#### Error field threshold in NBI heated H-modes

#### By Holger Reimerdes<sup>1</sup>

In collaboration with

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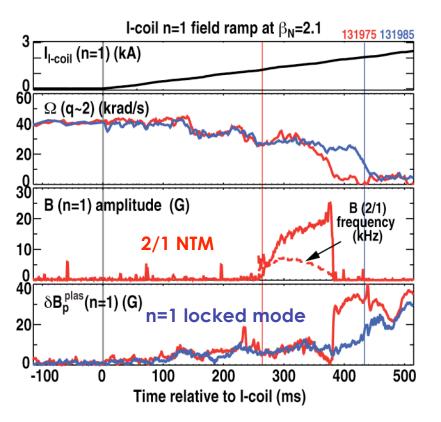
#### Outline/Main results

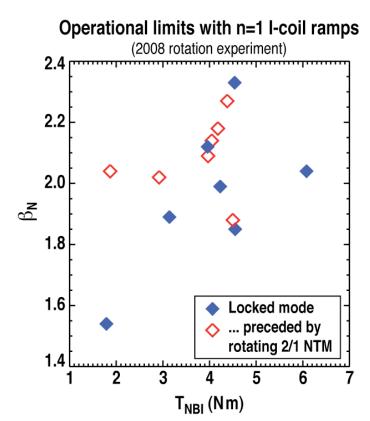
- Resonant braking leading to a loss of torque balance determines the "ultimate" n=1 error field threshold in NBI heated H-modes
- Decrease of n=1 error field tolerance with increasing  $\beta$  is caused by an increasing plasma amplification
- Plasma is sensitive to kink-resonant rather than pitch-resonant external fields
- Plasma response leads to a resonant and non-resonant magnetic torque





#### External non-axisymmetric "error" fields limit NBI heated H-modes by inducing locked modes or by "triggering" NTMs





- NTM is born in the plasma frame, i.e. it rotates with the plasma
  - NTM onset predominantly observed at higher  $\beta_N$  and lower NBI torque  $\rightarrow$  R. Buttery "Effect of 3D fields near the tearing beta limit" on Tuesday
- Locked mode is always born locked to the vessel → This talk



#### At low $\beta$ , NBI heating generally increases the error field tolerance

- Beneficial effect has been attributed to the toroidal torque associated
   with NBI heating leading to higher rotation [R.J. La Haye, et al., Nucl. Fusion (1992)]
  - Error field threshold (JET L-modes)
     consistent with

$$\delta B_{crit}^{ext} \propto \Omega_0^{0.5}$$

scaling ( $\Omega_0$  is the unperturbed rotation before the external field is applied) [E. Lazzaro, et al., *Phys. Plasmas* (2002)]

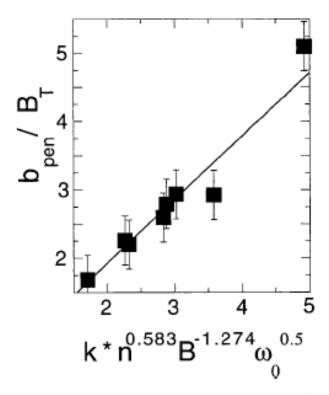


FIG. 7. Scaling of the penetration threshold vs power law  $\sim n^{0.58}B^{-1.274}\omega_0^{1/2}$  where  $\omega_0$  the local angular rotation frequency at the q=2 surface.

Figure from Lazzaro, et al., Phys. Plasmas (2002)



#### At intermediate values of $\beta$ , the increase of the error field tolerance with NBI heating (and hence $\beta$ ) roles over

• Early high  $\beta$  experiments in DIII-D have already revealed a strong reduction of the error field tolerance with  $\beta$ 

[R.J. La Haye, et al., Nucl. Fusion (1992)]

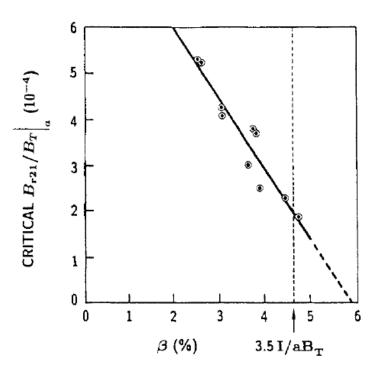


FIG. 10. Critical 2, I relative error field for instability in H-mode plasmas as a function of beta (left or left/right beams).

Figure from La Haye, et al., Nucl. Fusion (1992)

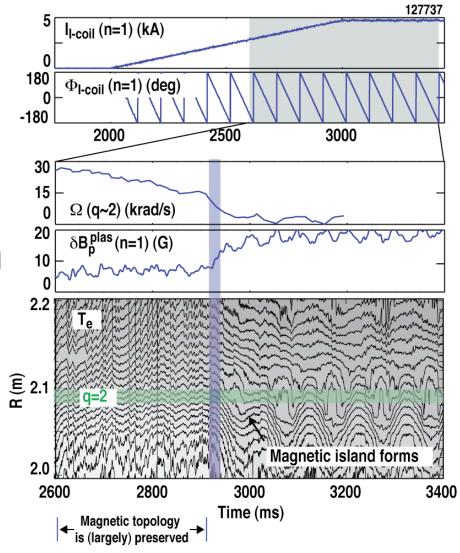


#### Error field tolerance in NBI heated H-modes is determined by resonant braking leading to a loss of torque balance

• Increase the amplitude of a slowly rotating (10Hz) externally applied n = 1 "error" field  $\delta B^{\rm ext} \propto I_{\rm l-coil}$ 



- Rotation evolution is described by resonant braking [Garofalo, et al., Nucl. Fusion 47 (2007) 1121]
  - At high rotation the resonant field is shielded, but exerts a torque
  - Rotation decrease is followed by a loss of torque balance
- Magnetic island observed only after rotation collapses





## Resonant magnetic braking torque leads to a bifurcation of the plasma rotation

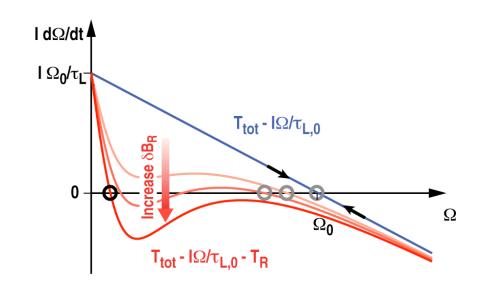
0D-model for plasma rotation

$$I \frac{d\Omega}{dt} = T_{\text{in}} - \frac{I\Omega}{\tau_{\text{L.O}}} - T_{\text{MB}}$$

with  $\tau_{\text{L},0}$  being the momentum confinement time without braking

• Assume a resonant magnetic braking torque with  $T_{\rm R} \propto \Omega^{-1}$  [R. Fitzpatrick, Nucl. Fusion (1993)]

$$T_{\rm MB} \rightarrow T_{\rm R} = K_{\rm R} \delta B_{\rm R}^2 \Omega^{-1}$$



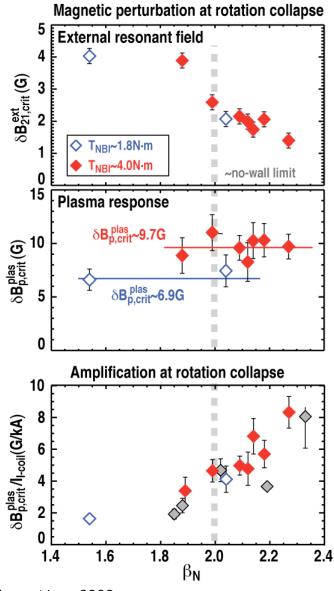
- Torque balance  $d\Omega/dt = 0$  when  $\Omega = \frac{T_{\rm in}\tau_{\rm L,0}}{2I} \pm \sqrt{\left(\frac{T_{\rm in}\tau_{\rm L,0}}{2I}\right)^2 \frac{K_{\rm R}\tau_{\rm L,0}}{I}} \delta B_{\rm R}^2$ 
  - Bifurcation at  $\Omega = \frac{\Omega_0}{2}$  (with  $\Omega_0 = \frac{I_{\rm in}\tau_{\rm L,0}}{I}$  being the unperturbed rotation), when resonant perturbation exceeds  $\delta B_{\rm R,crit} = T_{\rm in} \sqrt{\frac{\tau_{\rm L,0}}{4IK_{\rm R}}}$



## Decrease of n=1 error field tolerance with increasing $\beta_N$ is attributed to plasma amplification

[Reimerdes, et al., Nucl. Fusion (2009)]

- Decrease of critical external field  $\delta B_{21,\text{crit}}^{\text{ext}}$  (SURFMN) at  $T_{\text{NBI}} = \text{const.}$  is particularly strong above the no-wall limit
  - External field is also increasingly amplified
- Rotation collapse occurs at a fixed plasma response  $\delta B_{\rm p,crit}^{\rm plas}$
- Critical plasma response  $\delta B_{\rm p,crit}^{\rm plas}$  increases (as expected) with NBI torque  $T_{\rm NBI}$





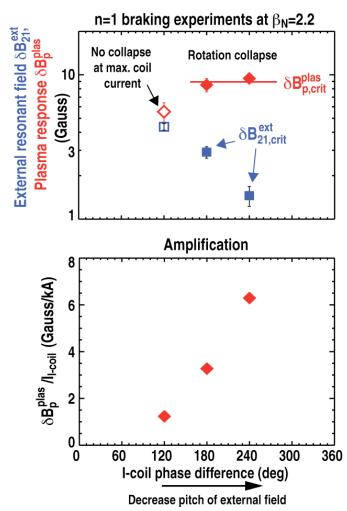
## Dependence on the poloidal spectrum of the external field is also attributed to plasma amplification

- Critical external field  $\delta B_{21,\text{crit}}^{\text{ext}}$  at const. NBI torque and const.  $\beta_{\text{N}}$  changes with I-coil phasing (by more than a factor of 3)
  - Amplification changes, too
- Rotation collapse occurs at a fixed plasma response  $\delta B_{\mathrm{p.crit}}^{\mathrm{plas}}$



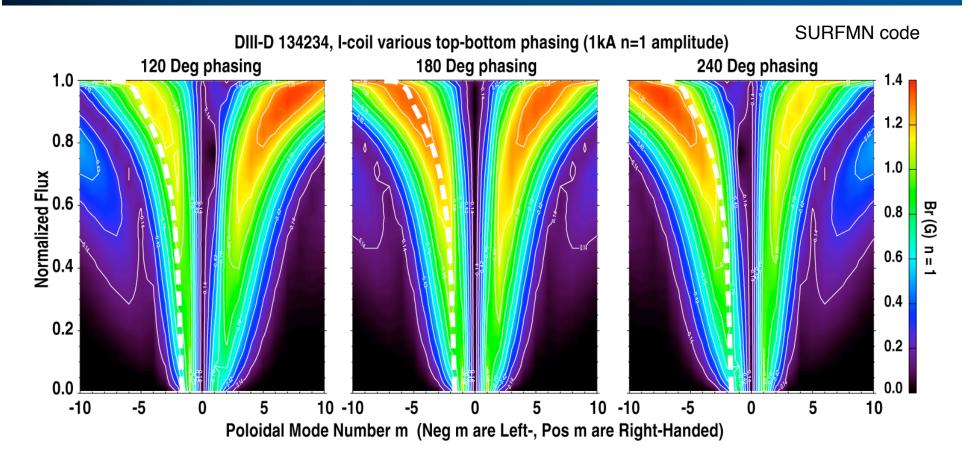
Resonant braking and hence error field tolerance is determined by the external field that is kink-mode resonant - not pitch-resonant at the q=2 surface

- Pointed out by Park, et al. for low density locked modes [Park, et al, Phys. Rev. Lett. (2007)]
- → Details in talk by M. Lanctot, "Measurement and modeling of 3D tokamak equilibria" on We





#### At the LFS, plasma is most sensitive to an external field with a lower pitch angle than the equilibrium field



$$\rightarrow \delta B_{\rm p}^{\rm plas} = 1.2G$$

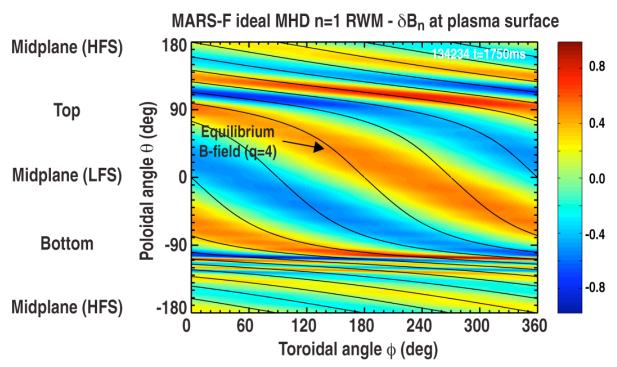
$$\rightarrow \delta B_{\rm p}^{\rm plas} = 3.3 {\rm G}$$

$$\rightarrow \delta B_{\rm p}^{\rm plas} = 6.3G$$



Largest response when m>n\*q components large

### Kink mode (and the most sensitive external field) does not always follow the equilibrium field



- Fourier harmonics of the external field that the plasma is most sensitive to depend on the geometry of the external coil (e.g. LFS vs. HFS coils)
  - Exact characterization requires several harmonics + their phases
- $\rightarrow$  Fourier harmonics of  $\delta B^{\rm ext}$  in straight field line coordinates are NOT an efficient description of the error field tolerance



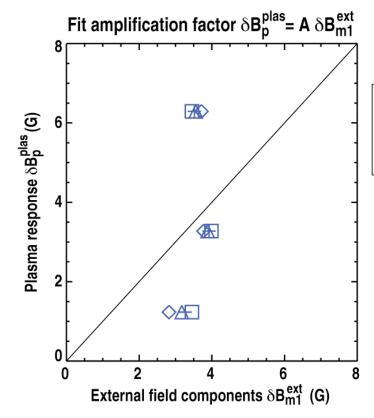
Correlate various Fourier harmonics of the external field (SURFMN) with the

measured plasma response

Fit amplification factor A

$$\delta B_{\rm p}^{\rm plas} = A \, \delta B_{\rm mn}^{\rm ext}(q)$$

 Resonant components match poorly



δΒ	Α	RMSD (G)
□ 2/1 (q=2)	3.56	1.30
+ 3/1 (q=3)	3.11	1.24
△ 4/1 (q=4)	2.97	1.20
♦ Br (a)	2.88	1.08



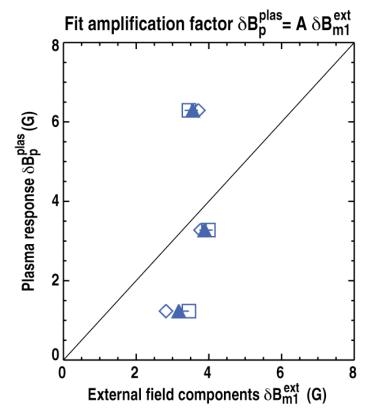
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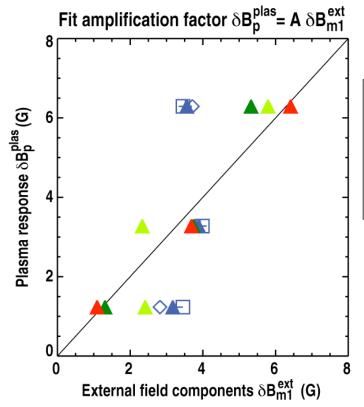
Fit amplification factor A

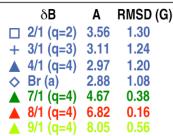
$$\delta B_{\rm p}^{\rm plas} = A \, \delta B_{\rm mn}^{\rm ext}(q)$$

- Resonant components match poorly
- Most sensitive field  $\delta B_{mn}$

$$m = 2nq$$

(consistent with M. Schaffer's rule of thumb)







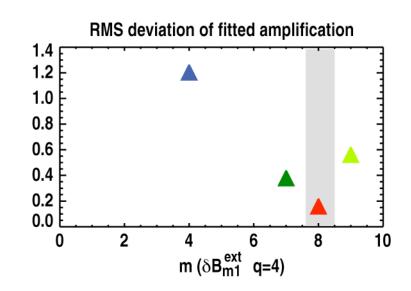
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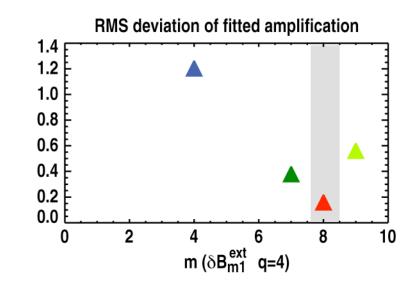
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(consistent with M. Schaffer's rule of thumb)



 $\rightarrow$  Use measured plasma response ( $\propto$  total perturbed field) for further studies



## Observed dependence of error field tolerance on torque input weaker than prediction for resonant braking

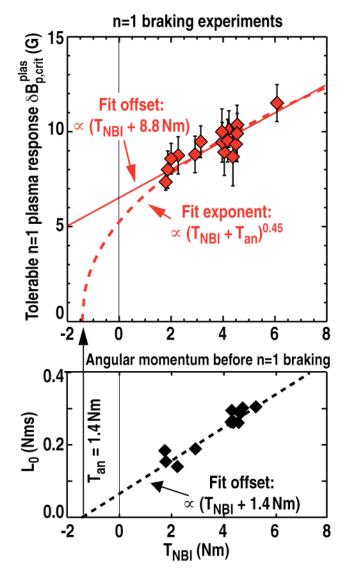
• Assuming a linear  $T_{NBI}$  dependence as predicted by the resonant braking model

$$\delta B_{\text{R,crit}} = T_{\text{in}} \sqrt{\frac{\tau_{\text{L,0}}}{4IK_{\text{R}}}}$$

leads to an offset that is too large to be explained by the anomalous torque  $(T_{can} = T_{in} - T_{NBI})$ 

• A fit based on an estimate of  $T_{an}$  from the angular momentum before n=1 braking yields

$$\delta B_{\rm p,crit}^{\rm plas} \propto T_{\rm in}^{0.45}$$





## Observed dependence of error field tolerance on torque input weaker than prediction for resonant braking

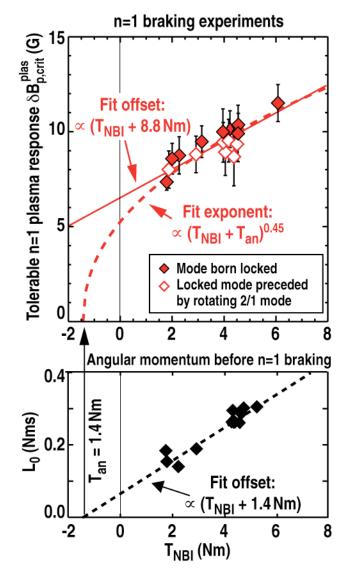
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## Input torque dependence of error field tolerance translates into a similar rotation dependence

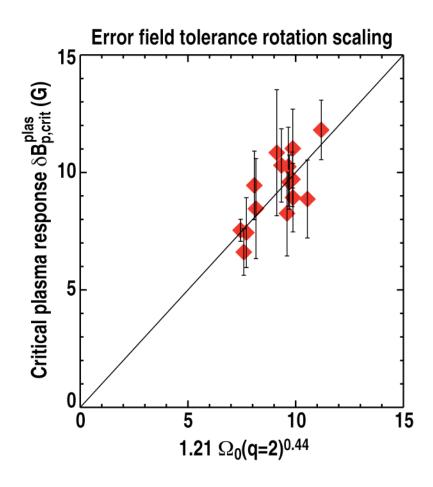
• A fit of the dependence of the critical plasma response on the unperturbed rotation  $\Omega_0$  yields

$$\delta B_{\rm p,crit}^{\rm plas} \propto \Omega_0^{0.44}$$

– Similar exponent for  $T_{\rm in}$  and  $\Omega_0$  expected since

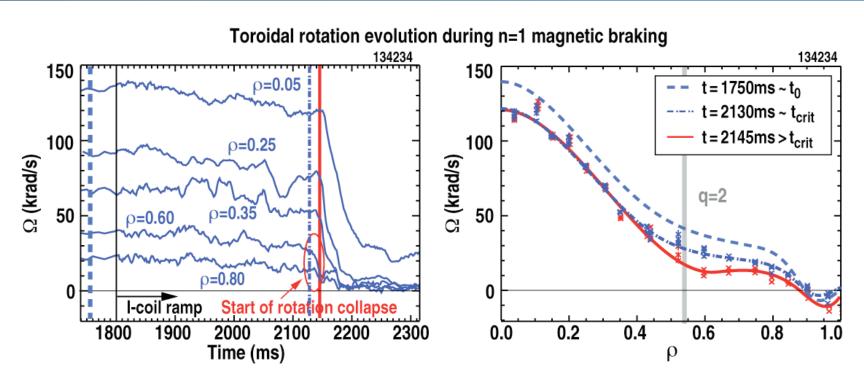
$$\Omega_0 = \frac{T_{\rm in} \tau_{\rm L,0}}{I}$$

Consistent with previous low β scalings [e.g. E. Lazzaro, et al., Phys. Plasmas (2002)]





#### Rotation damping prior to the rotation collapse shows no evidence of a localized braking torque



- Rotation decreases across the entire profile indicating a non-resonant braking mechanism
  - Resolution of a localized braking torque limited by uncertainty of  $\Omega'$  and  $\Omega''$
- Rotation collapse starts at the outer half of the profile

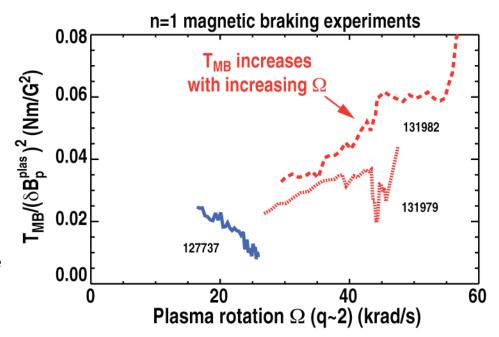


#### Measured rotation dependence of the braking torque reveals further evidence of a non-resonant component

• Measured angular momentum evolution yields magnetic braking torque  $T_{\rm MB}$ 

$$T_{\text{MB}} = T_{\text{NBI}} - \frac{L}{\tau_{\text{L},0}} - \frac{dL}{dt}$$

- Assume  $T_{\rm MB} \propto (\delta B^{\rm plas})^2$  to reveal rotation dependence



- At low rotation  $T_{\rm MB}$  increases with decreasing  $\Omega$  consistent with a resonant torque [R. Fitzpatrick, Nucl. Fusion (1993)]
- At high rotation  $T_{\text{MB}}$  increases with  $\Omega \to \text{typical for a non-resonant torque}$  [K.C. Shaing, Phys. Plasmas (2003)]



#### Additional non-resonant component reduces the resonant threshold and weakens the torque dependence

• Adding a non-resonant component  $f_{NR}\delta B$  of the perturbed field  $\delta B$  ( $\propto \delta B^{\text{plas}}$ ) to the magnetic braking torque in the 0D torque balance\*

$$I\frac{d\Omega}{dt} = T_{\text{in}} - \frac{I\Omega}{\tau_{\text{L},0}} - \frac{K_{\text{R}}(f_{\text{R}}\delta B)^{2}\Omega^{-1}}{\text{Resonant}} - \frac{K_{\text{NR}}(f_{\text{NR}}\delta B)^{2}\Omega}{\text{Non-resonant}}$$
braking torque braking torque

#### yields

for 
$$f_{NR}$$
=0:  $\delta B_{crit} = b_R T_{in}$   
for  $f_{NR} \neq 0$ :  $\delta B_{crit} = \sqrt{2} b_R T_e \left( \left( 1 + \left( T_{in} / T_e \right)^2 \right)^{0.5} - 1 \right)^{0.5}$ 

with 
$$b_{\rm R} = \frac{1}{2f_{\rm R}} \left(\frac{\tau_{\rm L,0}}{IK_{\rm R}}\right)^{0.5}$$
 and  $T_{\rm e} = \frac{I}{\tau_{\rm L,0}} \frac{f_{\rm R}}{f_{\rm NR}} \left(\frac{K_{\rm R}}{K_{\rm NR}}\right)^{0.5}$ 

Viscous torque at  $\Omega$  where resonant and non-resonant torque are equally important

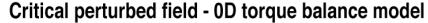


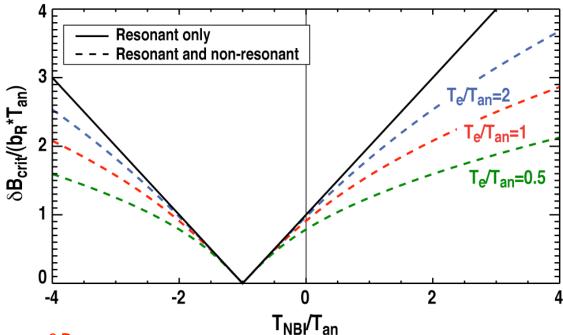
\*Neglect offset rotation in counter-Ip direction [A. Cole, et al., Phys. Rev. Lett. (2007), A.M. Garofalo, et al., Phys. Rev. Lett. (2009)]

#### A non-resonant braking component of the perturbed field lowers the tolerance for resonant magnetic field errors

• Increasing the non-resonant component  $f_{NR}$  decreases  $T_{e} = \frac{I}{\tau_{L,0}} \frac{f_{R}}{f_{NR}} \left(\frac{K_{R}}{K_{NR}}\right)^{0}$ 

$$T_{\rm e} = \frac{I}{\tau_{\rm L,0}} \frac{f_{\rm R}}{f_{\rm NR}} \left(\frac{K_{\rm R}}{K_{\rm NR}}\right)^{0.5}$$





- $\rightarrow$  Decreases  $\delta B_{crit}$
- $\rightarrow$  Weakens the  $T_{NBI}$  dependence of  $\delta B_{crit}$  (possible explanation for the negligible  $T_{NBI}$  dependence in NSTX [Park, et al., APS (2009)]?)



# Observed $\delta B_{\text{crit}}^{\text{plas}} \propto T_{\text{NBI}}^{0.45}$ in DIII-D consistent with a strong non-resonant component of the plasma response

• Adding a non-resonant component  $f_{NR}\delta B$  of the perturbed field  $\delta B$  to the magnetic braking torque in the 0D torque balance

$$I\frac{d\Omega}{dt} = T_{\text{in}} - \frac{I\Omega}{\tau_{1.0}} - K_{\text{R}} (f_{R} \delta B)^{2} \Omega^{-1} - K_{\text{NR}} (f_{NR} \delta B)^{2} \Omega$$

#### yields

for 
$$f_{NR}$$
=0:  $\delta B_{crit} = b_R T_{in}$   
for  $f_{NR}$ ≠0:  $\delta B_{crit} = \sqrt{2} b_R T_e \left( \left( 1 + \left( T_{in} / T_e \right)^2 \right)^{0.5} - 1 \right)^{0.5}$ 

with 
$$b_{\rm R} = \frac{1}{2f_{\rm R}} \left(\frac{\tau_{\rm L,0}}{IK_{\rm R}}\right)^{0.5}$$
 and  $T_{\rm e} = \frac{I}{\tau_{\rm L,0}} \frac{f_{\rm R}}{f_{\rm NR}} \left(\frac{K_{\rm R}}{K_{\rm NR}}\right)^{0.5}$ 

• Assuming a strong non-resonant component/large torque input  $T_{\rm e} << T_{\rm in}$  yields

$$\delta B_{\text{crit}} = \sqrt{2} b_{\text{R}} (T_{\text{e}} T_{\text{in}})^{0.5}$$



#### A non-resonant component in addition to the n=1 plasma response reduces the error field tolerance further

 Adding a non-resonant torque independent of the n=1 plasma response in the 0D torque balance (e.g. n=3, TBM, TF ripple)

$$I\frac{d\Omega}{dt} = T_{\text{in}} - \frac{I\Omega}{\tau_{\text{L},0}} - K_{\text{R}} (f_{\text{R}} \delta B)^2 \Omega^{-1} - K_{\text{NR}} (f_{\text{NR}} \delta B)^2 \Omega - K_{\text{NR}}^* (\delta B_{\text{NR}}^*)^2 \Omega$$

can be expressed by an effective momentum confinement time

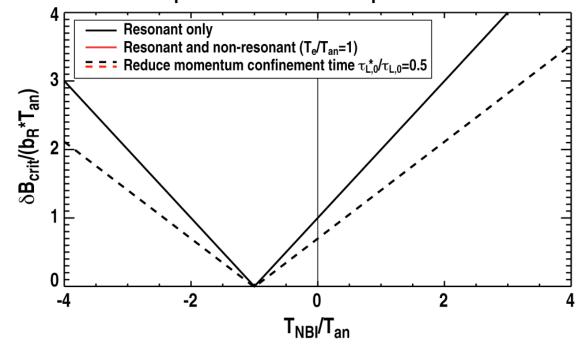
$$\tau_{L,0}^* = \left( \left( \tau_{L,0} \right)^{-1} + \frac{K_{NR}^*}{I} \left( \delta B_{NR}^* \right)^2 \right)^{-1}$$

• For zero and small  $f_{\rm NR}$ 

$$\delta B_{\rm crit} \propto \left( au_{\rm L,0}^* \right)^{0.5}$$

• For large  $T_{NR}$  the error field tolerance becomes independent of  $\tau_{L,0}^*$ 

#### Critical perturbed field - 0D torque balance model





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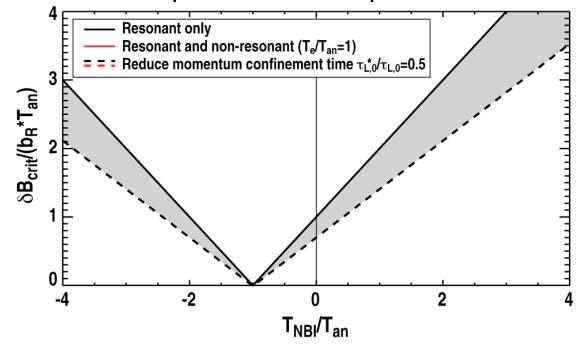
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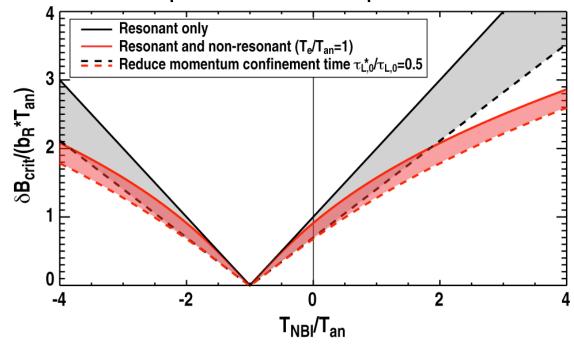
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• For zero and small  $f_{NR}$ 

$$\delta B_{\rm crit} \propto \left(\tau_{\rm L,0}^*\right)^{0.5}$$

• For large  $T_{NR}$  the error field tolerance becomes independent of  $\tau_{L,0}^*$ 

#### Critical perturbed field - 0D torque balance model





#### **Summary/Main results**

- Resonant braking leading to a loss of torque balance determines the "ultimate" n=1 error field threshold in NBI heated H-modes
- Decrease of n=1 error field tolerance with increasing  $\beta$  is caused by an increasing plasma amplification
- Plasma is sensitive to kink-resonant rather than pitch-resonant external fields (more in M. Lanctot's talk on We)
  - Fourier harmonics of the external field in straight field line coordinates are not an efficient description of the error field tolerance
  - For n=1 errors from the LFS, the plasma is most sensitive to the resulting m=2nq components
- Plasma response leads to a resonant and non-resonant magnetic torque
  - Non-resonant braking component reduces the benefit of additional torque input
  - Non-resonant braking component weakens the torque dependence consistent with experimental observations



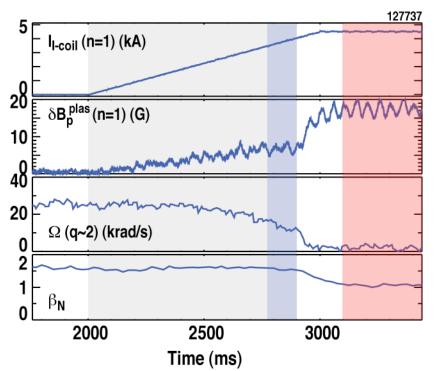


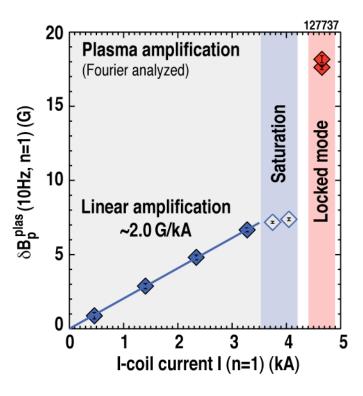
#### Additional slides



#### Plasma response to an external n=1 field is linear as long as the plasma is rotating sufficiently fast

- Linear amplification at  $\beta_N$ =const. despite a rotation reduction by factor 2
- Plasma response saturates prior to the rotation collapse
- Amplification large once the rotation has collapsed, the error field penetrated and a locked mode formed (despite reduction in  $\beta_N$ )



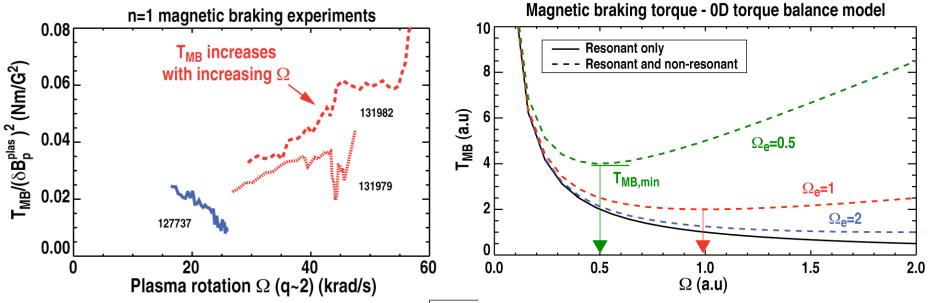




## Effect of simultaneous resonant and non-resonant braking

Perturbed field has a resonant and a non-resonant component

$$T_{\text{MB}} = K_{\text{R}} (f_R \delta B)^2 \Omega^{-1} + K_{\text{NR}} (f_{NR} \delta B)^2 \Omega$$

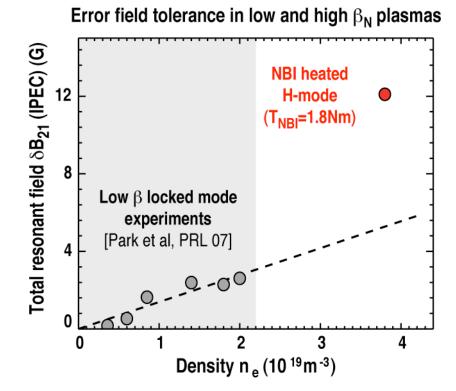


•  $T_{\rm MB}$  has a minimum for  $\Omega_{\rm e} = \frac{f_R}{f_{NR}} \sqrt{\frac{K_{\rm R}}{K_{\rm NR}}}$ , where resonant and non-resonant braking torques are equal



#### Plasma response and beneficial effect of NBI torque connect L- and H-mode error field threshold

- Ideal MHD plasma response (IPEC)
  has been successfully used to
  restore density dependence of
  locked mode threshold in L-modes
  [J.-K. Park, et al., Phys. Rev. Lett. 99 (2007)
  195003]
  - Calculate total resonant field at q=2 surface  $\delta B_{21}$ , if shielding currents were absent



- In H-mode, the error field threshold exceeds the extrapolation of L-mode experiments by a factor of 2
- >~40% increase expected based on extrapolation of measured T<sub>NBI</sub> dependence towards zero

