

Real-time control of tearing modes using a line-of-sight Electron Cyclotron Emission diagnostic

a system engineering approach

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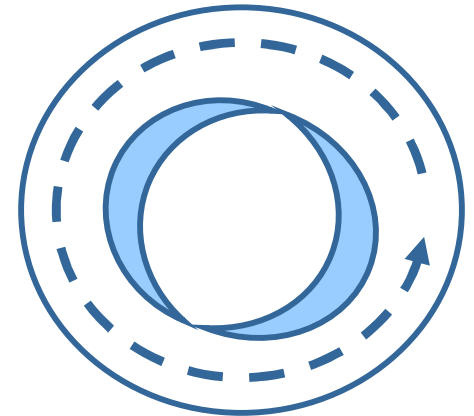


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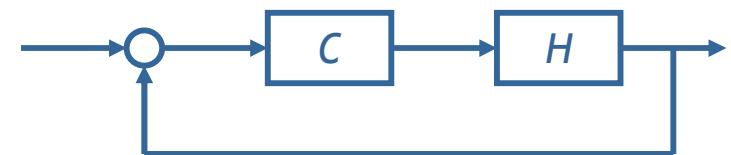
Real-time control of tearing modes

- Goal:
Establish a real-time tearing mode control system
- Localized ECRH/ECCD applied for stabilization and suppression:
 - Fast & accurate mode detection
 - Align ECRH/ECCD power deposition w.r.t. mode centre (“tracking”)
 - Modulate ECRH/ECCD power synchronously with mode rotation (up to 5 kHz)



- Why real-time feedback control ?

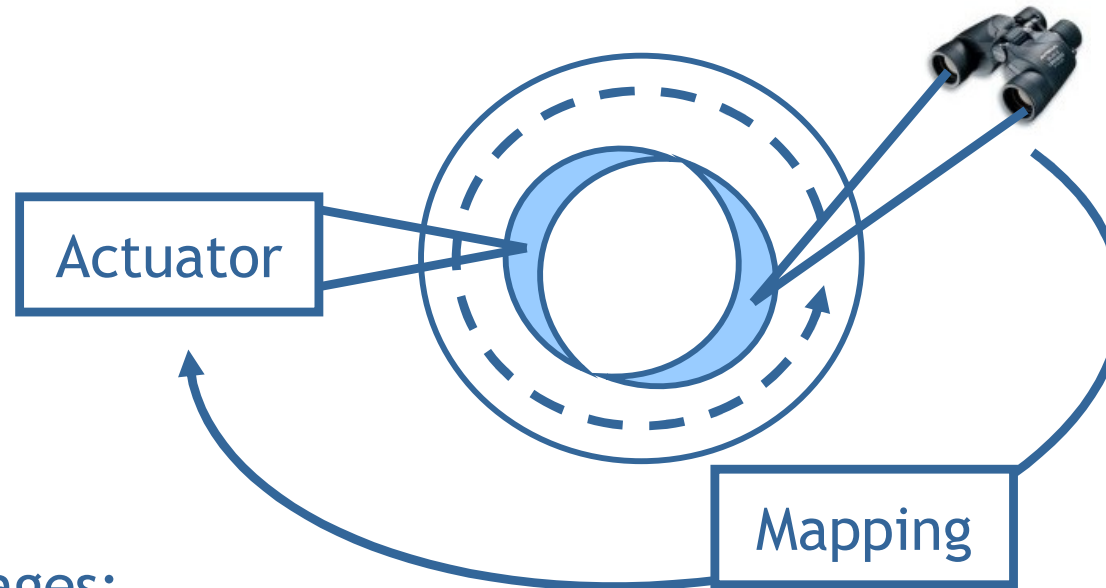
guarantees fast and accurate alignment (100 ms, 1-2 cm), disturbance rejection, robustness and stability





Real-time control of tearing modes

- In general, tearing mode control systems use:
 - Mapping between ECRH/ECCD actuator & diagnostics
 - Equilibrium reconstruction/estimation + beam tracing codes in feedback loop



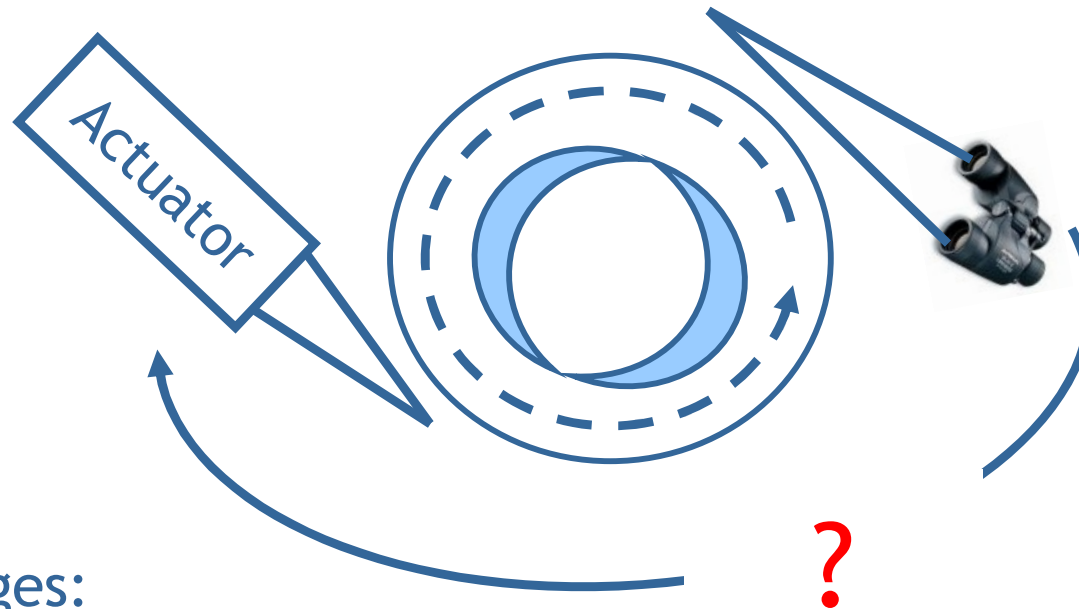
- Disadvantages:
 - Mapping introduces errors in control loop
 - Accurate calibration of actuator & sensor orientation required

(loss of orientation = loss of control)



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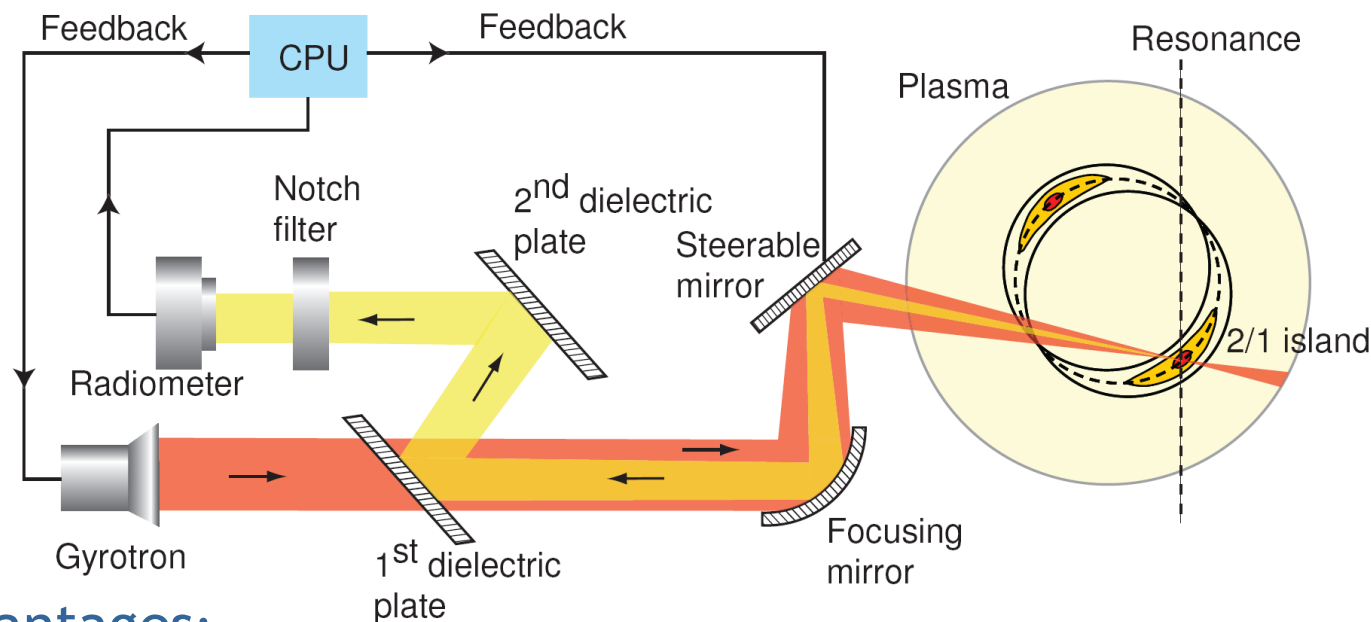
(loss of orientation = loss of control)



Real-time control of tearing modes

- Alternative: “line-of-sight principle”

→ Use ECE diagnostic as feedback sensor in sight-line of ECRH/ECCD beam



- Advantages:

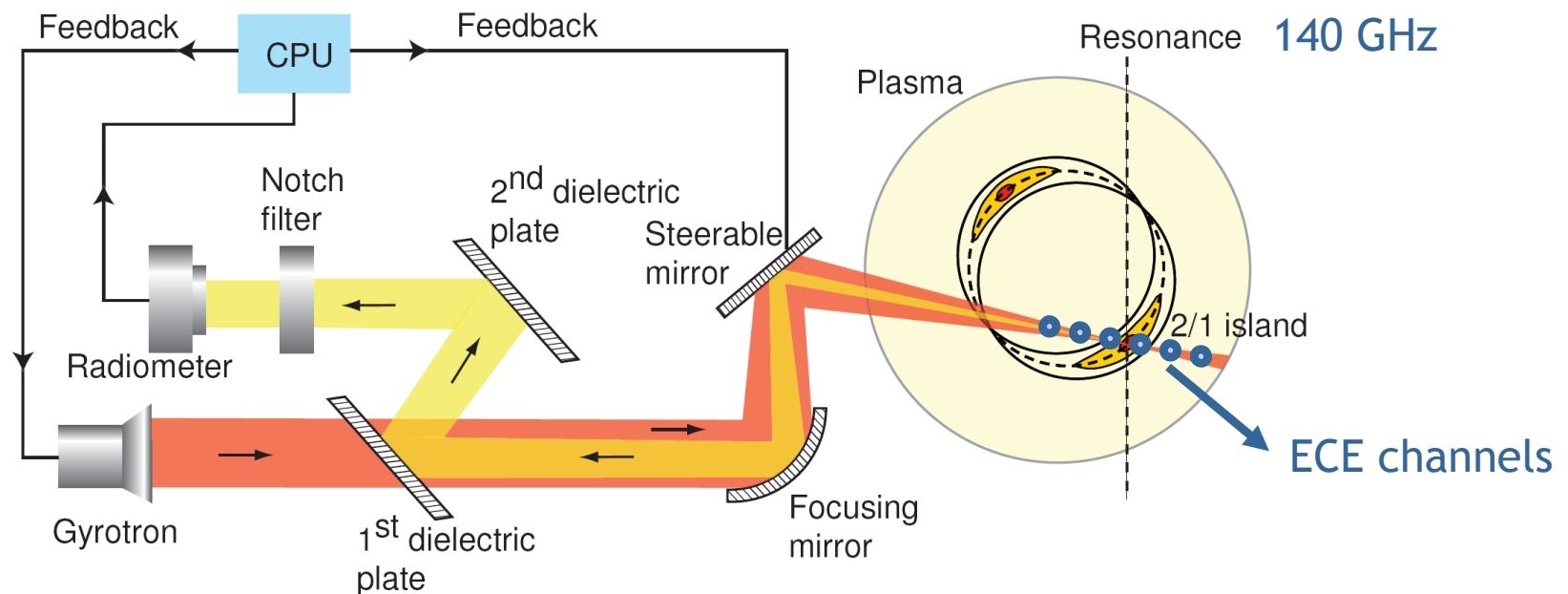
- Actuator and sensor are always aligned (refractive properties identical)
- Guarantees tearing mode control even when launcher orientation is perturb or calibration is lost
- Sensor is placed at distance from plasma (single access port needed)



Real-time control of tearing modes

- Alternative: “line-of-sight principle”

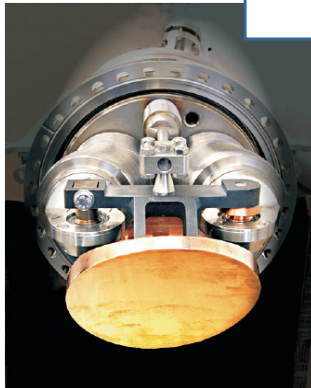
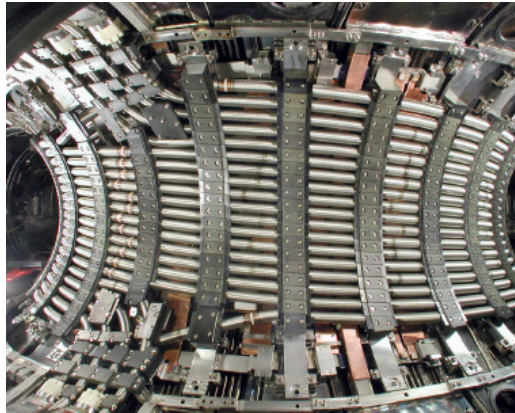
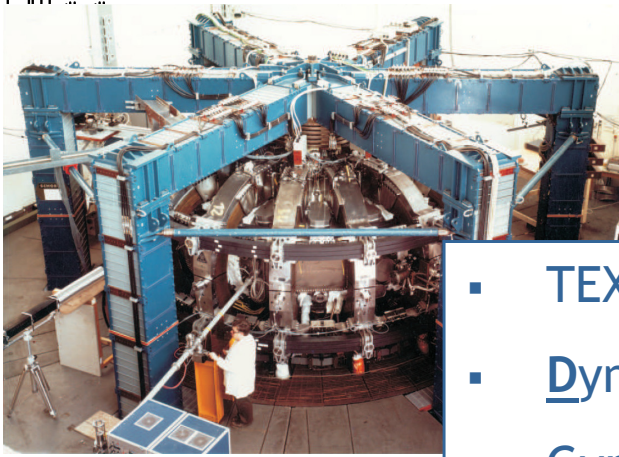
→ Use ECE diagnostic as feedback sensor in sight-line of ECRH/ECCD beam



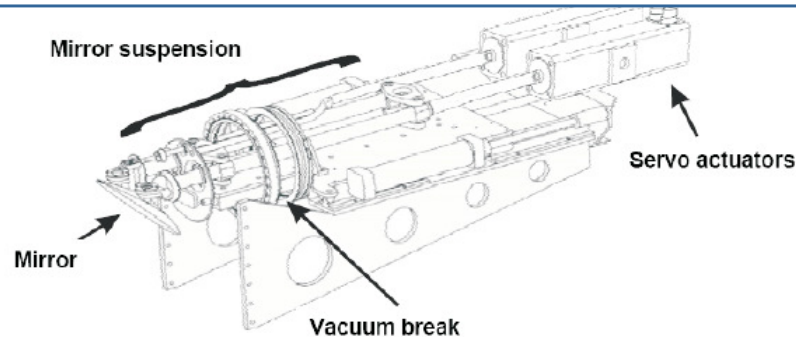
- Implementation in quasi-optical ECRH/ECCD transmission line on TEXTOR:
 - Radiometer: 6 channels, 132.5-147.5 GHz, 3 GHz spacing ~ 3 cm radial spacing
 - Frequency selective directional couplers separate **ECE** from **ECRH/ECCD** (nW power versus MW power)



Experimental instrumentation

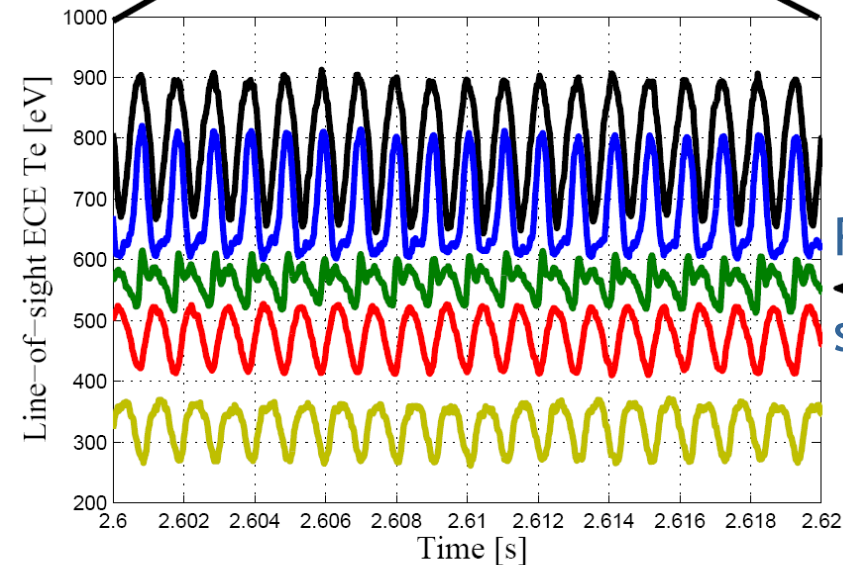
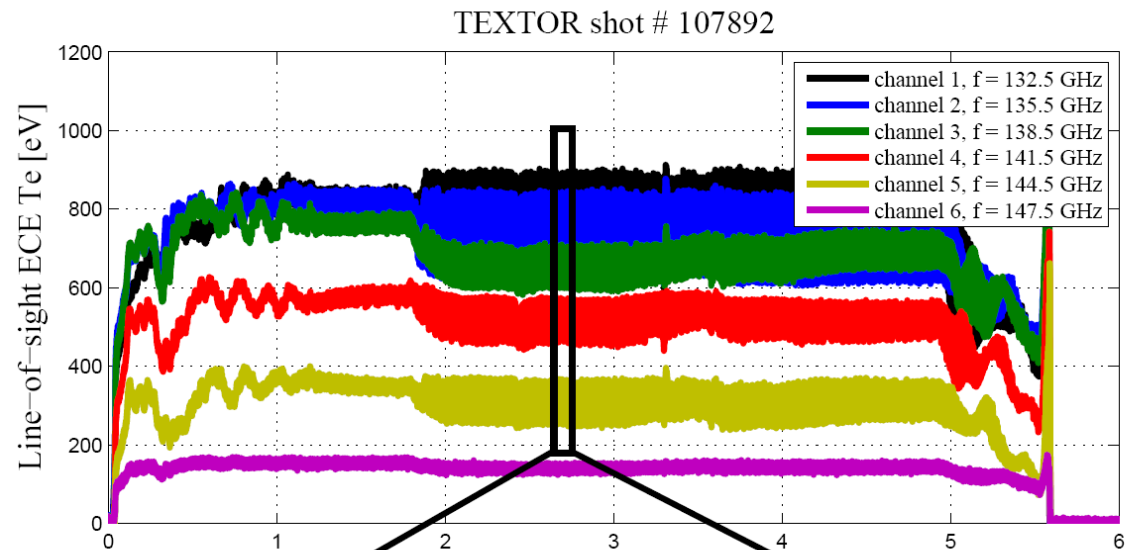
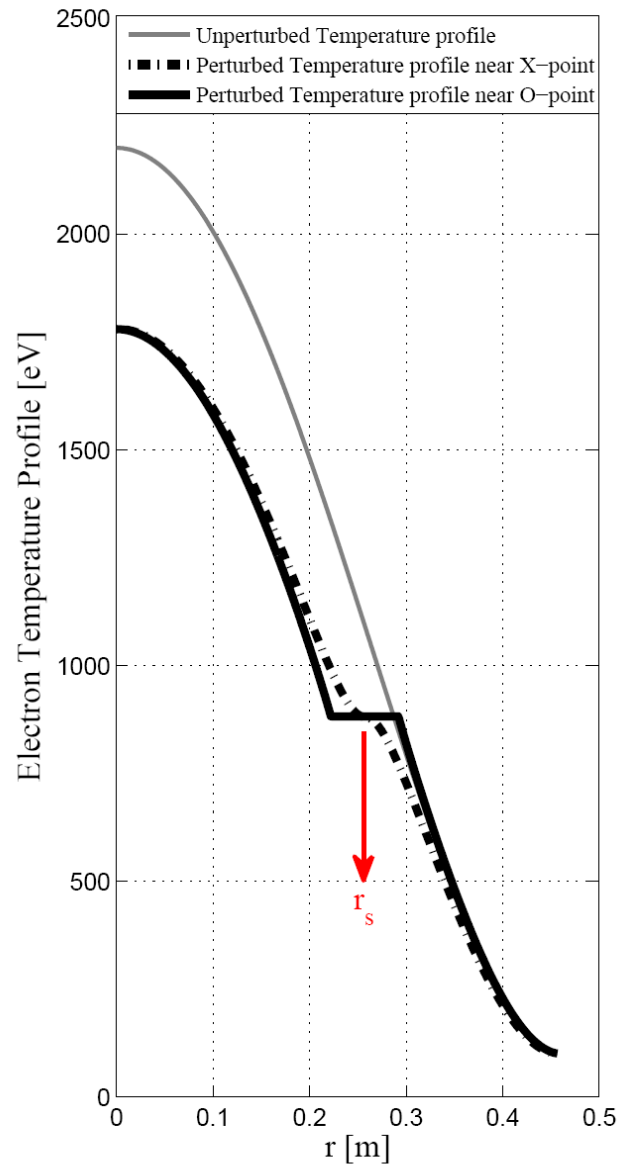


- TEXTOR ($R = 1.75 \text{ m}$, $a = 0.46 \text{ m}$)
- Dynamic Ergodic Divertor (perturbation field)
- Gyrotron 140 GHz, 1 MW, 10 s
- Bi-directional, steerable launcher (tor. & pol.)
- Line-of-sight ECE diagnostic
- National Instruments DAQ & RT control system
(Labview based, DAQ & Field Programmable Gate Array: sampling rate 100 kHz)





Real-time tearing mode identification



Rational surface r_s 180°



Real-time tearing mode identification

- Real time tearing mode detection from correlation between ECE fluctuations (*algorithm implemented on FPGA*):

“Compute normalized correlation between ECE channels and apply weighted average over all possible channel combinations”

Channel pair with 180° phase reversal

=

$f_{\text{EC, tearing mode}}$ GHz

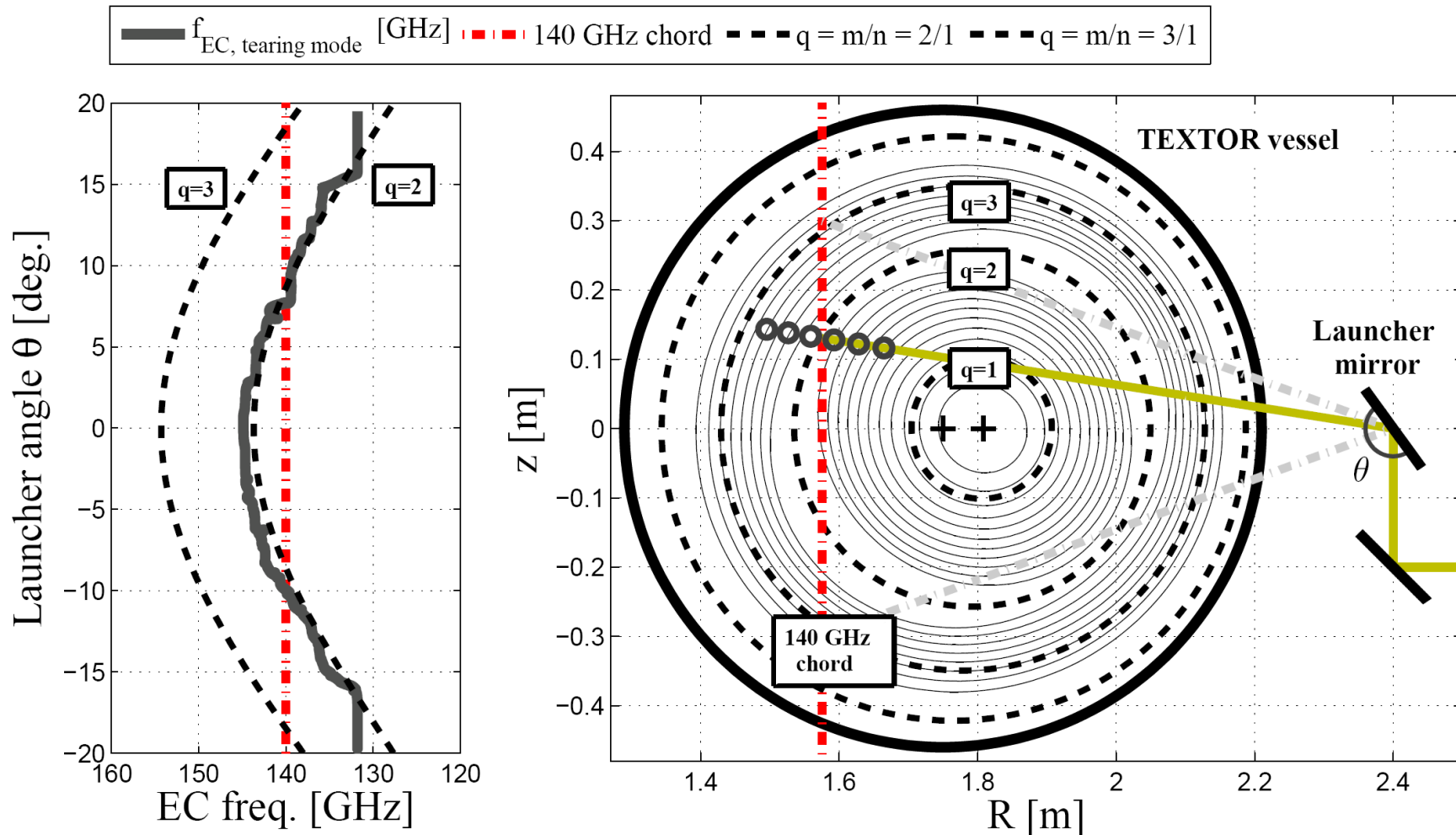
*Clock-rate
computation
on FPGA:*

16 μs

Estimate of mode location in the ECE spectrum for a given launcher orientation



Real-time tearing mode identification (Example)

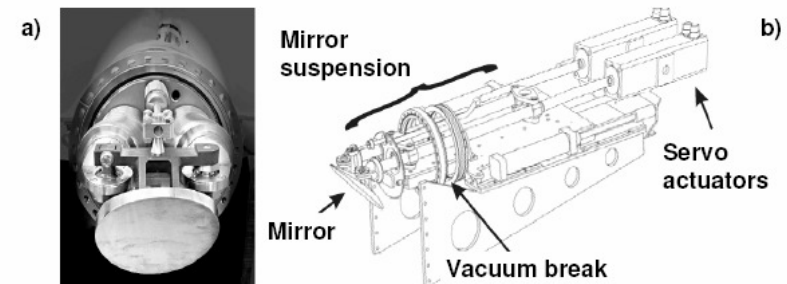
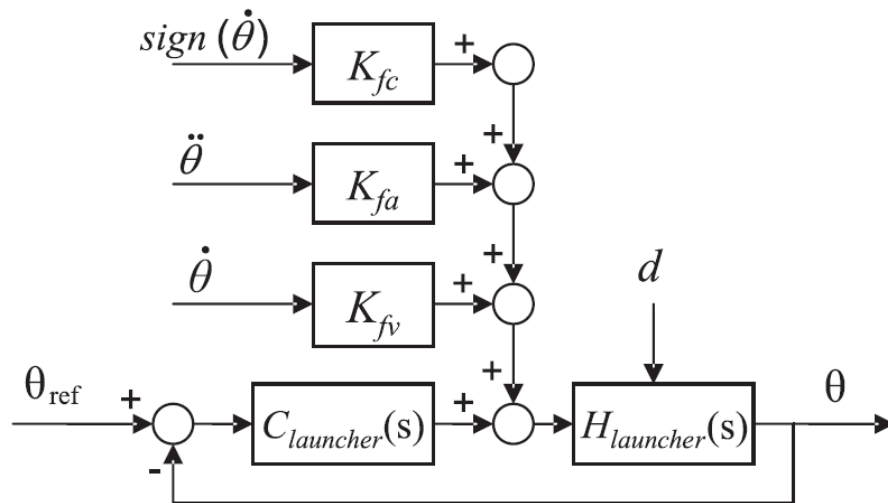


- Match actuator frequency 140 GHz with sensor frequency $f_{EC, \text{tearing mode}}$ GHz through launcher steering (elevation angle θ)



Real-time control loop

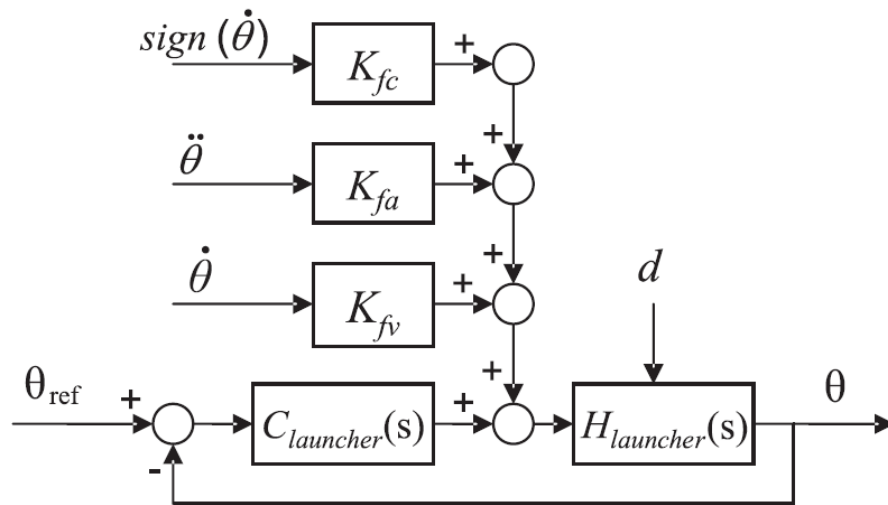
- Launcher control loop
 - Analysis launcher dynamics using Frequency Response Function measurement $H_{launcher}(s)$
 - Controller designed using “loop-shaping” in frequency domain
 - $C_{launcher}(s)$ = PID controller + lead/lag + low-pass filter
 - Feed-forward for friction compensation





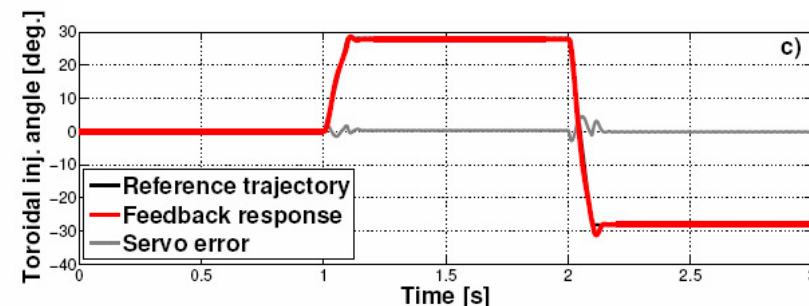
Real-time control loop

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Performance:

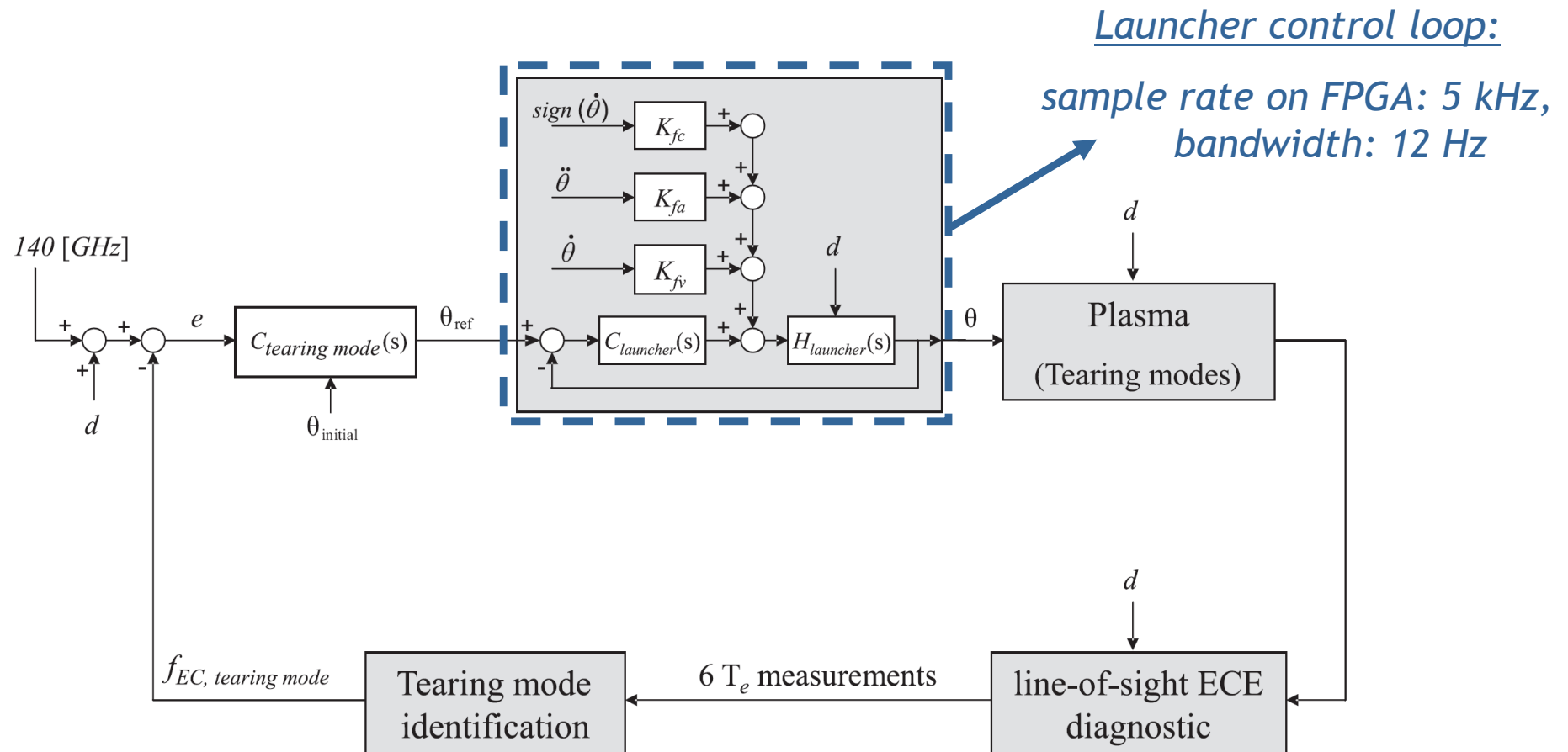
- Response: $\theta = \pm 30^\circ$ in 100 ms
- Max. steady-state positioning error: 0.6°
- Bandwidth: 12 Hz





Real-time control loop

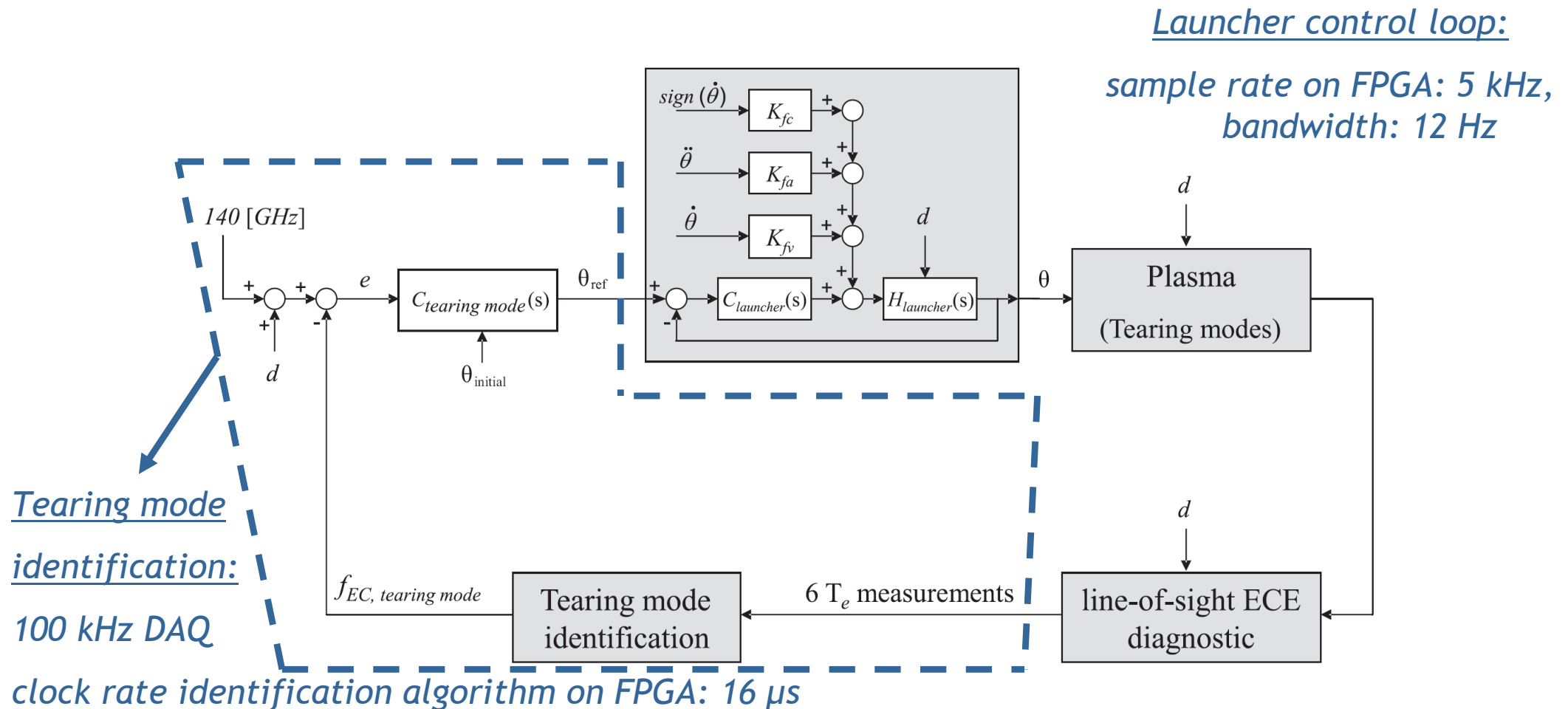
- Tearing mode “tracking” loop





Real-time control loop

- Tearing mode “tracking” loop





Real-time control loop

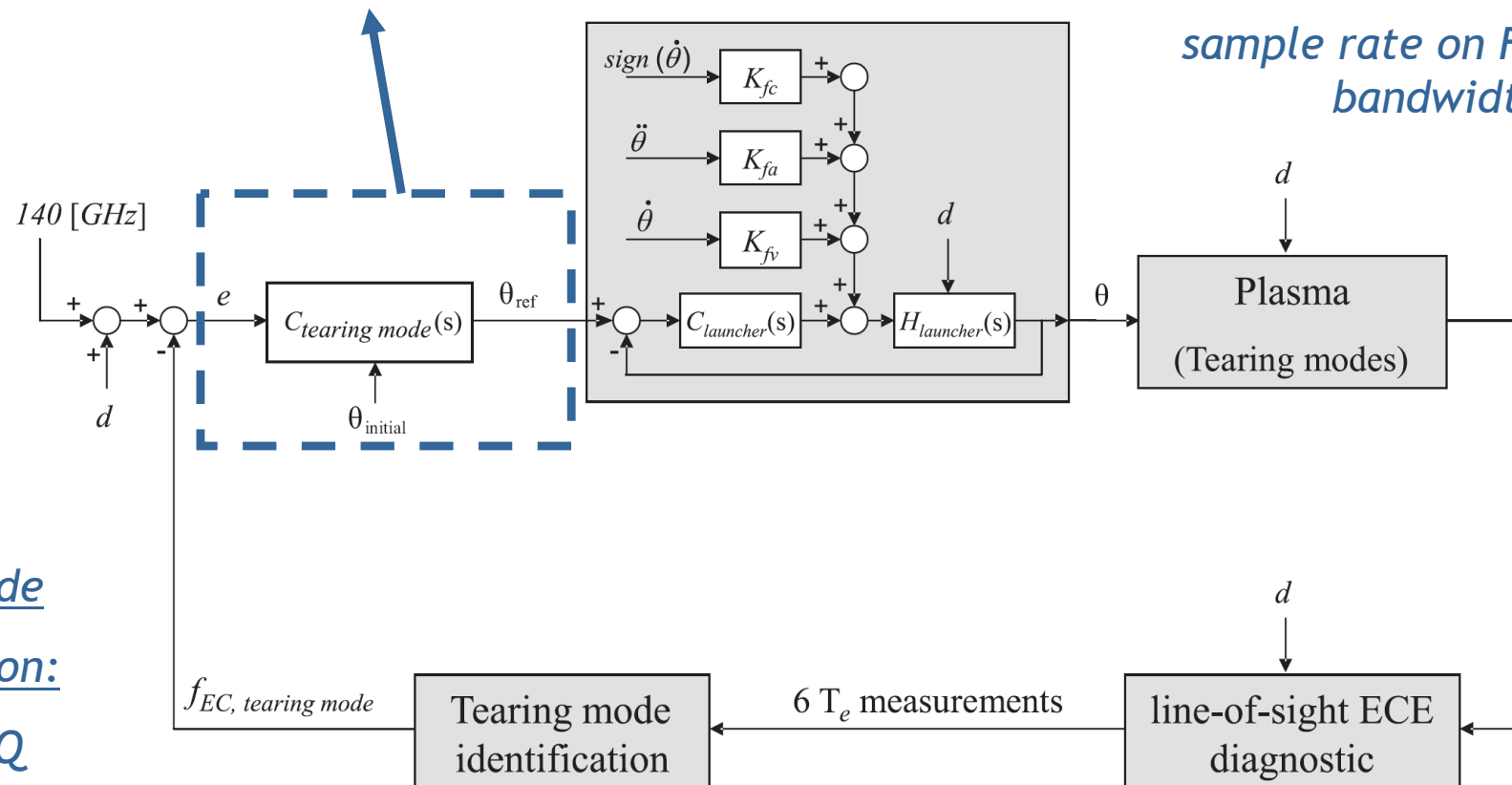
- Tearing mode “tracking” loop

- Minimize error: $e = 140 - f_{EC, \text{tearing mode}}$ [GHz]

- $C_{\text{tearing mode}}(s) = \text{PI controller} + \text{low-pass filter}$

Launcher control loop:

*sample rate on FPGA: 5 kHz,
bandwidth: 12 Hz*



Tearing mode
identification:

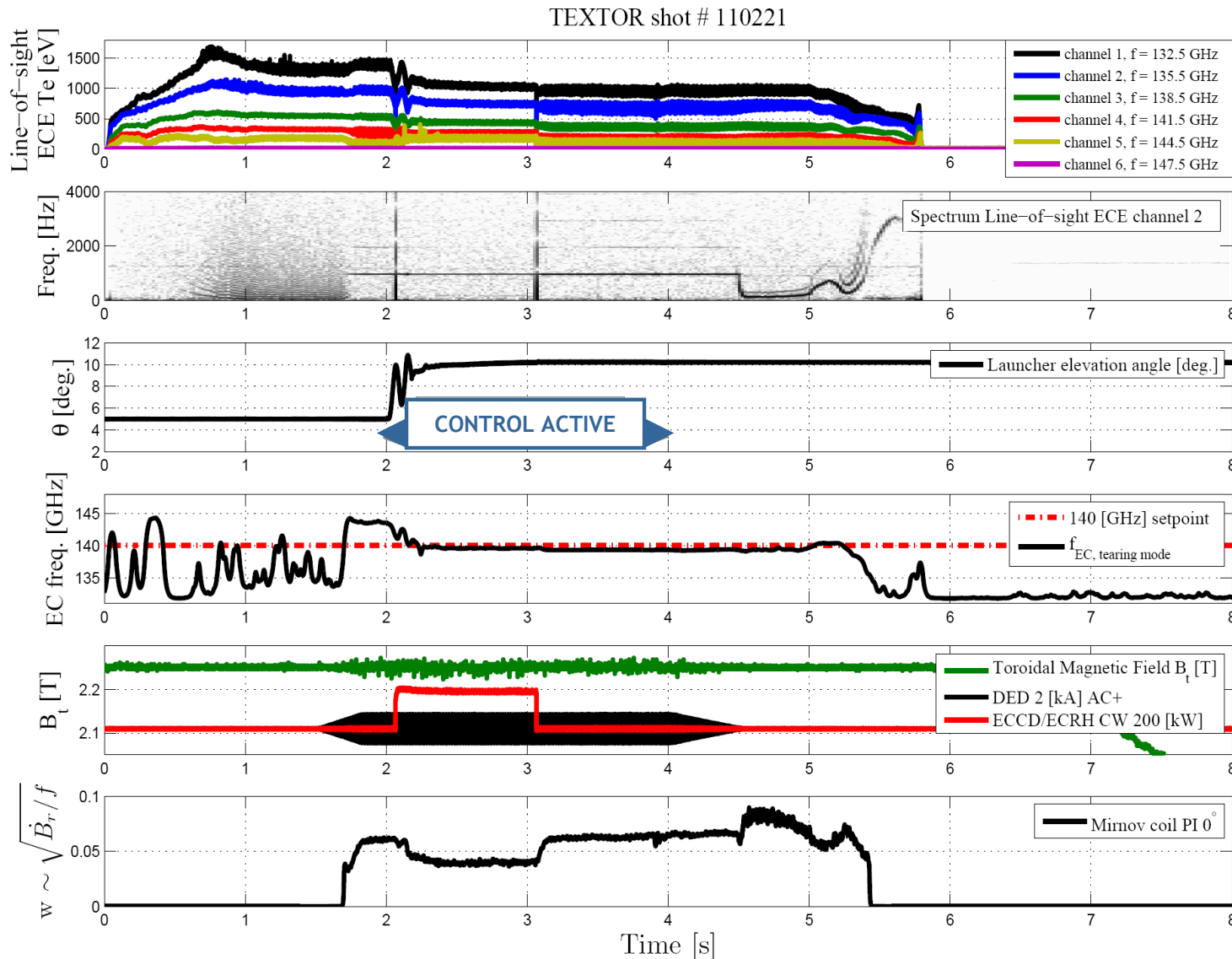
100 kHz DAQ

clock rate identification algorithm on FPGA: 16 μs



Experimental Results

2/1 tearing mode search-and-suppress



- $\theta_{\text{initial}} = 5^\circ$
- $B_t = 2.25$ T
- $I_p = 300$ kA

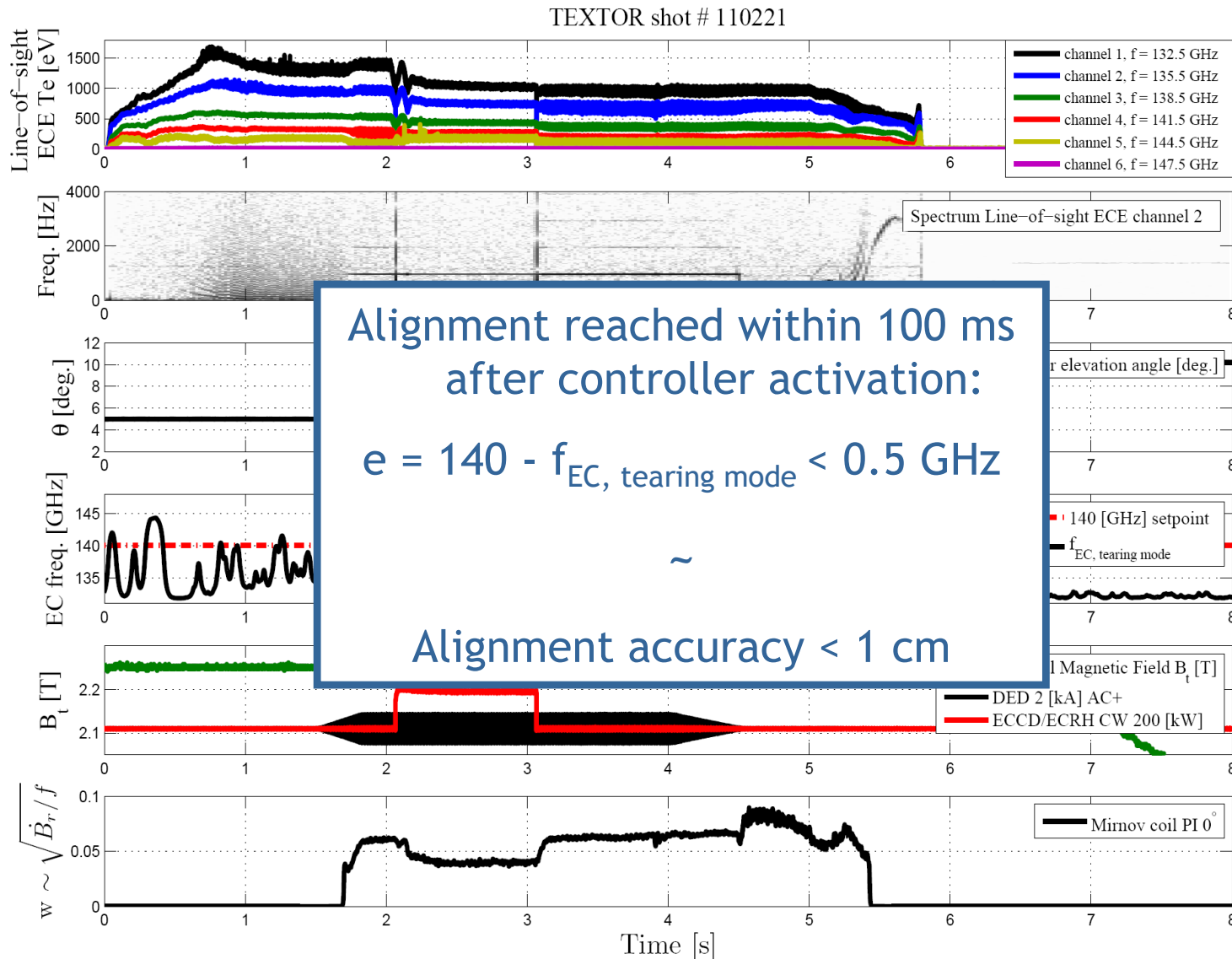
- Continuous ECRH/ECCD 200 kW, 1 sec.
- DED triggered
 $m/n = 2/1$ mode

- Controller active from $t = 2$ -4 sec.
- Automatic trigger gyrotron



Experimental Results

2/1 tearing mode search-and-suppress



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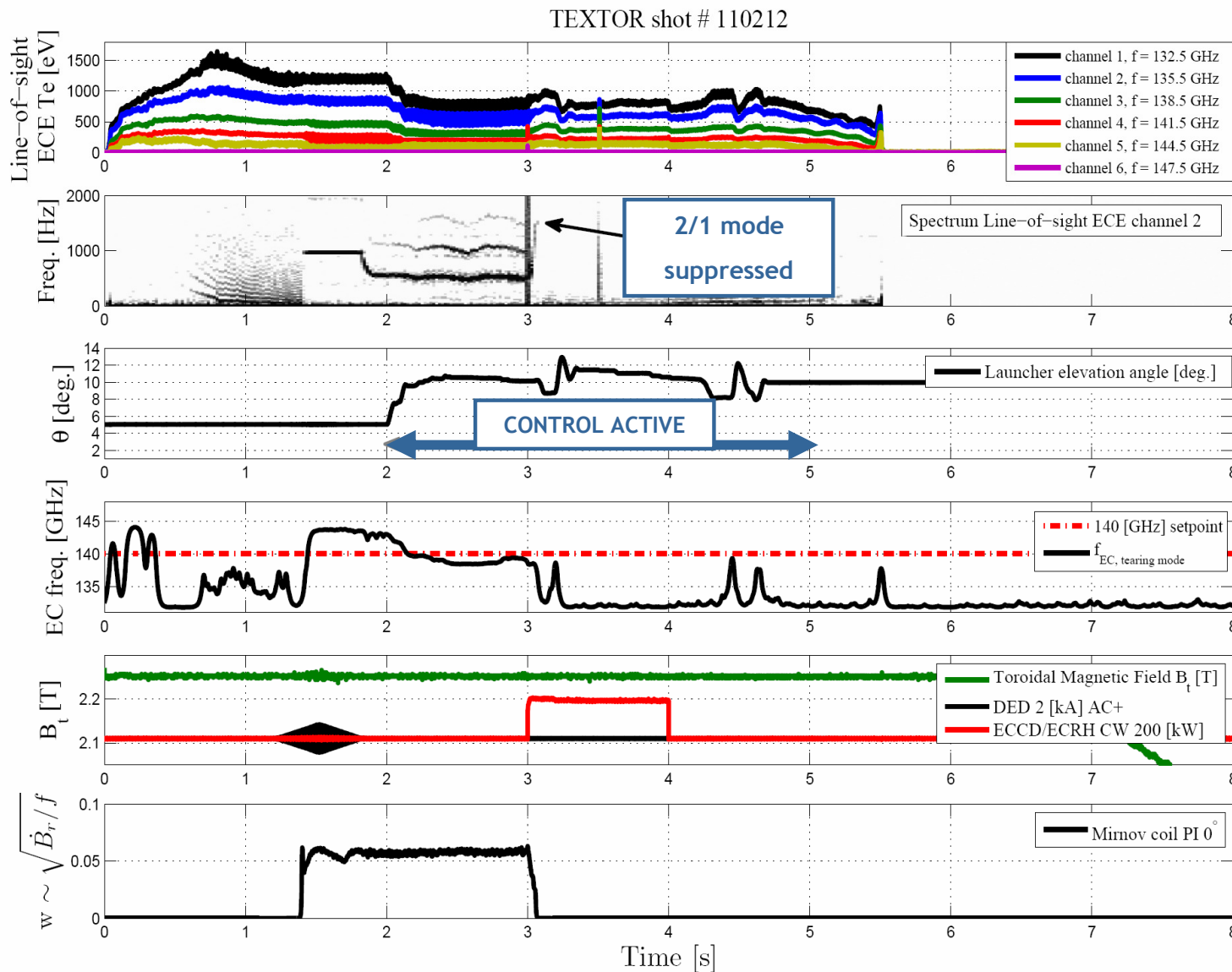
- Continuous ECRH/ECCD 200 kW, 1 sec.
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 $m/n = 2/1$ mode

- Controller active from $t = 2$ -4 sec.
- Automatic trigger gyrotron



Experimental Results

2/1 tearing mode complete suppression



- $\theta_{\text{initial}} = 5^\circ$
- $B_t = 2.25$ T
- $I_p = 300$ kA

- Continuous ECRH/ECCD 200 kW, $t = 3$ -4 sec.
- DED triggered $m/n = 2/1$ mode

- Controller active from $t = 2$ -5 sec.
- Mode suppressed at $t = 3.085$ sec.



Experimental Results

Next: Tearing mode tracking experiment

Ramp in toroidal magnetic field B_t

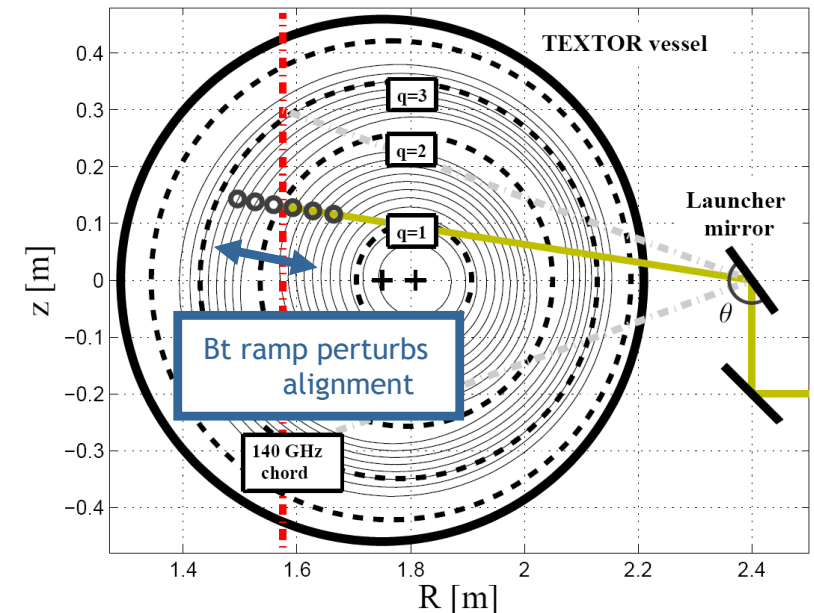


Mimic change in tearing mode location
(ECRH/ECCD deposition location and r_s perturbed)

- $B_t = 2.25\text{-}2.35\text{ T}$
- $I_p = 300\text{ kA}$



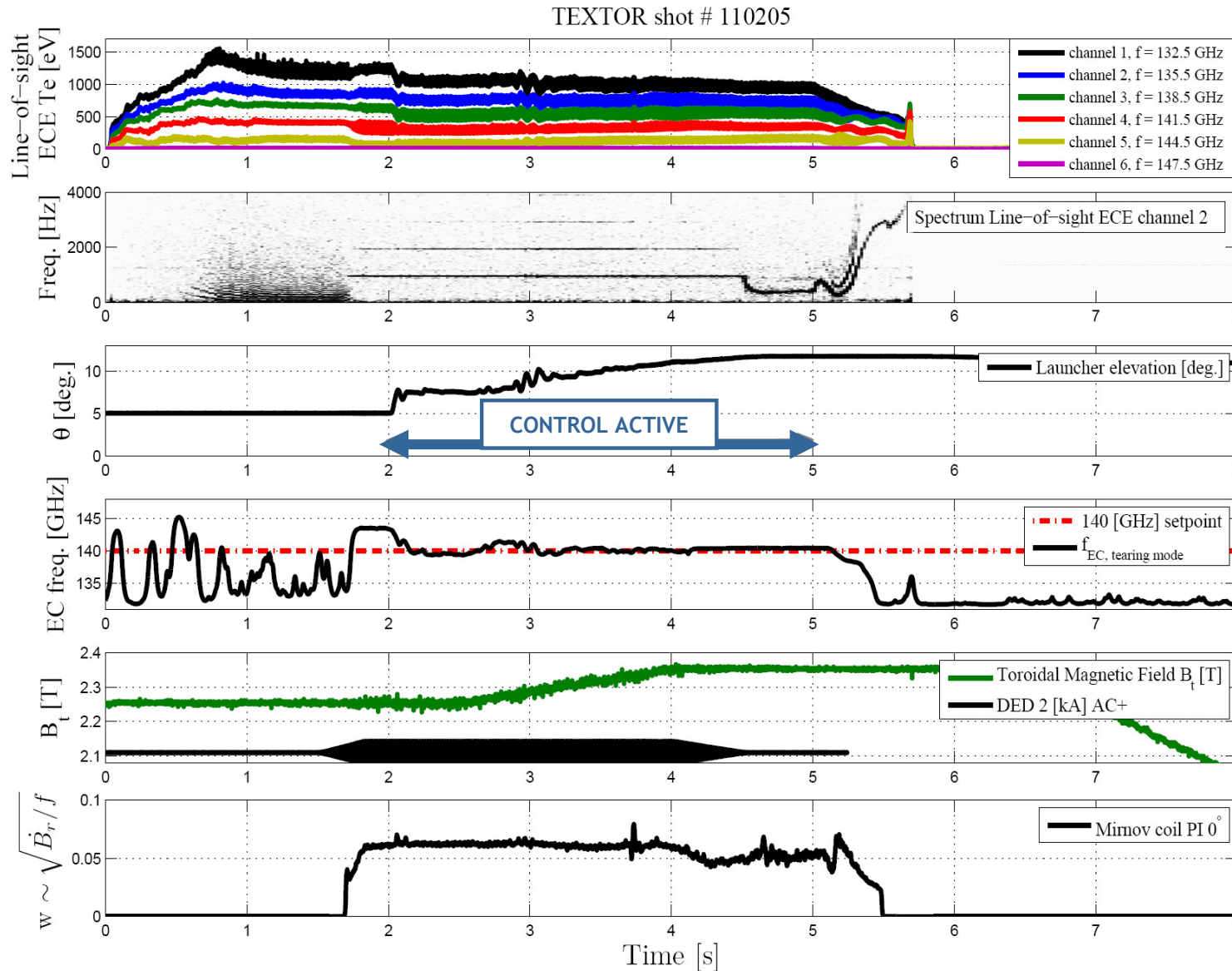
- 7 cm shift ECRH/ECCD deposition
- 0.5 cm shift r_s
- launcher should move $\sim 6^\circ$ up





Experimental Results

2/1 tearing mode tracking experiment



- $\theta_{\text{initial}} = 5^\circ$
- $B_t = 2.25\text{-}2.35$ T
- $I_p = 300$ kA

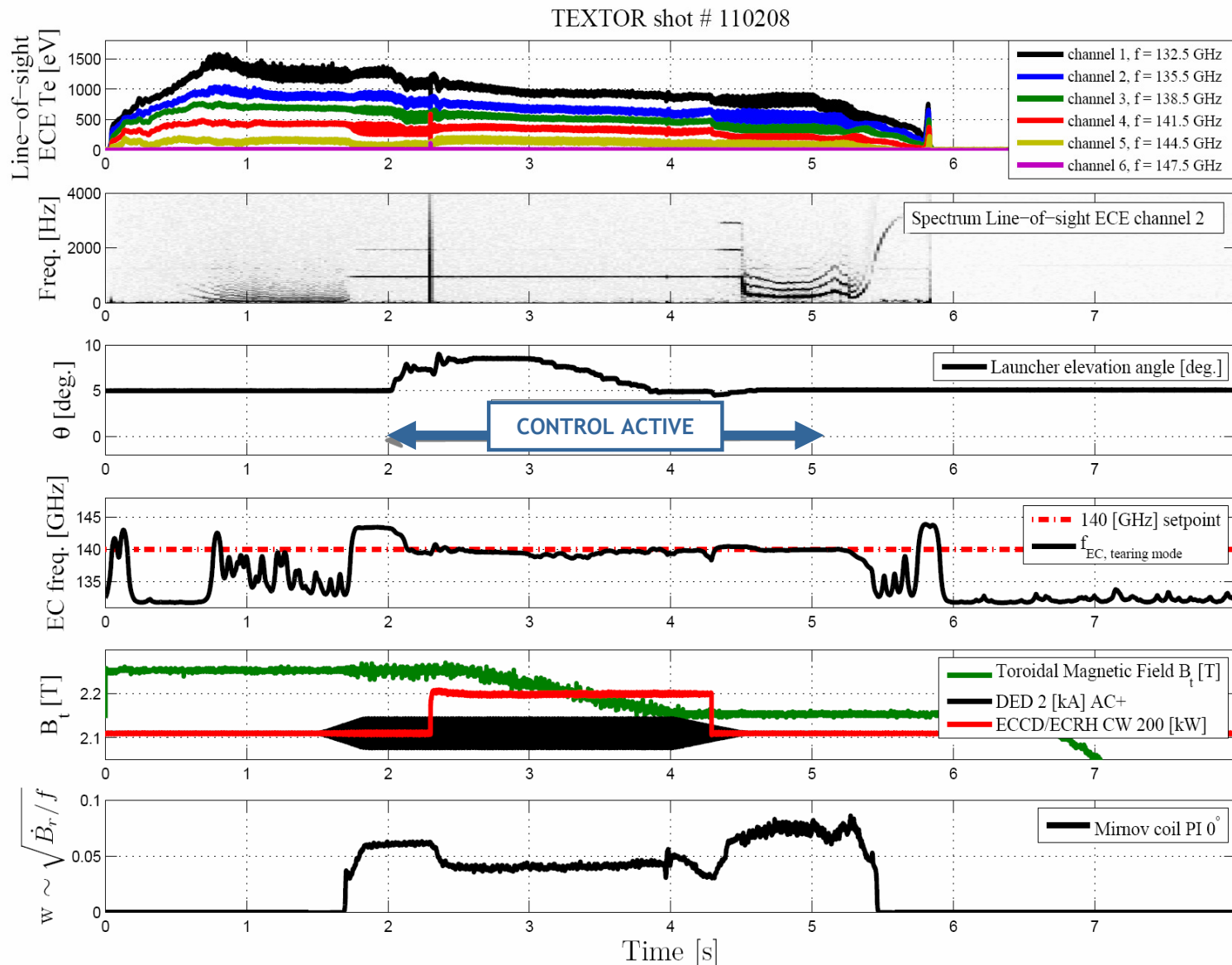
- No ECRH/ECCD
- DED triggered
 $m/n = 2/1$ mode

- Controller active
from $t = 2\text{-}5$ sec.
- Alignment
maintained during
 B_t ramp



Experimental Results

2/1 tearing mode tracking experiment



- $\theta_{\text{initial}} = 5^\circ$
- $B_t = 2.25\text{-}2.15 \text{ T}$
- $I_p = 300 \text{ kA}$

- Continuous ECRH/ECCD 200 kW, $t = 2.3\text{-}4.3 \text{ sec.}$
- DED triggered $m/n = 2/1 \text{ mode}$

- Controller active from $t = 2\text{-}5 \text{ sec.}$
- Alignment maintained during B_t ramp



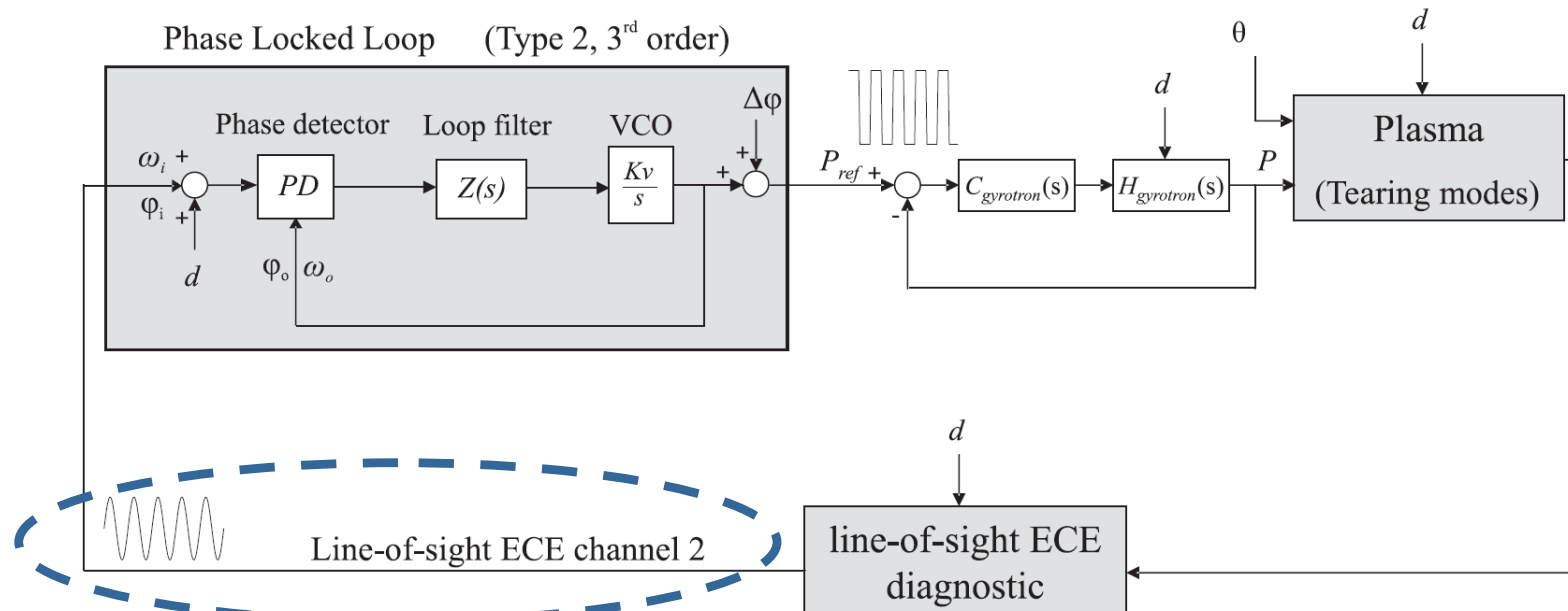
Real-time control loop

- Phase Locked Loop (synchronous ECRH/ECCD modulation on O-point)

Input PLL:

Line-of-sight ECE signal
(e.g. 2nd channel: 135.5 GHz)

- Monitor tearing mode's frequency and phase





Real-time control loop

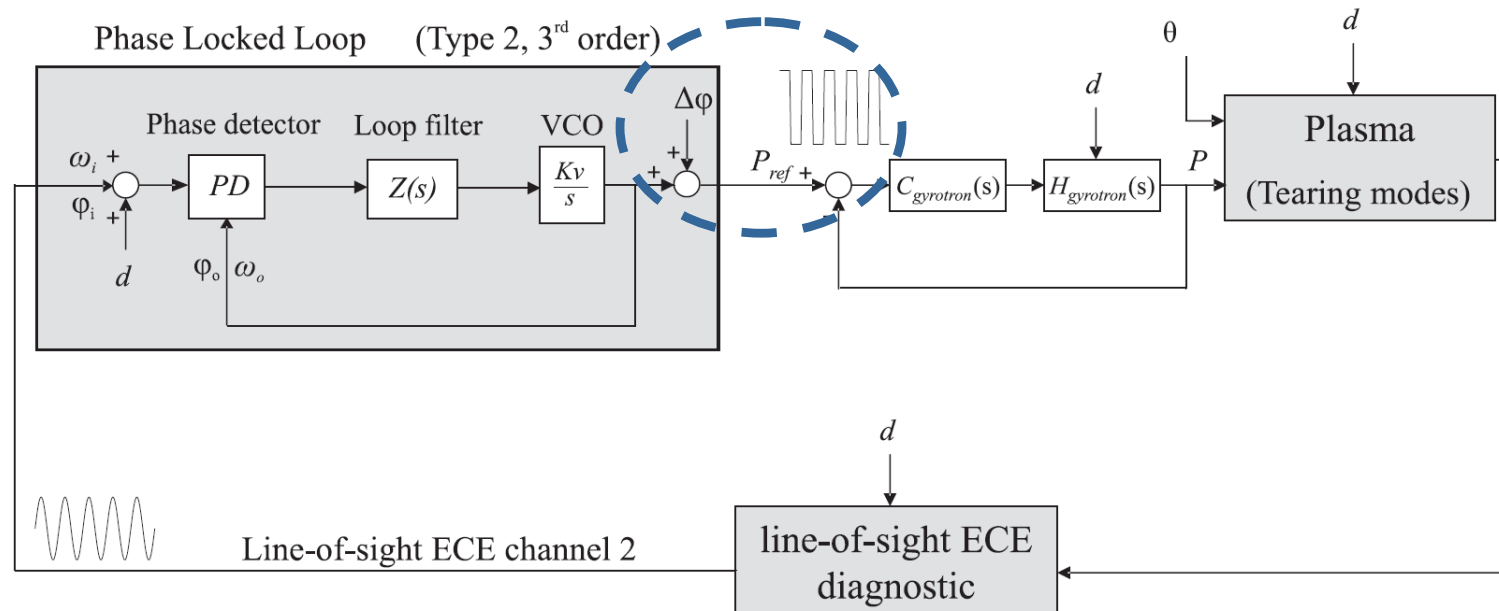
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Input PLL:

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Output PLL:

Block-wave with controlled frequency & phase
(maintains 90° phase difference relative to
1st harmonic of **noisy** ECE input signal)





Real-time control loop

- Phase Locked Loop (synchronous ECRH/ECCD modulation on O-point)

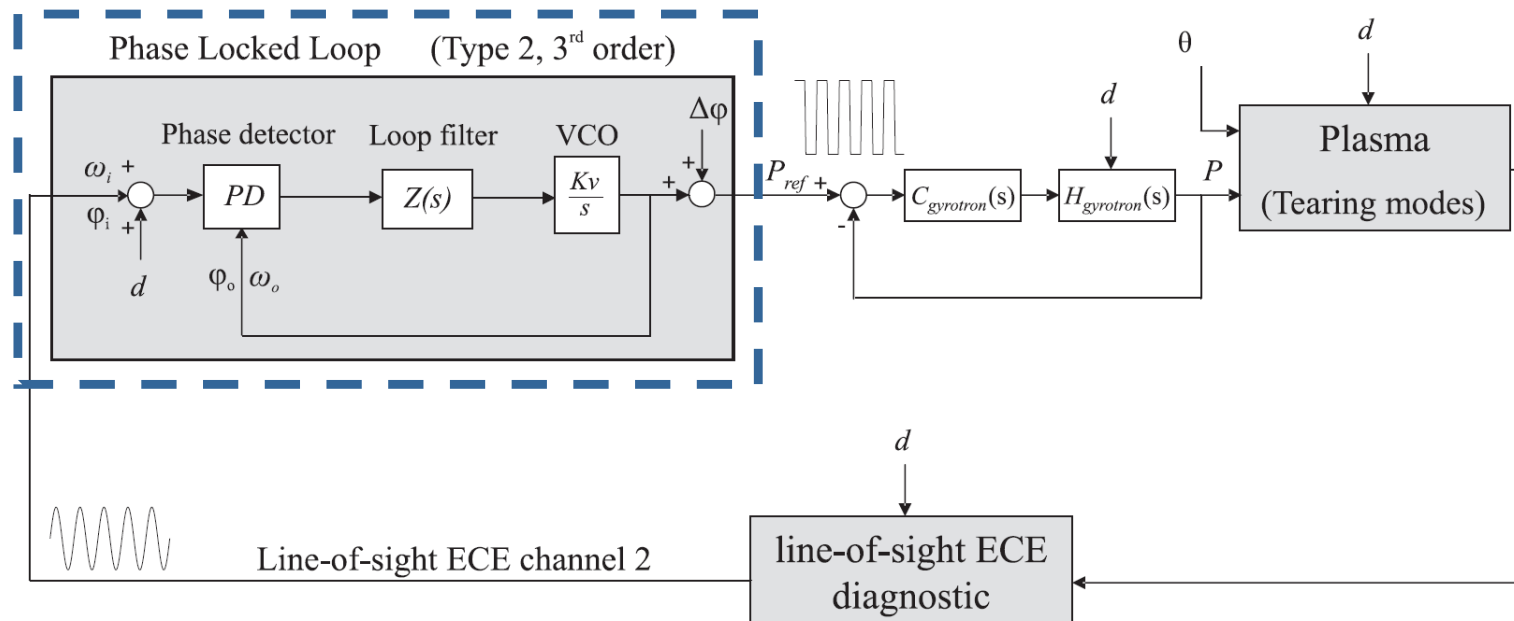
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PLL: operational domain: 300 Hz - 5 kHz





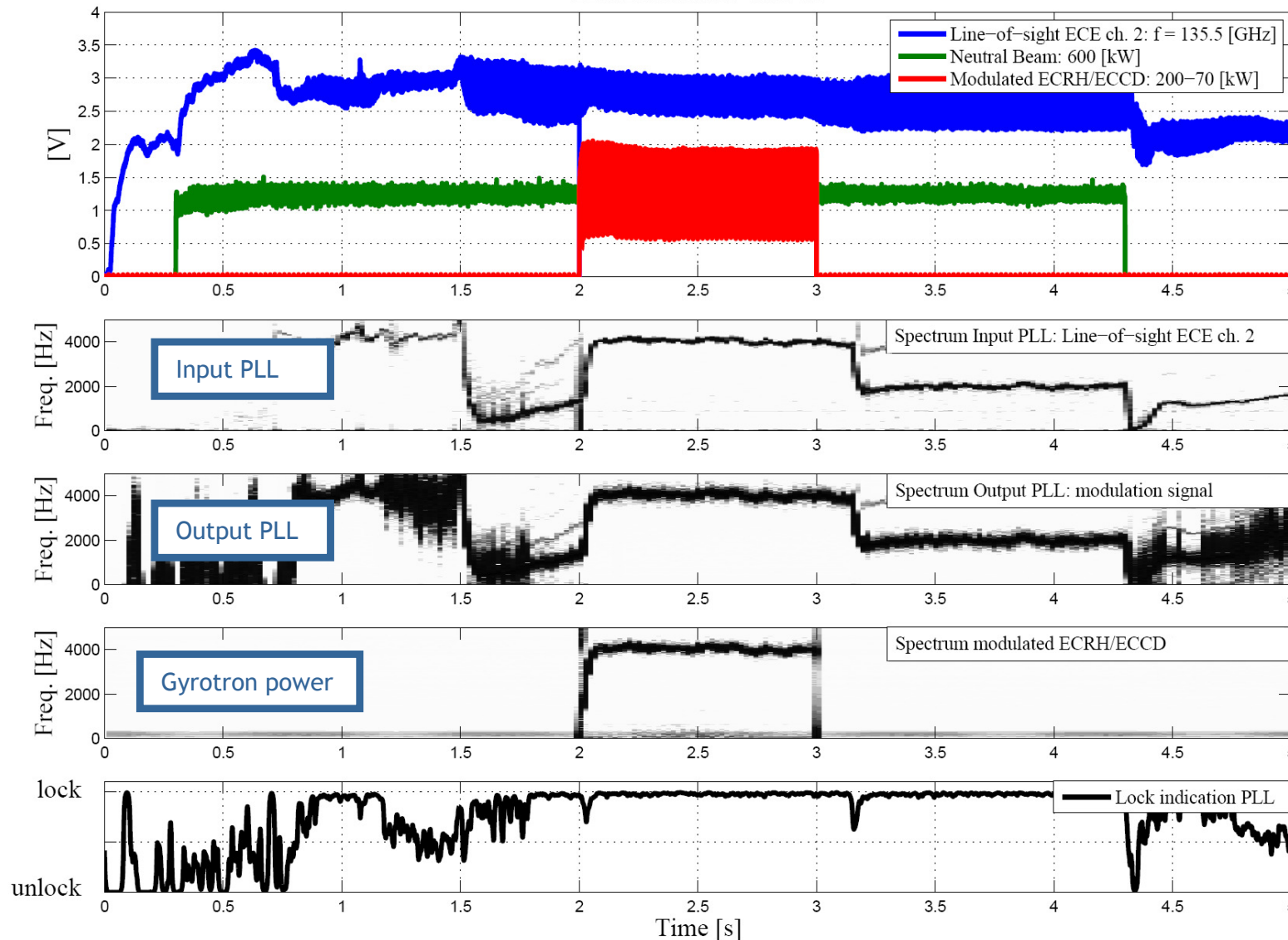
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Experimental Results

▪ Synchronous ECRH/ECCD modulation on O-point

TEXTOR shot # 110760



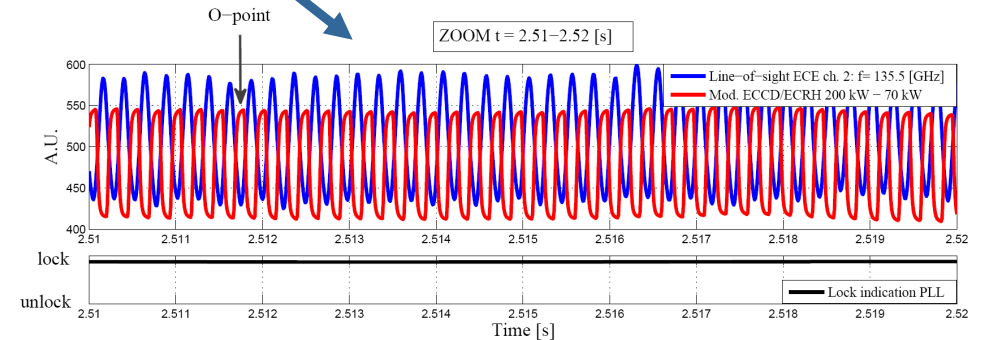
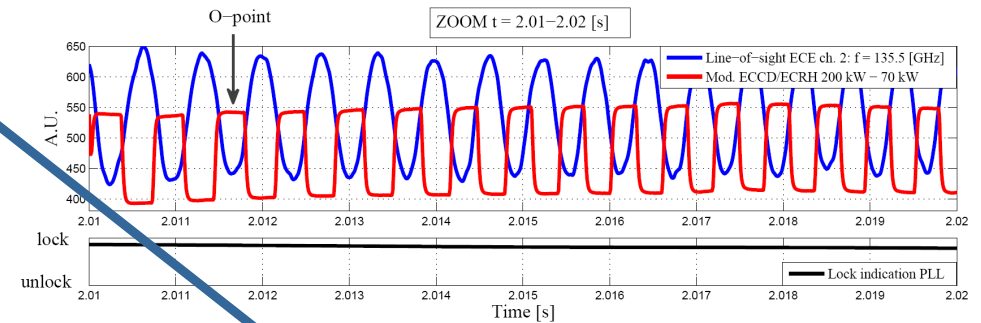
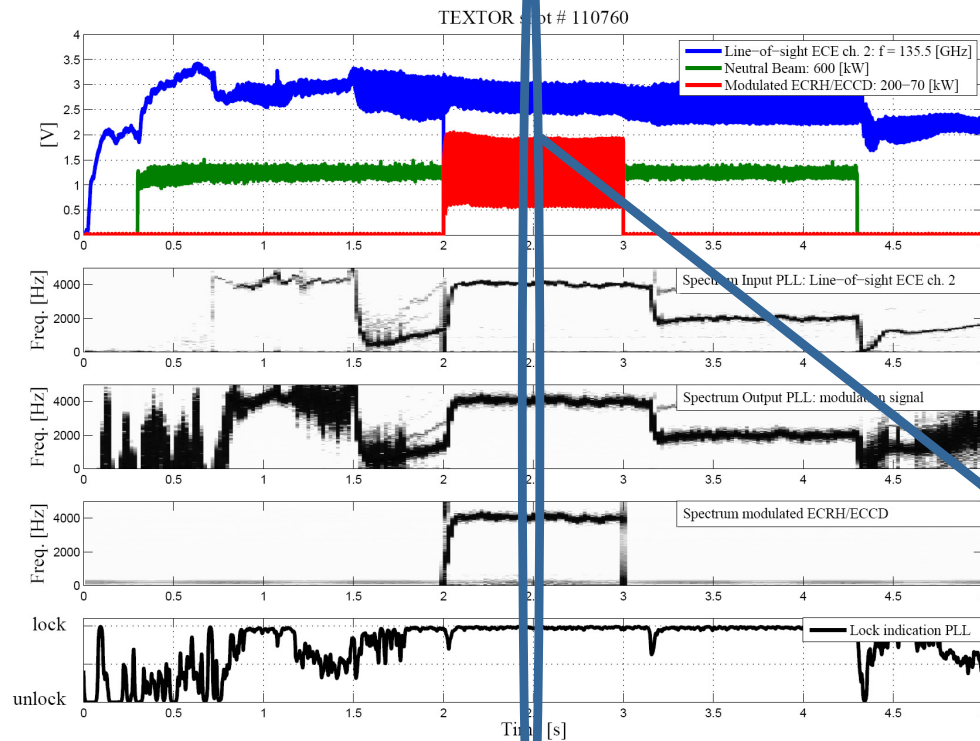
- $\theta_{\text{fixed}} = 10^\circ$
- $B_t = 2.25$ T
- $I_p = 300$ kA

- Modulated ECRH/ECCD
200 kW - 70 kW,
 $t = 2\text{-}3$ sec.
- Natural $m/n = 2/1$ mode
- Neutral Beam (co-direction) 600 kW



Experimental Results

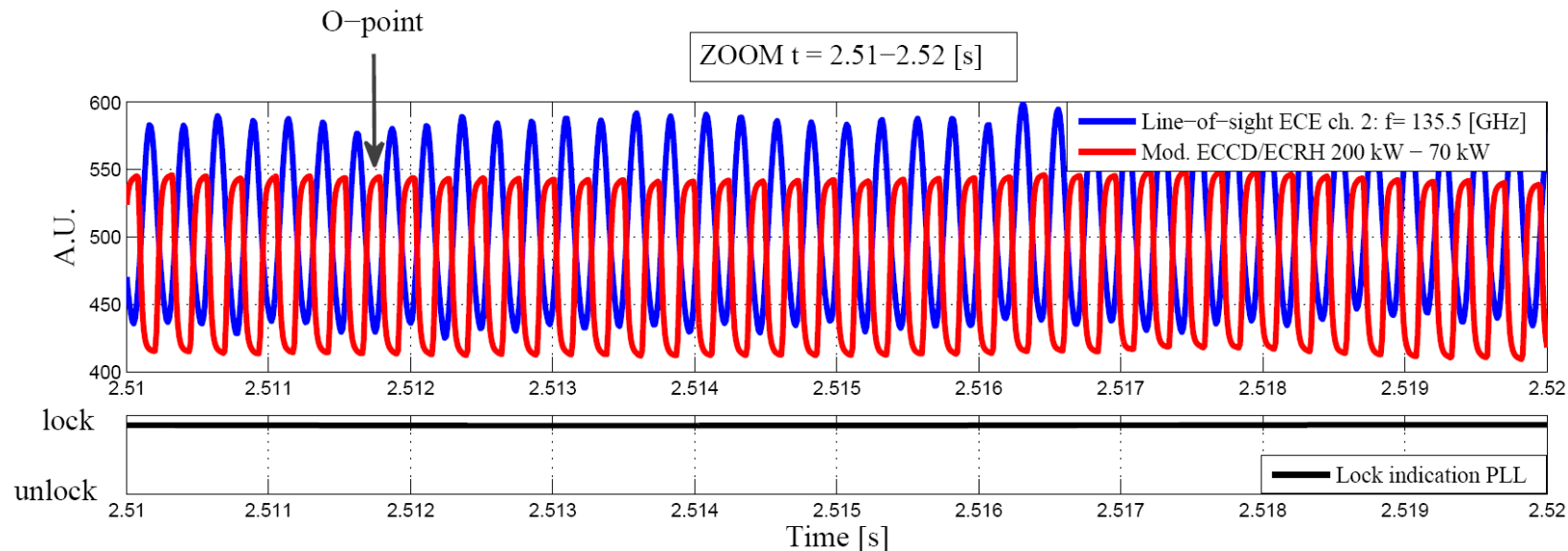
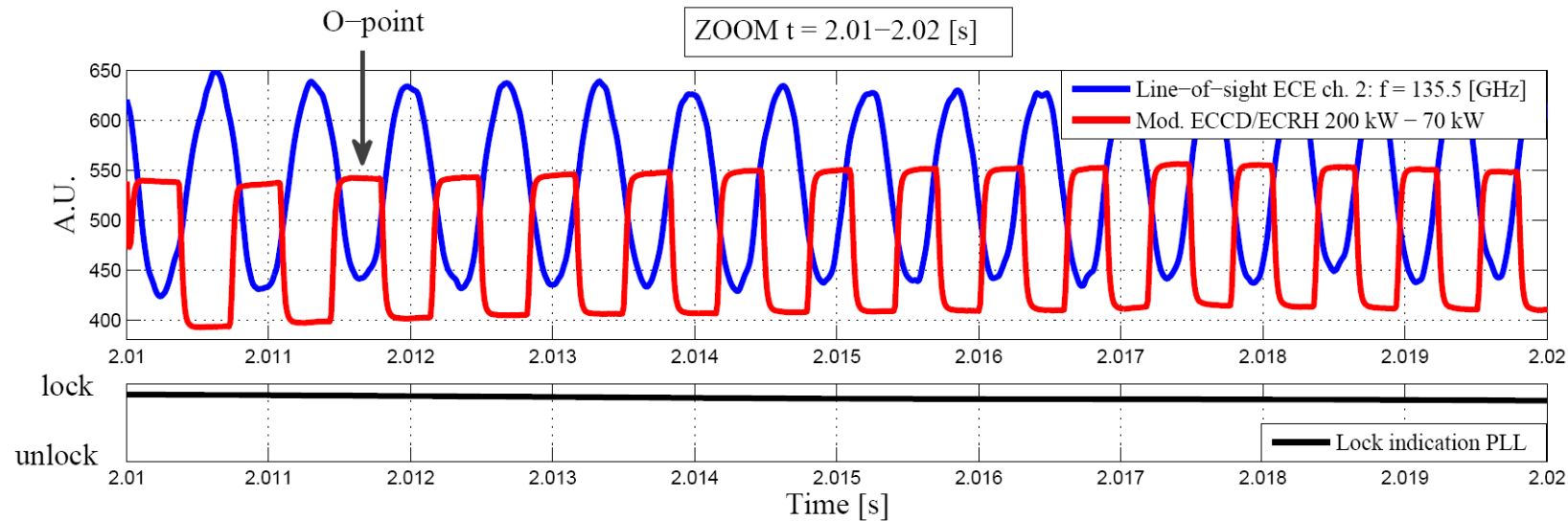
- Synchronous ECRH/ECCD modulation on O-point





Experimental Results

■ Synchronous ECRH/ECCD modulation on O-point





Conclusions

- Real-time tearing mode control system established on TEXTOR:
 - ☑ Line-of-sight ECE applied as feedback sensor in control loop with steer-able launcher and gyrotron as actuators
 - ☑ Algorithm for real-time detection of tearing modes implemented and demonstrated experimentally
 - ☑ Launcher dynamics analyzed and optimized through controller design (FB + FF)
 - ☑ ECRH/ECCD deposition aligned w.r.t. mode by matching actuator and sensor frequency in feedback loop (through launcher steering)



Conclusions

- Real-time tearing mode control system established on TEXTOR:
 - ☑ Alignment achieved accurately and fast with a simple controller
 - ☑ Tearing mode search-and-suppress demonstrated experimentally (both stabilization and full suppression achieved)
 - ☑ Tracking capabilities control system demonstrated experimentally (subject to Bt ramp; mimic perturbation on tearing mode location)
 - ☑ Synchronous ECRH/ECCD modulation on O-point of tearing mode using phase locked loop demonstrated experimentally



- Future developments:

- Implement “Line-of-sight ECE” in waveguide environment (long pulse operation)
- Design of advanced controllers (model-based, including tearing mode dynamics)
- Increase number of radiometer channels (enhanced mode identification)
- Full control over tearing mode’s width

- Open questions:

- How to deal with locked modes ?
- How to predict mode occurrence in advance ?



Questions ?

