

# Efficacy of current-driven resistive-wall-mode feedback control

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In collaboration with

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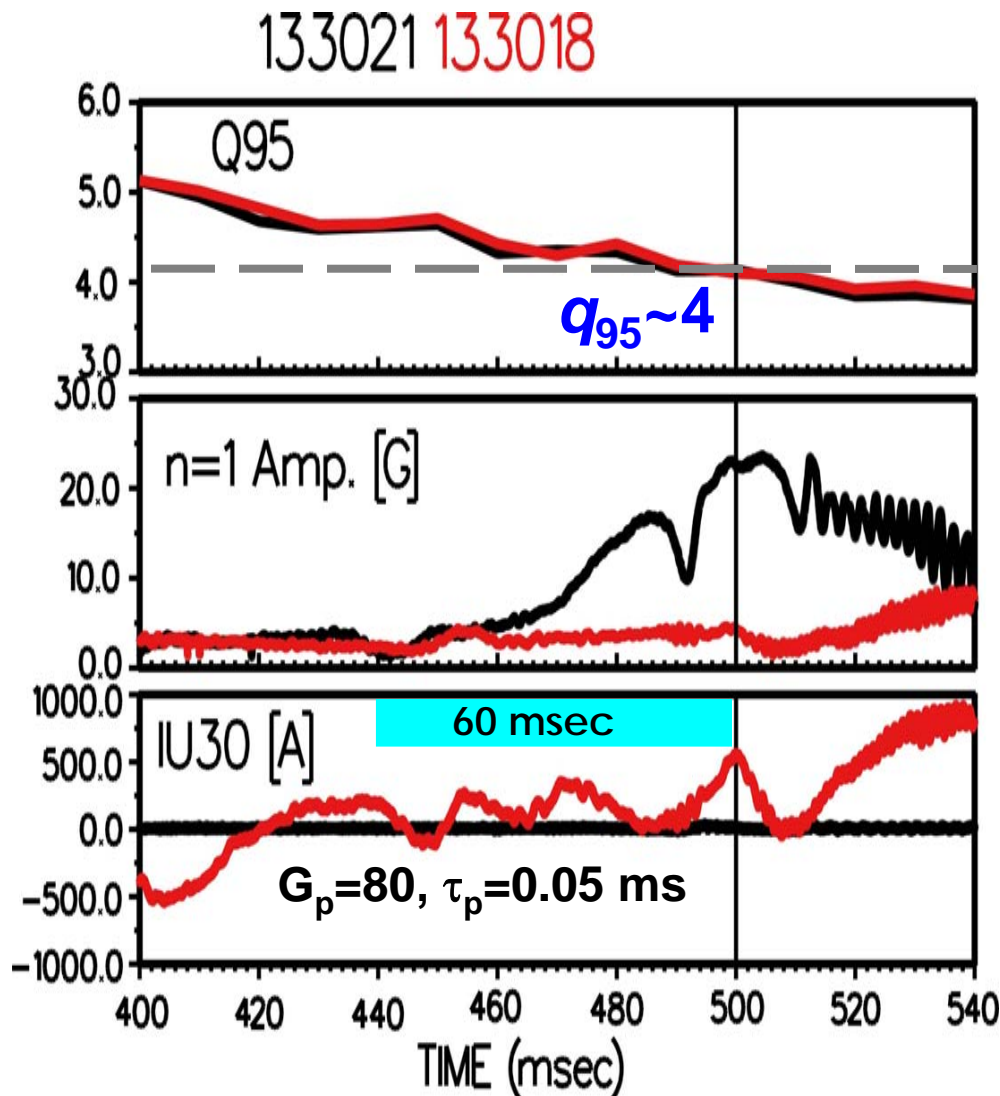
US-Japan Workshop on MHD Control, Magnetic Islands and  
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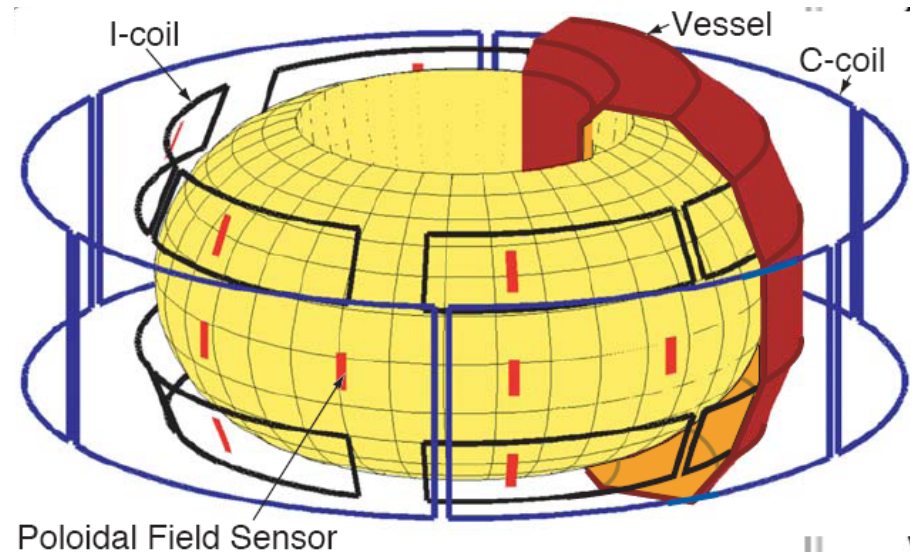
# The efficacy of feedback stabilization can be well addressed in terms of minimal plasma disturbances

- Highly reproducible current-driven RWM enables us to explore the RWM feedback control in detail
  - Due to the irreproducibility of pressure-driven RWMs, the RWM feedback process has not been evaluated thoroughly.
  - The RWM feedback control can be assessed using a reproducible RWM target at  $q_{95} \sim 4$ .
- The feedback stabilization efficacy needs to be assessed based on both internal and external plasma responses

# Complete feedback stabilization of current-driven RWM at $q_{95} \sim 4$ has been achieved in DIII-D



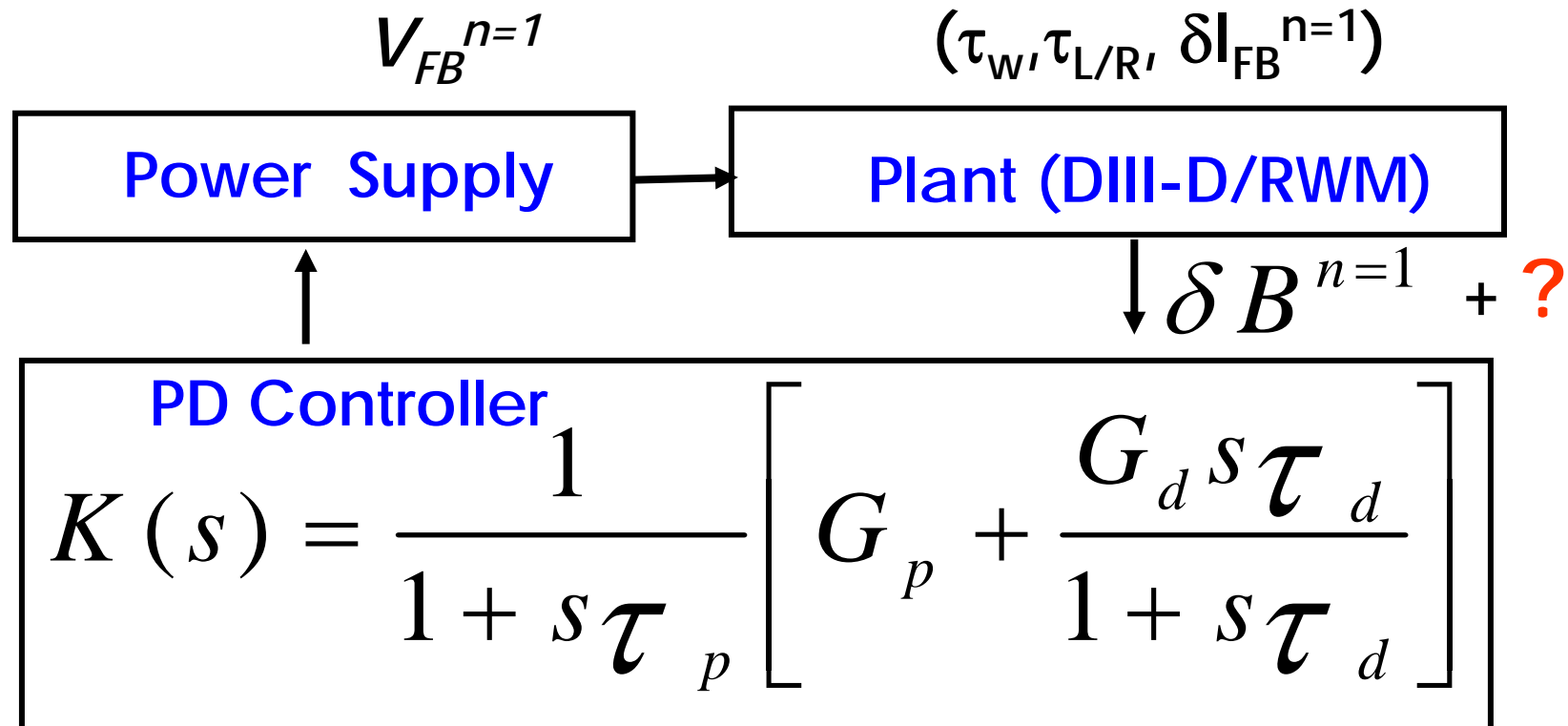
- Ohmic discharge with high current ramp-up rate
- Tools
  - Internal coils (“I-coils”): Direct Feedback + Dynamic error field correction (EFC)
  - External coils (“C-coils”): Static EFC





# The RWM feedback control loop is fully equipped with slow and fast time scale actuators

- Feedback loop ( $\tau_p \ll \tau_w$ )

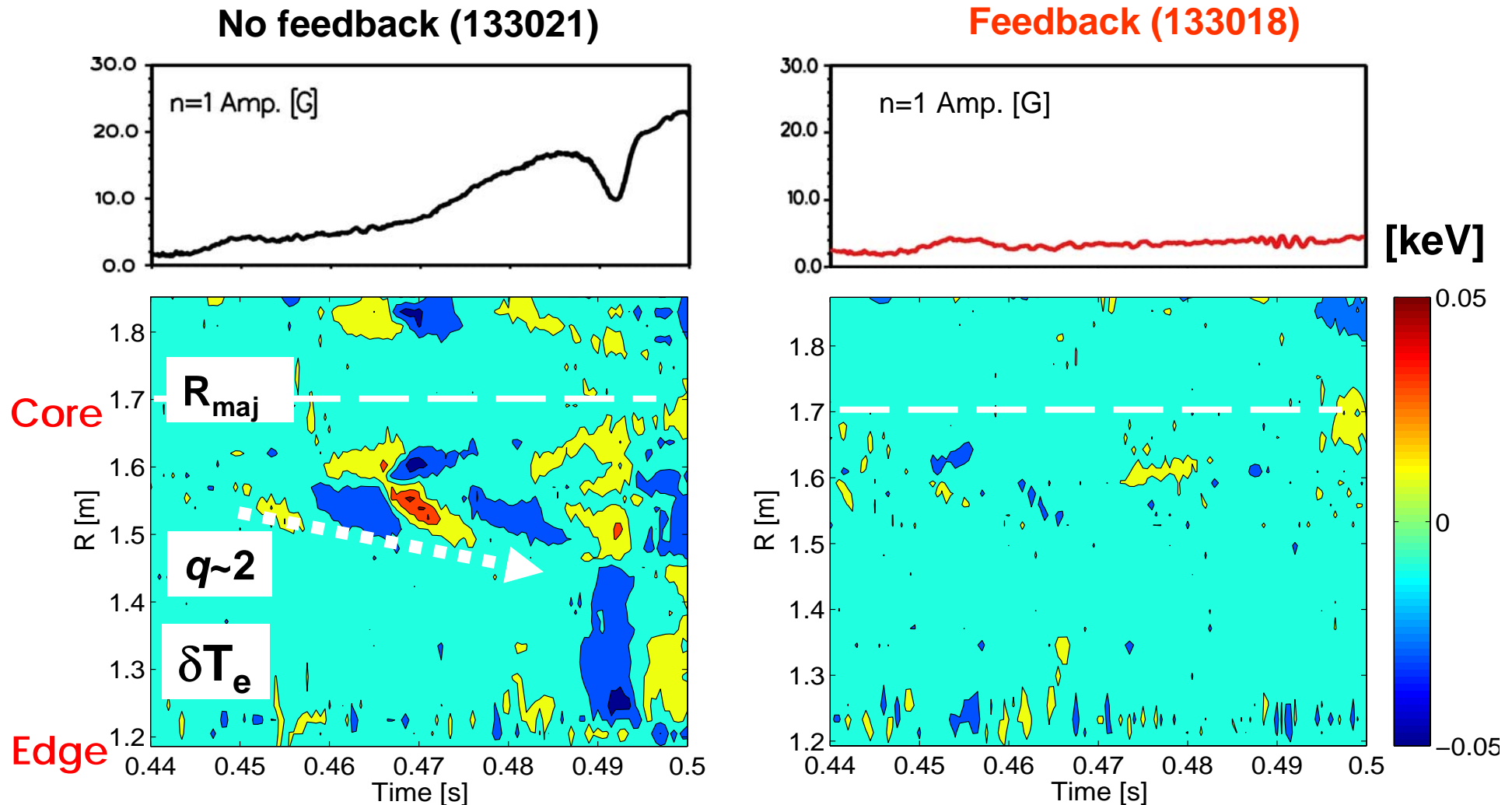


$G_{p,d}$  : Gain     $\tau_{p,d}$  : time constant  
 where p - proportional, and  
 d - derivative

# Key results

- Current-driven RWM at  $q_{95} \sim 4$  was completely stabilized by the RWM feedback control with  $G_p$  only.
- The use of derivative gains ( $G_d=10G_p$ ) expanded the stable range of proportional gains.
  - Reducing a phase lag in time avoids any mismatch between RWM and applied field.
  - High gain scan results suggest the contributions of the I-coils necessary for DEFC
- A phase-shifted  $n=1$  field in the direction of co- $I_p$  rotation is more effective than in the opposite direction.

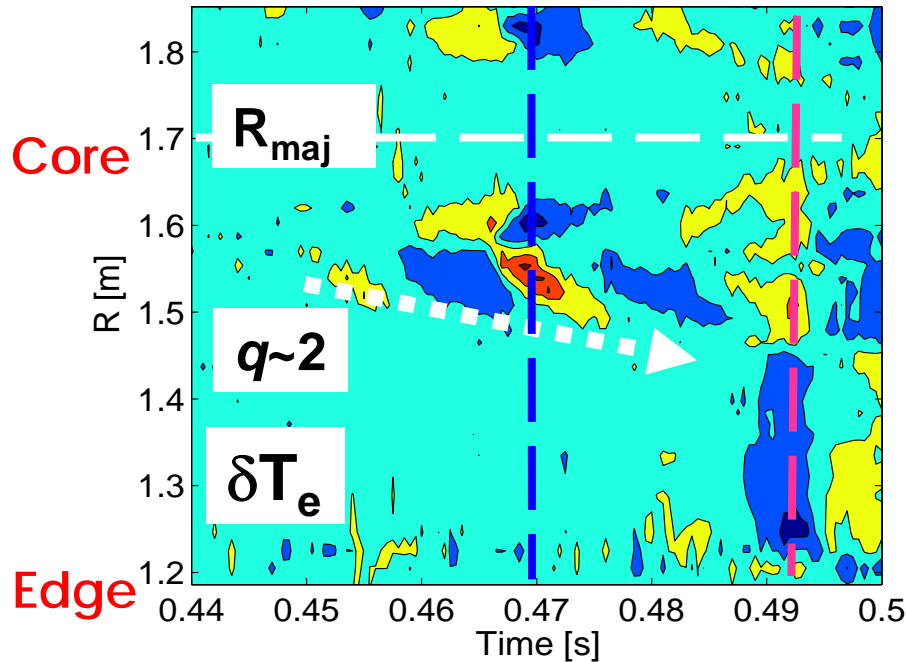
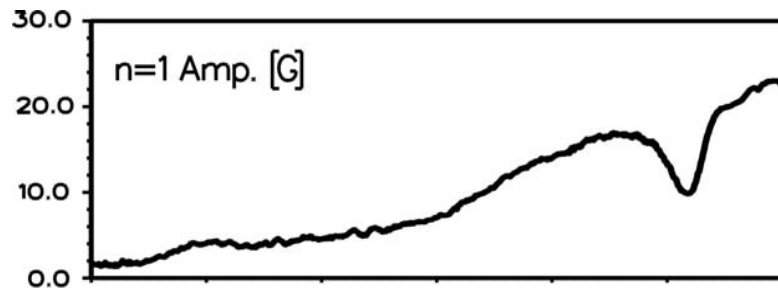
# The RWM-associated internal structures are eliminated by RWM feedback control



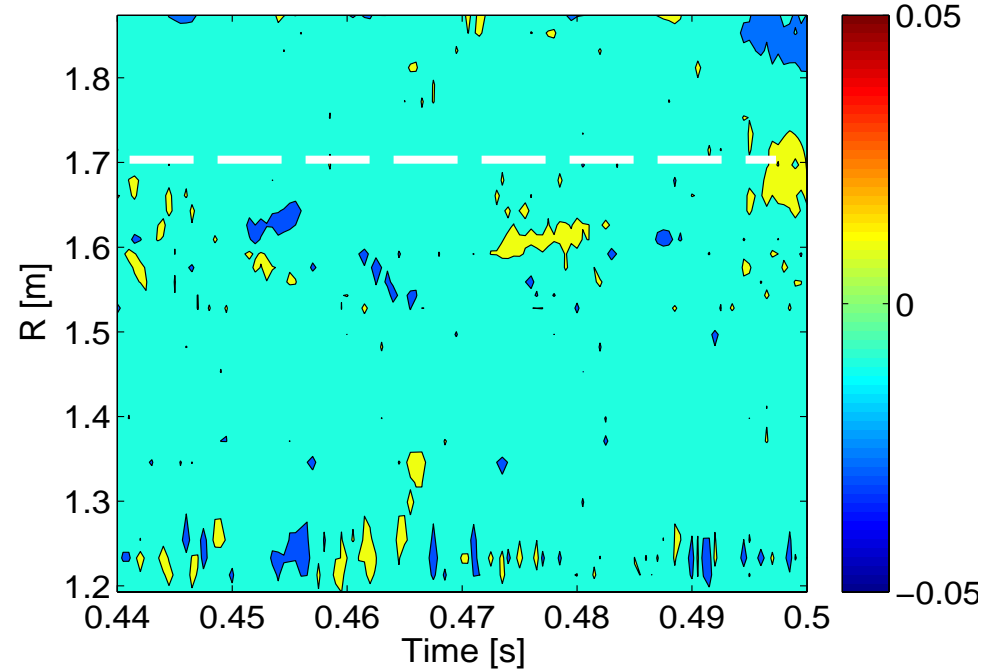
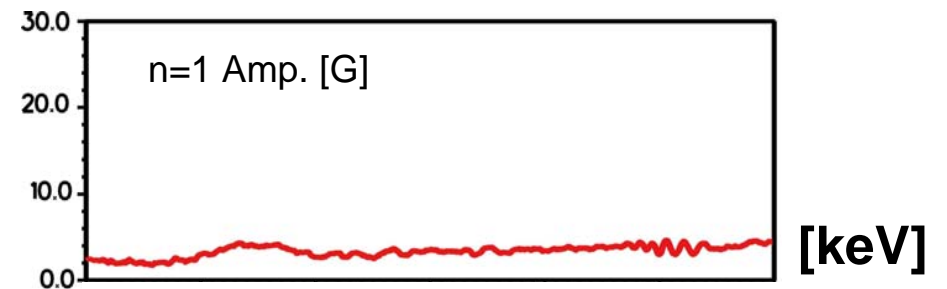
- RWM-induced edge disturbance is also suppressed.

# The $|\delta T_e|_{\max}$ is reduced by more than a factor of 2 with optimized feedback

No feedback (133021)



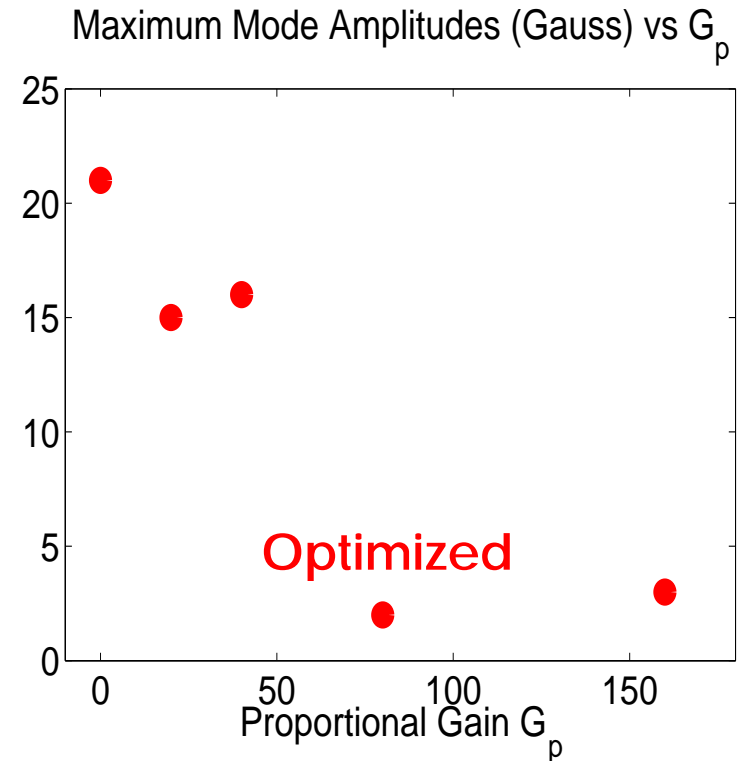
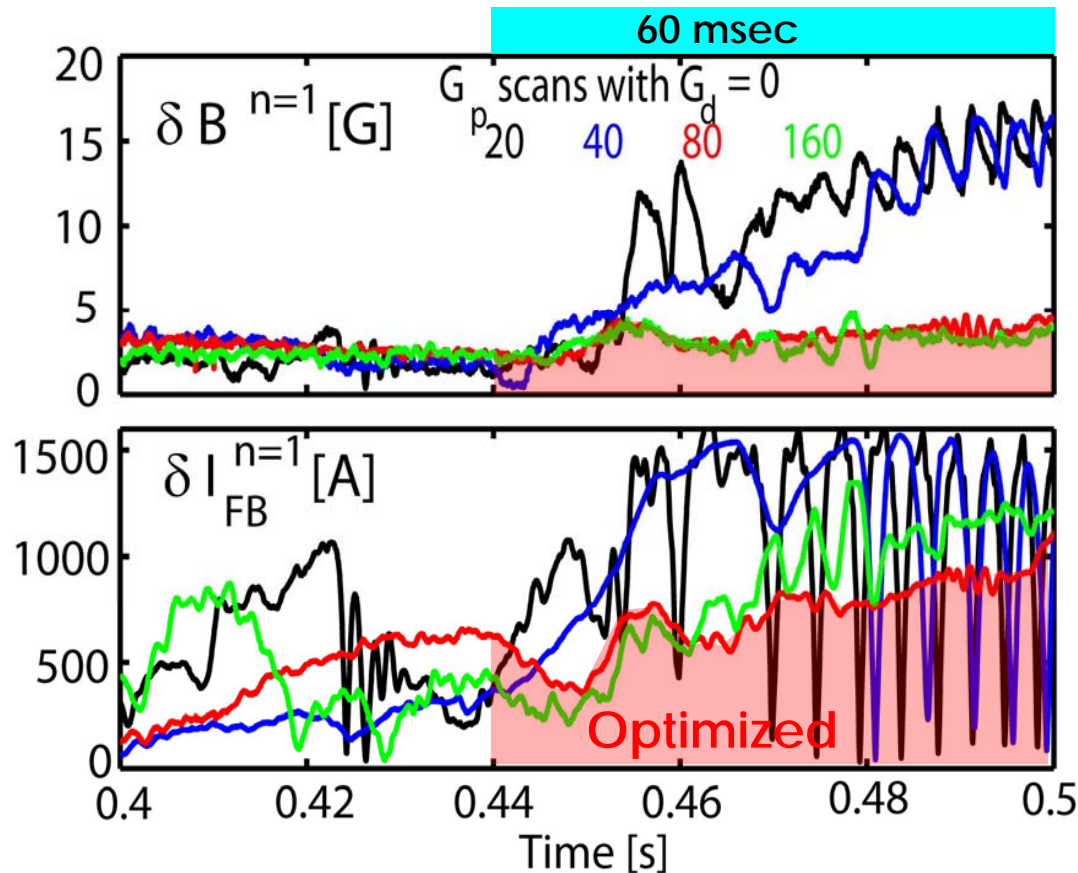
Feedback (133018)



$(|\delta T_e|_{\max})_{\text{No FBK}}: 40 \sim 50 \text{ eV}$

$(|\delta T_e|_{\max})_{\text{optimized}} < 20 \text{ eV}$

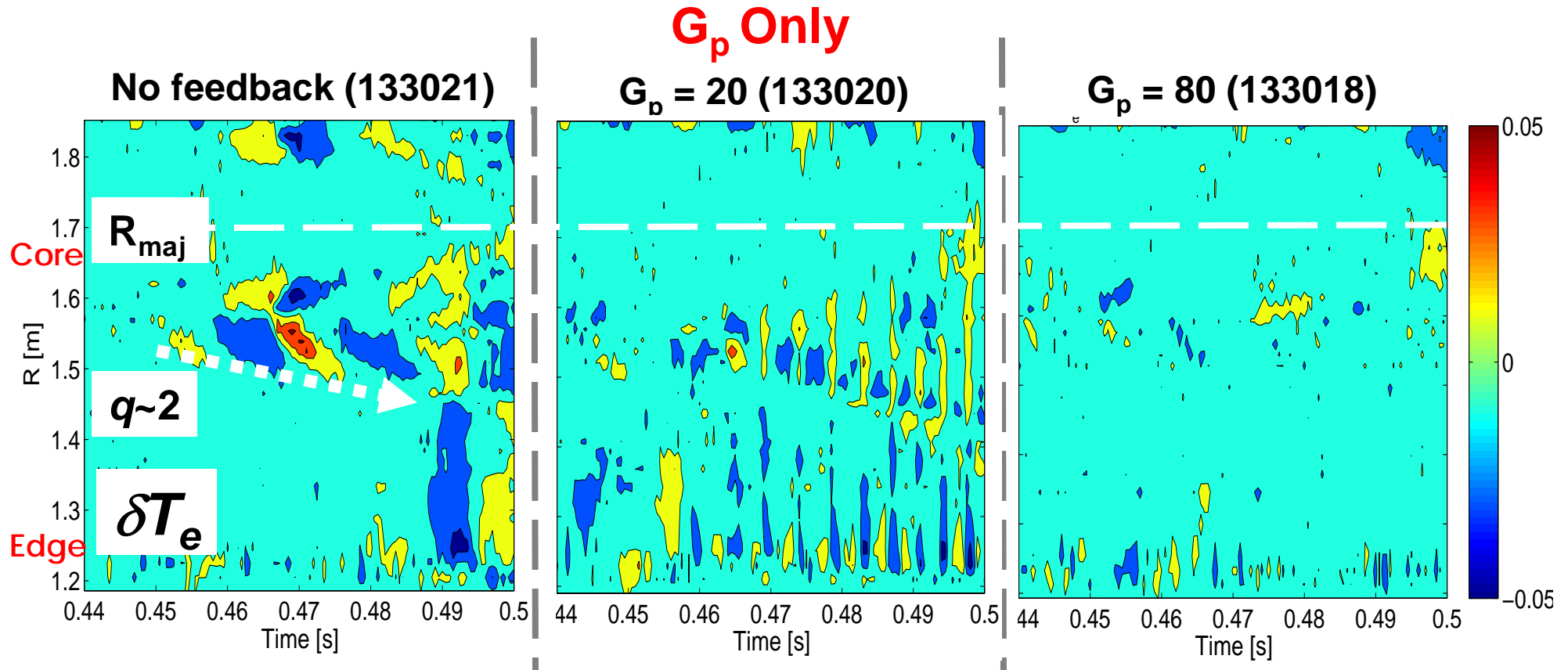
# The optimized gain ( $G_p=80$ ) has been found with $G_p$ only



- As the gain approaches the optimal level, the mode growth rate decreases as expected.



# Sub-optimal gain is not only less effective in suppressing the RWM but also disturbs the plasma edge

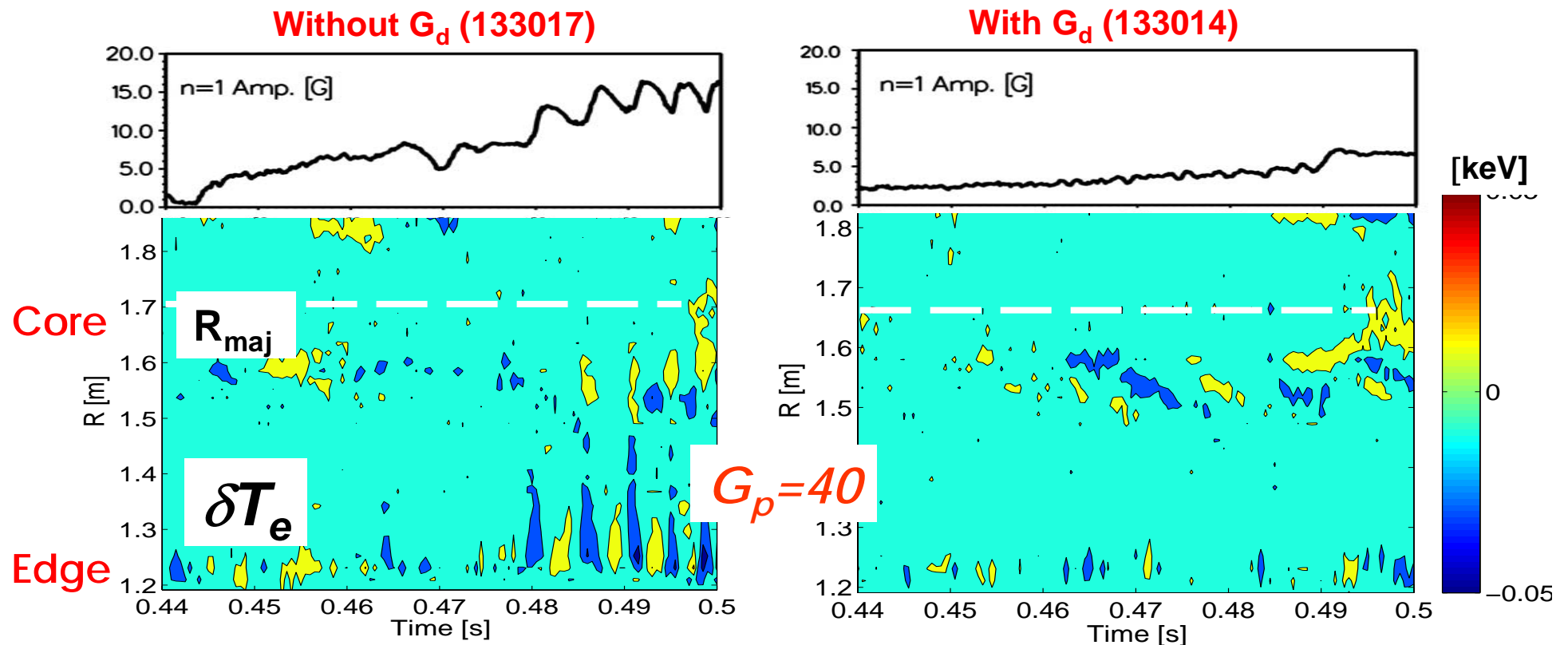


- Meanwhile, the edge disturbances are not observed at the over-optimal gain (e.g.  $G_p = 160$ ).

# Key results

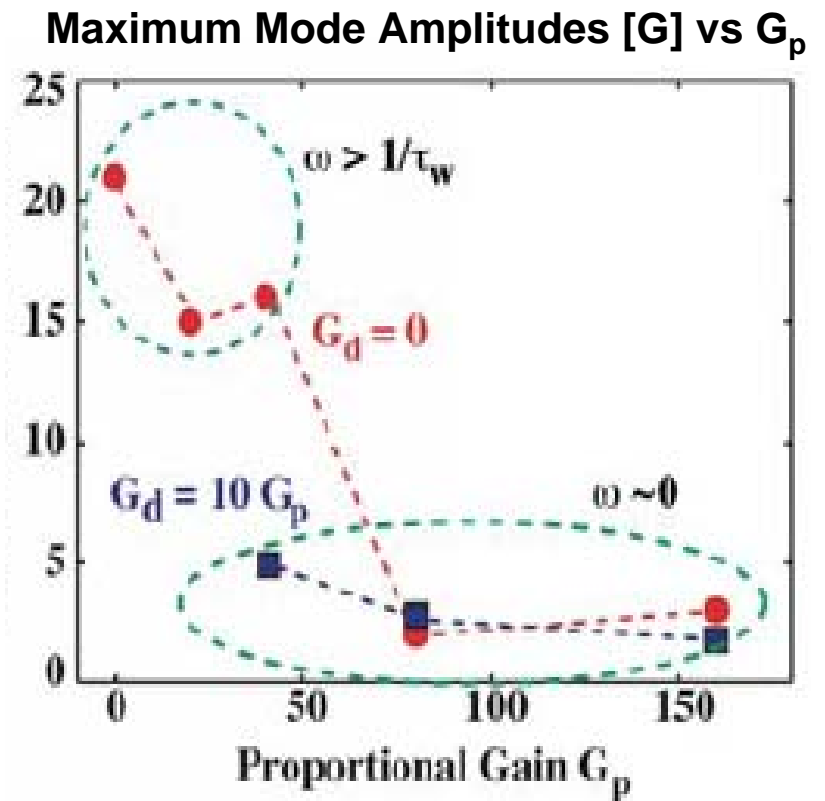
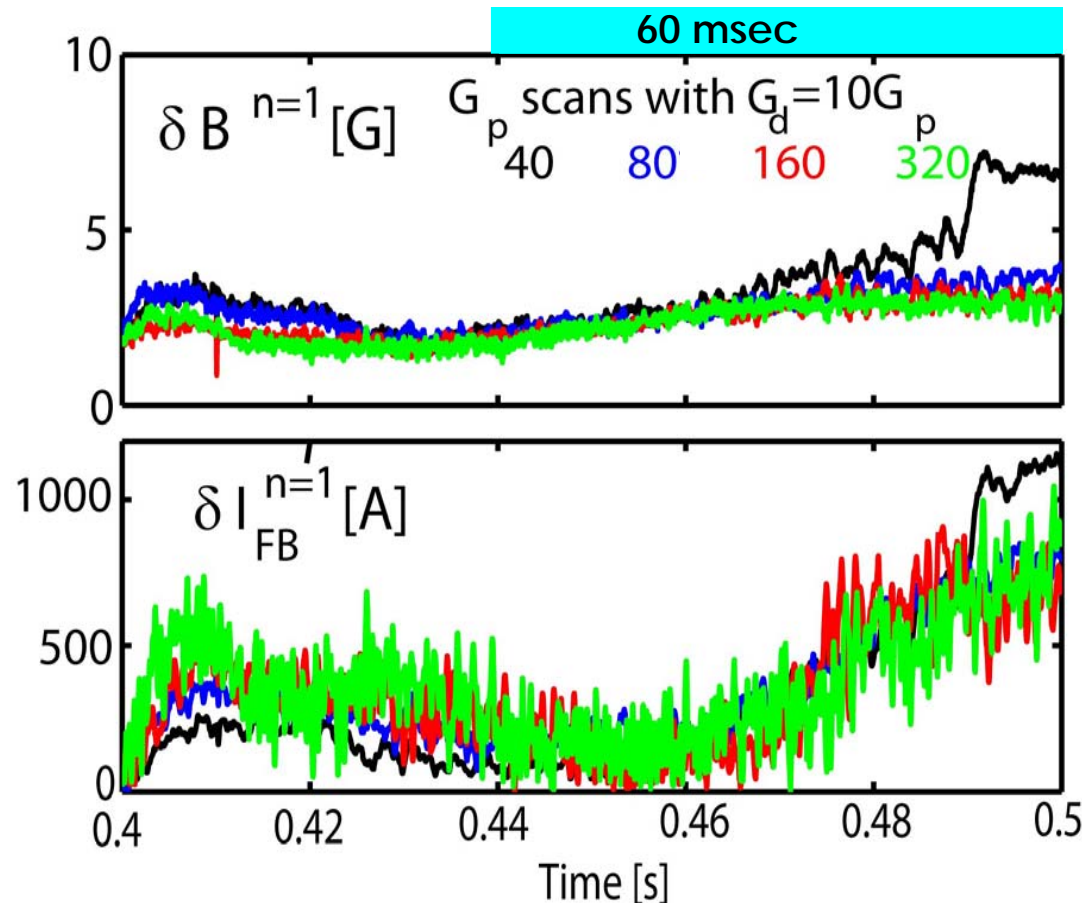
- ✓ Current-driven RWM at  $q_{95} \sim 4$  was completely stabilized by the RWM feedback control with  $G_p$  only.
- The use of derivative gains ( $G_d=10G_p$ ) expanded the stable range of proportional gains.
  - Reducing a phase lag in time avoids any mismatch between RWM and applied field.
  - High gain scan results suggest the contributions of the I-coils necessary for DEFC
- A phase-shifted  $n=1$  field in the direction of co- $I_p$  rotation is more effective than in the opposite direction.

# The use of derivative gain broadened the effective gain range for RWM feedback stabilization at $q_{95} \sim 4$



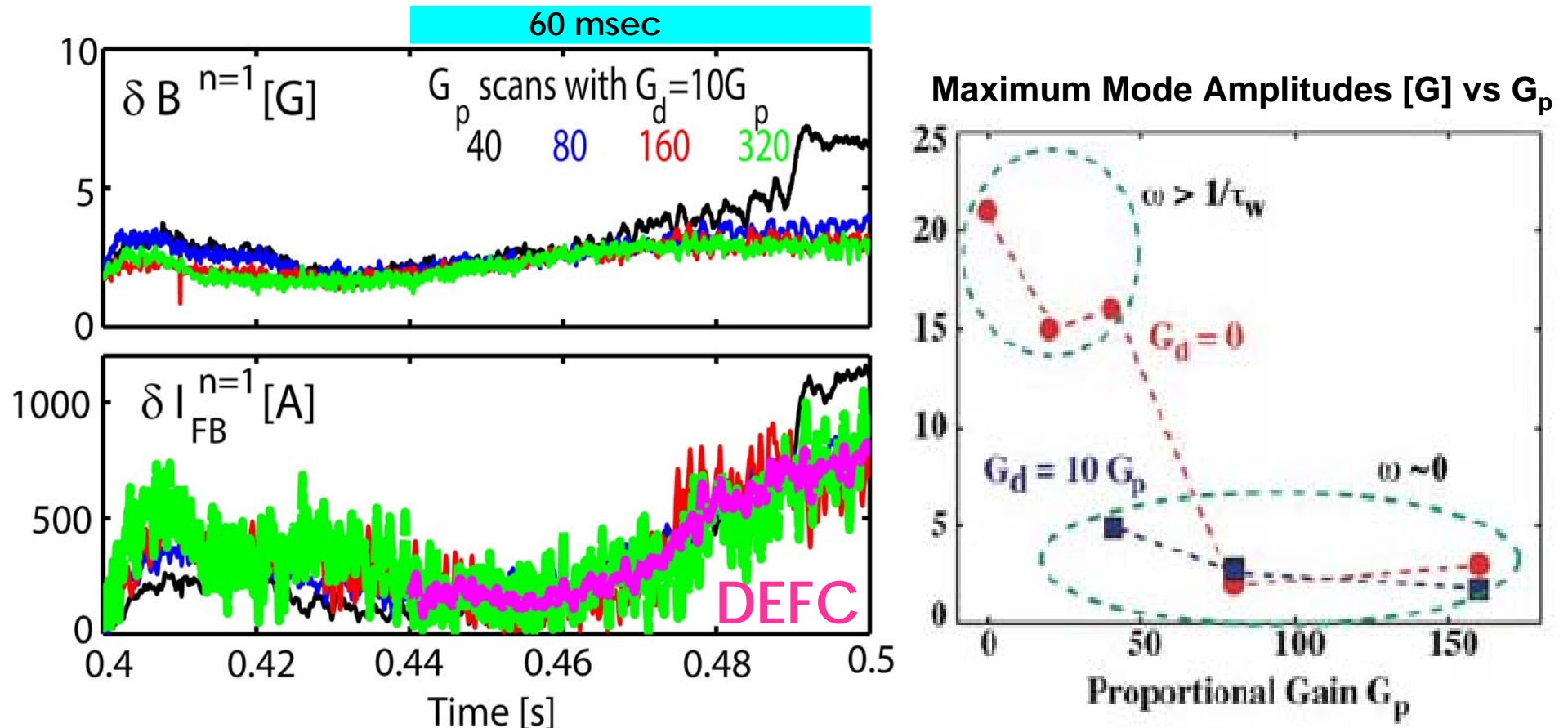
- The addition of  $G_d$  minimizes the phase lag in time between RWM and the applied field.
- A value of  $G_d = 10G_p$  is chosen to use voltage controller 'effectively' as **current controller**, based on  $\tau_d$  and  $\tau_{L/R}$  of the feedback system.

# Direct RWM control is the dominant stabilization process, while good error field correction is prerequisite



- Similarly finite amplitude of the coil currents at various  $G_p$  values indicate the EFC portion necessary for effective stabilization.

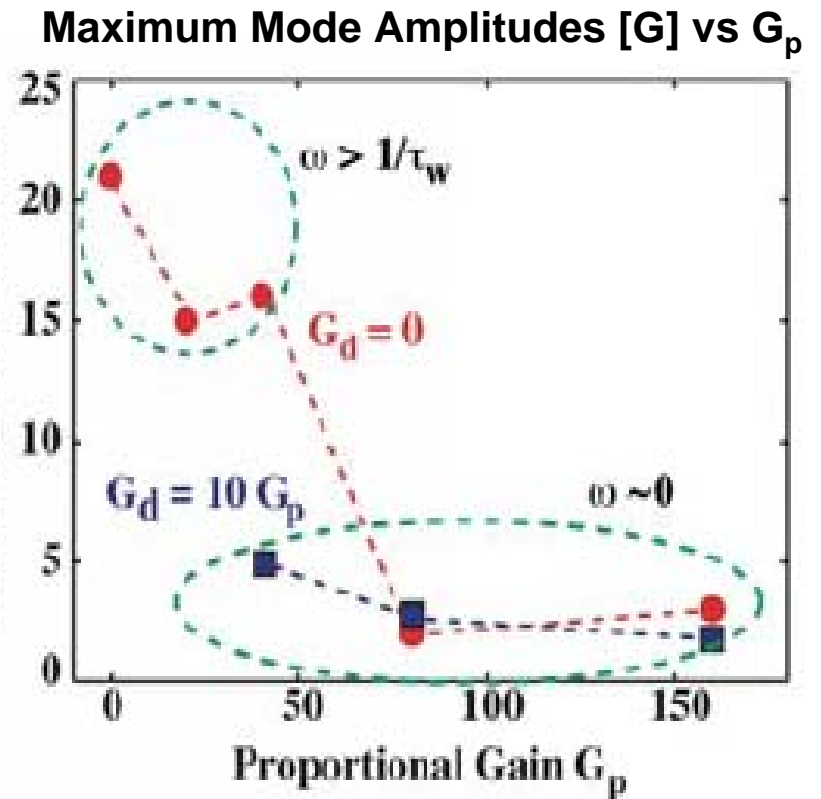
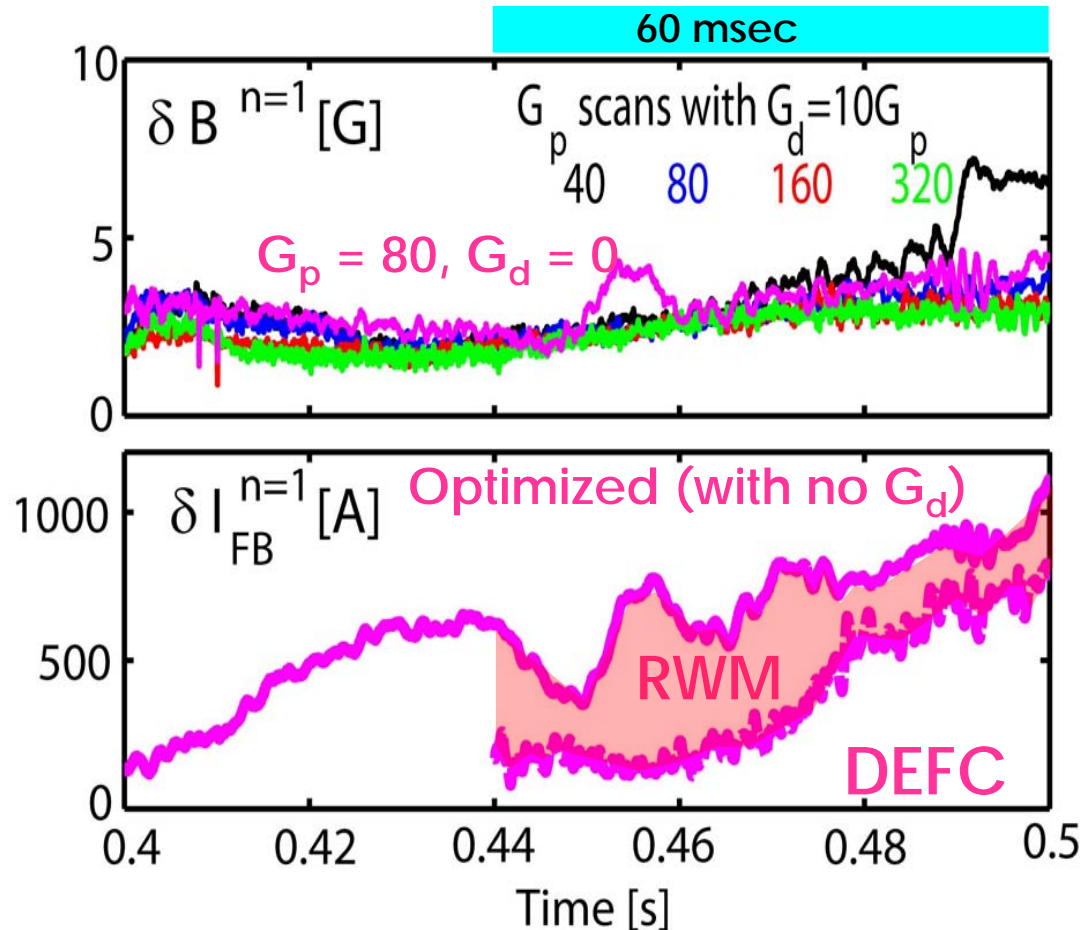
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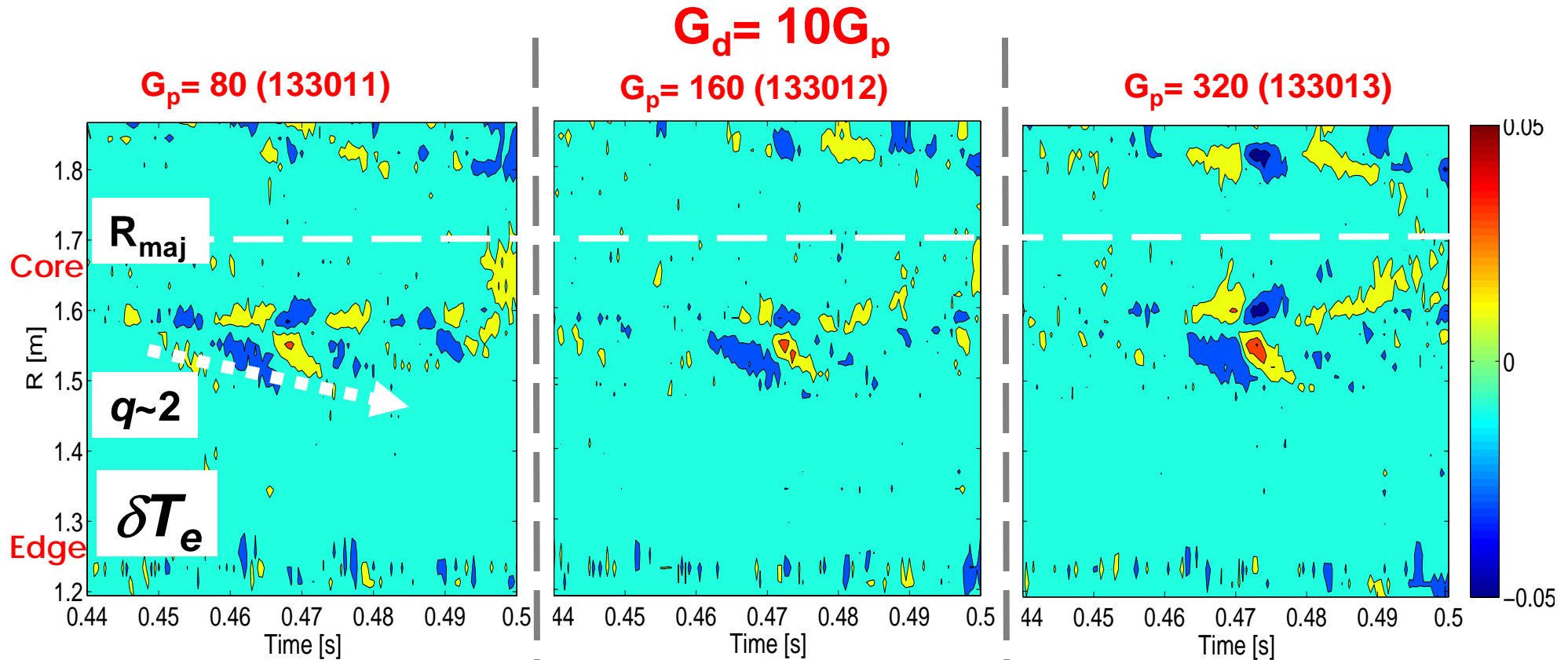
# Direct RWM control is the dominant stabilization process, while good error field correction is prerequisite



Complete stabilization  
= RWM + DEFC

- From the known DEFC, the portion of the coil current necessary for the direct RWM control can be extracted.

# The efficacy of the feedback stabilization needs to be cautiously assessed based on magnetics alone

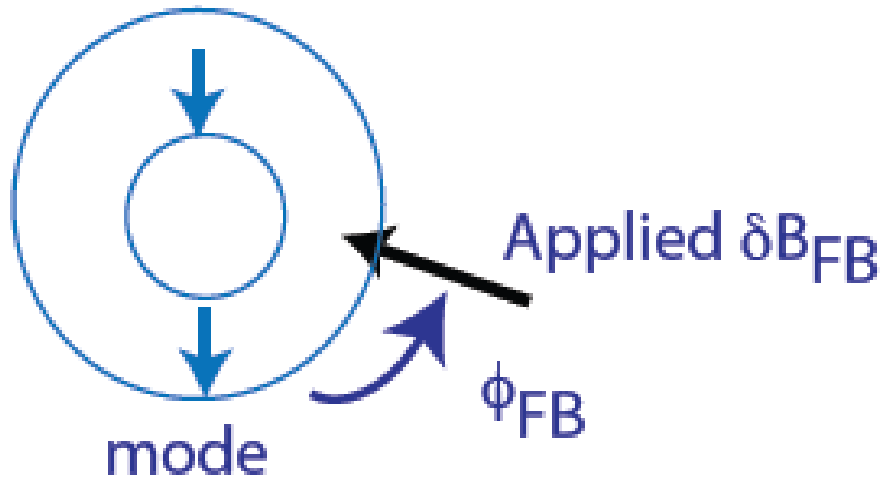


- Similar plasma responses based on magnetics may not reflect the detailed evolution of the RWM-associated internal structures.
- The choice of  $G_d$  may not be optimal yet (likely due to mode coupling to coil currents,  $(\tau_{L/R})_{eff} \neq \tau_{L/R}$ )

# Key results

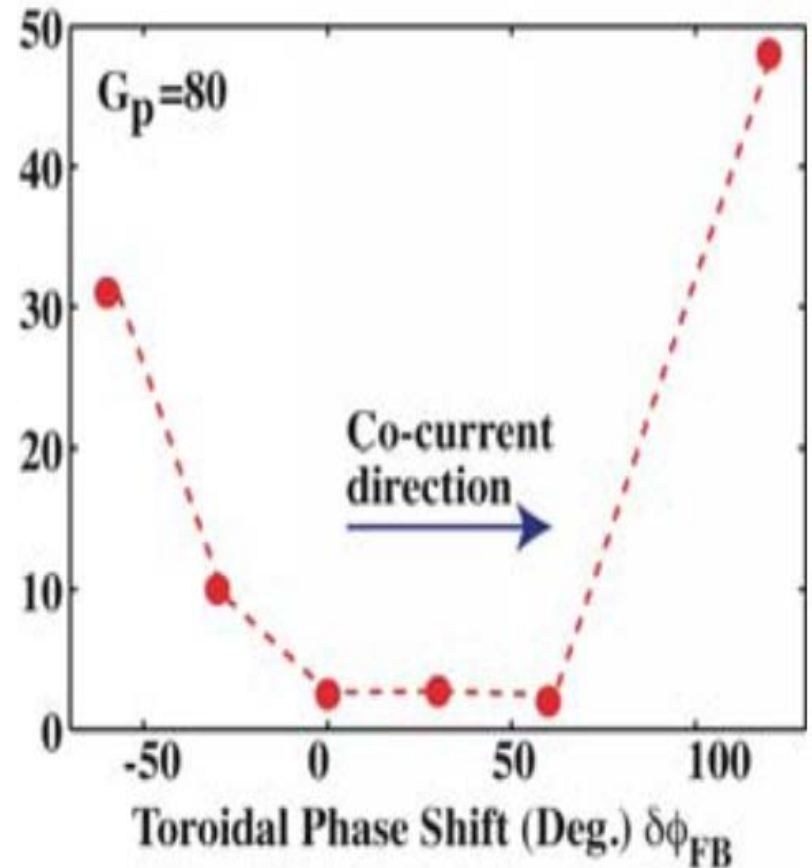
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- ✓ The use of derivative gains ( $G_d=10G_p$ ) expanded the stable range of proportional gains.
  - Reducing a phase lag in time avoids any mismatch between RWM and applied field.
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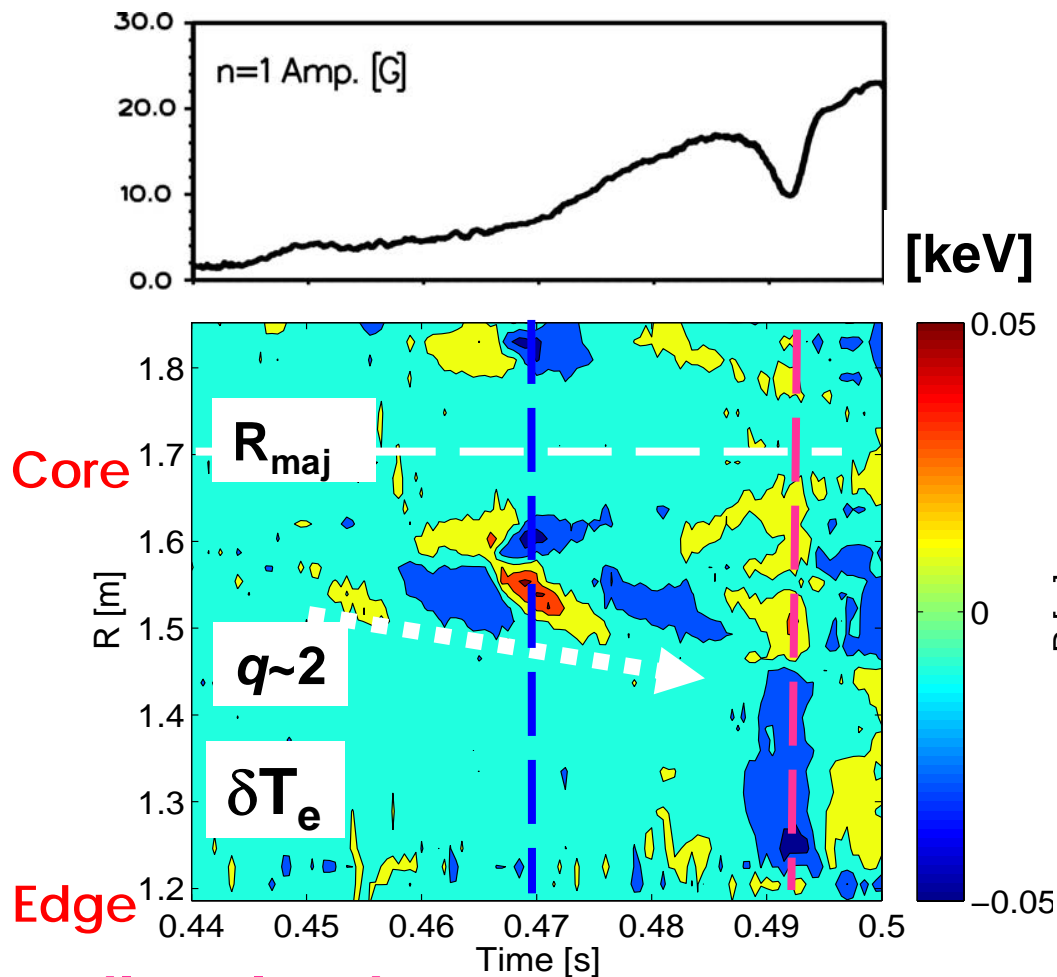
- A range of preferred toroidal phase shifts ahead of the RWM exists for effective feedback

Maximum Mode Amplitudes [G] vs  $\delta\phi_{FB}$

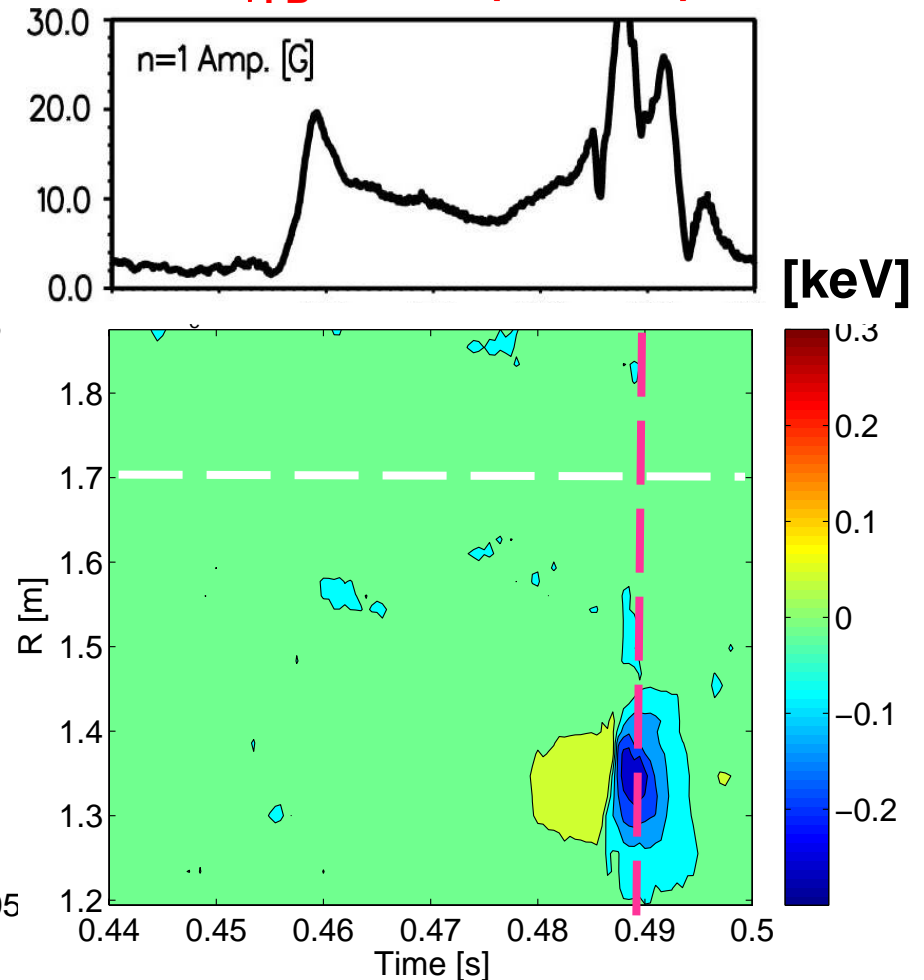


# An unfavorably phase-shifted $\delta B_{FB}$ may form edge disturbance near a pitch-resonant surface

No feedback (133021)



$\delta\phi_{FB} = -60^\circ$  (133025)



$(|\delta T_{elmax}|)_{No\ FBK} : 40 \sim 50\ eV$

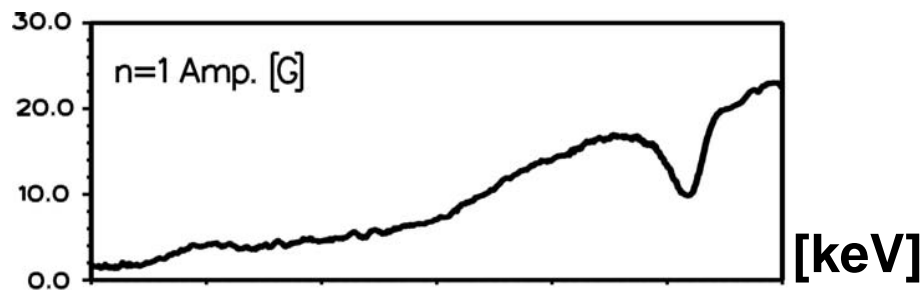
$|\delta T_{elmax}| \sim 250\ eV$

$= 6 \times (|\delta T_{elmax}|)_{No\ FBK}$

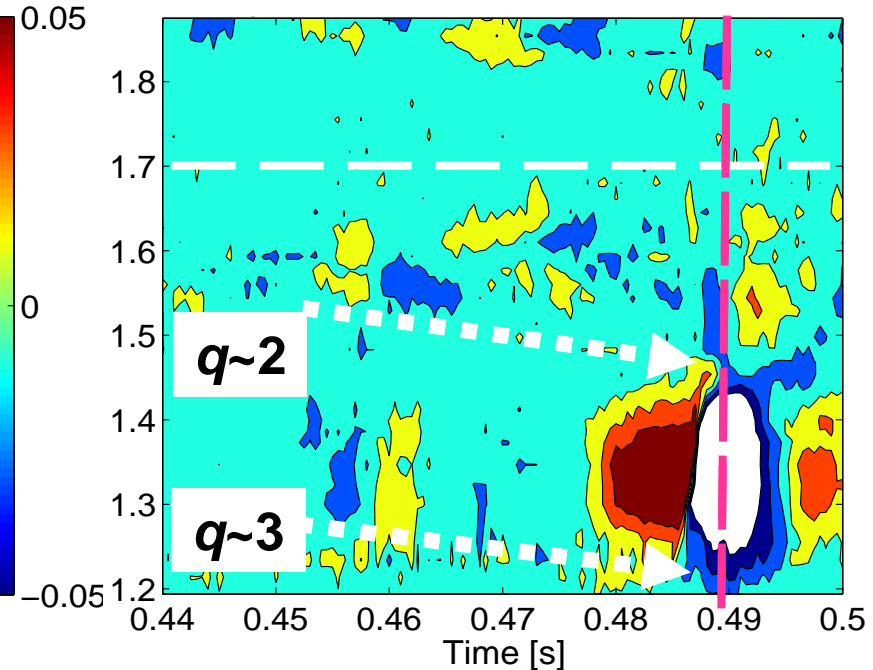
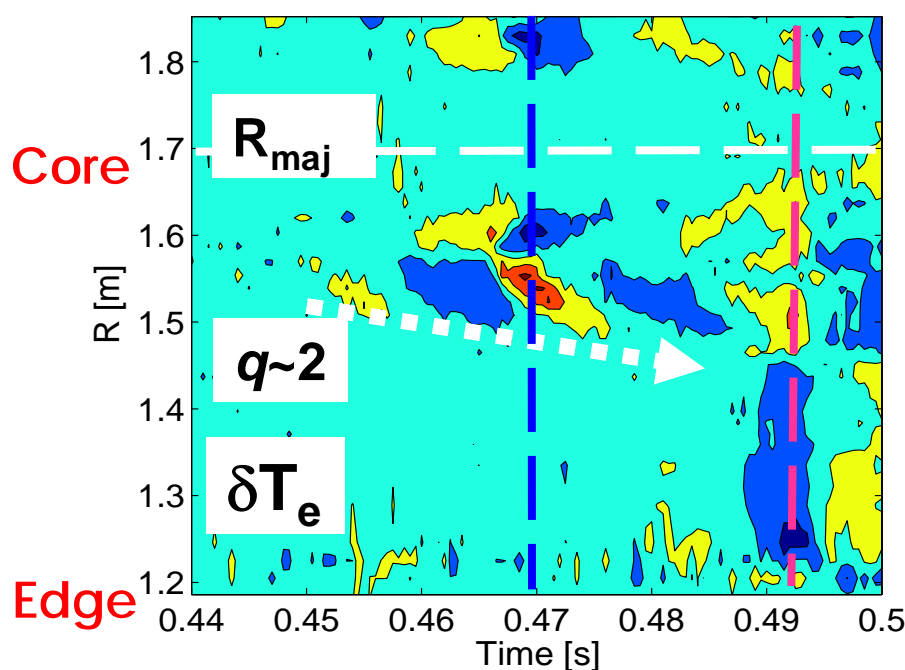
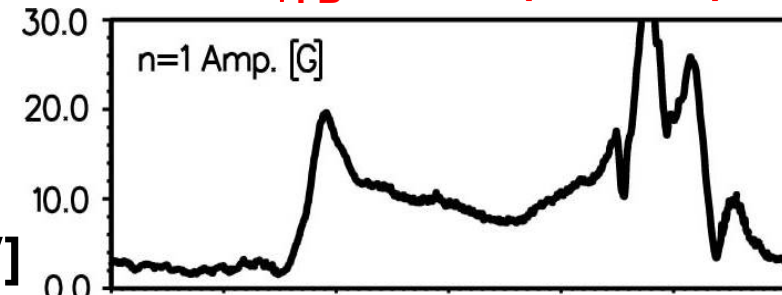


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$(|\delta T_{e|_{max}})_{No\ FBK} \sim 40 \sim 50\ eV$

$|\delta T_{e|_{max}} \sim 250\ eV$

$= 6 \times (|\delta T_{e|_{max}})_{No\ FBK}$

# Caveats to note

- Slowly growing RWM may play a role of ‘error’ field.
  - Once a certain level is reached, the RWM-induced magnetic islands are widespread in the outer region of the plasma.
  - Such RWM-induced magnetic islands consist of a mixture of poloidal modes (e.g. multiple resonant surfaces).
- In comparison, the EF-driven edge structure may be relevant to a pitch-resonant surface inside the plasma (e.g.  $m/n = 3$  (or  $2$ )/1 ?).
- Meanwhile, the edge disturbances during the sub-optimal gains might not have been from the same mechanism, in that
  - The edge disturbances are formed in the outermost region first, and then propagate inward, as a residual stray field increases without having a pitch resonant surface. -> kink?
  - BUT, the addition of  $G_d$  appears to prevent RWM+EF from making edge disturbances.

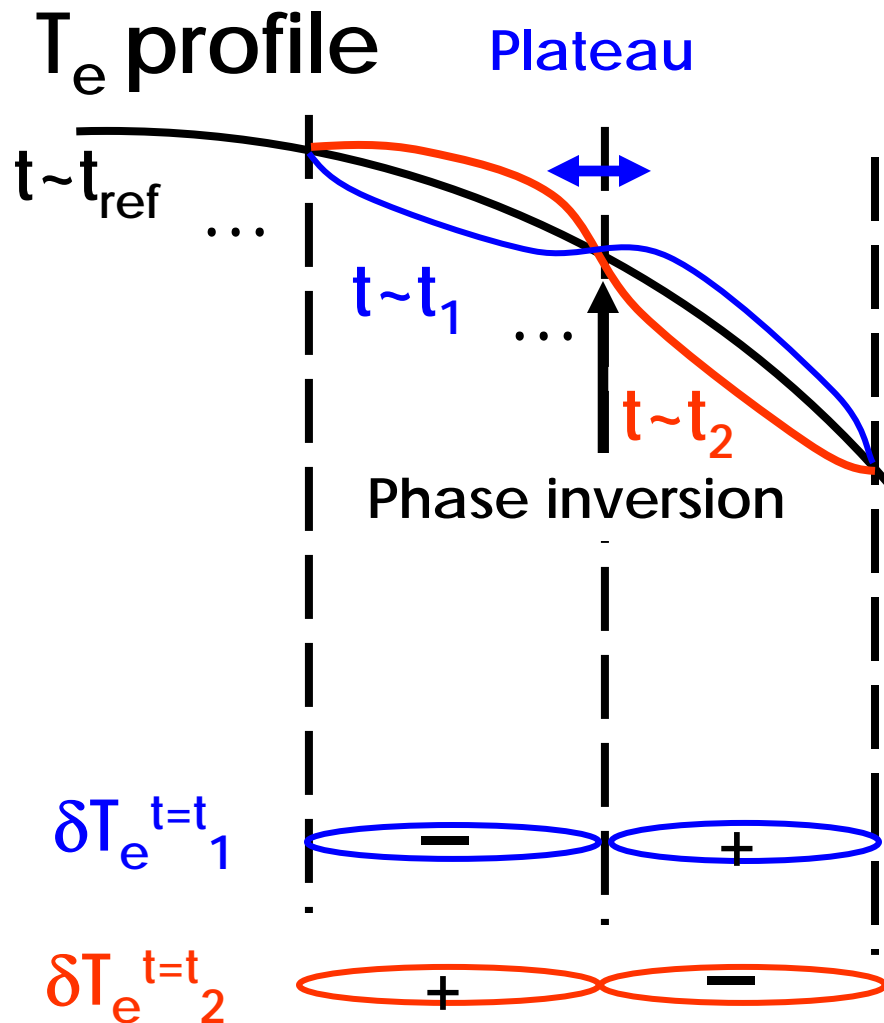
# Conclusions

- Current-driven RWM at  $q_{95} \sim 4$  was completely stabilized by the RWM feedback control.
  - An optimized proportional gain ( $G_p=80$ ) has been found without using derivative gain.
  - The use of derivative gains ( $G_d=10G_p$ ) expanded the stable range of proportional gains.
    - Reducing a phase lag in time avoids any mismatch between RWM and applied field.
    - Similarly finite amplitudes at various gains suggest the DEFC portion necessary for effective stabilization.
- A phase-shifted  $n=1$  field in the direction of co- $I_p$  rotation is more effective than in the opposite direction.

## Conclusions (cont'd)

- The efficacy of the feedback stabilization needs to be cautiously assessed based on magnetics alone
- The success of stabilization of the current-driven RWM at  $q_{95} \sim 4$  is primarily due to the direct RWM control, while a good error field correction is overlaid.
- Similar feedback performance is expected even for the pressure-driven RWM in high- $\beta$  plasmas, as long as the difference of the plasma responses between low and high- $\beta$  plasmas is properly addressed.

# Open question about magnetic islands



- Does a kink mode form a magnetic island?
- Is plateau essential for magnetic island?
- If so, what degree of flatness is necessary ?
- When the  $\delta T_e$  becomes a tiny 'wiggle' without plateau, is it still magnetic island?
- Should the inversion radius be located at a rational surface?