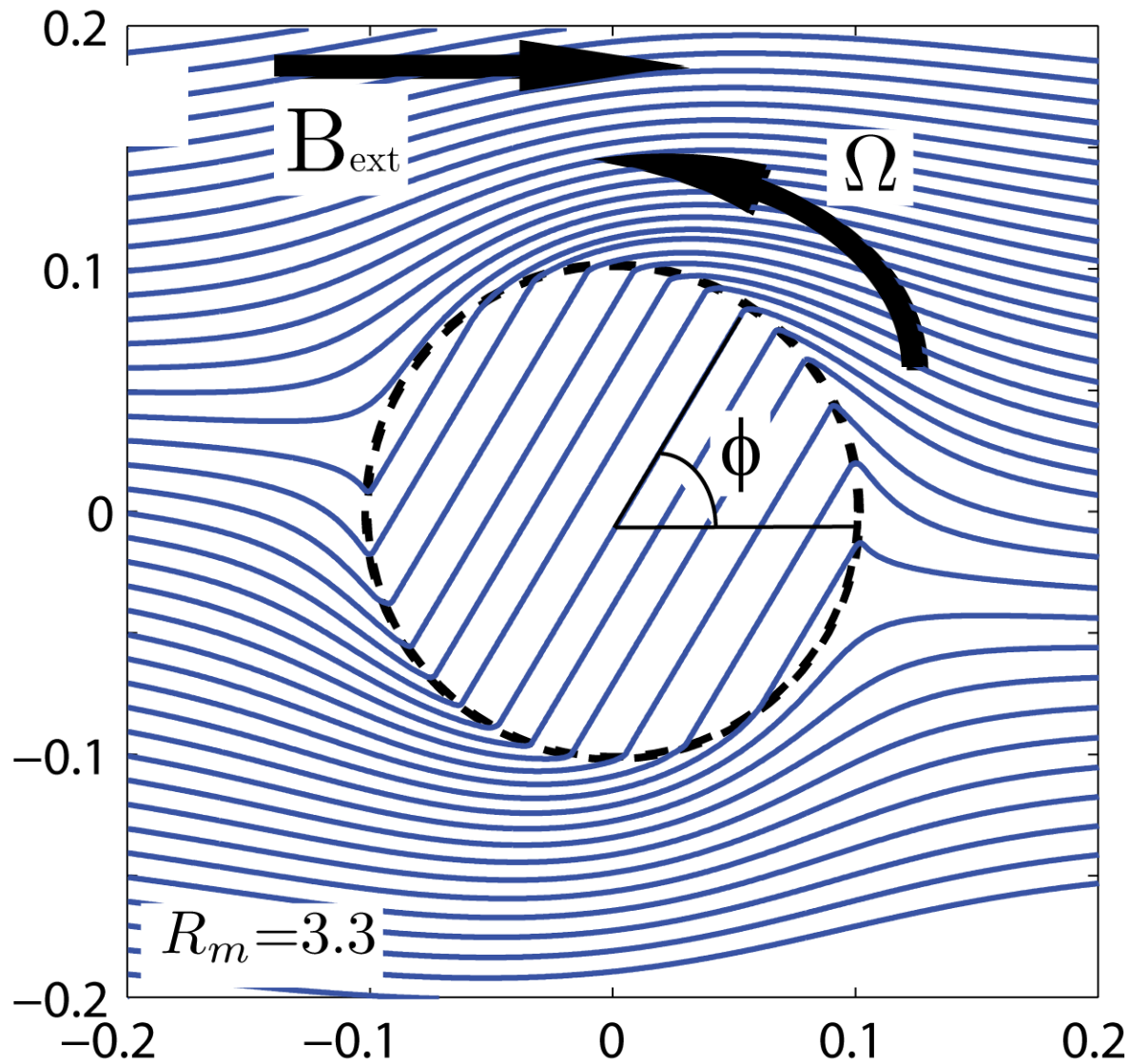


# Consider vertical field penetration





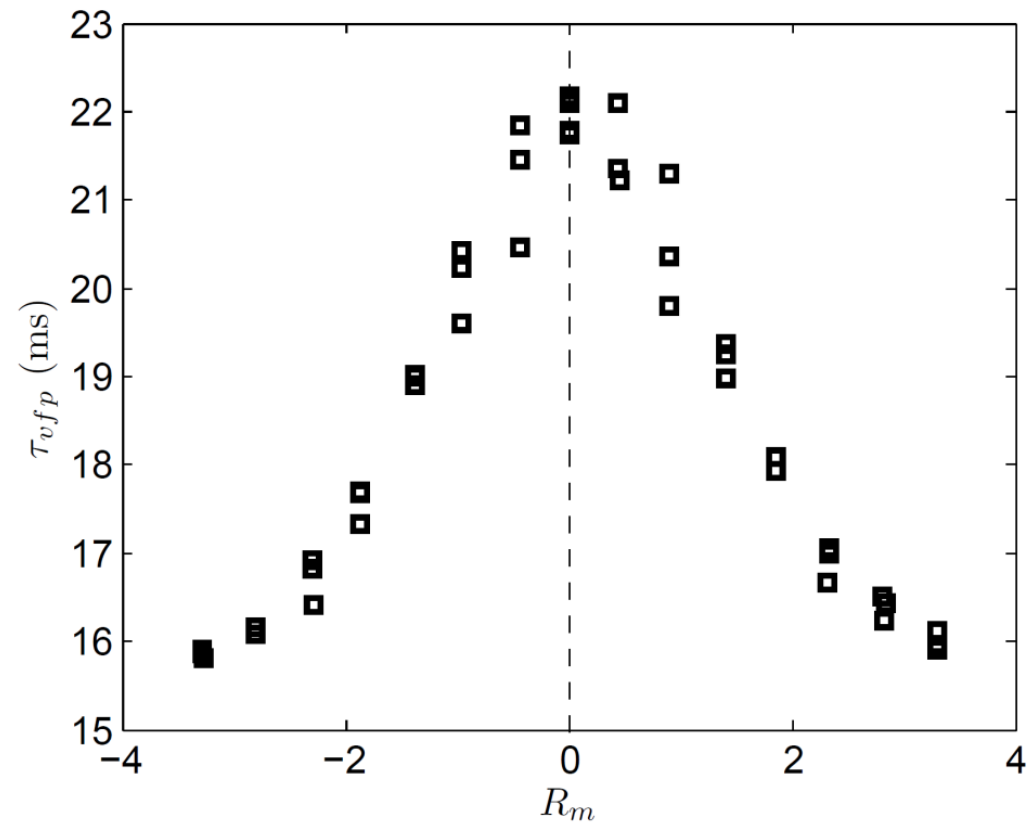
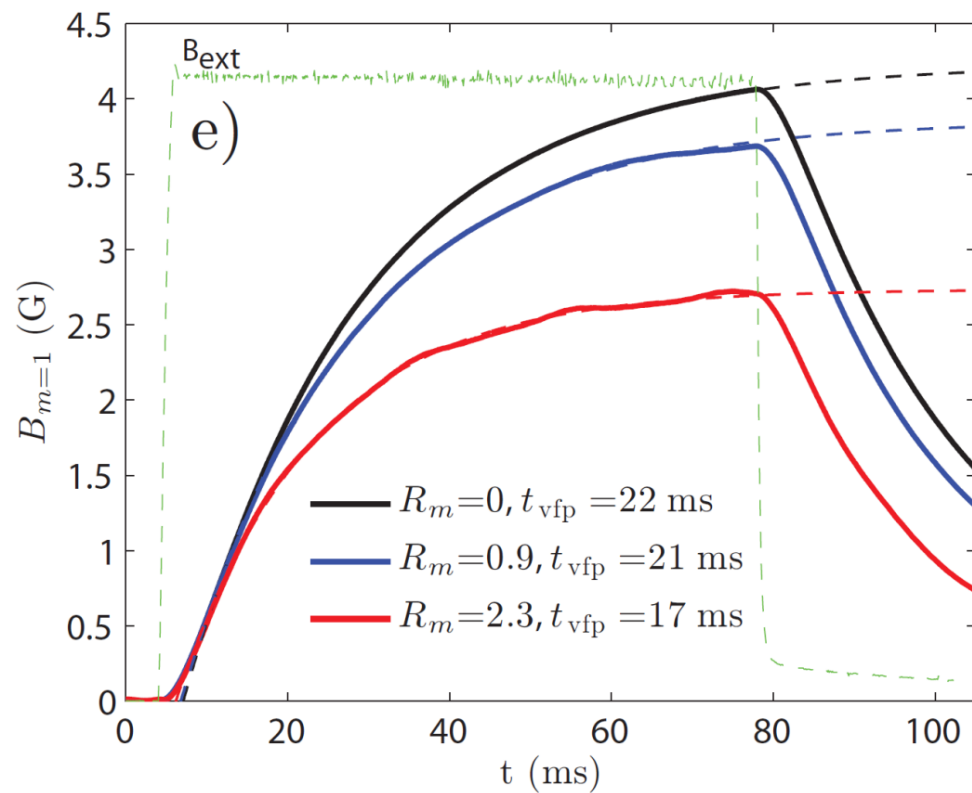
# Consider vertical field penetration



# Penetration time *decreases* as wall rotates



- Error field reaches a *smaller* value *faster*
- This is a consequence of *differential* rotation



# Model for thin-wall calculations:



- Vacuum field structure is (long cylinder approximation)

$$B_r(r, \theta) = \Re [(A_0 - A_1 r^{-2}) e^{-i\theta}]$$

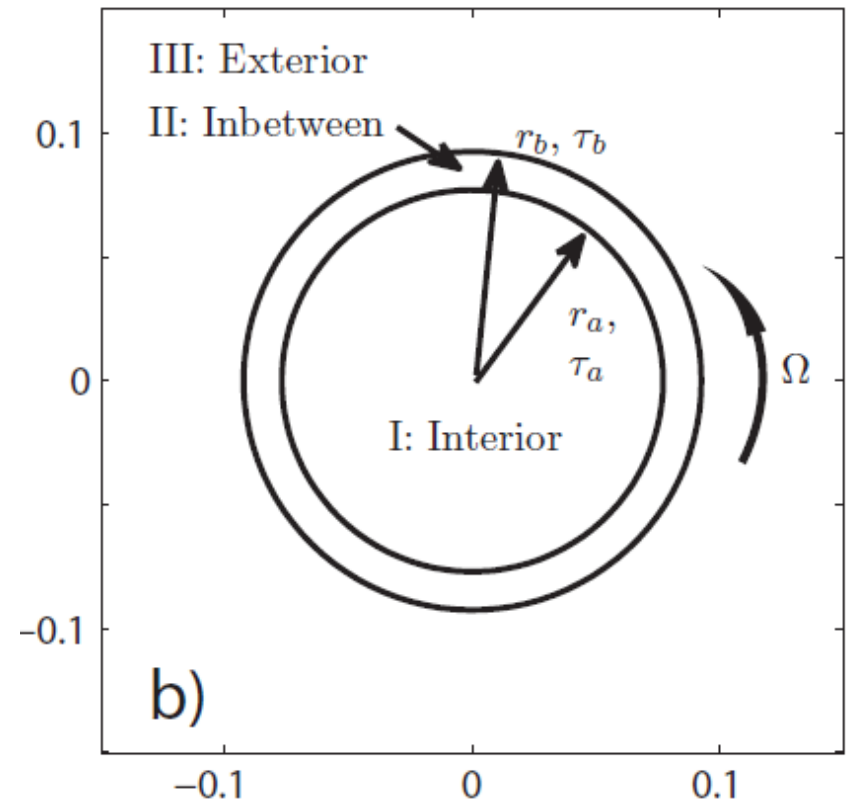
$$B_\theta(r, \theta) = \Re [(-i(A_0 + A_1 r^{-2})) e^{-i\theta}]$$

- Thin-wall matching:

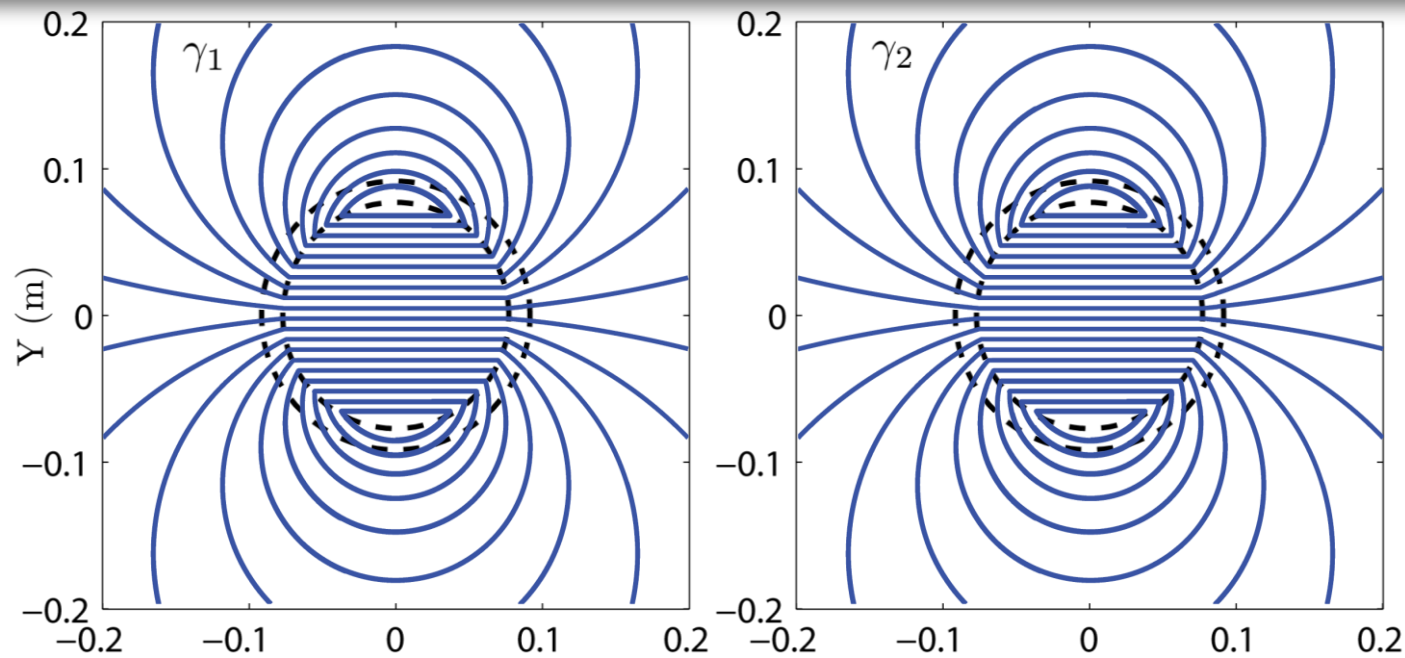
$$B_r \Big|_{r=r_w^-}^{r=r_w^+} = 0$$

$$B_\theta \Big|_{r=r_w^-}^{r=r_w^+} = i(\gamma + i\Omega) \tau_w B_r$$

- Matrix for unknown coefficients generated
  - Non-trivial solutions are the Eigenmodes



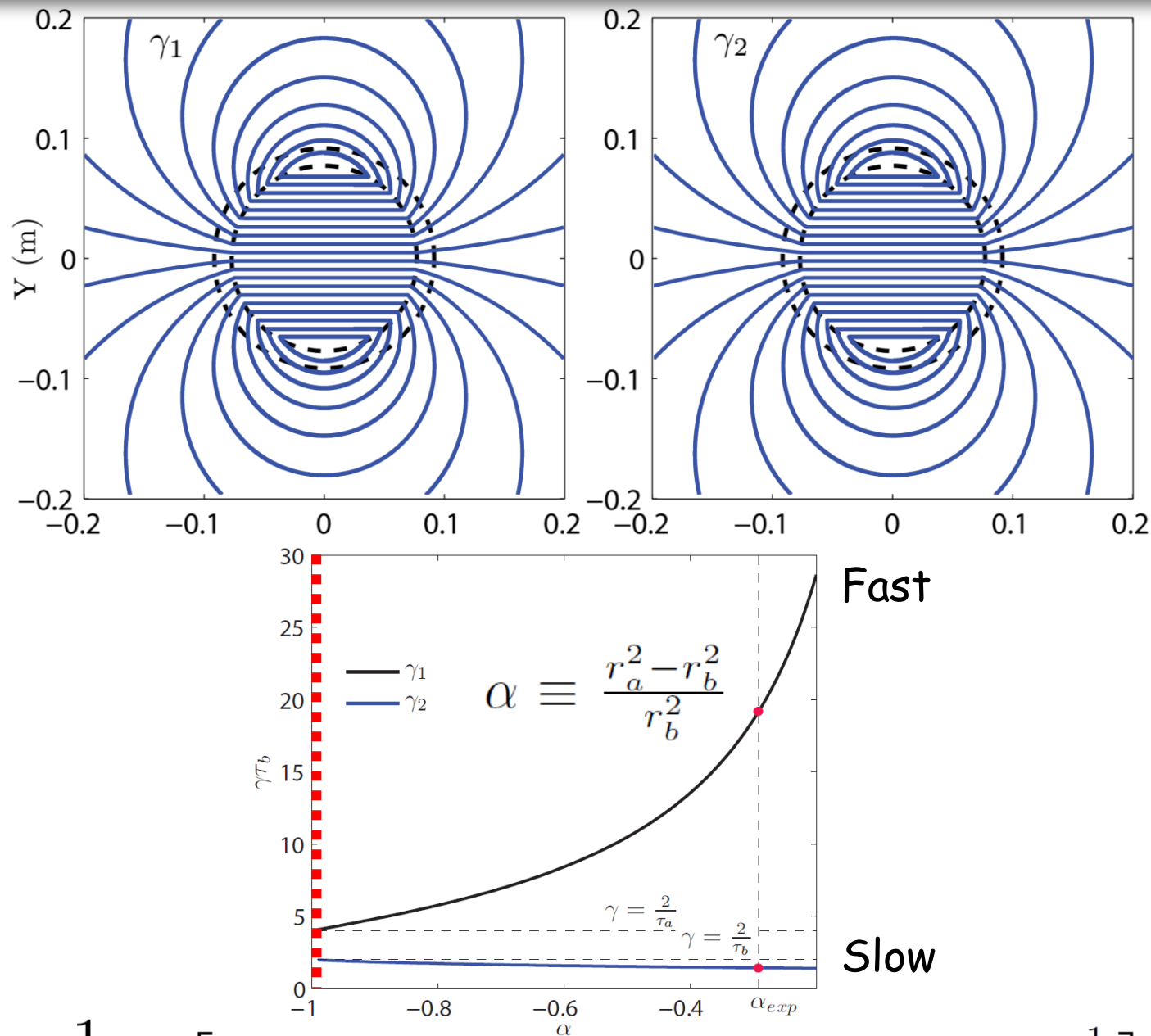
# Consider single wall m=1 Eigenmodes



$$\gamma = \frac{2}{\tau_a} - i\Omega$$

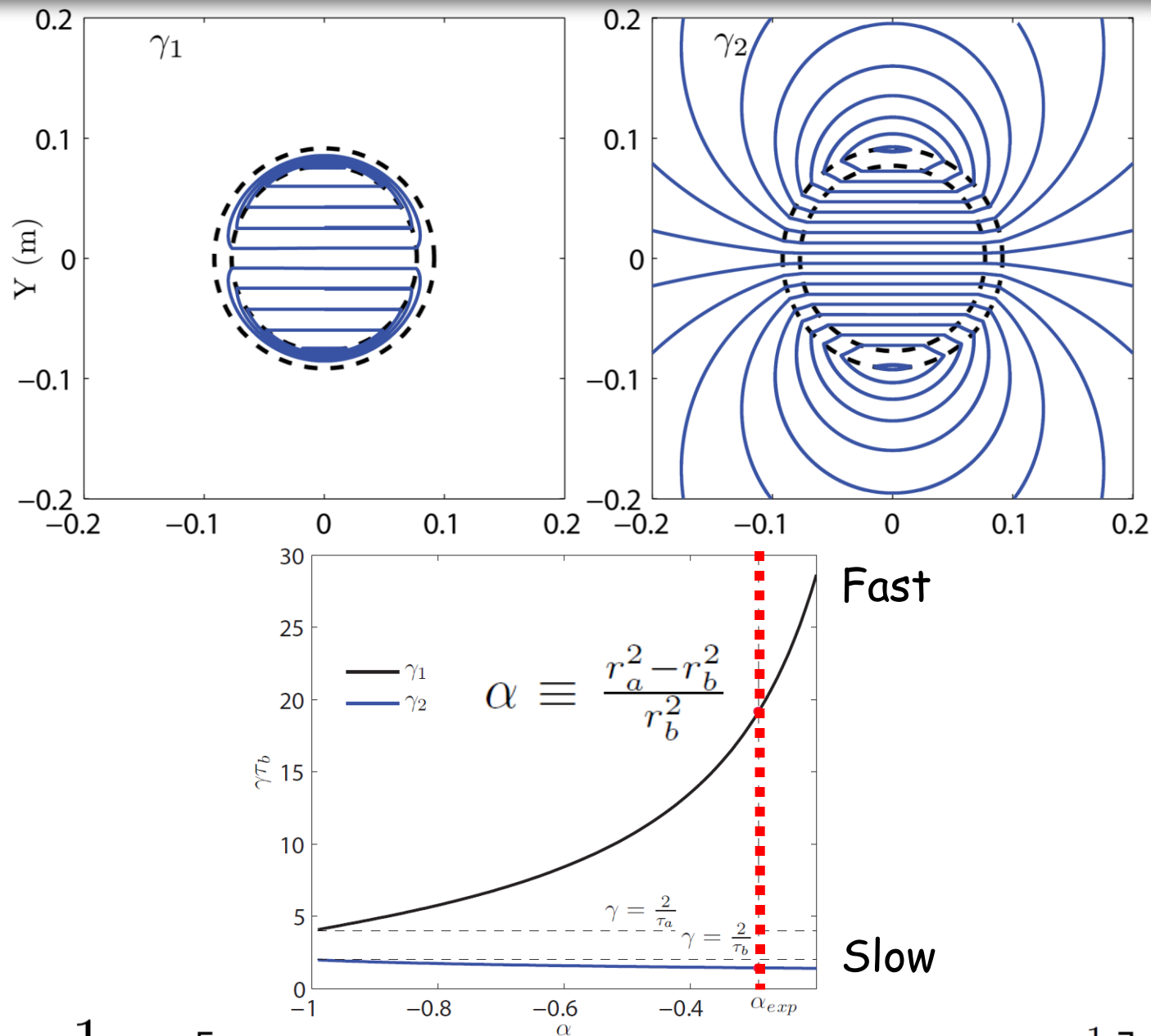


# Introduce coupling from second wall



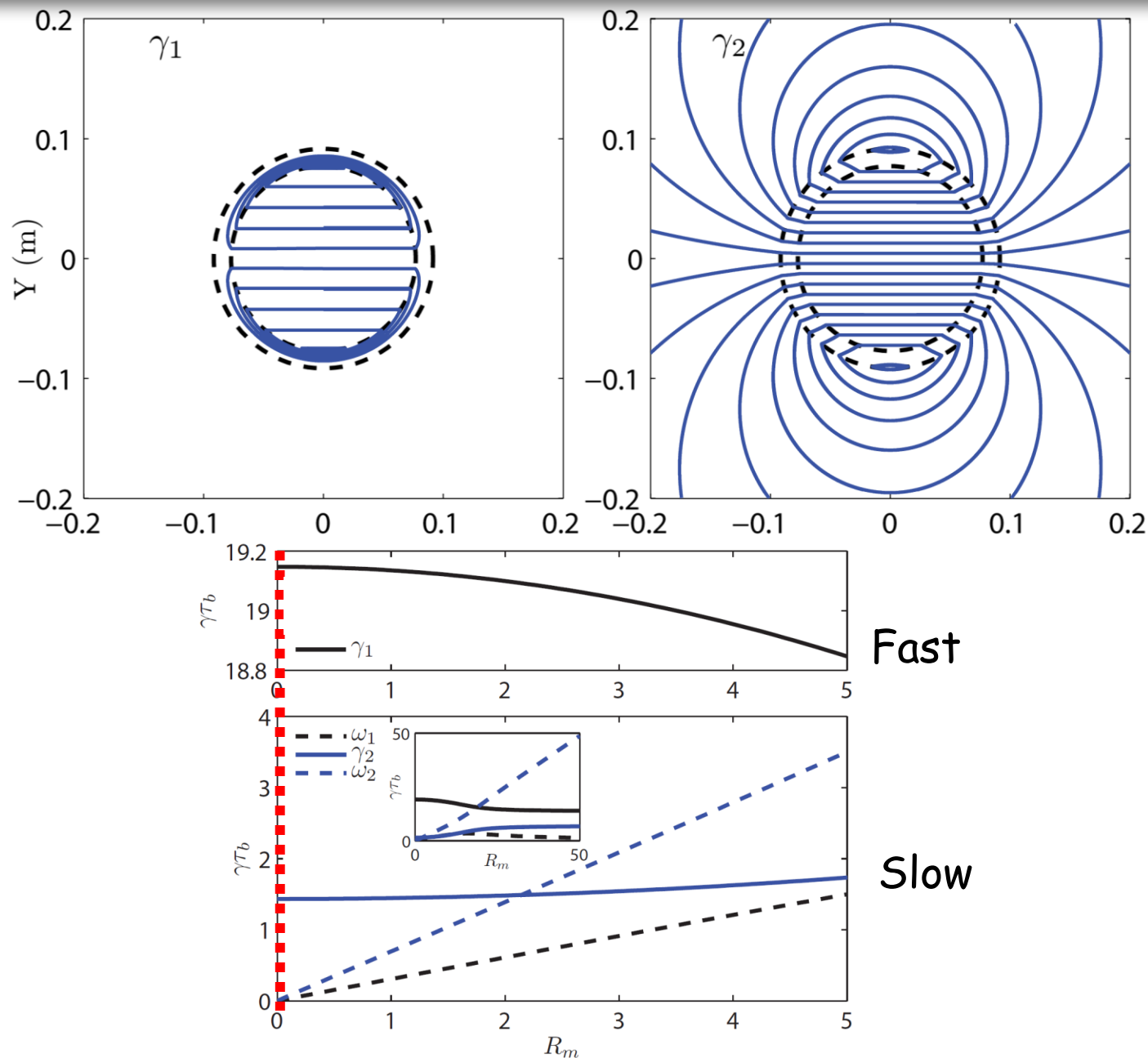
$$\gamma = -\frac{1}{\tau_a \tau_b \alpha} \left[ \tau_a + \tau_b \pm \left[ (\tau_a + \tau_b)^2 + 4\alpha \tau_a \tau_b \right]^{\frac{1}{2}} \right]$$

# Introduce coupling from second wall



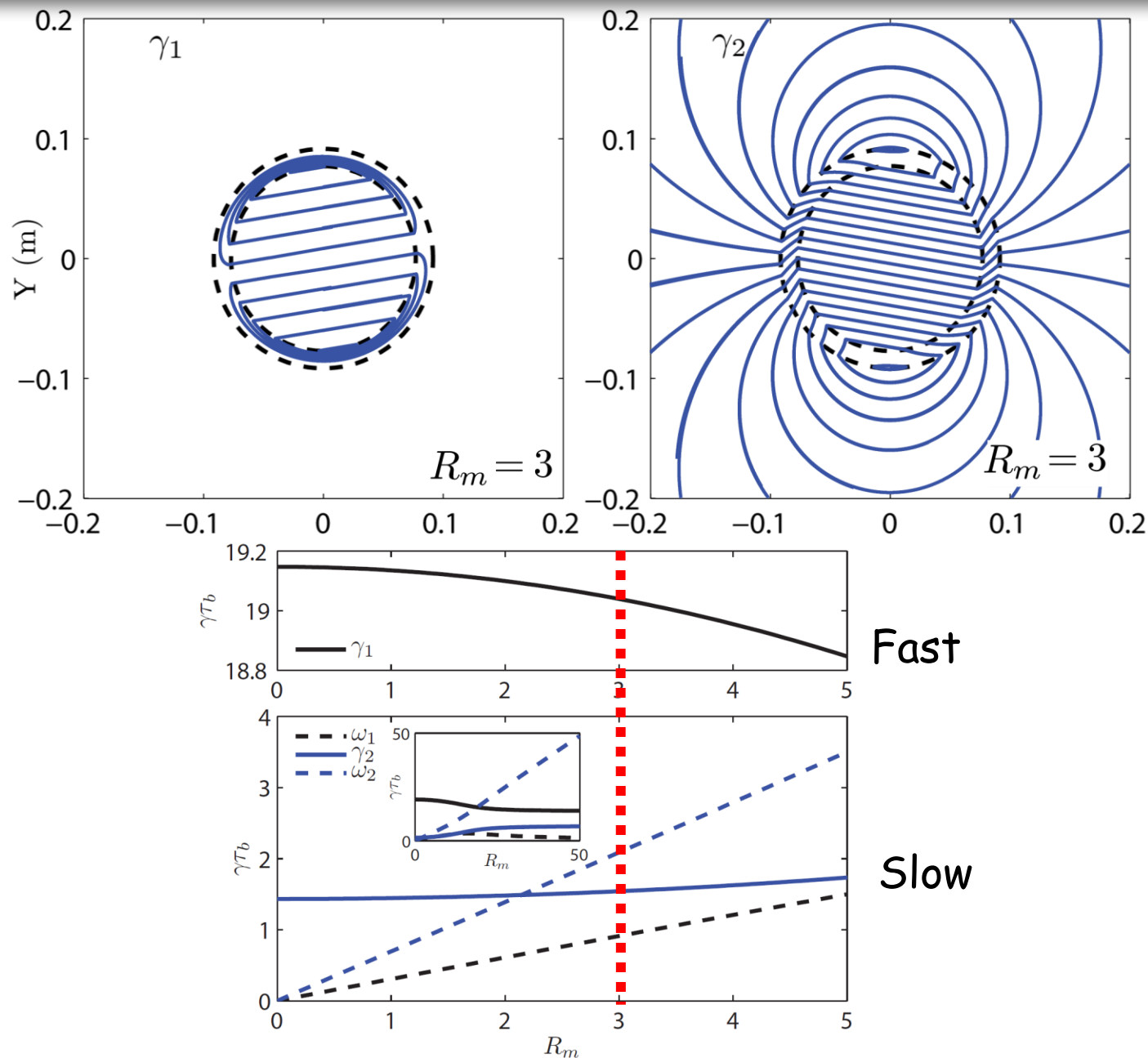
$$\gamma = -\frac{1}{\tau_a \tau_b \alpha} \left[ \tau_a + \tau_b \pm \left[ (\tau_a + \tau_b)^2 + 4\alpha \tau_a \tau_b \right]^{\frac{1}{2}} \right]$$

# Introduce differential wall rotation



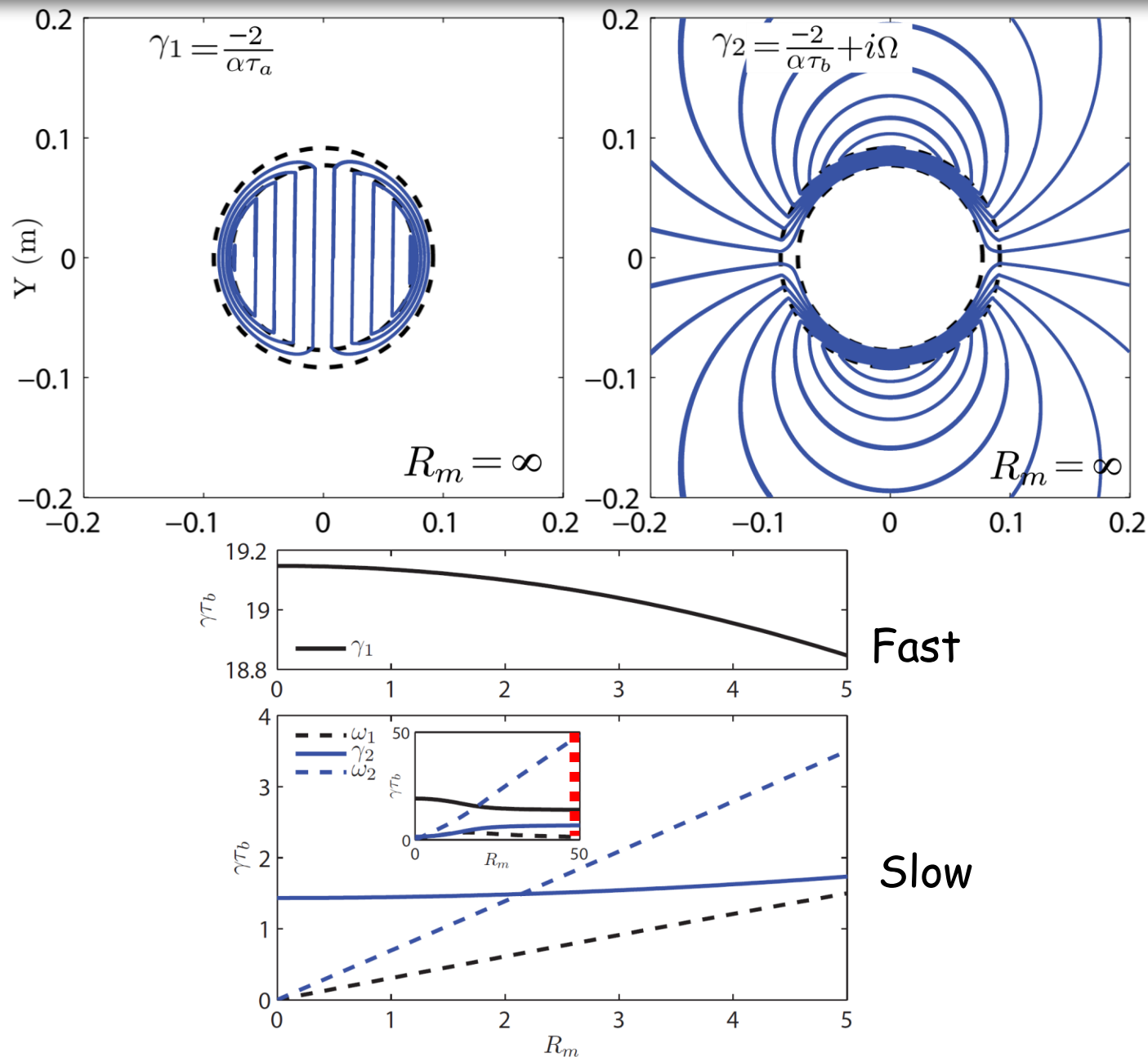
$$\gamma = -\frac{\tau_a + \tau_b}{\tau_a \tau_b \alpha} - i\frac{\Omega}{2} \pm \frac{1}{\tau_a \tau_b \alpha} \left[ \left[ (\tau_a + \tau_b)^2 + 4\alpha \tau_a \tau_b - \frac{\Omega^2}{4} (\tau_a \tau_b \alpha)^2 \right] + i\Omega \tau_a \tau_b \alpha (\tau_a - \tau_b) \right]^{\frac{1}{2}}$$

# Introduce differential wall rotation



$$\gamma = -\frac{\tau_a + \tau_b}{\tau_a \tau_b \alpha} - i\frac{\Omega}{2} \pm \frac{1}{\tau_a \tau_b \alpha} \left[ \left[ (\tau_a + \tau_b)^2 + 4\alpha \tau_a \tau_b - \frac{\Omega^2}{4} (\tau_a \tau_b \alpha)^2 \right] + i\Omega \tau_a \tau_b \alpha (\tau_a - \tau_b) \right]^{\frac{1}{2}}$$

# Introduce differential wall rotation

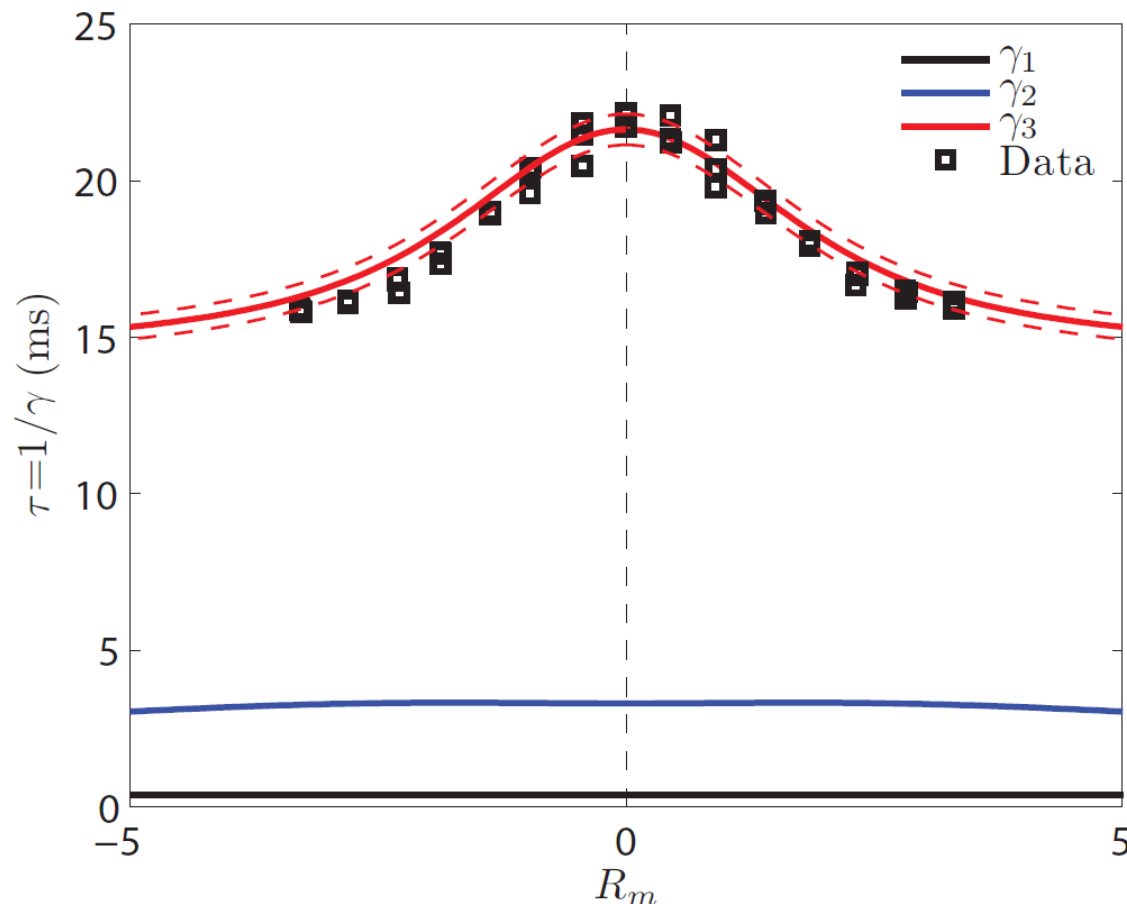


$$\gamma = -\frac{\tau_a + \tau_b}{\tau_a \tau_b \alpha} - i\frac{\Omega}{2} \pm \frac{1}{\tau_a \tau_b \alpha} \left[ \left[ (\tau_a + \tau_b)^2 + 4\alpha \tau_a \tau_b - \frac{\Omega^2}{4} (\tau_a \tau_b \alpha)^2 \right] + i\Omega \tau_a \tau_b \alpha (\tau_a - \tau_b) \right]^{\frac{1}{2}}$$

# Speeding up of slow root is the observation



- Results of calculation consistent with data
  - Dotted lines are +/- 2% on wall time
  - No free parameters
- This would not be observed on single-wall system

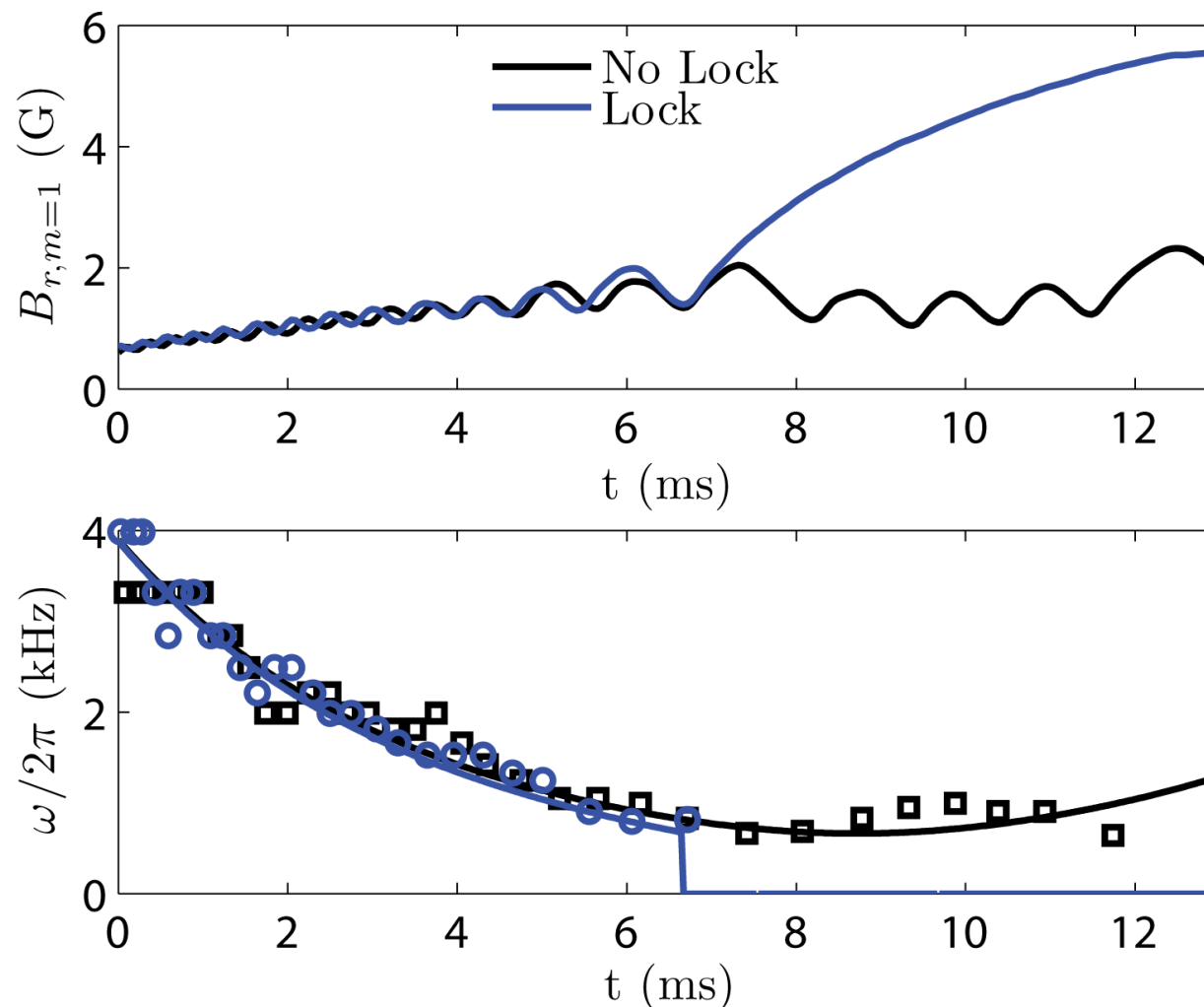




# Mode locking observed in device



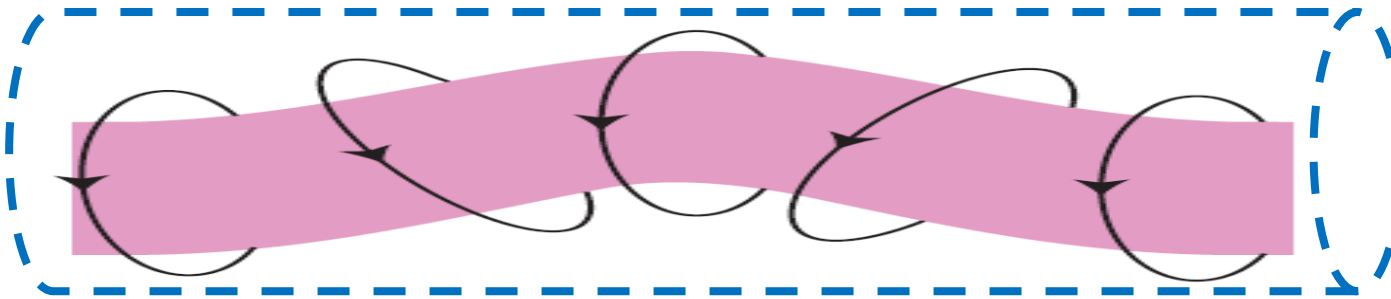
- We explore this phenomenon in greater detail



# Simple torque balance model



$$\int_{\mathcal{V}} \vec{r} \times \left[ \rho \left( \frac{\partial \vec{V}}{\partial t} + \vec{V} \cdot \nabla \vec{V} \right) \right] d\mathcal{V} = \int_{\mathcal{V}} \vec{r} \times \left[ -\nabla P - \nabla \cdot \bar{\bar{\Pi}} + \nabla \cdot \bar{\bar{T}} \right] d\mathcal{V}$$

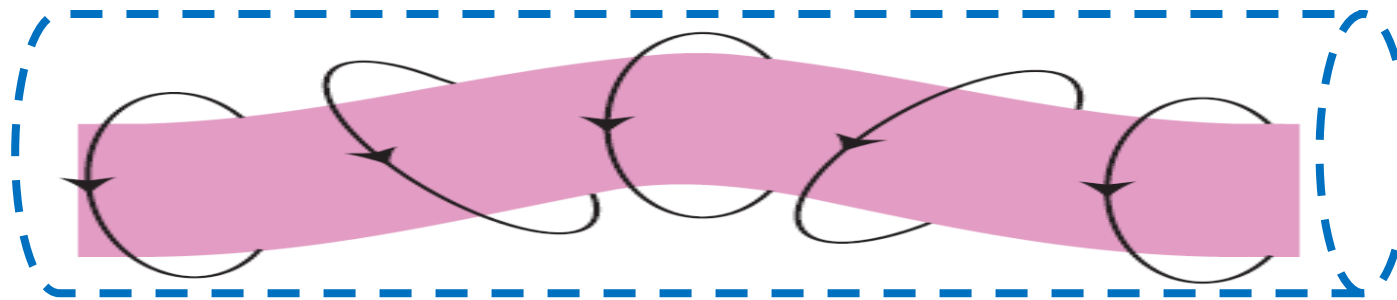


Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

# Simple torque balance model



$$\int_{\mathcal{V}} \vec{r} \times \left[ \rho \left( \frac{\partial \vec{V}}{\partial t} + \vec{V} \cdot \nabla \vec{V} \right) \right] d\mathcal{V} = \int_{\mathcal{V}} \vec{r} \times \left[ -\nabla P - \nabla \cdot \bar{\bar{\Pi}} + \nabla \cdot \bar{\bar{T}} \right] d\mathcal{V}$$



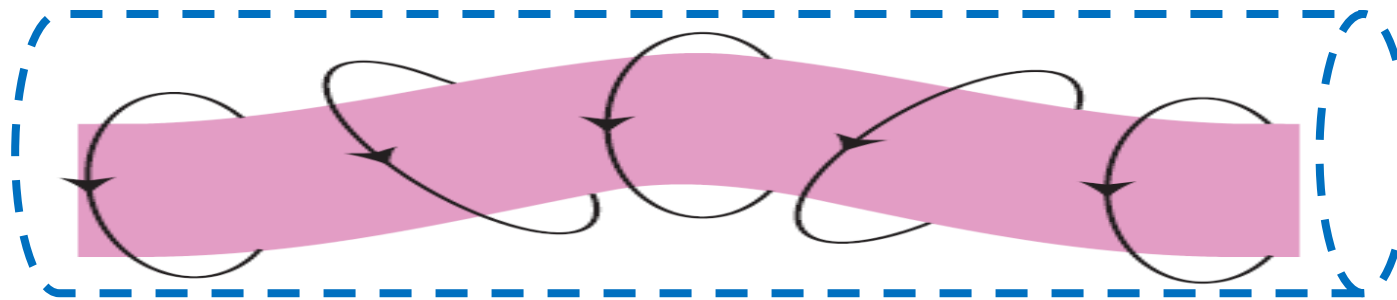
Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

- Treat plasma as rigid rotor, such that  $V_{\theta} = r\omega$ 
  - Viscosity is infinite, dissipation present, like a motor

# Simple torque balance model



$$\int_{\mathcal{V}} \vec{r} \times \left[ \rho \left( \frac{\partial \vec{V}}{\partial t} + \vec{V} \cdot \nabla \vec{V} \right) \right] d\mathcal{V} = \int_{\mathcal{V}} \vec{r} \times \left[ -\nabla P - \nabla \cdot \bar{\bar{\Pi}} + \nabla \cdot \bar{\bar{T}} \right] d\mathcal{V}$$



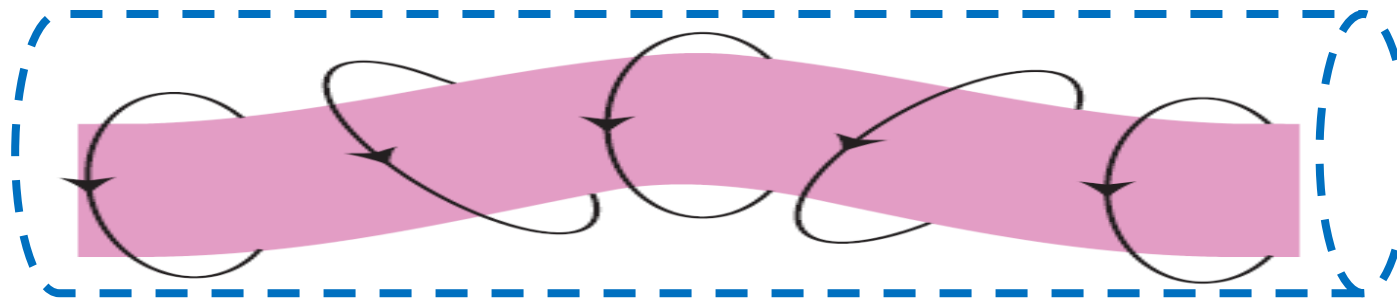
Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

- Treat plasma as rigid rotor, such that  $V_{\theta} = r\omega$ 
  - Viscosity is infinite, dissipation present, like a motor
- Torques act on whole plasma

# Simple torque balance model



$$\int_{\mathcal{V}} \vec{r} \times \left[ \rho \left( \frac{\partial \vec{V}}{\partial t} + \vec{V} \cdot \nabla \vec{V} \right) \right] d\mathcal{V} = \int_{\mathcal{V}} \vec{r} \times \left[ -\nabla P - \nabla \cdot \bar{\bar{\Pi}} + \nabla \cdot \bar{\bar{T}} \right] d\mathcal{V}$$



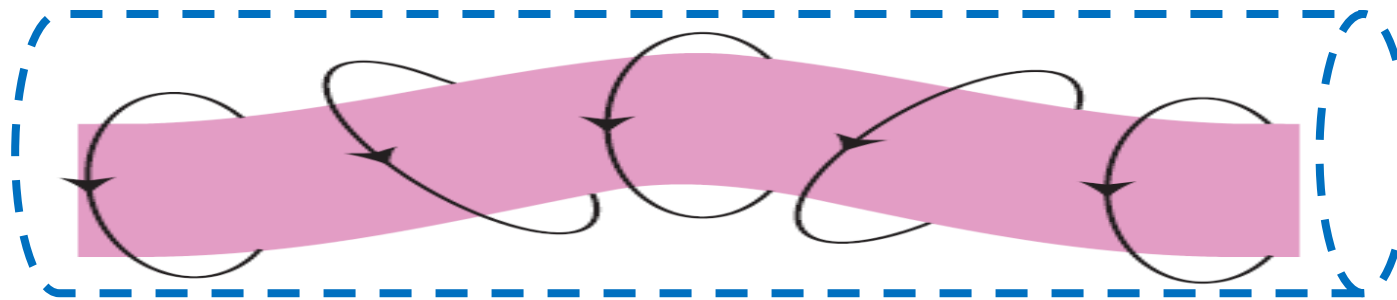
Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

- Treat plasma as rigid rotor, such that  $V_{\theta} = r\omega$ 
  - Viscosity is infinite, dissipation present, like a motor
- Torques act on whole plasma
- Inertia is negligible

# Simple torque balance model



$$0 = r_a \int_S \hat{\theta} \cdot \frac{1}{\mu_0} \left[ \vec{B} \vec{B} - \frac{1}{2} B^2 \vec{I} \right] \cdot d\vec{S}$$



Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

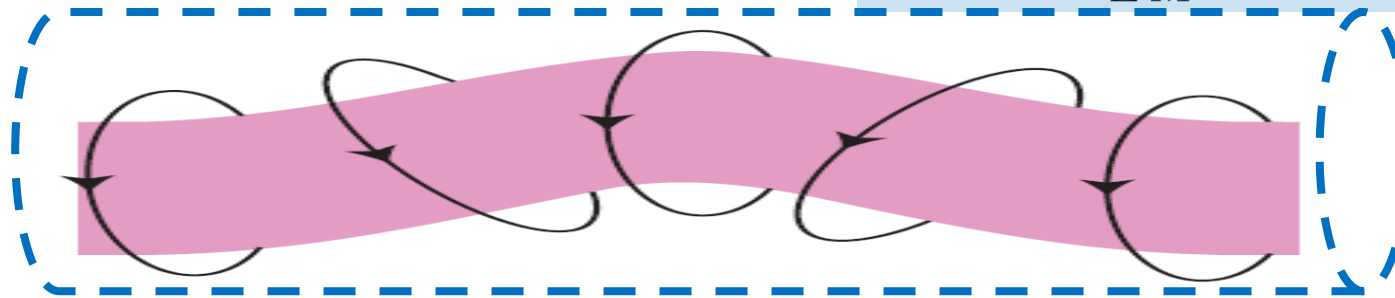
- Treat plasma as rigid rotor, such that  $V_\theta = r\omega$ 
  - Viscosity is infinite, dissipation present, like a motor
- Torques act on whole plasma
- Inertia is negligible
- Only electromagnetic torques remain
  - Field is decomposed:  $\vec{B} = B_{m=0} + B_{\text{ext}} + \tilde{B}e^{-i\omega t}$



# Simple torque balance model



$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}}(\Omega_0 - \omega)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}} + \underbrace{A_{\text{ext}} \sin(\theta)}_{\Gamma_{\text{ext}}}$$



Volume  $\mathcal{V}$   
Surface  $\mathcal{S}$

- Treat plasma as rigid rotor, such that  $V_\theta = r\omega$ 
  - Viscosity is infinite, dissipation present, like a motor
- Torques act on whole plasma
- Inertia is negligible
- Only electromagnetic torques remain
  - Field is decomposed:  $\vec{B} = B_{m=0} + B_{\text{ext}} + \tilde{B}e^{-i\omega t}$

# EM Torque extended for wall rotation



- Perform a cycle-average, torque takes this form

$$\Gamma_{EM} = \frac{Lr_a^2}{\mu_0} \int_0^{2\pi} \langle \tilde{B}_\theta \tilde{B}_r \rangle d\theta$$

- We know the field structure,  
experimental geometry

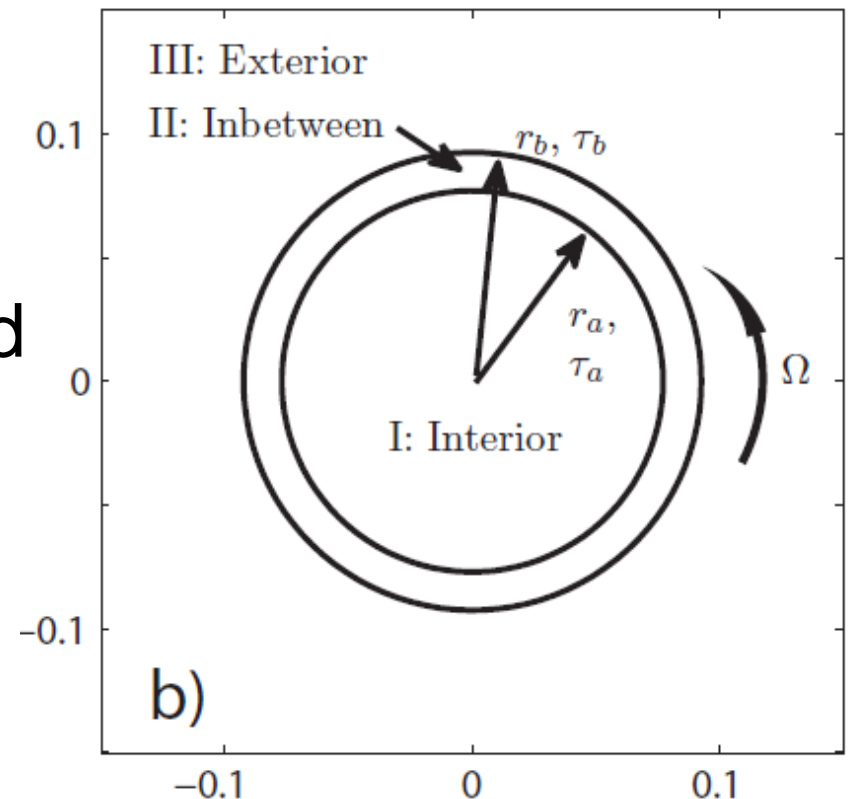
$$B_r(r, \theta) = \Re [(A_0 - A_1 r^{-2}) e^{-i\theta}]$$

$$B_\theta(r, \theta) = \Re [(-i(A_0 + A_1 r^{-2})) e^{-i\theta}]$$

- Thin-wall matching again used

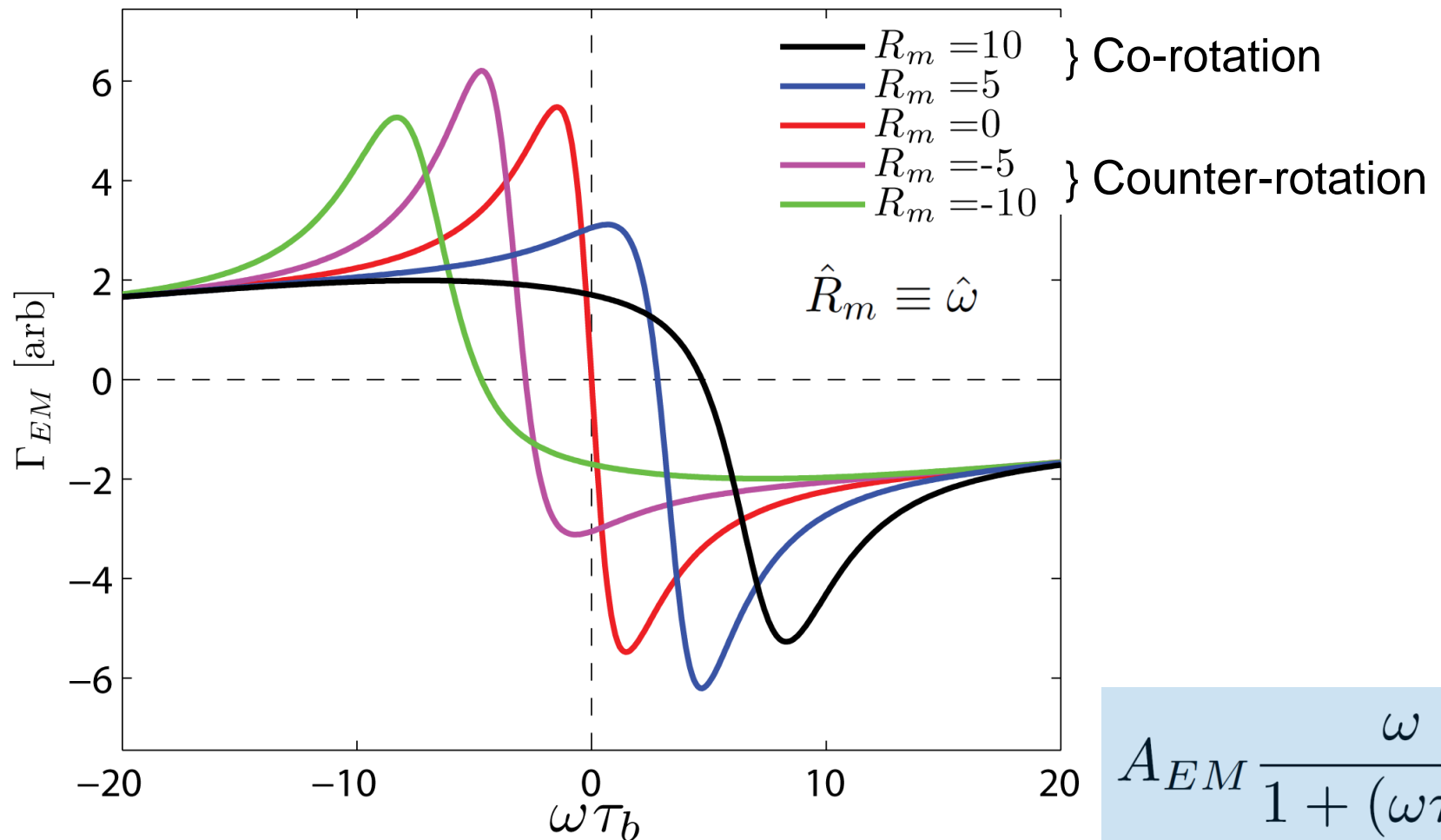
$$B_r \Big|_{r=r_w^-}^{r=r_w^+} = 0$$

$$B_\theta \Big|_{r=r_w^-}^{r=r_w^+} = i(\gamma + i\Omega) \tau_w B_r$$



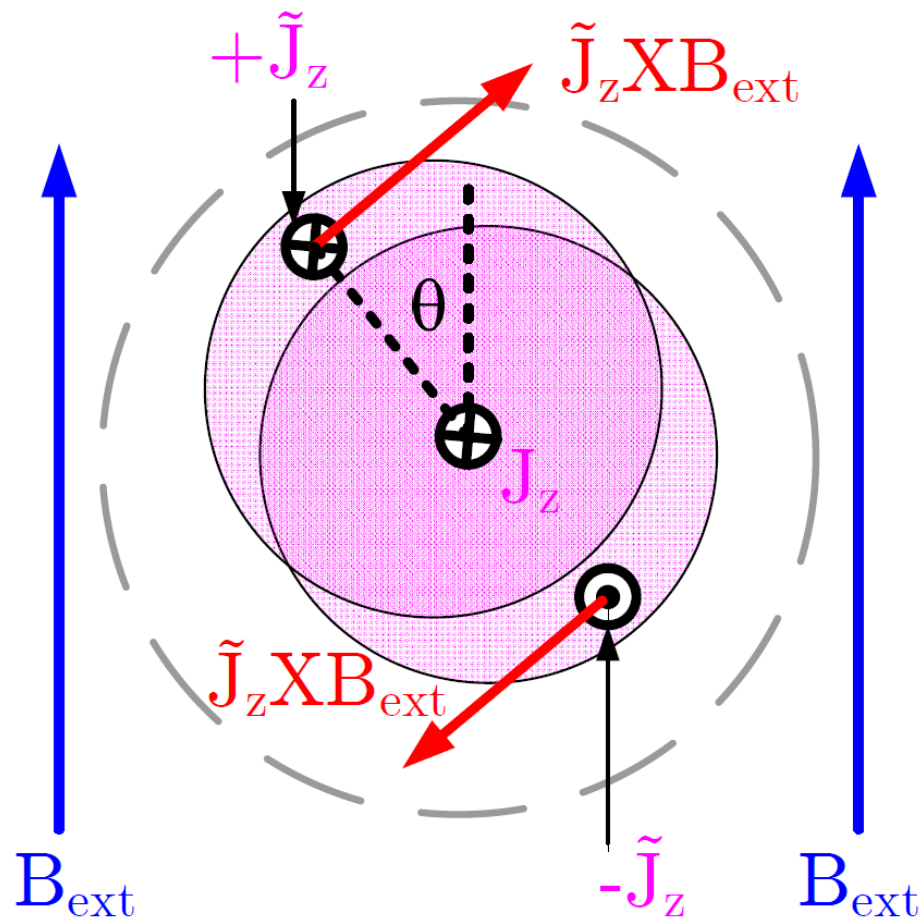


- Curves are Doppler shifted and skewed by wall rotation



$$\underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}}$$

# Error field torque depends on alignment

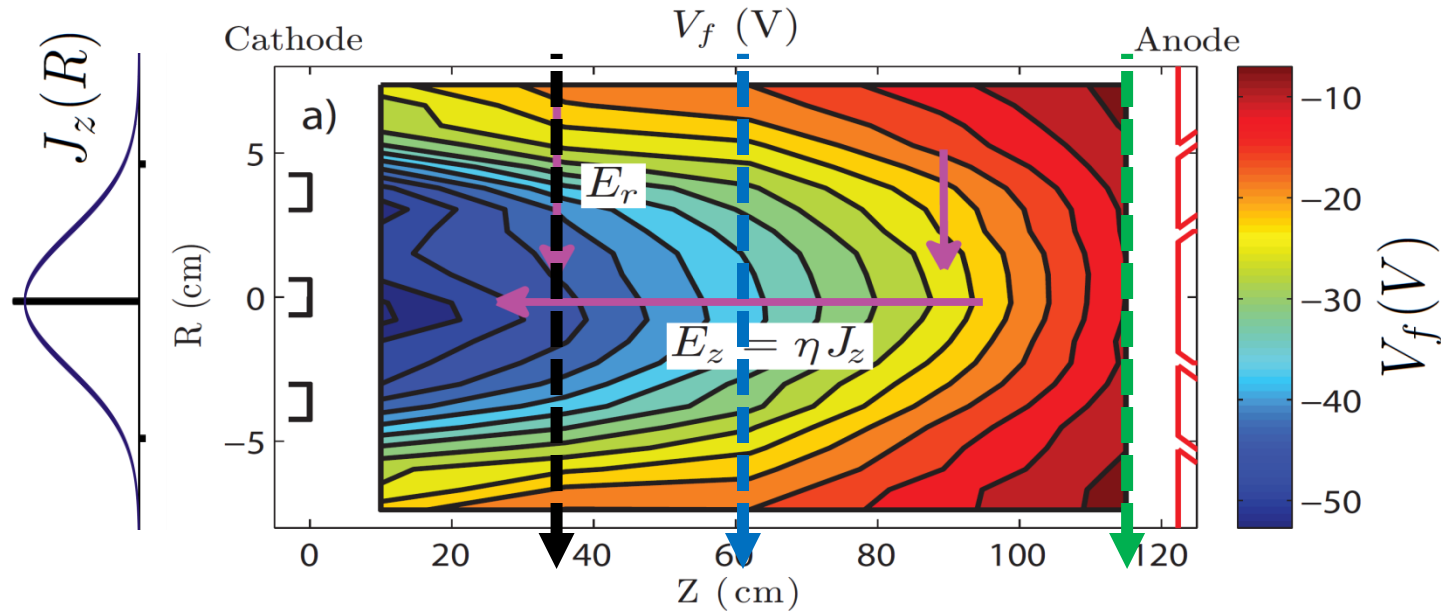


$$\Gamma_{\text{ext}} = 2 \left( \frac{L\pi}{\mu_0} \right) B_{\text{ext}} \tilde{b} \sin \theta$$

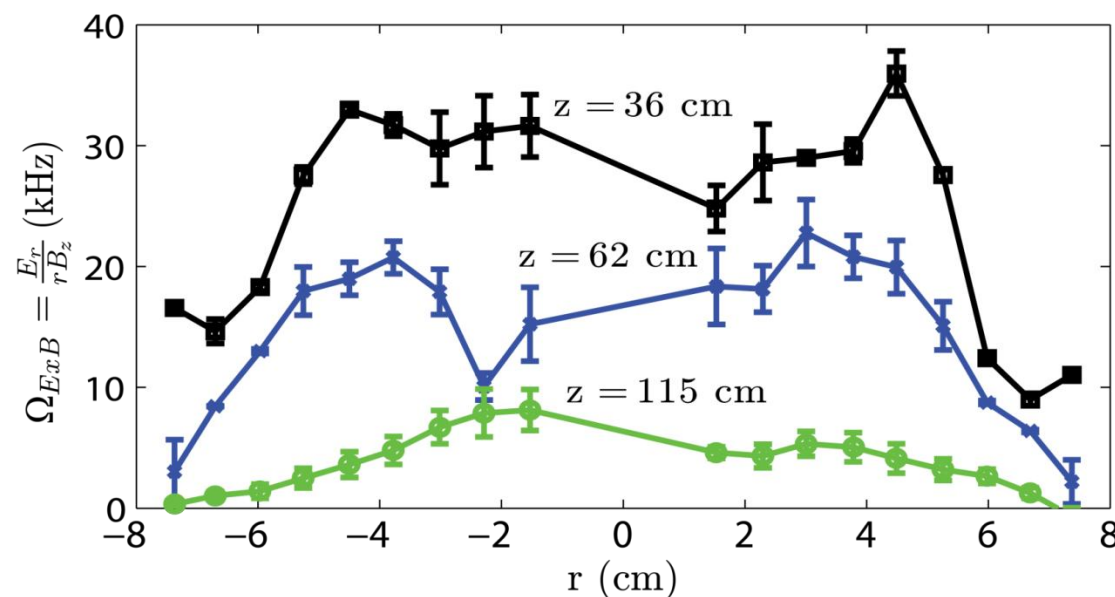
$$\Gamma_{\text{ext}} = \underbrace{A_{\text{ext}} \sin(\theta)}_{\Gamma_{\text{ext}}}$$

- We leave general the relationship between  $\tilde{b}$  and  $B_{\text{ext}}$ 
  - Both are measured

# Offset torque from $E \times B$ rotation



- We measure a radial electric field in the plasma



# Phenomenological restoring torque



- Consider consequence of:  $\omega = \Omega_{\text{ExB}} + \delta\omega$

$$E_r + V_\theta B_z = \eta_\perp J_r \quad V_\theta = r\omega$$

$$J_r = \frac{r B_z}{\eta_\perp} \delta\omega$$

$$\Gamma_{res} = \hat{\theta} \cdot r_a \int_V \vec{J}_0 \times \vec{B}_0 dV$$

$$= L \int_0^{2\pi} d\theta \int_0^{r_p} r^2 J_r B_z dr$$

$$= \frac{\pi}{4} \frac{L B_z^2 r_p^4}{\eta_\perp} (\Omega_{\text{ExB}} - \omega) = \underbrace{A_{\text{res}} (\Omega_0 - \omega)}_{\Gamma_{res}}$$

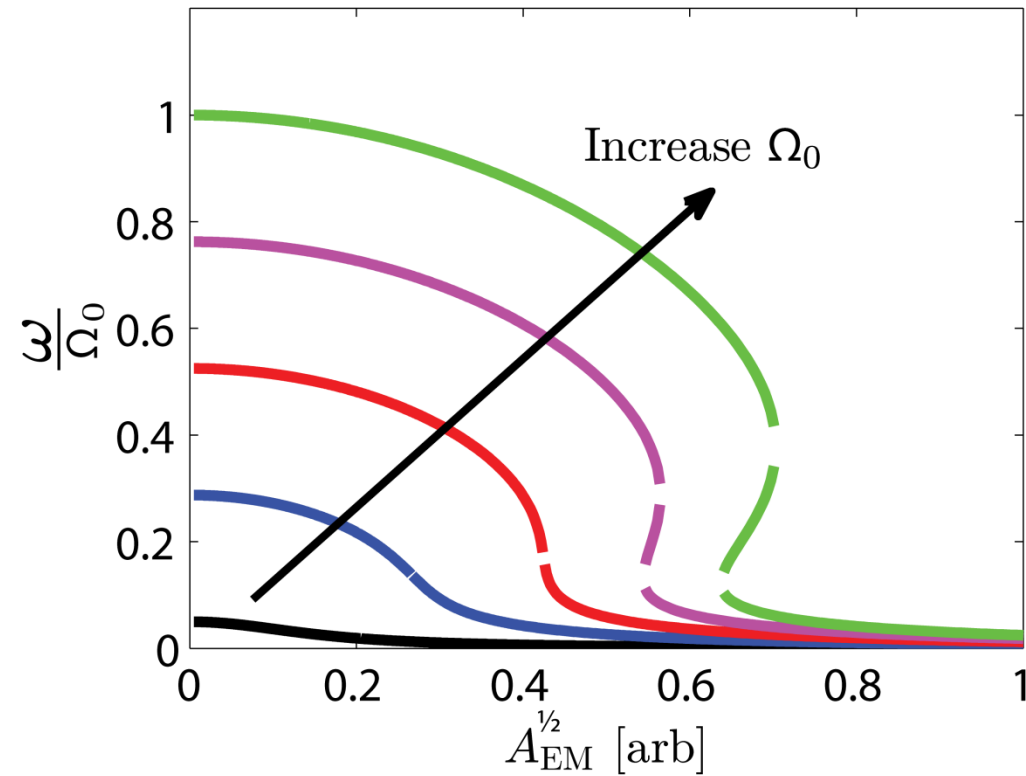
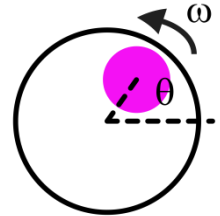
- Would be infinite in ideal MHD
- Comparable to other torques in our cold plasma



# Canonical torque balance



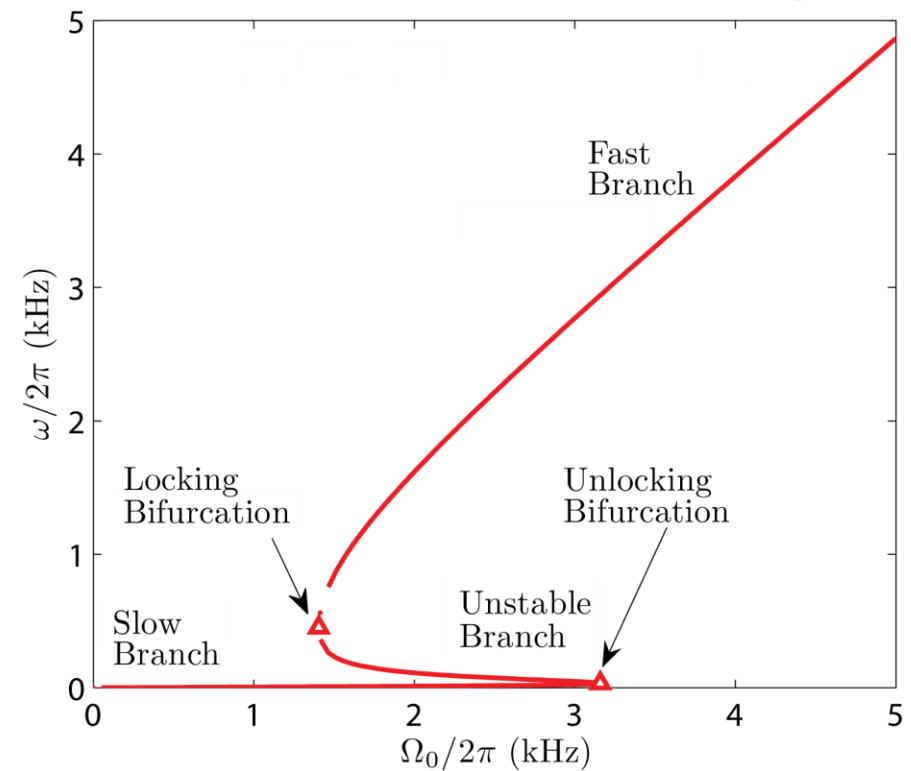
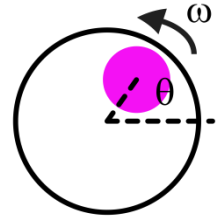
$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}}(\Omega_0 - \omega)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}}$$



# Canonical torque balance



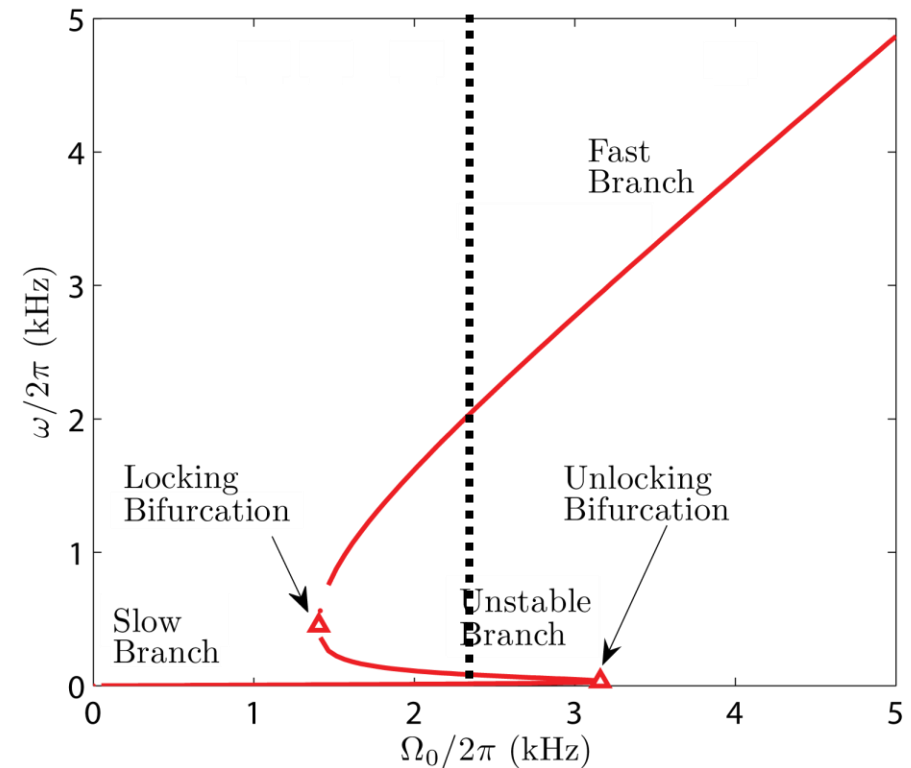
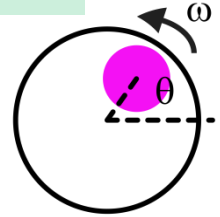
$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}}(\Omega_0 - \omega)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}}$$



# Error field broadens torque curve



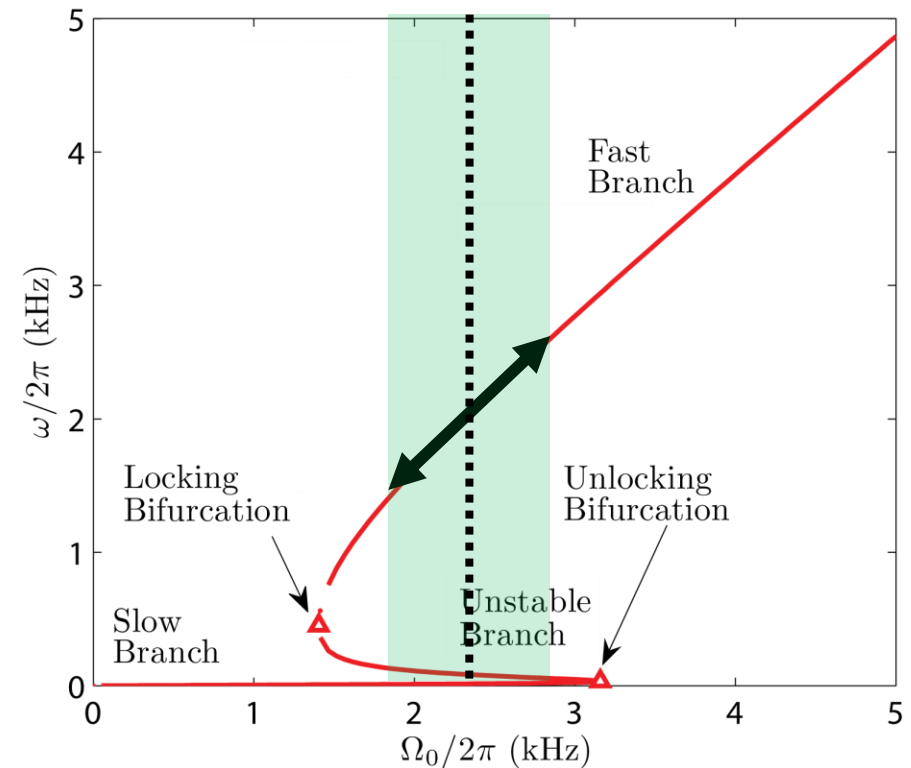
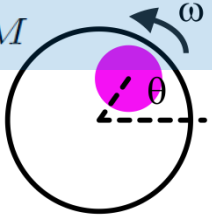
$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}}(\Omega_0 - \omega)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}} + \underbrace{A_{\text{ext}} \sin(\theta)}_{\Gamma_{\text{ext}}}$$



# Error field broadens torque curve



$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}} \left( \left( \Omega_0 + \frac{A_{\text{ext}}}{A_{\text{res}}} \sin(\theta) \right) - \omega \right)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}}$$

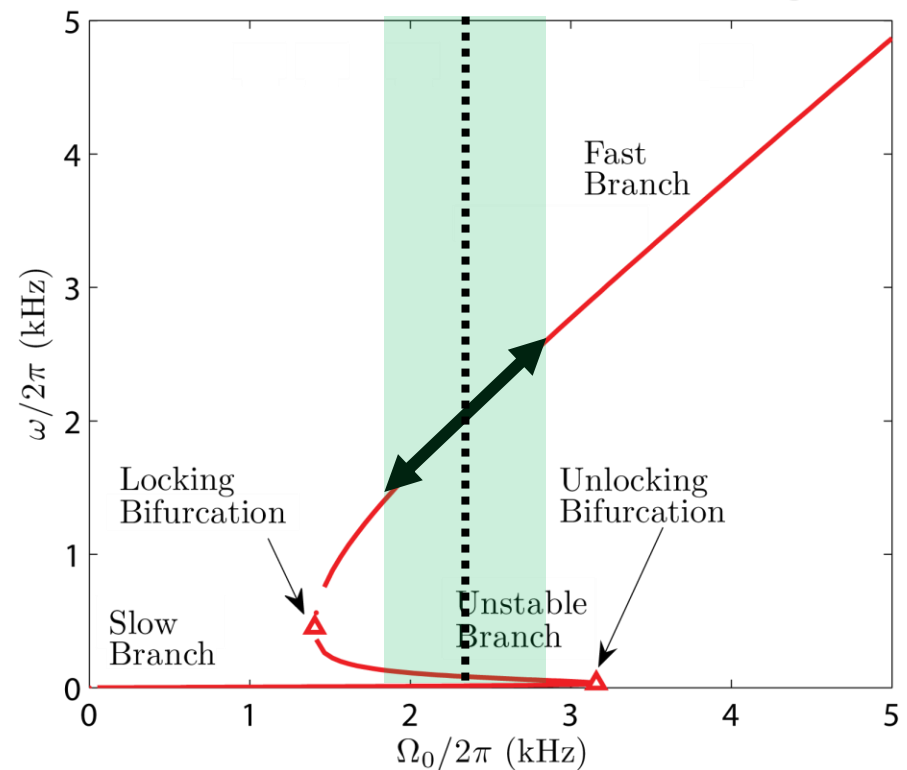
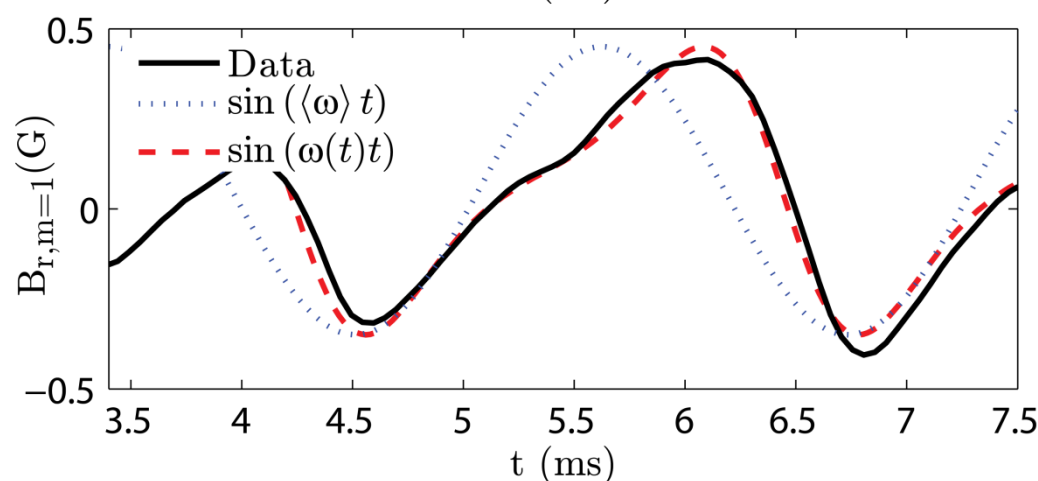
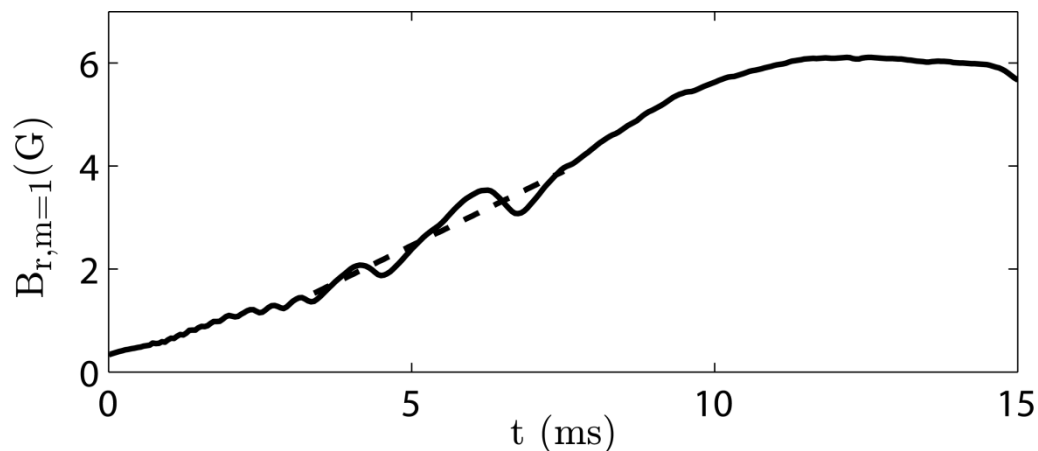
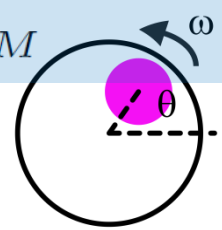


$$\Omega_{0,\text{eff}} = \Omega_0 + \frac{A_{\text{ext}}}{A_{\text{res}}} \sin \theta$$

# $\omega$ is not constant through a cycle



$$I\dot{\omega} = 0 = \underbrace{A_{\text{res}} \left( \left( \Omega_0 + \frac{A_{\text{ext}}}{A_{\text{res}}} \sin(\theta) \right) - \omega \right)}_{\Gamma_{\text{res}}} - \underbrace{A_{EM} \frac{\omega}{1 + (\omega\tau_w)^2}}_{\Gamma_{EM}}$$



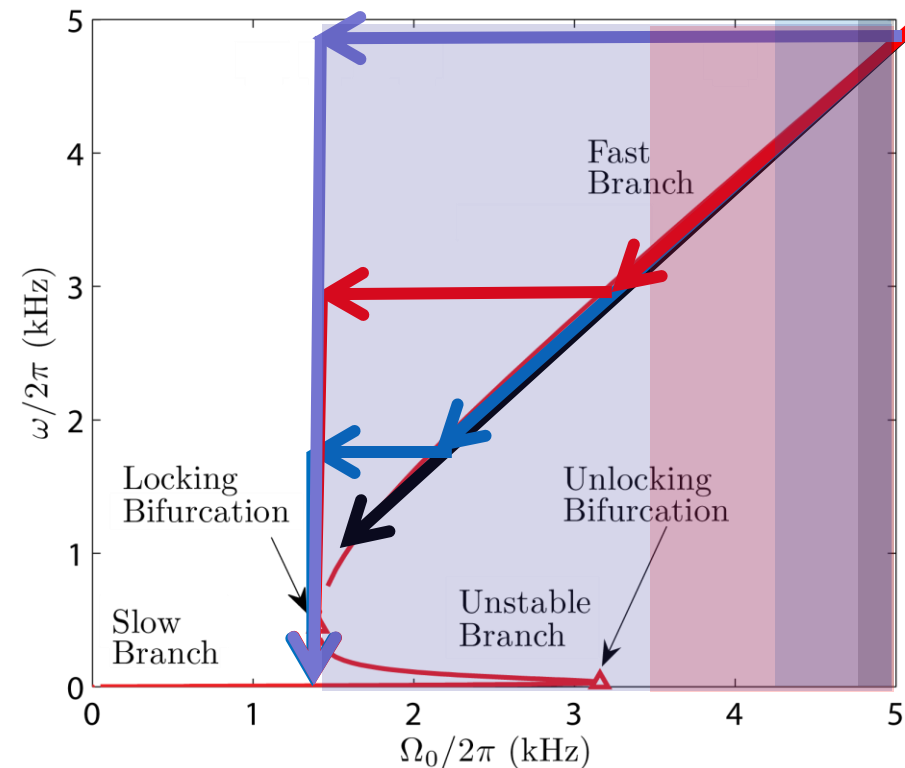
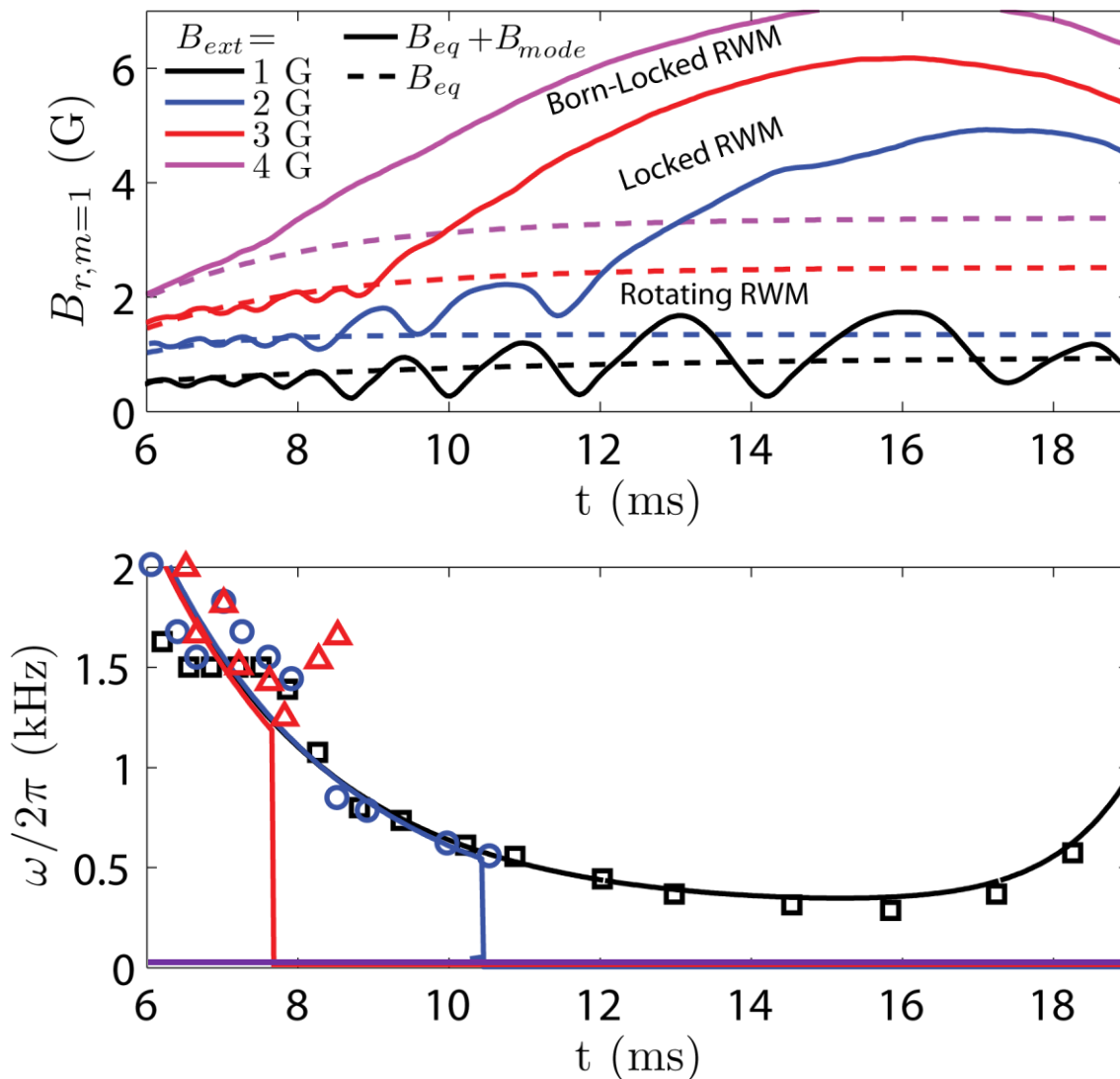
$$\omega(t) = \langle \omega \rangle + \tilde{\omega} \sin(\langle \omega \rangle t)$$

$$\Omega_{0,\text{eff}} = \Omega_0 + \frac{A_{\text{ext}}}{A_{\text{res}}} \sin \theta$$

# $m = 1$ error field aids mode-locking



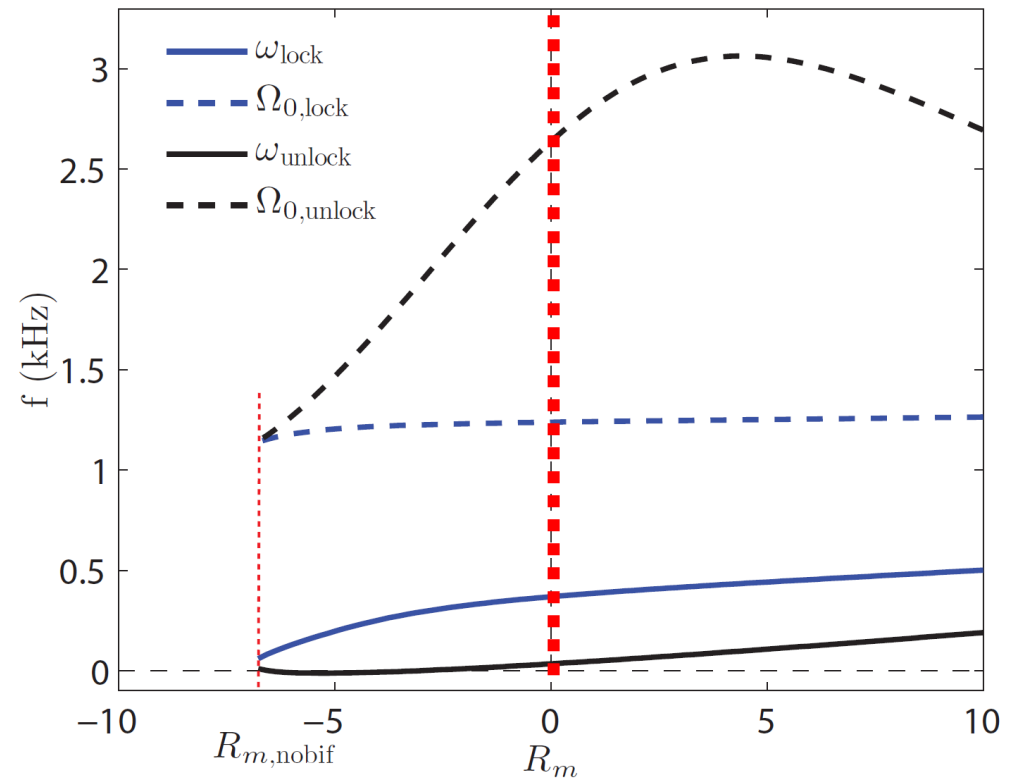
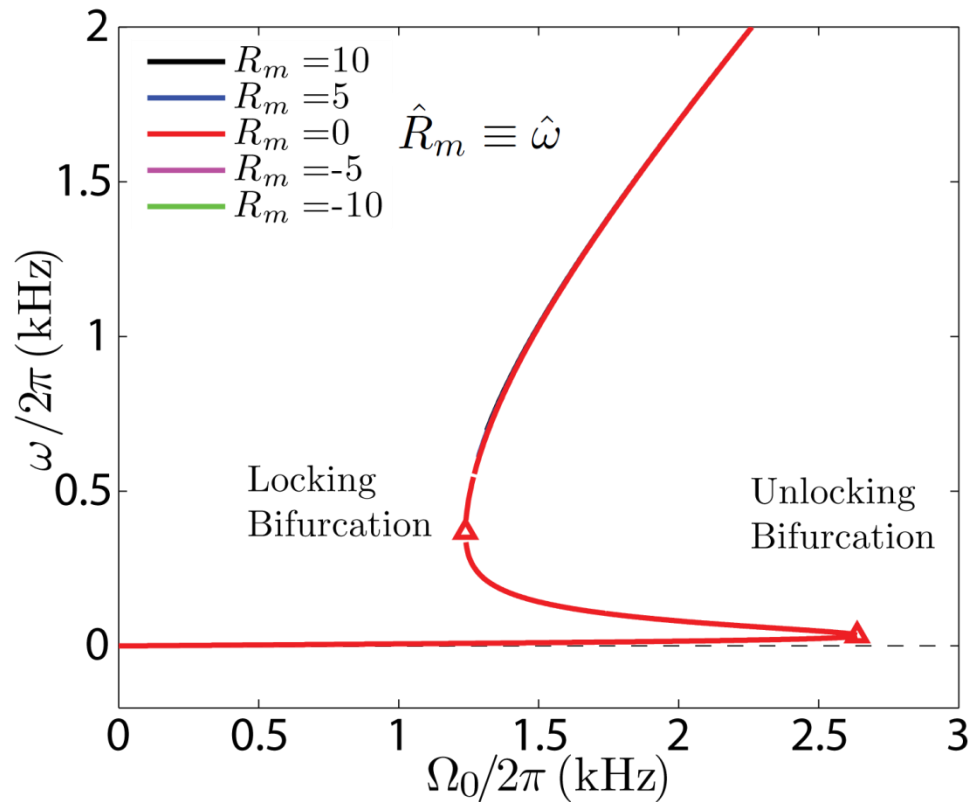
- Error field defines locking regime



$$\Omega_{0,\text{eff}} = \Omega_0 + \frac{A_{\text{ext}}}{A_{\text{res}}} \sin \theta$$

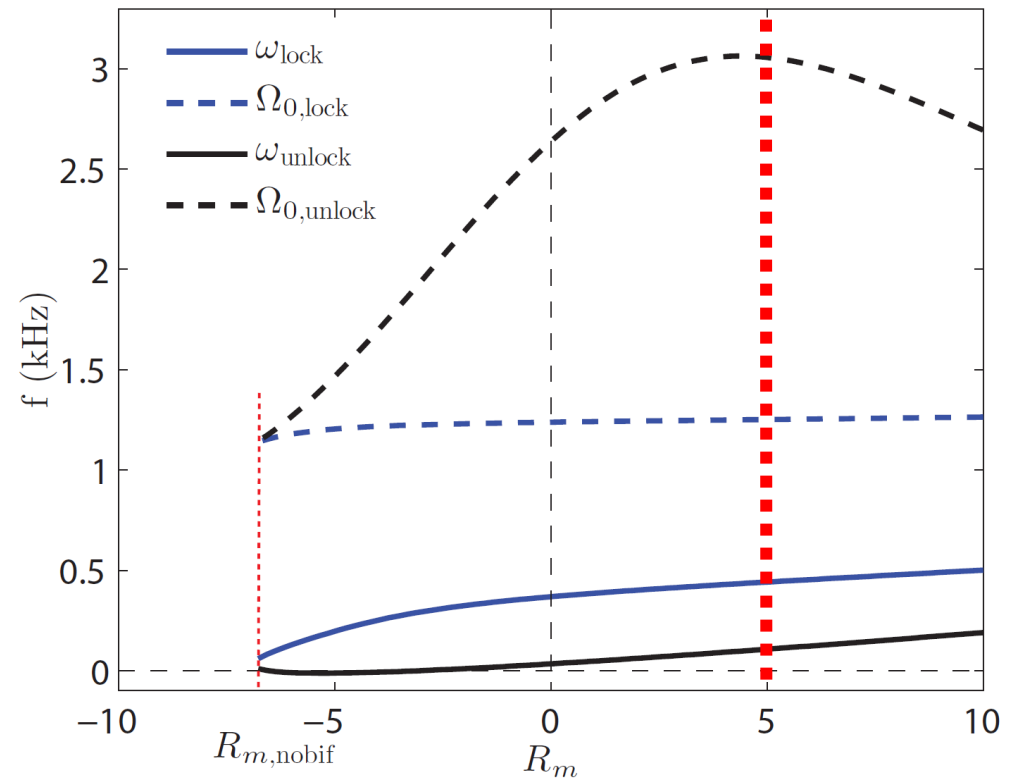
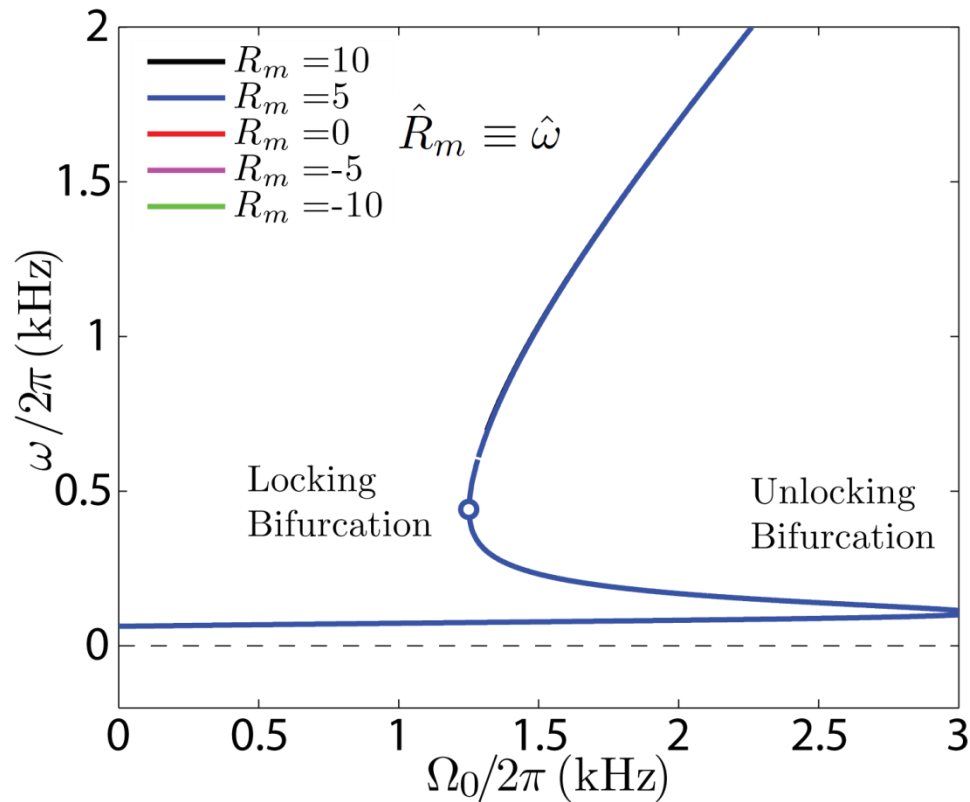


# Bifurcations altered by wall rotation



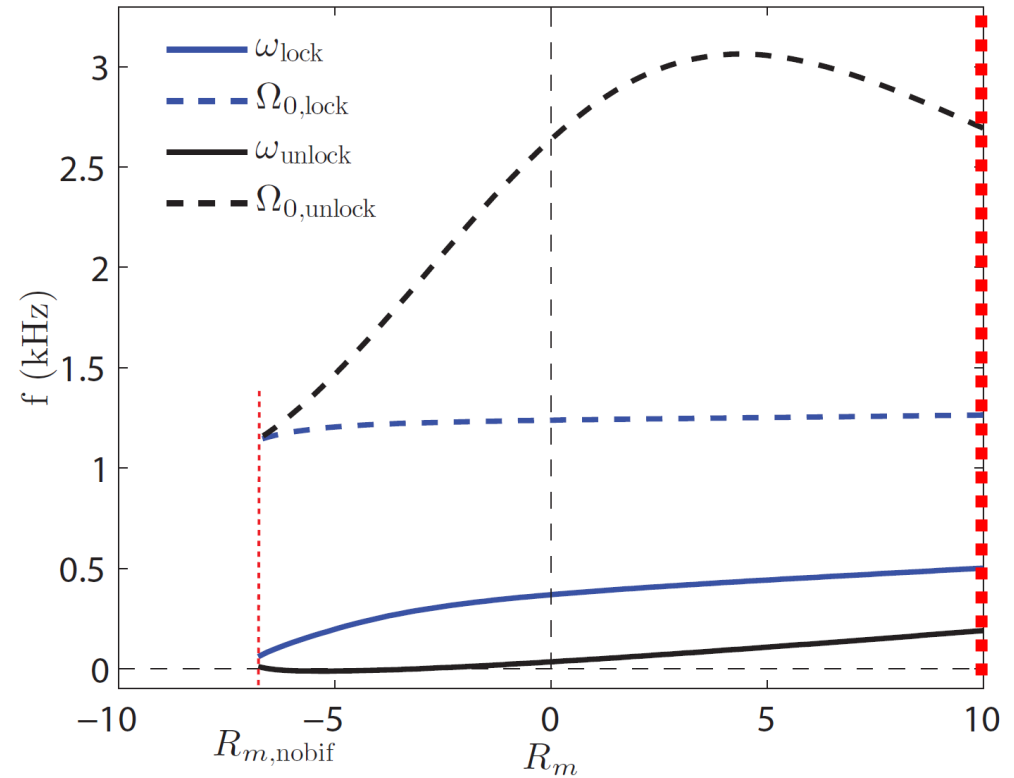
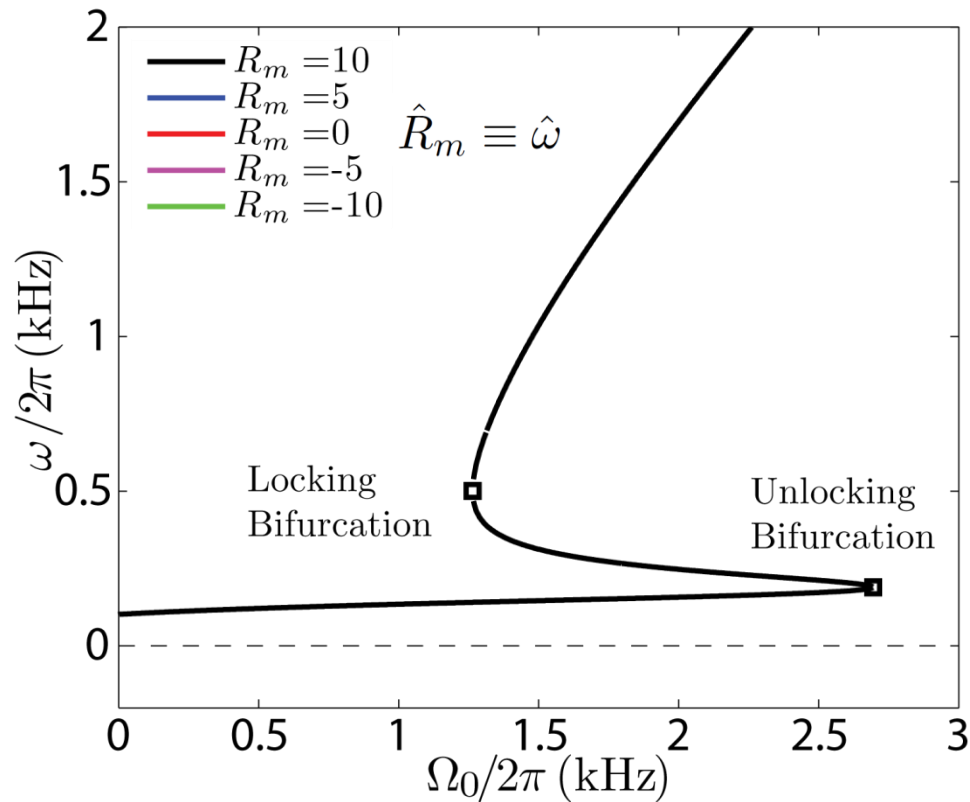
$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



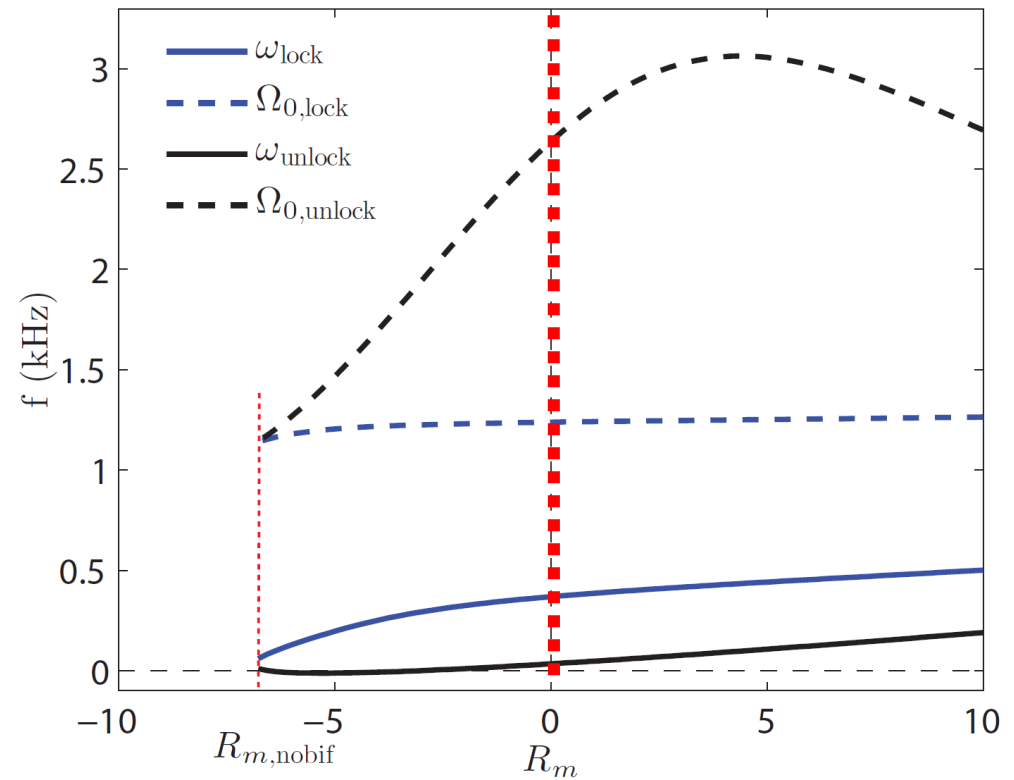
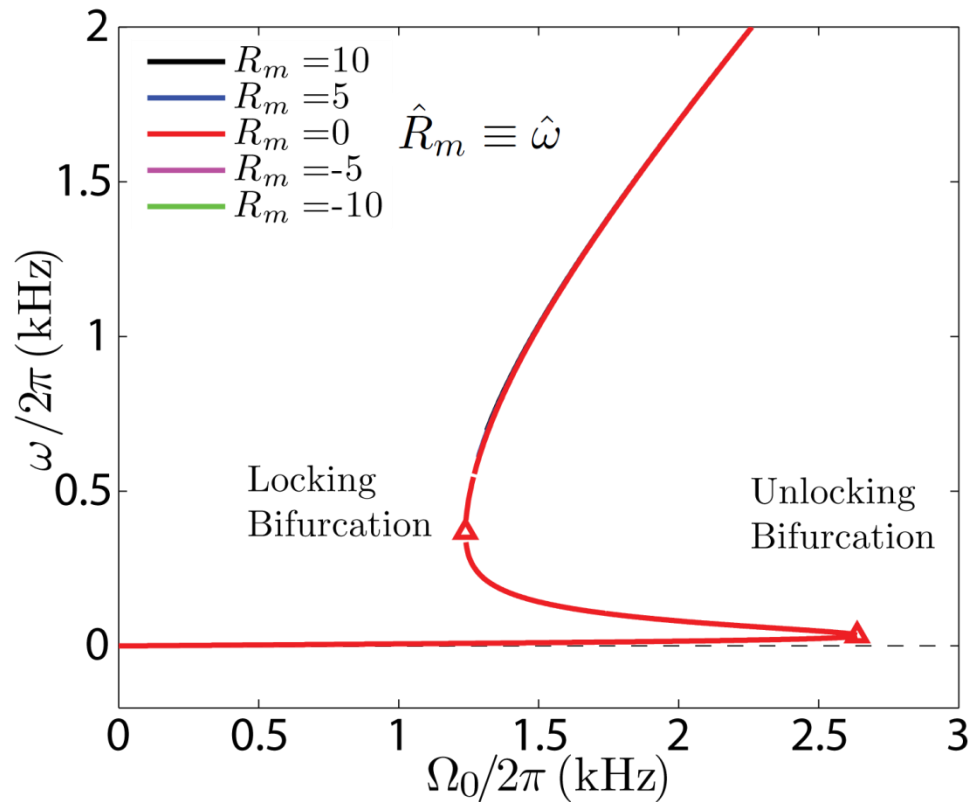
$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



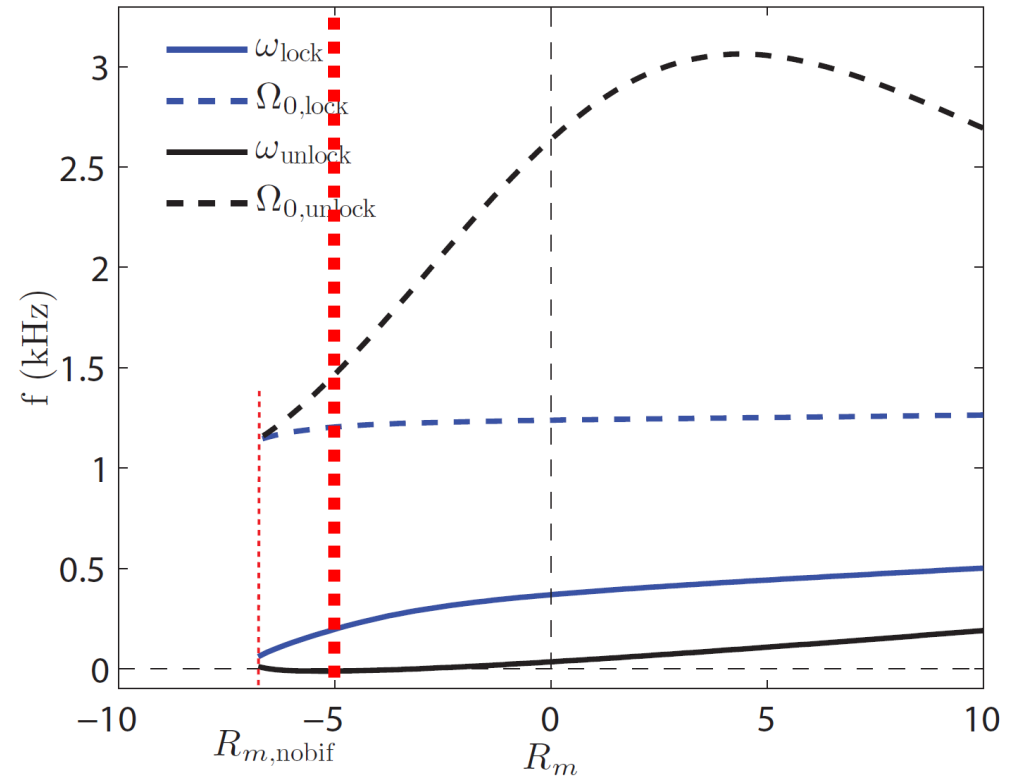
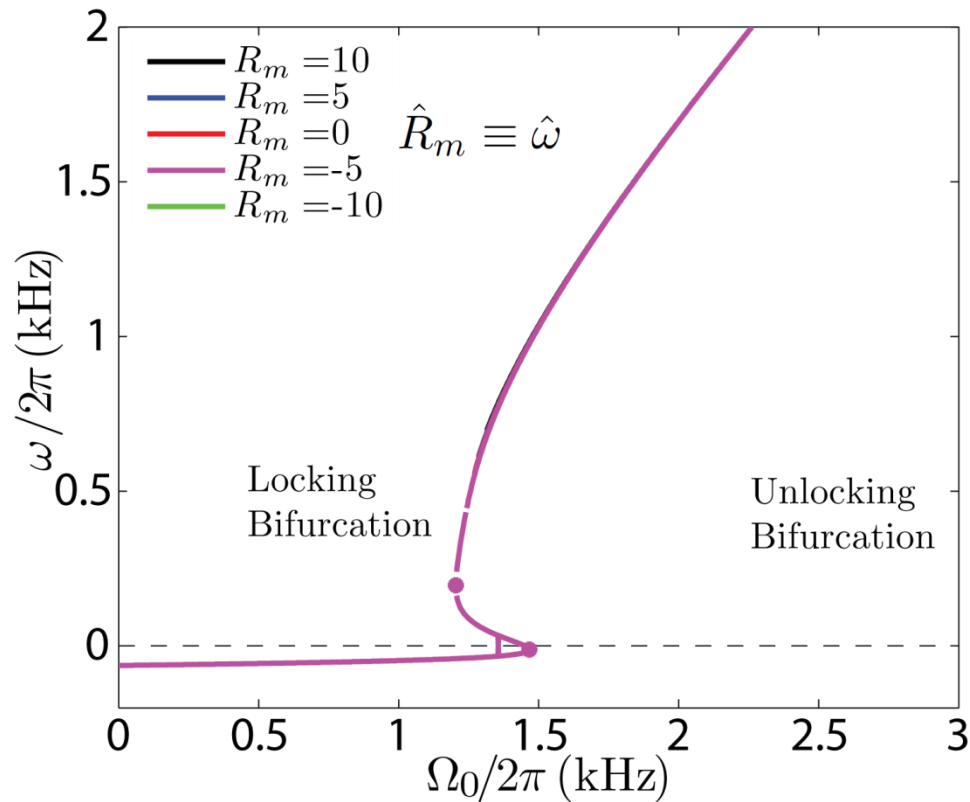
$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



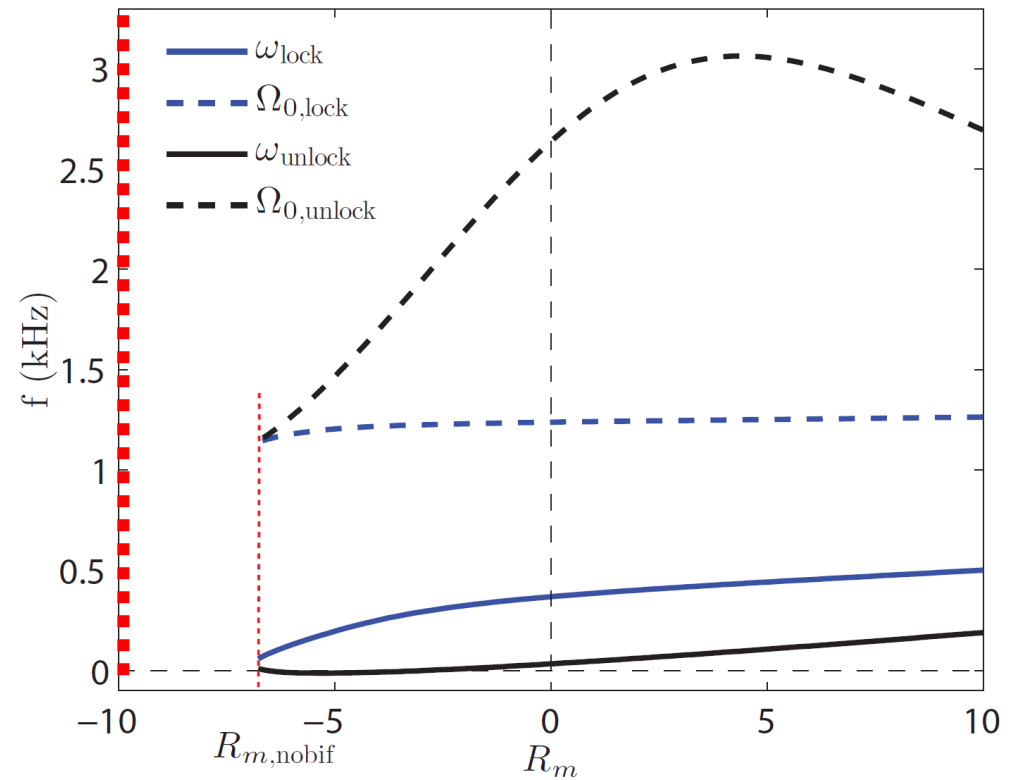
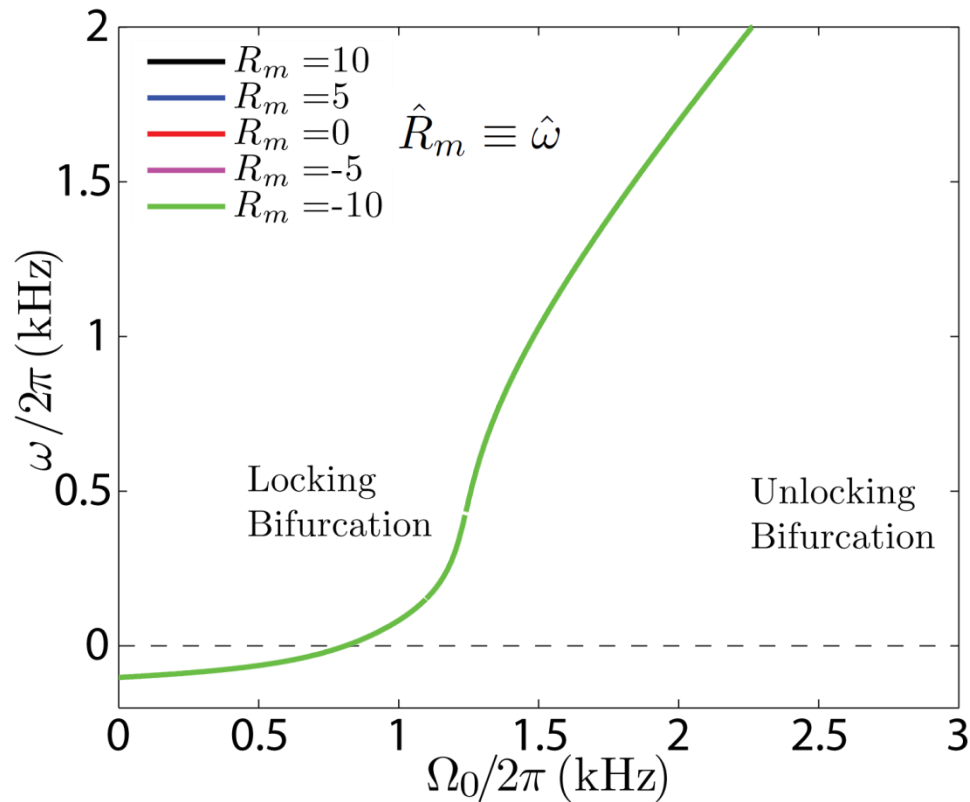
$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



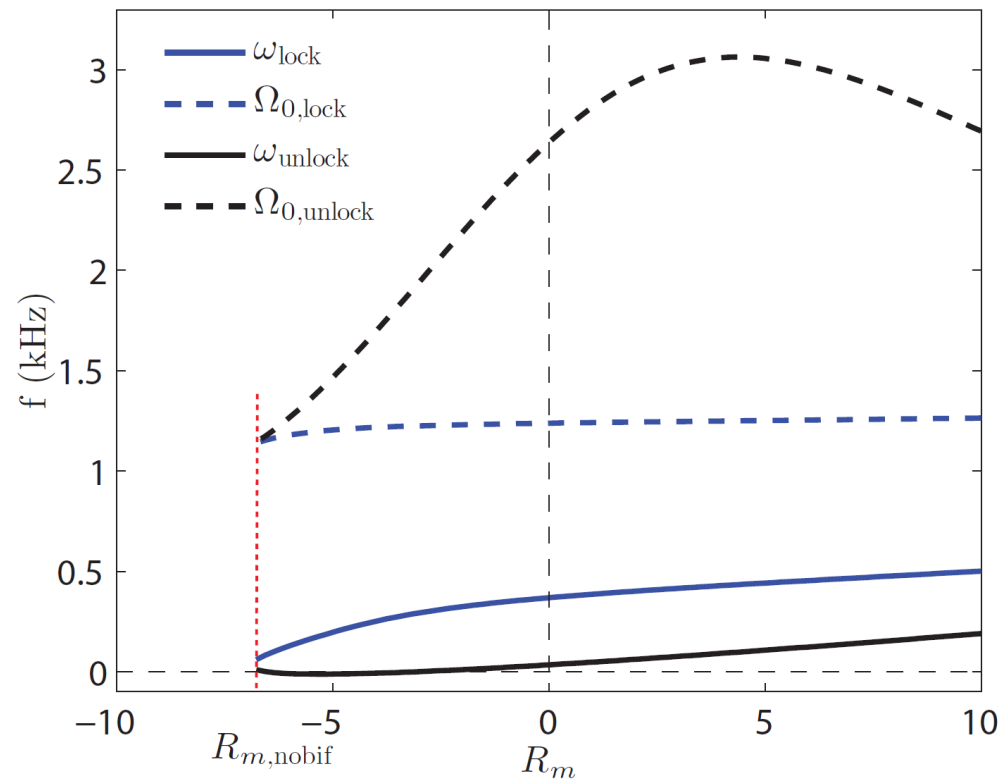
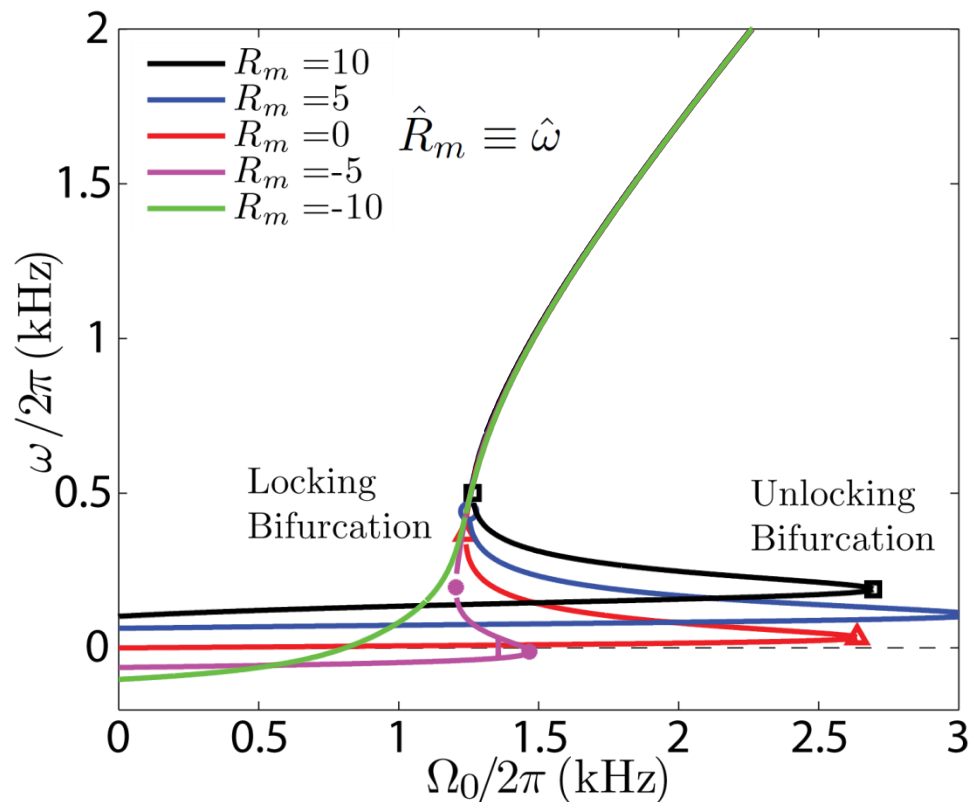
$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



$$\hat{R}_m \equiv \hat{\omega}$$

# Bifurcations altered by wall rotation



$$\hat{R}_m \equiv \hat{\omega}$$

Feedback alters the torque balance, and it depends on the phase

# Conclusions



- Vertical field penetration time decreases as wall rotation increases
- RWM mode-locking in our device shows similar phenomenology to the torus
- Mode-locking modifications by wall rotation explored and demonstrated
  - Active control of  $E \times B$  rotation through bias plates would further this study
  - Analogy to feedback gain will be pursued