

Predictor-based MIMO closed-loop system identification of the EXTRAP T2R reversed-field pinch external plasma response

E Olofsson¹, P Brunsell¹, J Drake¹,
C Rojas², H Hjalmarsson²



¹ Fusion Plasma Physics, ² Automatic Control
School of Electrical Engineering (EES)
Royal Institute of Technology (KTH) Stockholm, Sweden

MHD Control Workshop
Madison, November 15-17 2010

Overview

1

Introduction

- EXTRAP T2R
- The method of dither injection

2

Vector ARX & eigensystem realisation

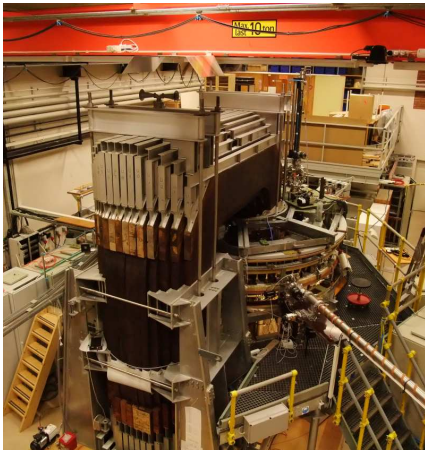
- Overview & results
- Signal model & methods

3

Summary

- Recap

EXTRAP T2R reversed-field pinch (@KTH)



Parameters

- major radius $R=1.24$ m
- plasma minor radius $a=18.3$ cm
- shell norm minor radius $r/a = 1.08$
- shell time constant $\tau_{shell}=6.3$ ms
- plasma current $I_p=80\text{-}160$ kA
- electron temperature $T_e=200\text{-}400$ eV
- pulse length $\tau_{pulse} \leq 90$ ms

Unstable plant

Without stabilisation plasma
“terminates” after $\sim 10\text{-}15$ ms.

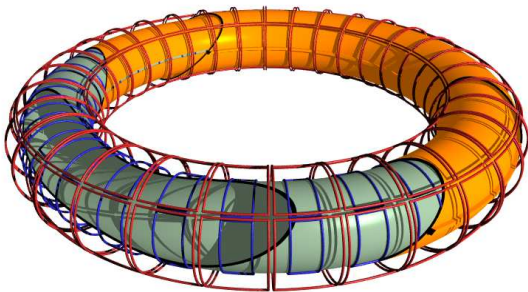
Resistive shell & saddle coils

Location

Sensors inside **shell**.

Actuators outside.

Vacuum vessel
innermost.



RFP RWMs

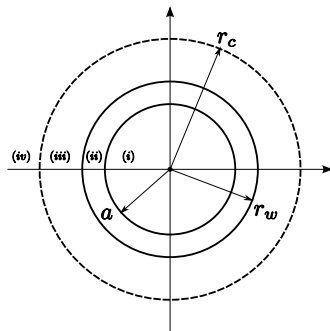
It can be shown that

$$\tau_{m,n} \dot{b}_r^w = \hat{\gamma}_{m,n} b_r^w + a_{m,n} b_r^c \quad (1)$$

where $\hat{\gamma}$ can be computed from an (ideal MHD) RWM dispersion relation,

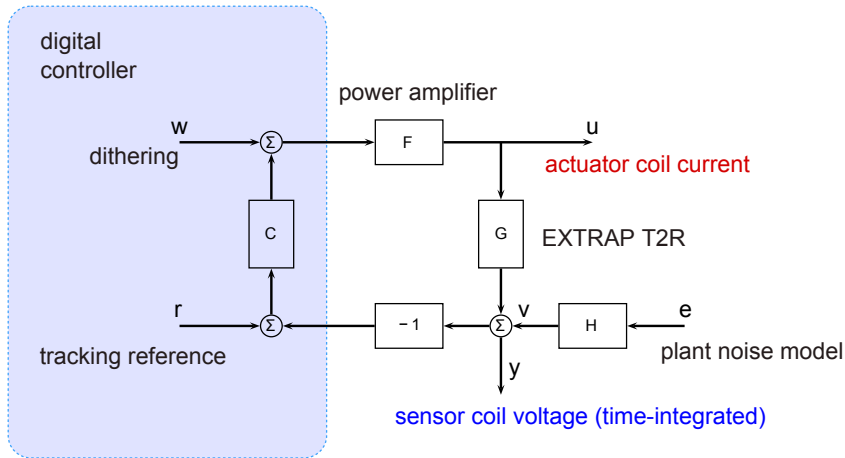
$$\tau_{m,n} = -\tau_w \frac{I_m^{w'} K_m^{w'}}{1 + \frac{m^2}{(n/R)^2 r_w^2}} > 0, \text{ and}$$

$a_{m,n} = -d(n/R)^2 r_c I_m^{w'} K_m^{c'} > 0$. For T2R a cylindrical 1D MHD shooting code is appropriate.

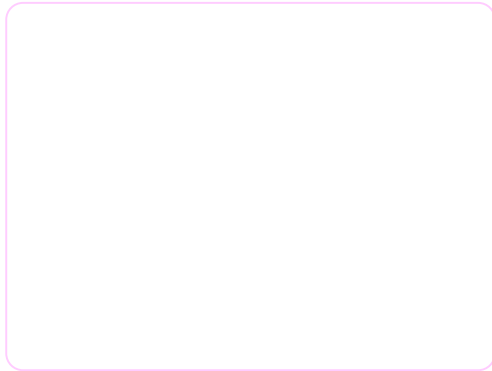


T2R stabilisation; the generalised control loop

Rack of PIDs; the control workhorse

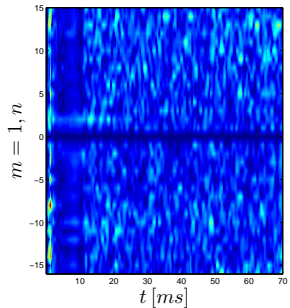


T2R dithering; $r = 0, w \neq 0$



System identification

T2R shot #21816: injected pseudo-randomised dithering.



RFP spectrum from dithering experiments

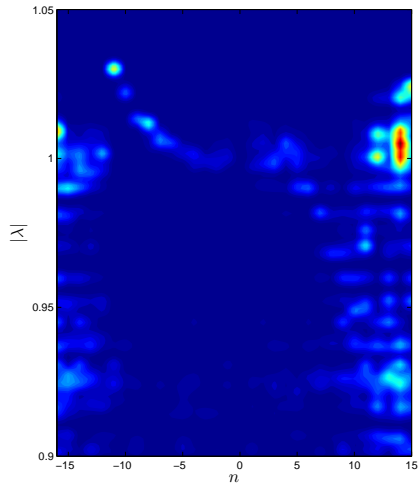
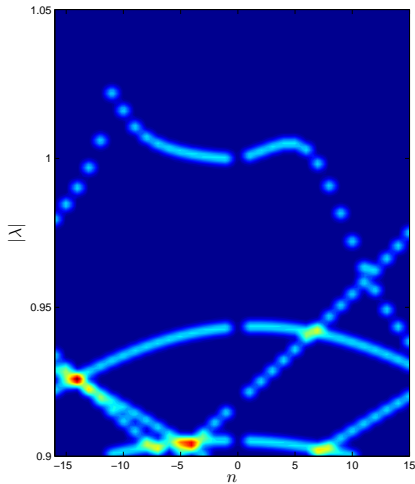
Towards RFP autodetect & autotune?

Multi-input multi-output (MIMO)

- 1 T2R is inherently multivariate; modes are global spatial structures
- 2 MIMO system identification is computationally challenging
- 3 An efficient approach could be to use vector autoregressive exogeneous signal models (ARXs)
- 4 The ARX possess some favourable asymptotic approximation properties for linear time-invariant systems (LTIs)
- 5 Background note: in e.g. industrial MPC projects sysid is the substantial piece (90% of cost)

Comparison of theory & dither experiment analysis

Cylindrical resistive shell theory (left); “nonregularised” system identification (right)



Some observations & remarks

Method

- Not step-response measurement; full spectrum autodetect
- More shots \Rightarrow more statistics \Rightarrow better precision
- LTI assumed; “truth” of this hinges on RFP equilibrium
- Model control-relevant; acquired under operating conditions

Some observations & remarks

Method

- Not step-response measurement; full spectrum autodetect
- More shots \Rightarrow more statistics \Rightarrow better precision
- LTI assumed; “truth” of this hinges on RFP equilibrium
- Model control-relevant; acquired under operating conditions

Obtained spectrum

- Resemblance of RFP theory without regularisation
- “Unexpected” features: high- n density of unstable modes
- Possibilities?
 - 1 Method bias; coloured noise, closed-loop influence
 - 2 Real physics; pressure-driven ideal nonresonant MHD shell modes (observed in HBTX1C, P.M. Cox PPCF 1990)

The autoregressive exogeneous (ARX) model

Vector ARXs can be estimated very efficiently. But it is overparameterised.

The

ARX(n_α, n_β)

$$\mathbf{y}(k) = \sum_{i=1}^{n_\alpha} A_i \mathbf{y}(k-i) + \sum_{i=1}^{n_\beta} B_i \mathbf{u}(k-i) + \mathbf{e}(k) \quad (2)$$

is here used as a vehicle to estimate a general

Discrete-time LTI MIMO state-space system

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k) \quad (3)$$

$$\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) \quad (4)$$

Predictor form & Markov block coefficients

Various tools to go from (2) to (3)-(4).

Predictor recast of vector ARX

$$\hat{\mathbf{x}}(k+1) = A_K \hat{\mathbf{x}}(k) + B_K \begin{pmatrix} \mathbf{u}(k) \\ \mathbf{y}(k) \end{pmatrix} \quad (5)$$

$$\hat{\mathbf{y}}(k) = C_K \hat{\mathbf{x}}(k) \quad (6)$$

so that the impulse response matrices

Markov coefficient

$$H(k) = C_K A_K^k B_K \in \mathbb{R}^{n \times (n+m)}, \quad k \geq 0 \quad (7)$$

are stable. Here n is the number of outputs and m the number of inputs.

The eigensystem realisation algorithm (ERA)

Creates a particular LTI state-space system from the impulse response

ERA is based on the singular value decomposition (SVD) of

Hankel matrix

$$H_0^{f,p} = \begin{pmatrix} H(0) & H(1) & H(2) & \dots & H(p-1) \\ H(1) & H(2) & H(3) & \dots & \\ H(2) & H(3) & H(4) & \dots & \\ H(3) & \dots & & & \\ \vdots & & & & \\ H(f-1) & \dots & & & H(f+p-2) \end{pmatrix} \quad (8)$$

i.e. a factorisation $H_0^{f,p} = U\Sigma V^T$. From U, Σ, V it is then possible to extract/compute an estimate of the system matrices (A, B, C) of (3)-(4). The eigenvalues/eigenvectors of A are then visualised.

What was done

(and some extrapolation)

- 1 Dither-injected RFP experiments performed
- 2 Direct MIMO LTI discrete-time state-space system estimation
- 3 Comparison to ideal MHD resistive shell theory
- 4 Autodetected model looks “physical” and is control-relevant by construction (RWM control mainly)
- 5 Most unstable empirical eigenmode is monochromatic and directly mapped to theory
- 6 Possible immediate extension: general and systematic approach to measure the in situ experimental plasma response (wanted in e.g. RMP & ELM research)

Some references

Thank you for your attendance.

- P.M. Cox. "Pressure-driven thin-shell instabilities in HBTX1C". *Plasma Physics and Controlled Fusion*, 32(14):1321, 1990.
- J.N. Juang, R.S. Pappa. "An eigensystem realization algorithm for modal parameter identification and model reduction". *Journal of Guidance, Control and Dynamics*, 8(5):620-627, 1985.
- C. Bishop, "An intelligent shell for the toroidal pinch" *Plasma Physics and Controlled Fusion*, vol. 31, no. 7, pp. 1179-1189, 1989. <http://stacks.iop.org/0741-3335/31/1179>
- P. Brunzell et al., "Initial results from the rebuilt EXTRAP T2R RFP device", *Plasma Physics and Controlled Fusion*, vol. 43, no. 11, p. 1457-1470, 2001
- P. Brunzell et al., "Feedback stabilization of multiple resistive wall modes", *Physical Review Letters*, vol. 93, no. 22, p. 225001, 2004. <http://link.aps.org/abstract/PRL/v93/e225001>
- T. Söderström, P. Stoica, "System identification". *Prentice Hall*, 1989.
- S.J. Qin. "An overview of subspace identification". *Computers and Chemical Engineering*, 30:1502-1513, 2006.
- E. Olofsson, H. Hjalmarsson, C. Rojas, P. Brunzell, and J. Drake, "Vector dither experiment design and direct parametric identification of reversed-field pinch normal modes", *Proceedings of the 48th IEEE Conference on Decision and Control*, December 2009
- E. Olofsson, C. Rojas, H. Hjalmarsson, P. Brunzell, and J. Drake, "Closed-loop MIMO ARX estimation of concurrent external plasma response eigenmodes in magnetic confinement fusion", *Proceedings of the 49th IEEE Conference on Decision and Control*, accepted (to appear), December 2010 (**precursor study**)
- E. Olofsson. "Closed-loop control and identification of resistive shell magnetohydrodynamics for the reversed-field pinch". *Licentiate Thesis*, TRITA-EE 2010:019, Royal Institute of Technology (KTH), May 2010.