

# Feedback stabilization of tearing modes in RFPs with a resistive wall ABOVE the ideal wall limit

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\*J. M. Finn, “Control of magnetohydrodynamic modes with a resistive wall above the wall stabilization limit”, *Phys. Plasmas* **13**, 082504 (2006).

# Background

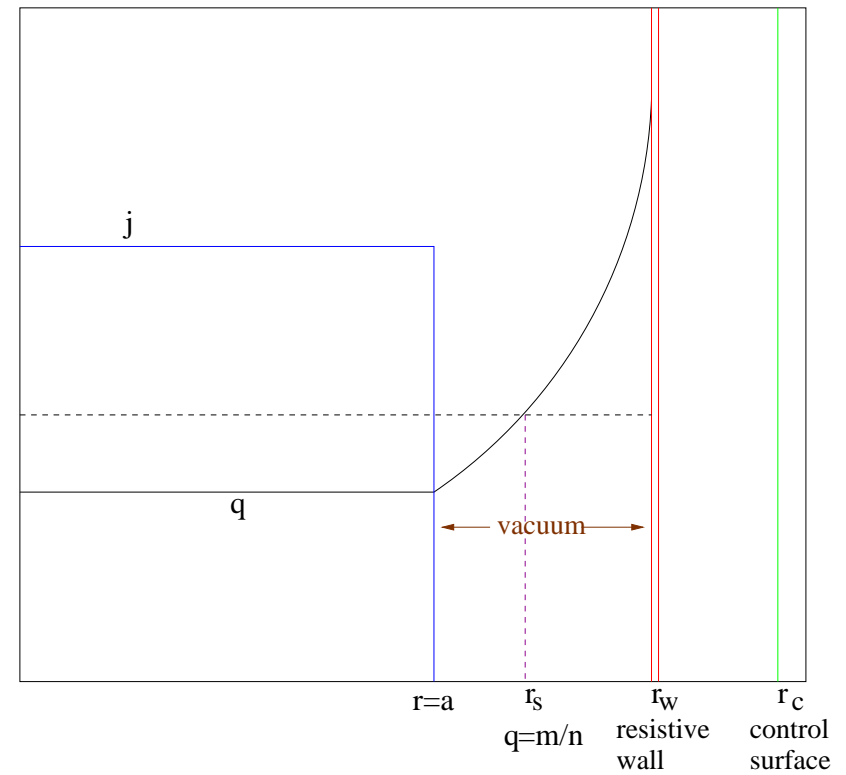
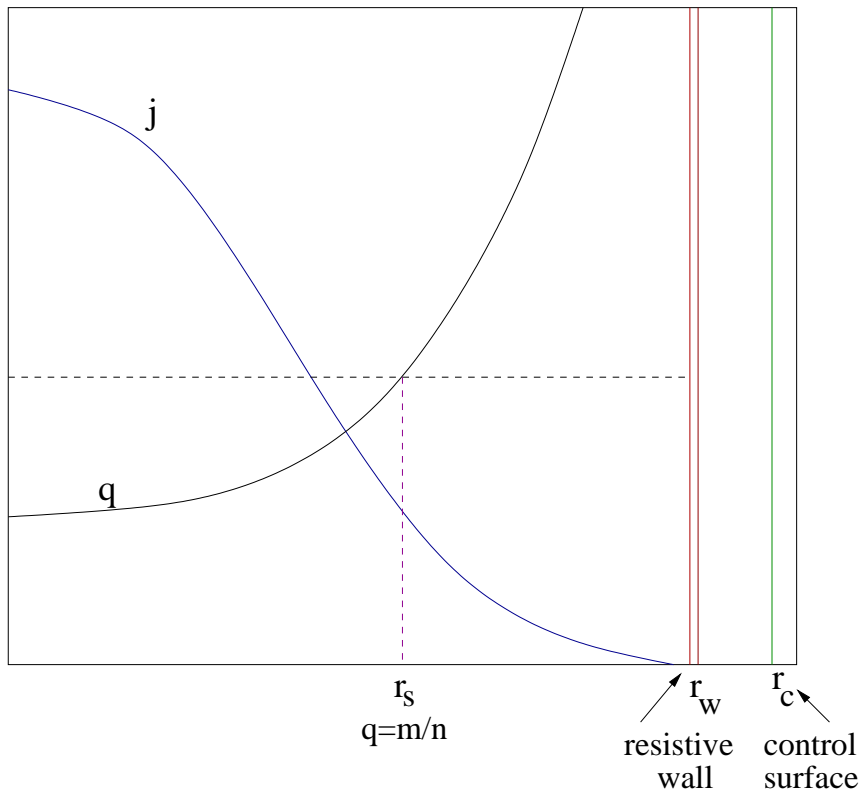
- Known: resistive wall modes can be unstable when PC wall stabilizes
- Earlier work: feedback: sensing  $\tilde{B}_r$  or  $\tilde{B}_\theta$  (normal or tangential)
- Tokamaks or RFPs – increasing or decreasing  $q(r)$  profile
- New: we sense a **linear combination** of  $\tilde{B}_r$  and  $\tilde{B}_\theta$
- New: stability of *tearing modes* is possible **ABOVE** the wall stabilization regime. **For ideal modes? No.**
- Related to *virtual wall* of Bishop (1989)? For  $Re(\omega) = 0$ , sort of. Otherwise, no.
- Applications: stabilizing the  $m = 0$  or the  $m = 1$  modes in RFPs for single RFPs; possibly control the amplitude of neoclasical tearing modes in tokamaks.

## RADIAL AND TANGENTIAL SENSING (REVIEW)

- ✓ Tangential ( $\tilde{B}_\theta$ ) sensing was found to work better than radial ( $\tilde{B}_r$ ) sensing [Y. Q. Liu, A. Bondeson et al., *Phys. Plasmas* **2000**; C. M. Fransson et al., *Phys. Plasmas* **2000**; A. Bondeson et al., *Nucl. Fusion* **2002**; M. S. Chu et al., *Nucl. Fusion* **2003**; M. S. Chu et al., *Phys. Plasmas* **2004**, J. M. Finn, *Phys. Plasmas* **2004**].
- ✓ Tangential appears to work better because it is less sensitive to  $m \rightarrow m \pm 1$  coupling due to coils
- ✓ Works better in DIII-D too.

# MODEL

- ✘ Cylindrical tokamak model, reduced ( $R/a \gg 1$ ) resistive MHD equations, resistive wall (RW) at plasma edge, control flux (single  $m, n$ ) applied at  $r_c$



## Resistive wall tearing mode – reduced MHD

$$\mathbf{B} = \nabla\psi \times \hat{z} + B_0\hat{z} \quad \mathbf{j} = j_z\hat{z} = -\nabla_{\perp}^2\psi$$
$$\mathbf{B} \cdot \nabla\tilde{j}_z + \tilde{\mathbf{B}} \cdot \nabla j_z = \rho d\omega/dt \quad \nabla_{\perp}^2\tilde{\psi} - \frac{m}{r} \frac{j'_z}{\mathbf{k} \cdot \mathbf{B}} \tilde{\psi} = 0 \quad vac.$$

Matching at  $r = r_s$  ( $q = m/n$ ) – visco-resistive ct. *psi* tearing matching condition:

$$[\psi']_{r_t} = \gamma\tau_t\psi(r_t) \quad \tau_t \sim \mu^{1/6}/\eta_p^{5/6}(k \cdot B)^{1/3}$$

Matching at  $r = r_w$  – resistive wall – thin wall (ct. *psi*) matching condition:

$$[\psi']_{r_w} = \gamma\tau_w\psi(r_w) \quad \tau_w \sim r_w\delta/\eta_w$$

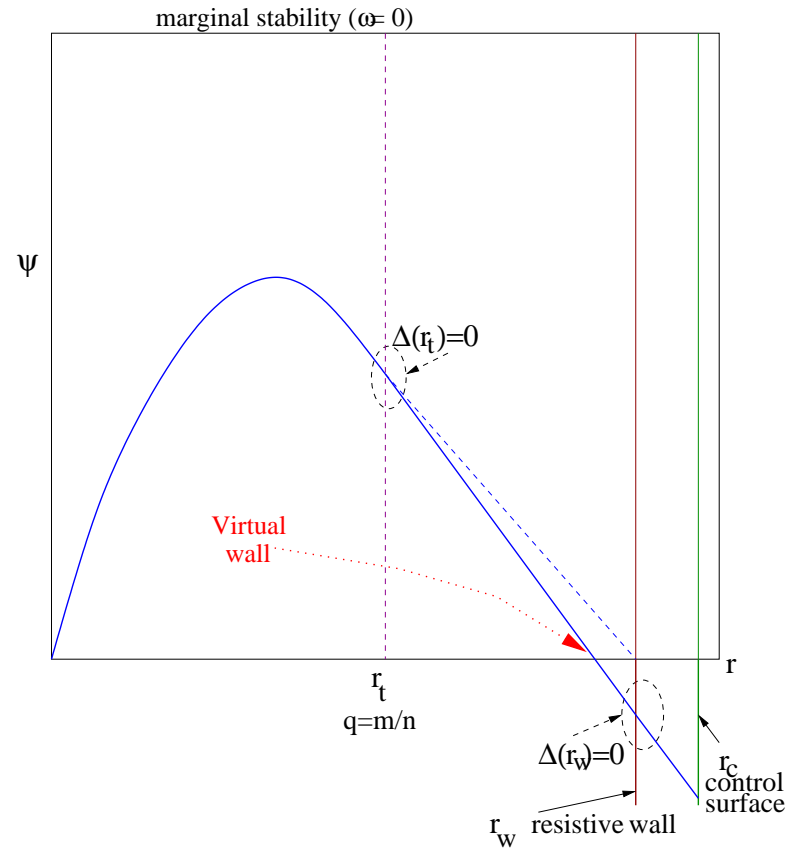
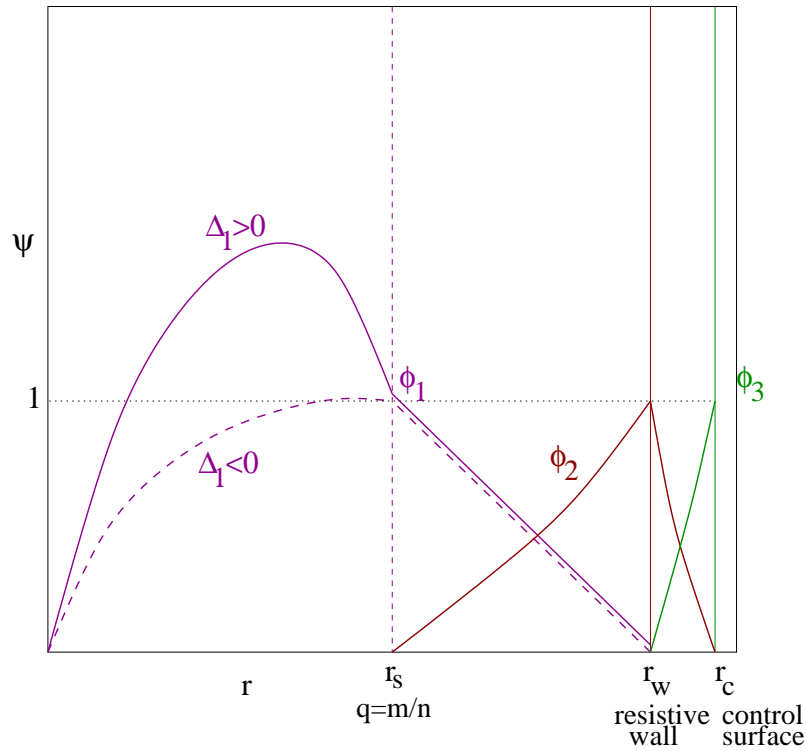
# FEEDBACK MODEL

Feedback – linear combination of radial field  $\psi(r_c) = -G\psi(r_w)$  and poloidal field  $\psi(r_c) = K\psi'(r_w-)$  [ $\tilde{B}_r = im\psi/r$ ;  $\tilde{B}_\theta = -\partial\psi/\partial r$ ]

$$\psi(r_c) = -G\psi(r_w) + K\psi'(r_w-)$$

$$\tilde{B}_r(r_w) \propto \psi(r_w) \quad \dots \quad \tilde{B}_\theta(r_w-) \propto \psi'(r_w-)$$

# RW TM (cont)



$\Delta_1 < 0 \implies$  TM is stable with PC (perfectly conducting) wall at  $r_w$

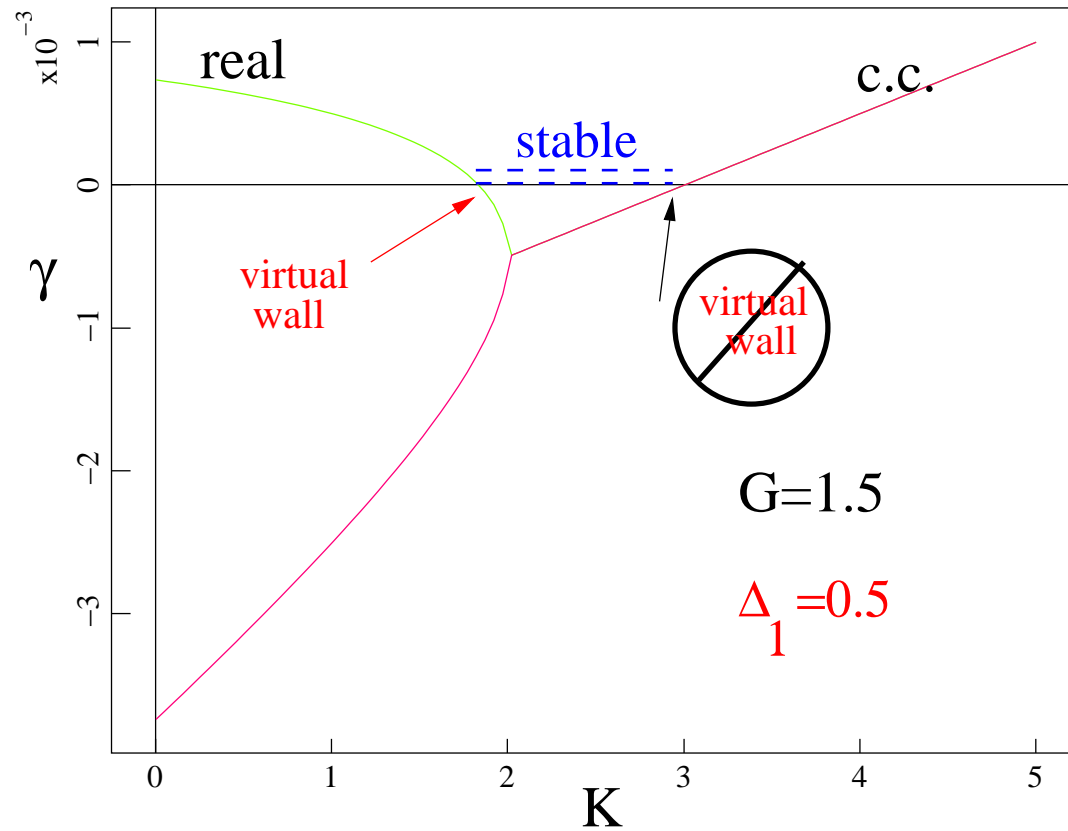
$\Delta_1 > 0 \implies$  TM is unstable with PC wall at  $r_w$

$$\begin{bmatrix} \Delta_1 - \gamma\tau_t & l_{12} & 0 \\ l_{21} & \Delta_2 - \gamma\tau_w & l_{23} \\ -Kl_{21} & -G + Kl_{22}^{(-)} & 1 \end{bmatrix} \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} = 0$$

$$\begin{bmatrix} \frac{\Delta_1}{\tau_t} - \gamma & \frac{l_{12}}{\tau_t} \\ \frac{l_{21}(1 - Kl_{23})}{\tau_w} & \frac{\Delta_2 - l_{23}(G - Kl_{22}^{(-)})}{\tau_w} - \gamma \end{bmatrix} \begin{bmatrix} \alpha_1 \\ \alpha_2 \end{bmatrix} = 0$$

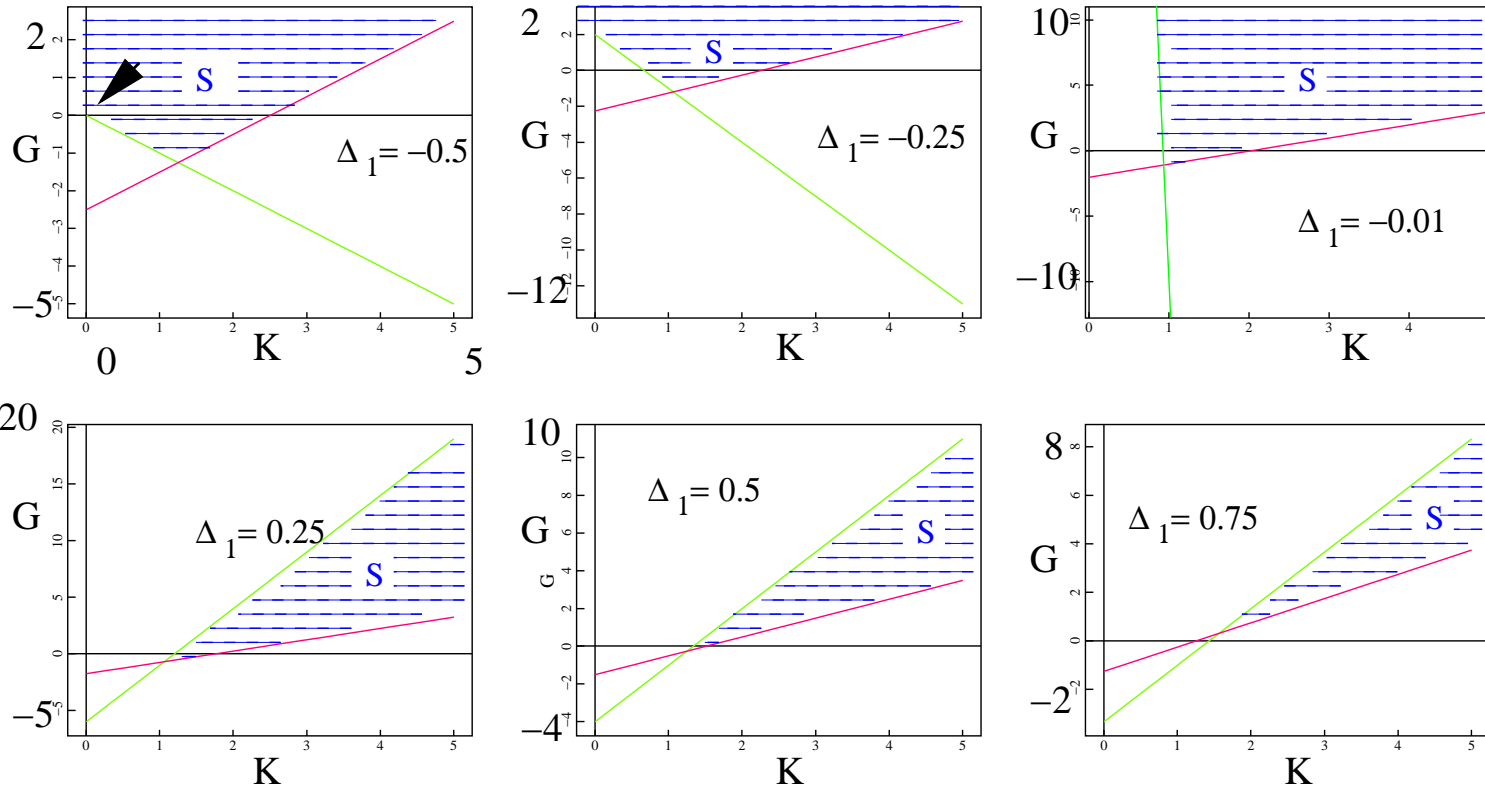


# Stability conditions



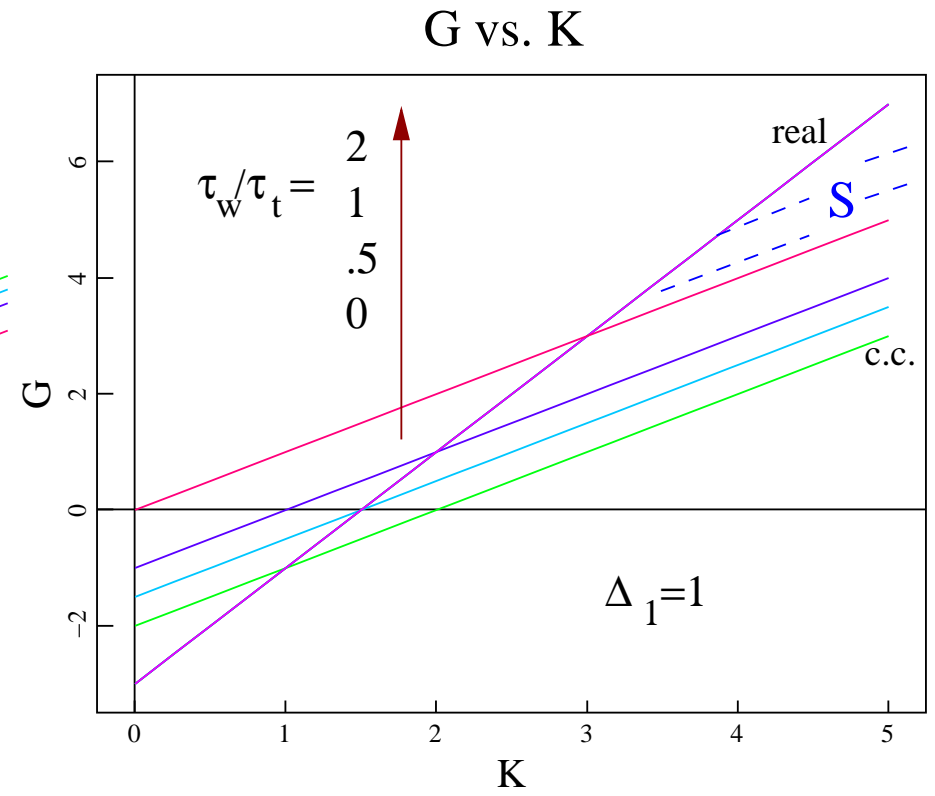
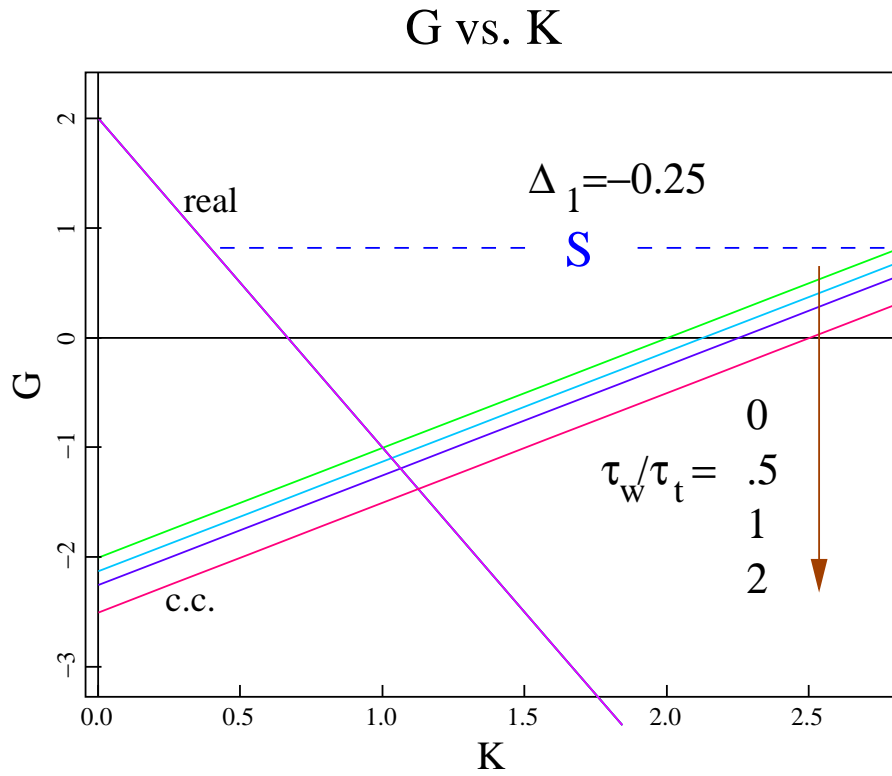
# Stability regimes in $G, K$

$\tau_w/\tau_t = 1$  : Real marginal ... C.c. marginal ... Stable region



**Always a stability window!** Thinner, with large  $G, K$ , for large  $\Delta_1$ . For  $\Delta_1$  large enough,  $G$  and  $K$  are both required.

# The effect of $\tau_w/\tau_t$



## The effect of $\tau_w/\tau_t$ :

Making resistive wall thicker or less resistive ( $\tau_w$  larger)

- $\tau_w/\tau_t$  helps in the wall stabilization regime ( $\Delta_1 < 0$ ). Slow penetration of flux from mode in the plasma slows mode.
- Harms above wall stabilization regime ( $\Delta_1 > 0$ ). Prevents penetration of the feedback flux.

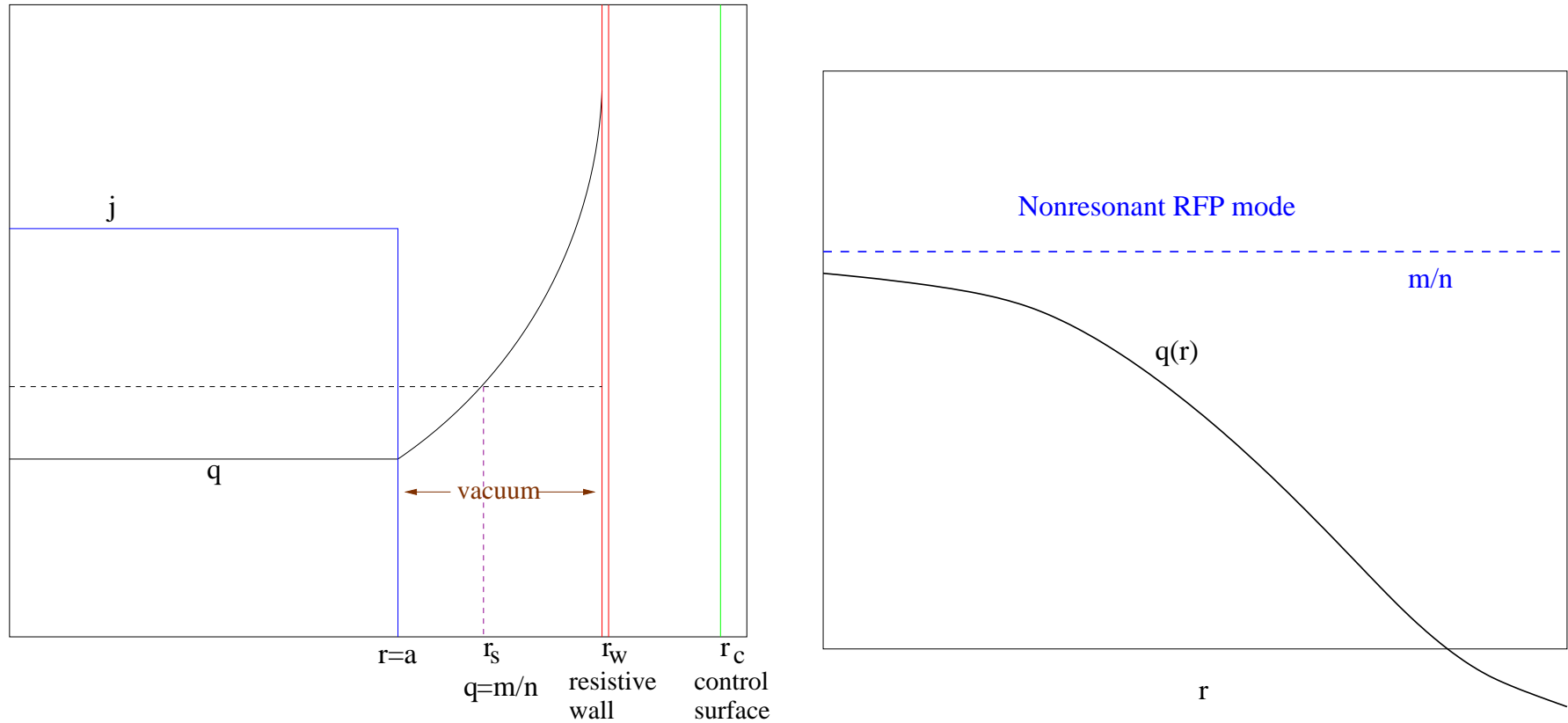
## Feedback based on tangential field outside the resistive wall

$$\psi(r_c) = -G\psi(r_w) + K\psi'(r_w+)$$

↑↑

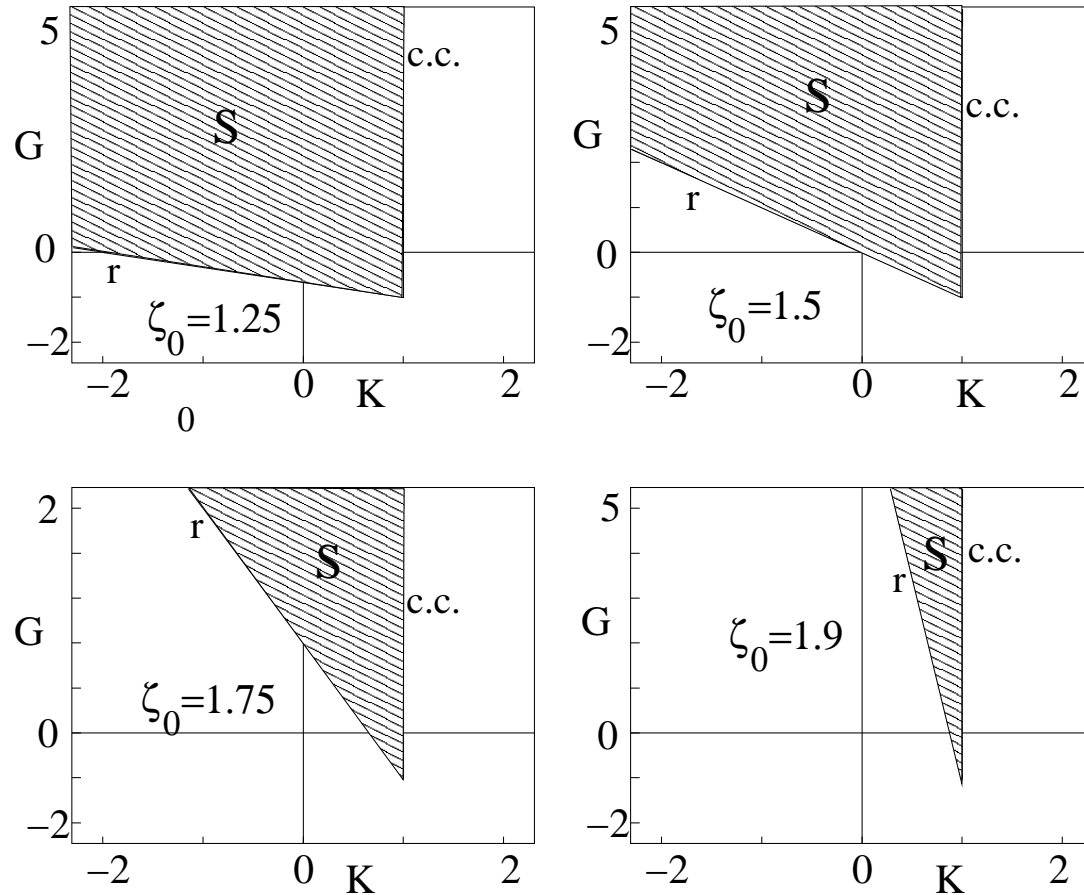
No stabilization above  $\Delta_1 = 0$ , where tearing mode is wall stabilized.

# Ideal plasma nonresonant external modes – mode rational surface in vacuum. Non-resonant RFP modes



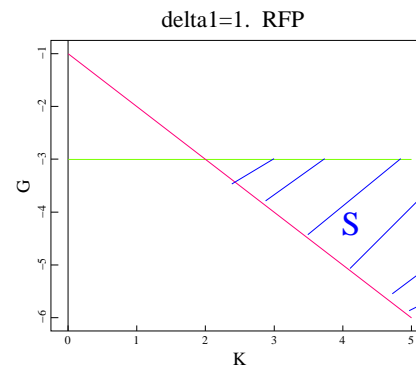
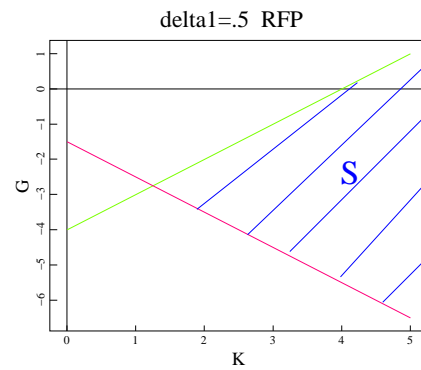
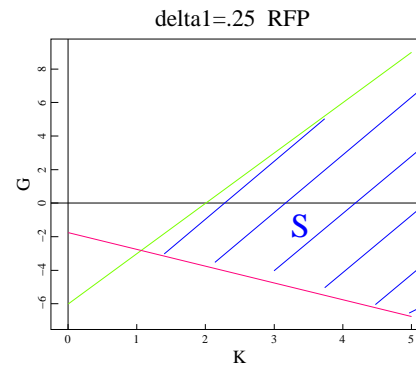
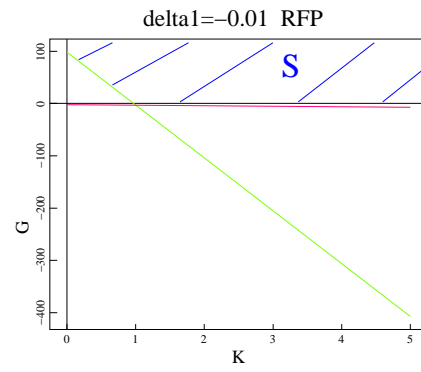
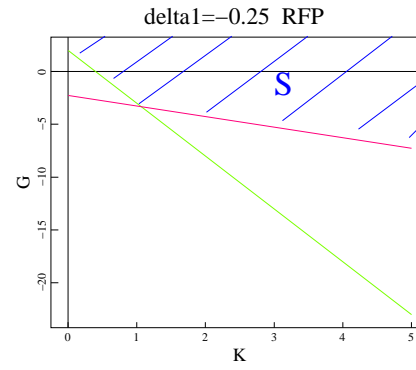
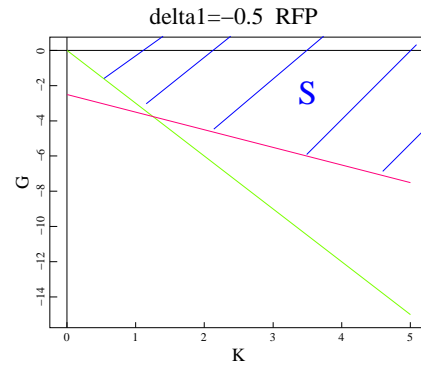
Wall stabilization:  $1.5 < \zeta_0 < 2.0$

# Ideal external kink (tokamak)



Tokamak-like geometry with mode rational surface in the vacuum. Unstable  
 $\zeta_0 > 2$ .

# RFP-like $q$ profiles – tearing





## Finally, ideal plasma resonant modes (RFP)

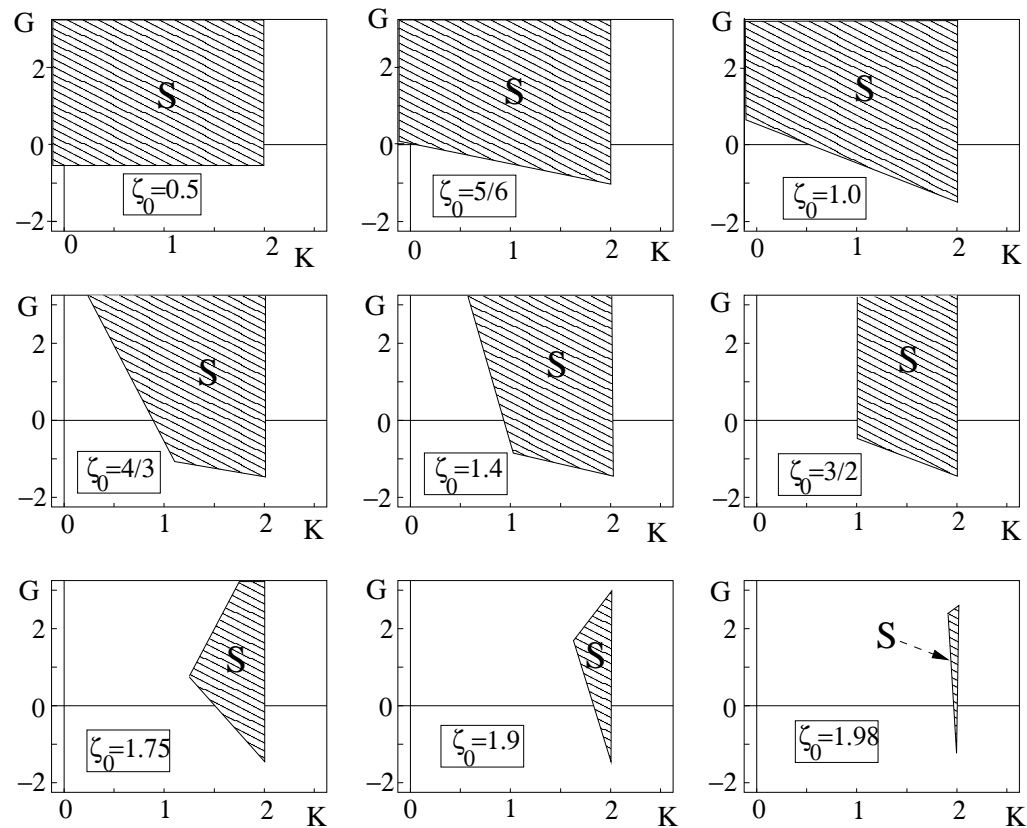
Plasma resistive layer at  $r = r_t$

Jump in  $j$  or in  $p$  at  $r = a$

Resistive wall at  $r = r_w$

Control at  $r = r_c$

$$\begin{bmatrix} \Delta_1 - \gamma\tau_t & l_{12} & 0 \\ l_{21} & \Delta_2 + \frac{\zeta_0}{1 + \rho\gamma^2/F_a^2} & l_{23} \\ 0 & l_{32}(1 - l_{34}K) & \Delta_3 - \gamma\tau_w - l_{34}(G - l_{33}^{(-)}K) \end{bmatrix} \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} = 0$$



Stable region of  $(K, G)$  space vanishes for  $\zeta_0 > 2$  (ideal mode with PC wall). A stable region exists **BELOW** this.

## Summary

- Tearing modes (tokamak or RFP): linear feedback sensing radial magnetic field and tangential field can stabilize the tearing mode below **and above** the threshold for stability with a PC wall. Some relation with virtual wall of Bishop ('89) when  $Re(\omega) = 0$ .
- Increasing  $\tau_w/\tau_t$  (making wall more conducting) increases the range  $(K, G)$  of stability for  $\Delta_1 < 0$  ... **decreases(!)** the range for  $\Delta_1 > 0$ . Easy to understand.
- Using radial field and **external** tangential field can stabilize for  $\Delta_1 < 0$  but not for  $\Delta_1 > 0$ .
- **Resonant or non-resonant ideal modes: can stabilize below threshold for stability with PC wall, but **not** above.**
- Applications: stabilizing  $m = 1$  or  $m = 0$  modes in RFPs; perhaps controlling the amplitude of neoclassical tearing modes in tokamaks.