

# The basic question of wall times

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**Thanks to B. Davis (pppl IDL master) !!!!!!**

Outline:

- 1) Equations for wall currents & eigenvalue analysis
- 2) Examine simplest problem a rectangular plate
- 3) Examine standard DIII-D vacuum vessel
- 4) Field penetrating a wall, compare models with many vs. 1 time constant.
- 5) Conclusions & recommendations

## Equations for wall times

Many people stop at  $\frac{\eta}{\mu_0} \nabla^2 \vec{B} = -\frac{\partial \vec{B}}{\partial t}$

$$\nabla \cdot \vec{B} = 0, \quad \vec{B} = \nabla \times \vec{A}$$

$$\nabla \times \vec{E} = -\dot{\vec{B}}$$

$$\nabla \times \vec{B} = \mu_0 \vec{J}$$

$$\vec{E} = \eta \vec{J}, \quad \nabla \cdot \vec{J} = 0$$

Write equations in terms of currents,  
Use the standard definitions & assumption

$$\int_{\text{volume}} \vec{w} \cdot \left( \eta \vec{J} + \dot{\vec{A}} + \nabla \phi \right) dv = - \int_{\text{volume}} \vec{w} \cdot \dot{\vec{A}}_{\text{external}} dv$$

$$\vec{J}(\vec{r}, t) = \sum_{\substack{\text{all} \\ \text{elements}}} I_k(t) \vec{w}_k(\vec{r})$$

Where the  $w_k$  are shape functions (closed loops of current)

This gives the standard set of familiar circuit equations

Circuit equations are a set of simultaneous o.d.e.

$$[L]_{NxN} \{ \dot{I} \}_{Nx1} + [R]_{NxN} \{ I \}_{Nx1} = \{ V \}_{Nx1}$$

With eigenvalues ( time constants  $\tau_k$ ) & eigenvectors  $\{ \xi_k \}$

We may express any answer in terms of the eigenvectors

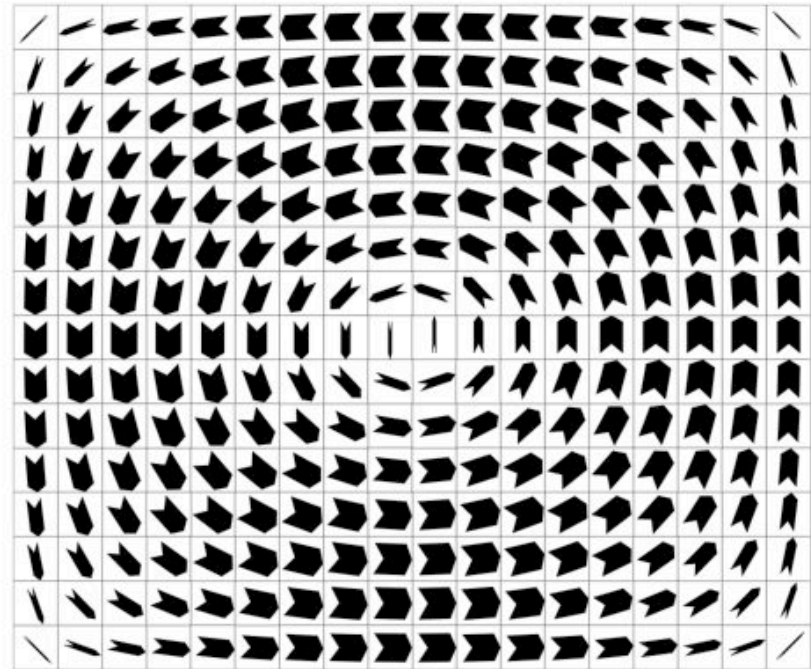
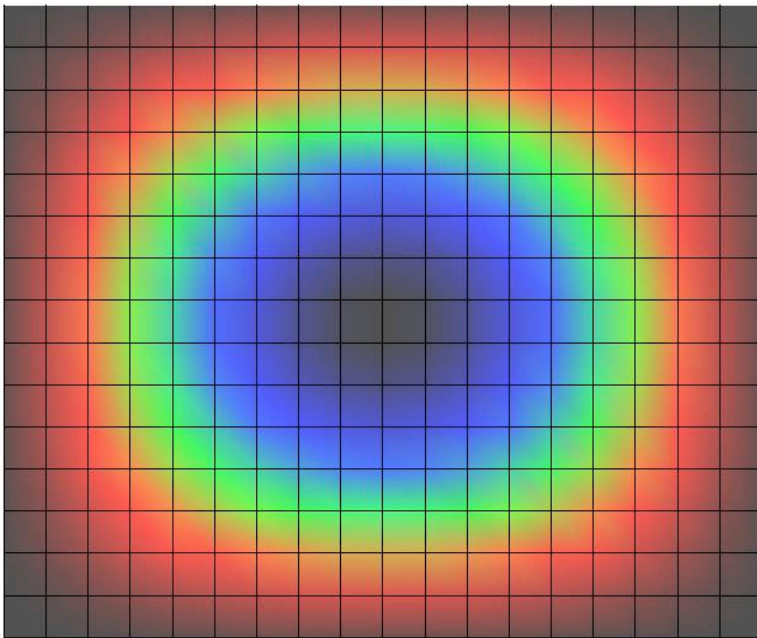
$$\{ I(t) \}_{Nx1} = \sum_{k=1}^N \{ \xi_k \}_{Nx1} c_k(t) = \left[ \begin{array}{ccc} \{ \xi_1 \}_{Nx1} & \dots & \{ \xi_N \}_{Nx1} \end{array} \right]_{NxN} \{ c(t) \}_{Nx1}$$

$$\{ I(t) \} = [\Psi] \{ c(t) \}, \quad \{ c(t) \} = [\Psi]^{-1} \{ I(t) \}$$

We can find the most important modes by looking at the largest values of the vector  $\{ c(t) \}$ . We may reconstruct the result with a subset of modes

We examine the modes & time constants of a thin plate  
1.8 x 1.5 x 0.01 [m] with resistivity = 130.e-08 [ohm m]  
In this model we have 270 equations / modes

Stream function graphics & Eddy current plots

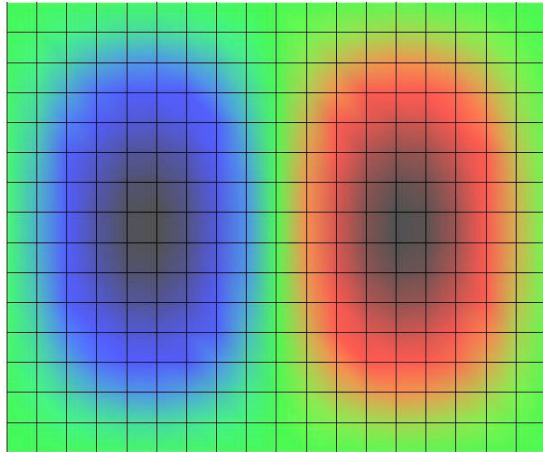


The slowest mode (shown above) is #270

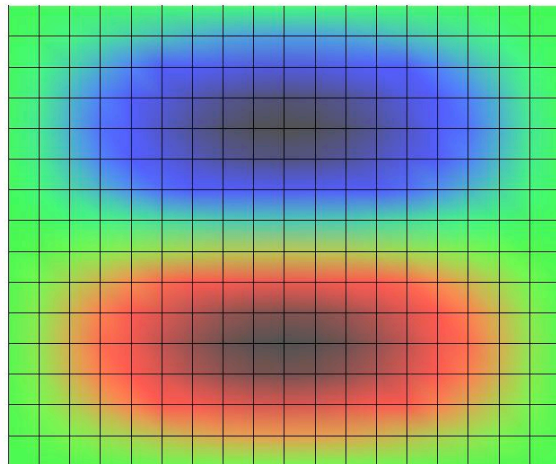
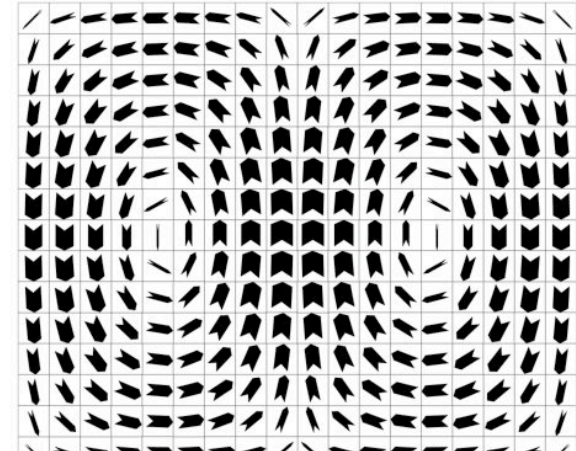
Time constant =  $\tau_{270} = 1.521e-3$  s



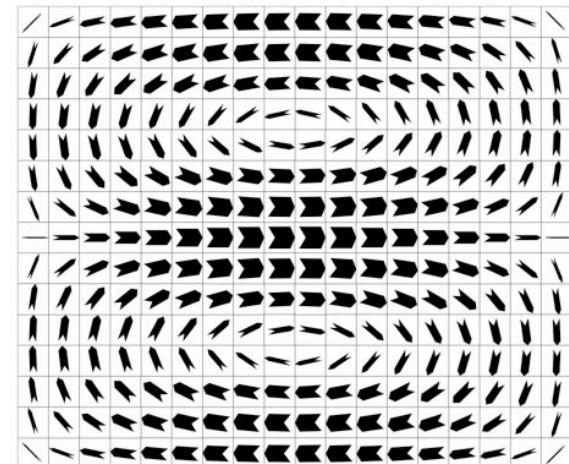
The following illustrates the slowest modes (in order)



$\tau_{260}=1.082e-3$  s  
mode #269

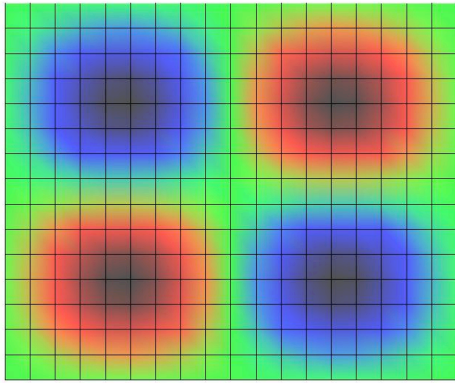


$\tau_{268}=9.675e-4$  s  
mode #268

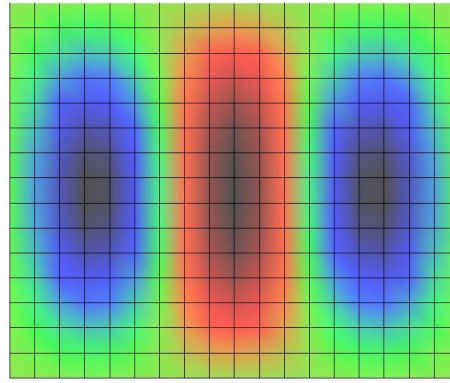


Y  
Z X

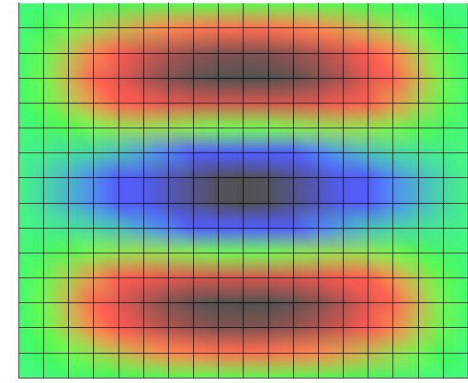
The following illustrates the slowest modes (in order)



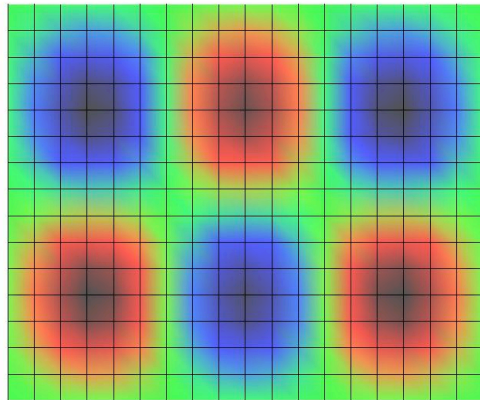
$8.185e-4$  s  
mode #267



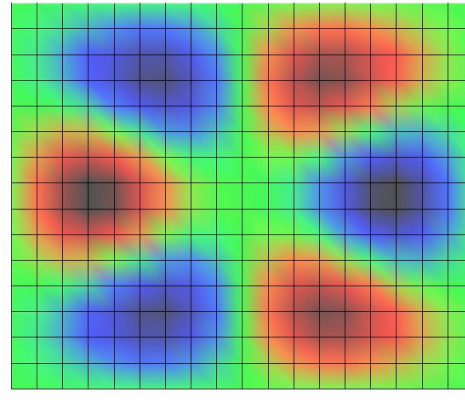
$7.904e-4$  s  
mode #266



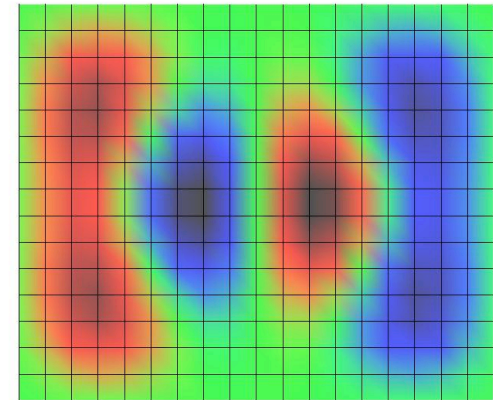
$6.765e-4$  s  
mode #265



$6.689e-4$   
mode #264

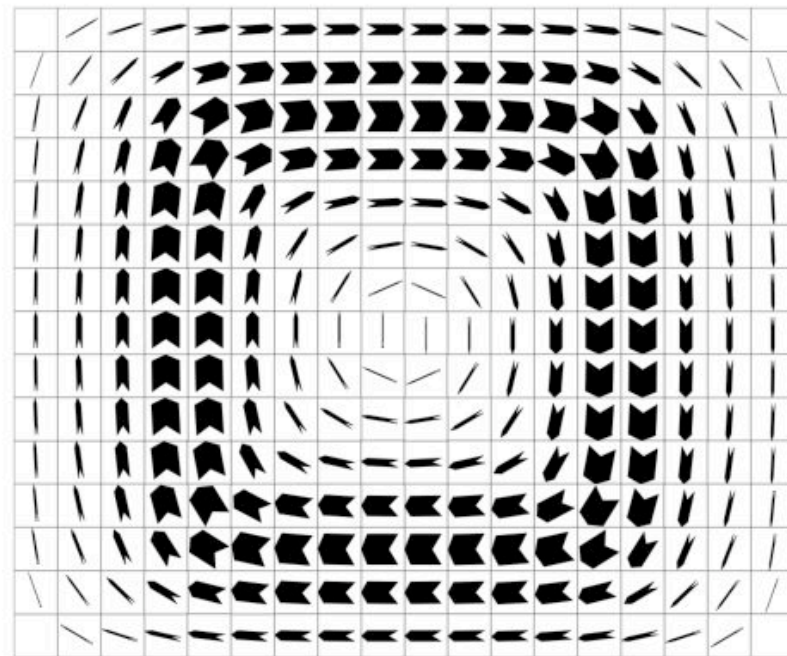
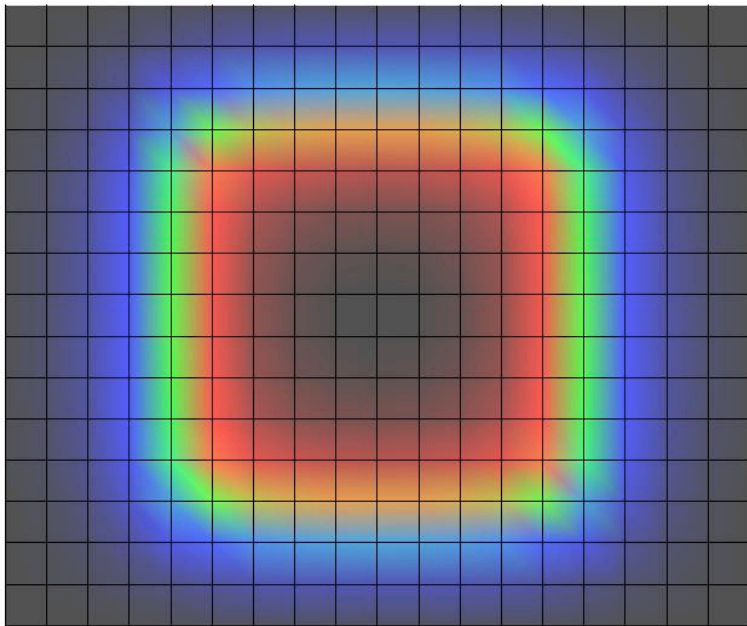


$6.227e-4$  s  
mode #263



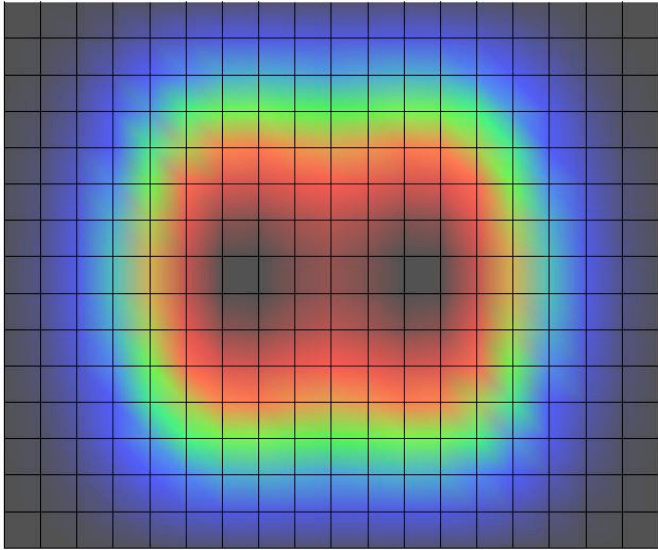
$6.136e-4$  s  
mode #262

Examine fast time scale current response in plate  
produced by current step in square (1x1 [m]) coil.  
Coil is 0.1 [m] from plate

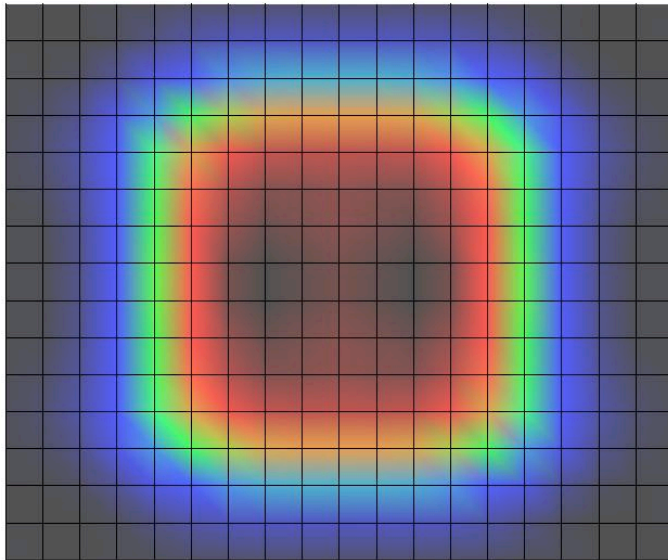
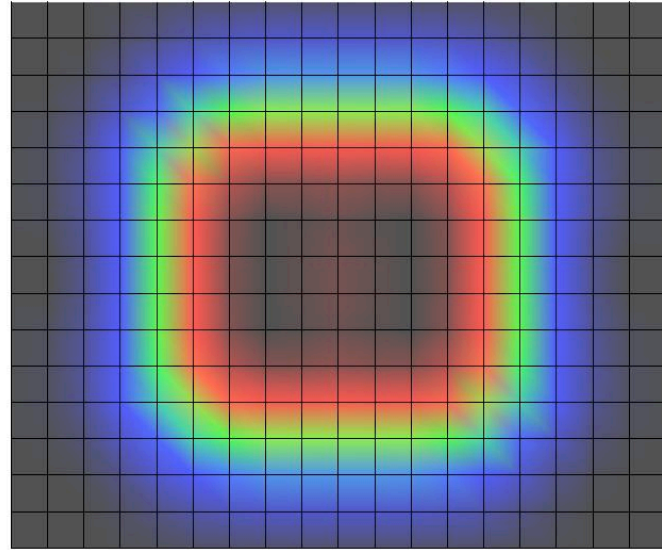




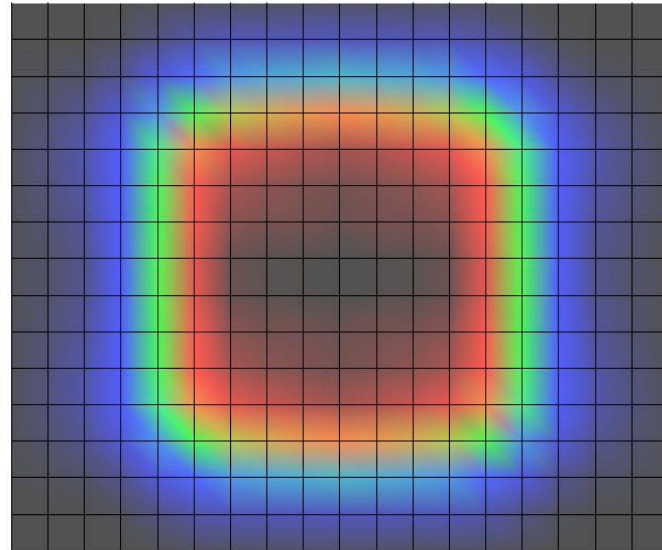
best 2 mode approximation



best 4 modes

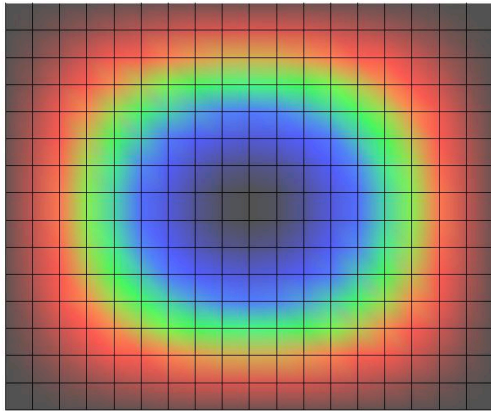


best 6 modes

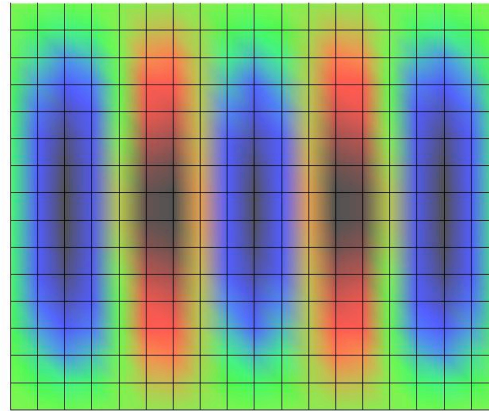


best 8 mode approximation

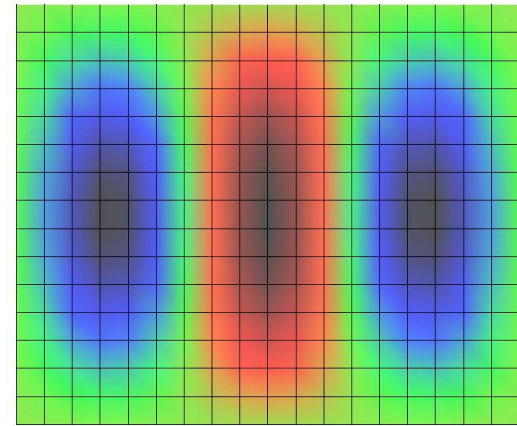
Most important ( highest  $c_k$  or 'weight') shown below



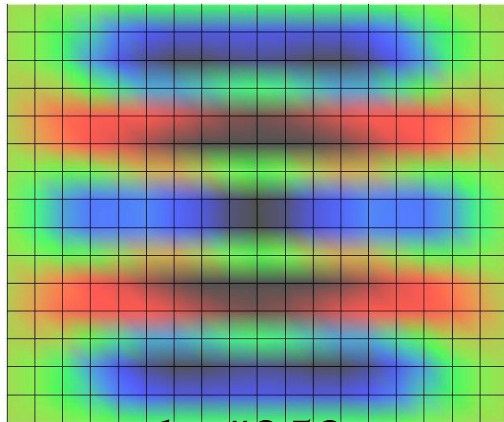
mode #270  
wt=-0.852e-2  
0.152e-2 s



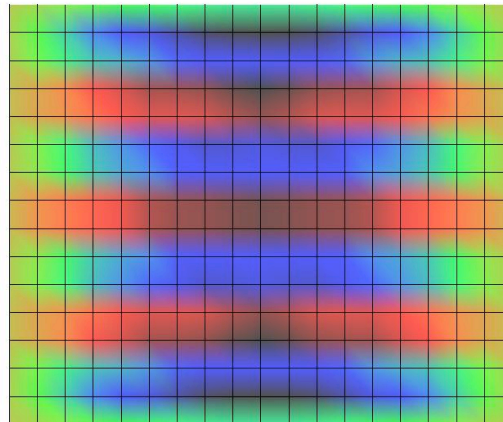
mode #258  
wt = 0.2058e-2  
0.498e-3 s



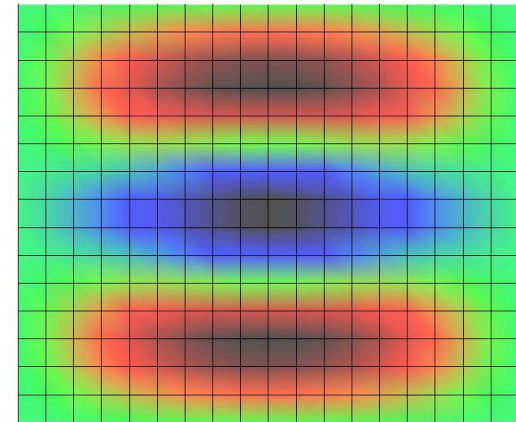
mode #266  
wt = 0.130e-2  
0.790e-3 s



mode #252  
wt = 0.122e-2  
0.417e-3 s

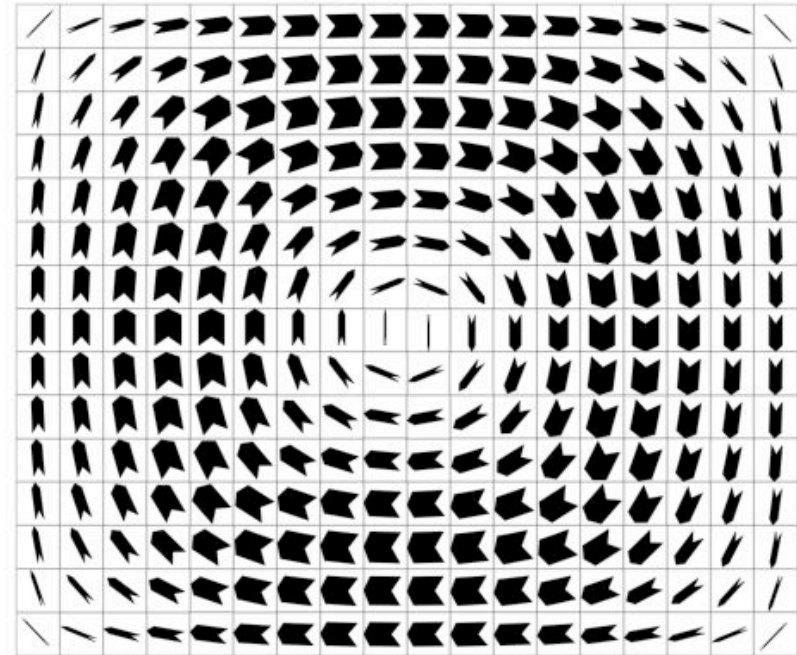
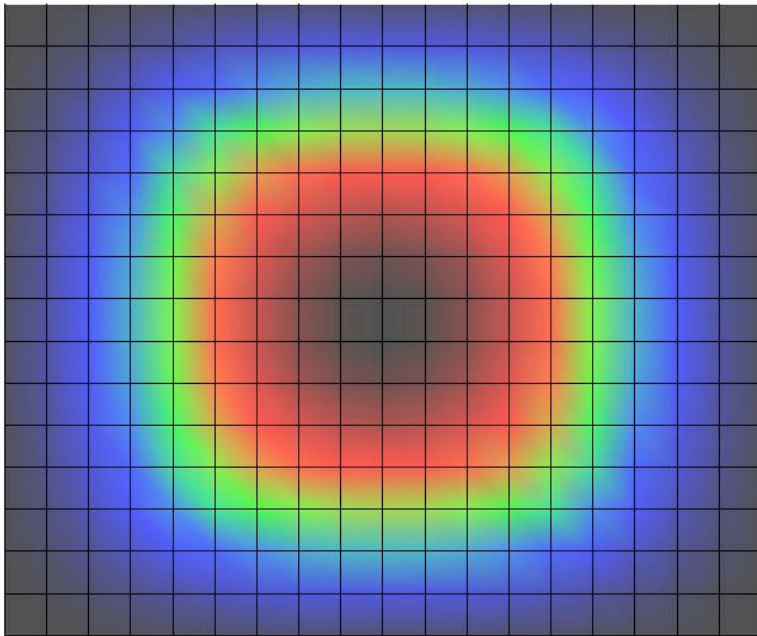


mode #232  
wt = 0.978e-3  
0.298e-3 s



mode #265  
wt = 0.765e-3  
0.676e-3 s

Examine steady state (resistive response) in same plate



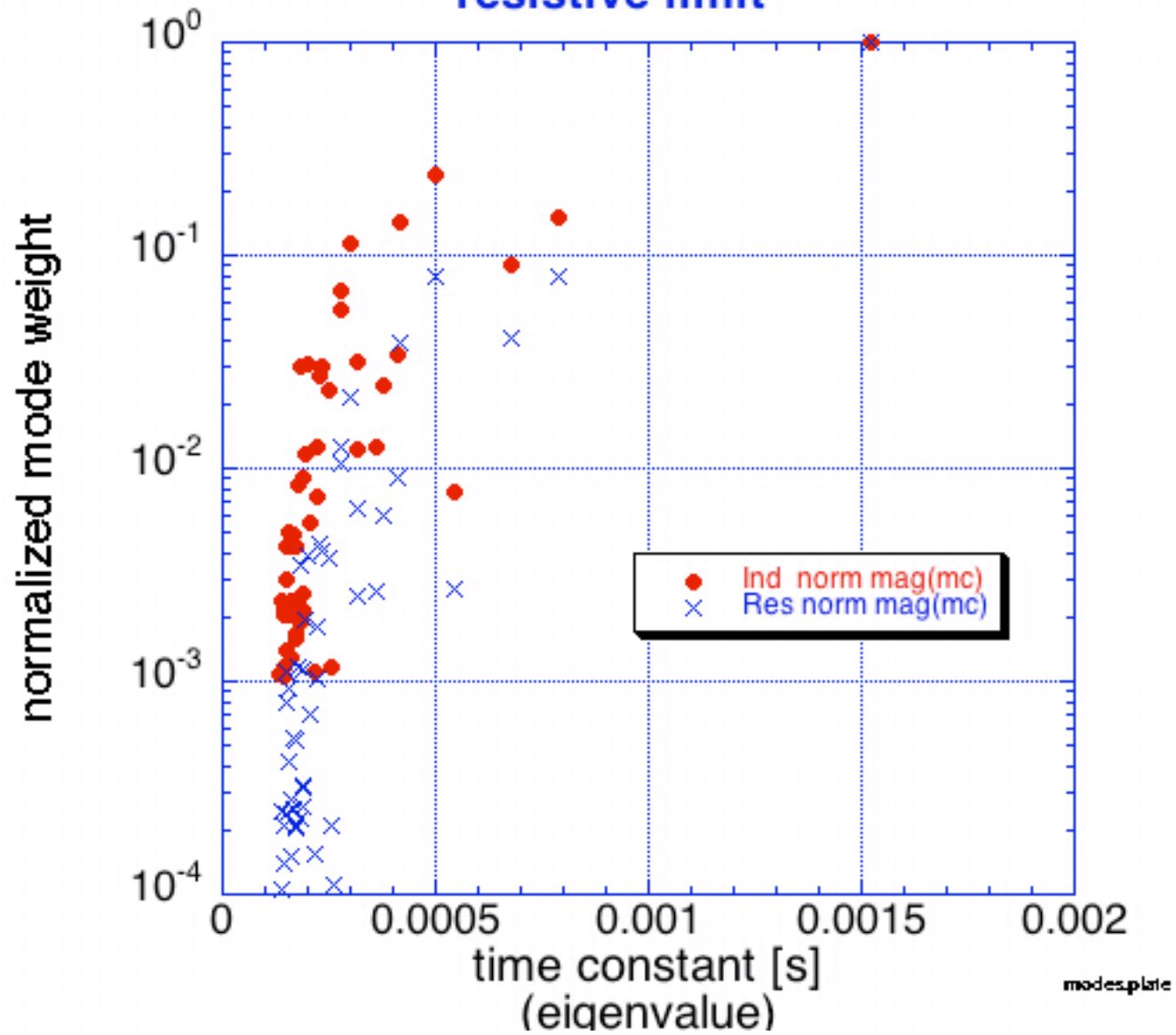
Y  
Z X



# 50 largest mode weights for flat rectangular plate

inductive limit

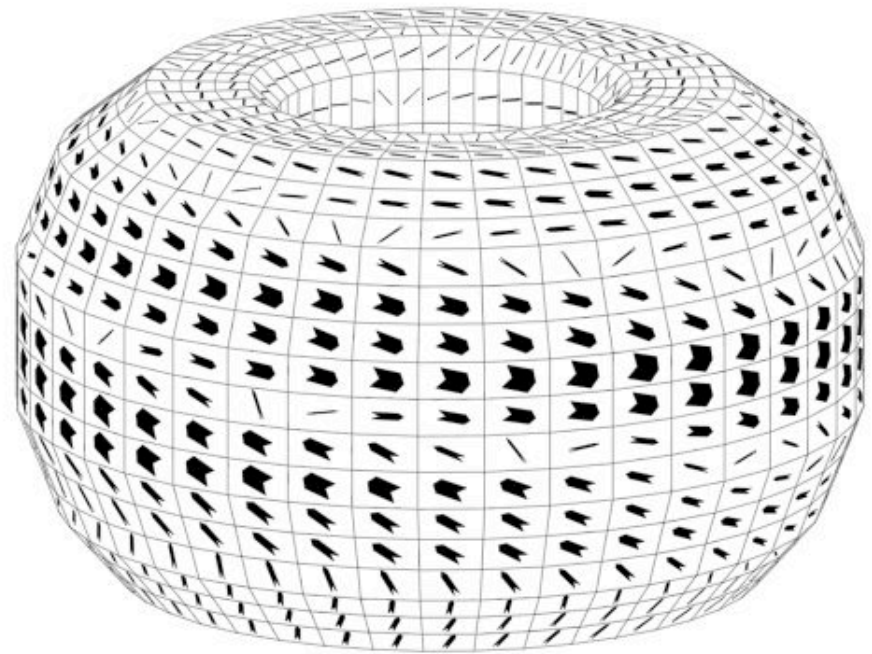
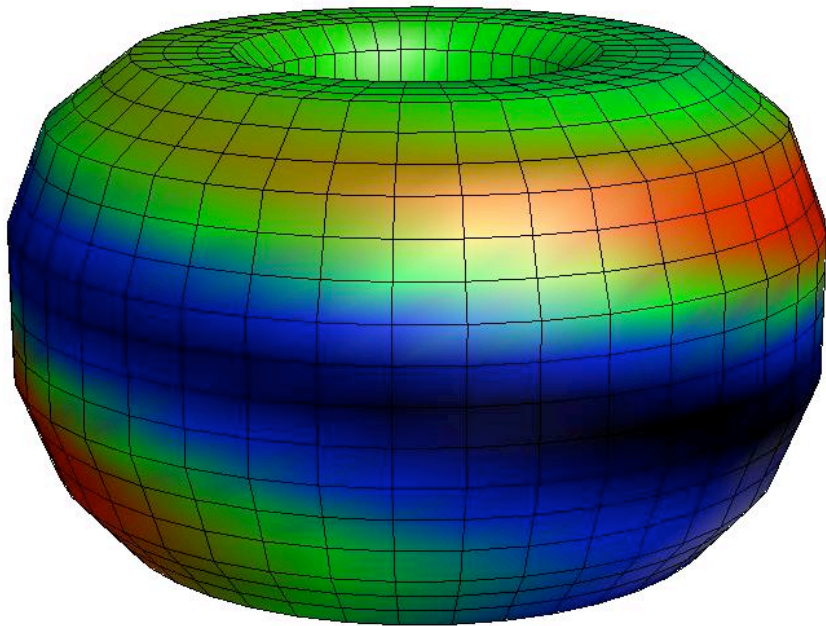
resistive limit



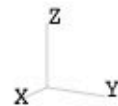
Examine fast time scale response in standard DIII-D model

(thick 'belly band', remainder thin, constant resistivity)

Using  $B_n$  from A.Turnbull (GATO) analysis of shot #92544

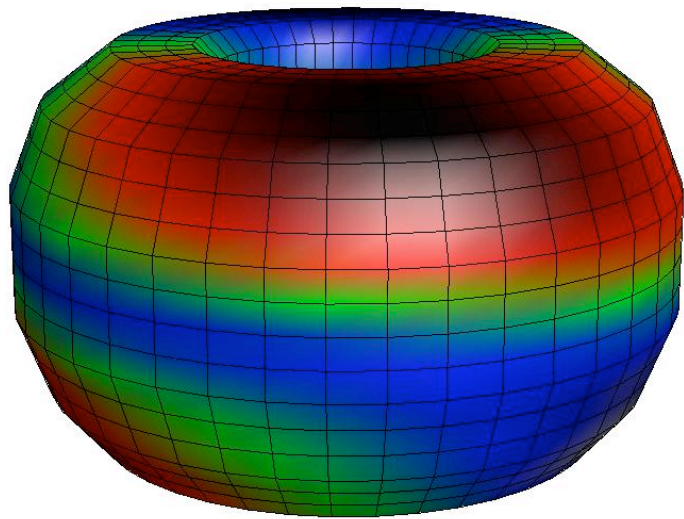


1281 equations/modes

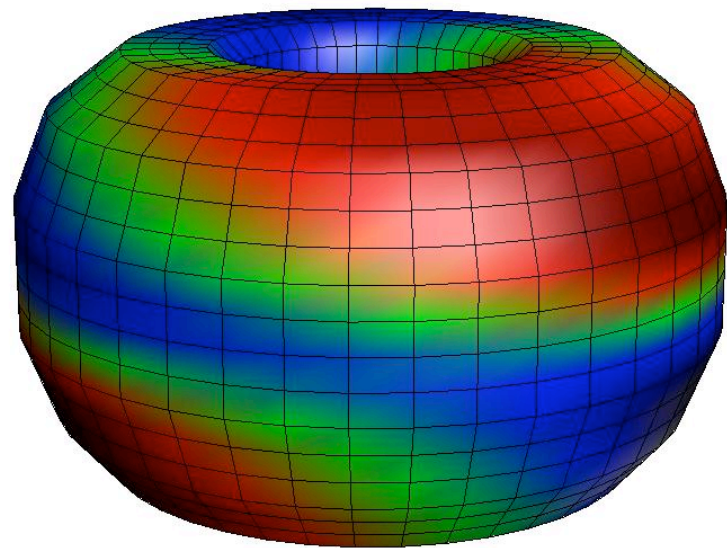




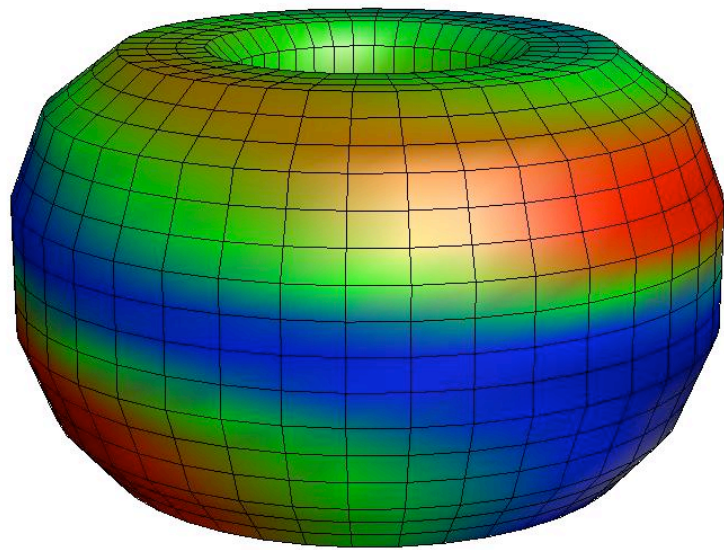
2 best modes



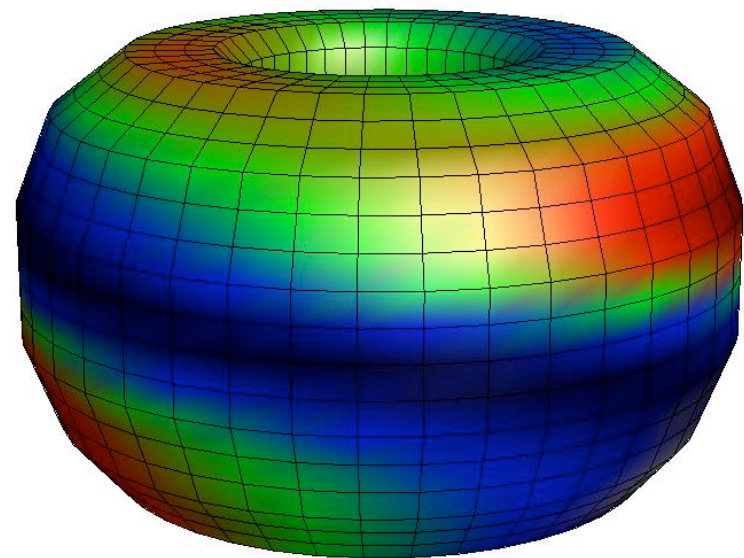
4 best modes



6 best modes

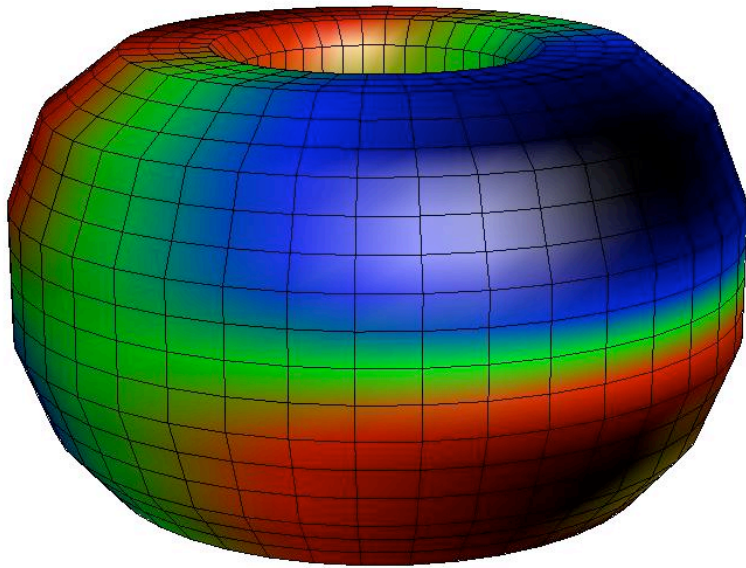


8 best modes

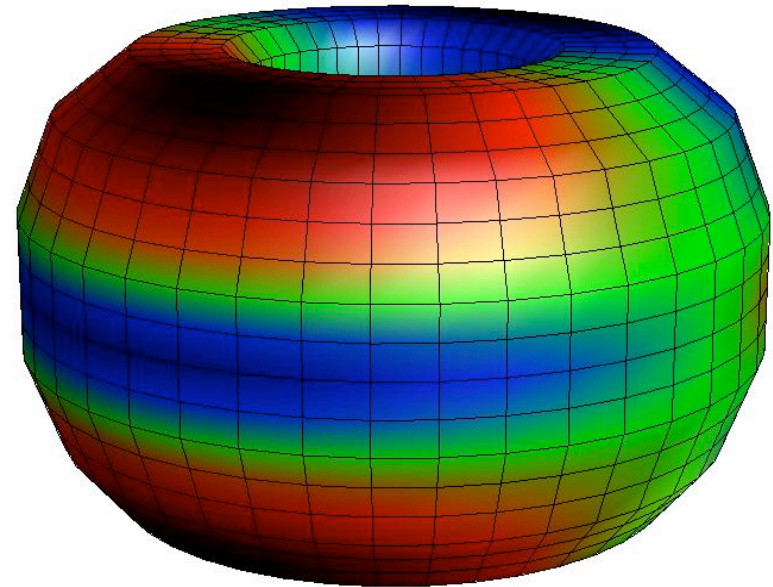


Most important modes ( greatest weights ) follow:

**We never see a helical mode !!!!!**

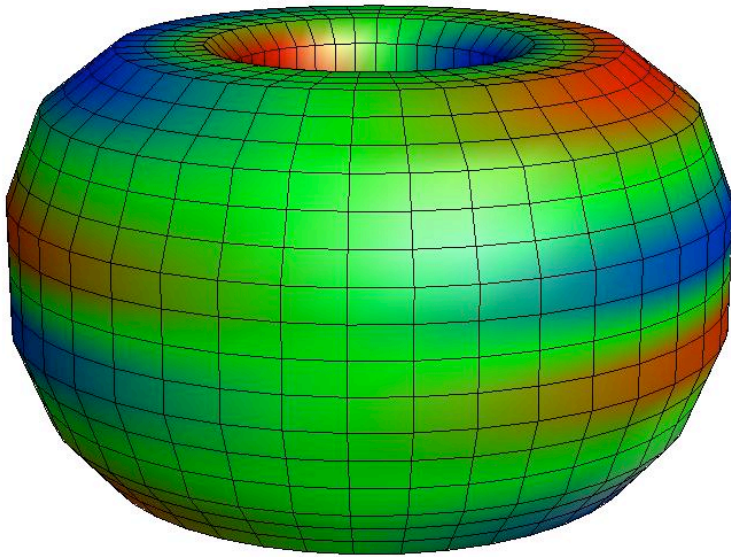


mode # 1278  
wt = -0.108e-1  
0.555e-2 s  
greatest contribution

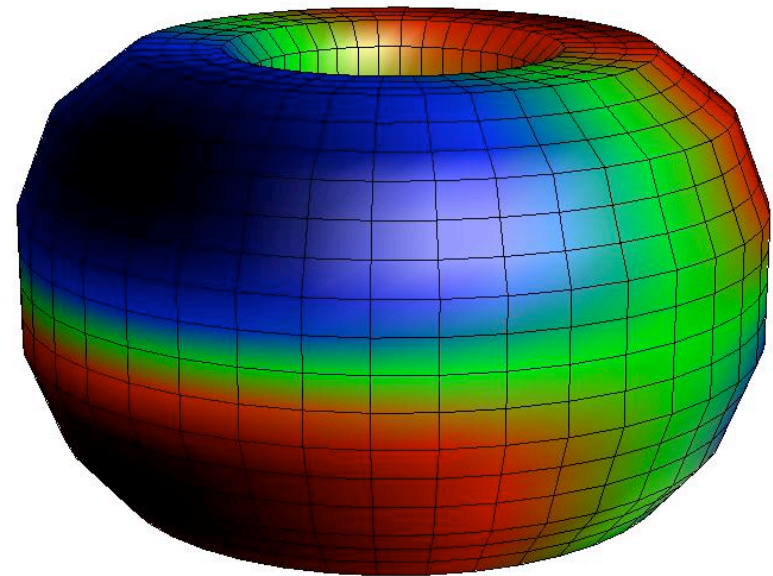


mode #1260  
wt = 0.899e-2  
0.3068e-2 s

Most important modes ( greatest weight ) follow:



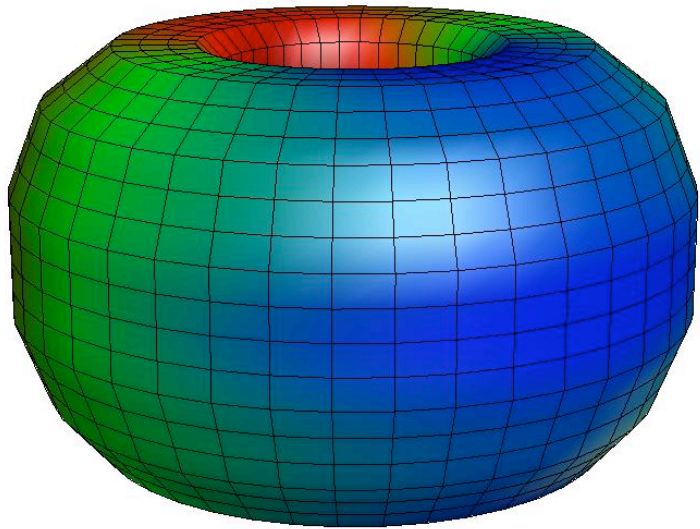
mode #1231  
wt =  $-0.669e-2$   
 $0.2043e-2$  s



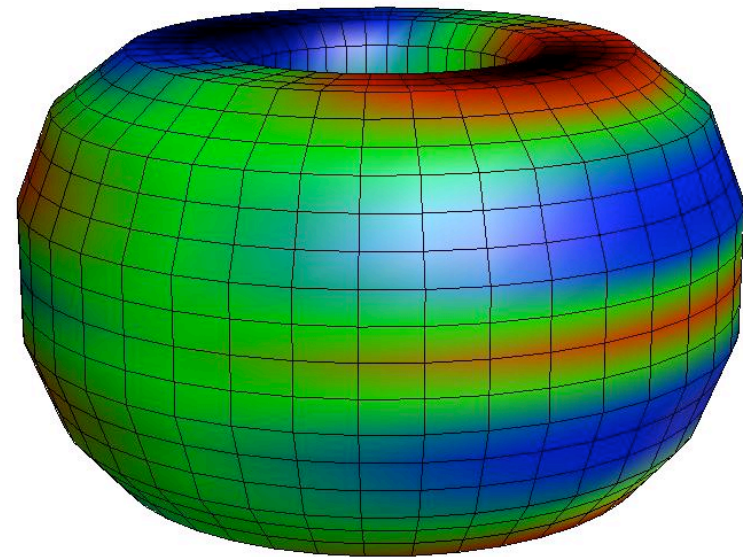
mode #1277  
wt =  $0.600e-2$   
 $0.555e-2$  s



Most important modes ( greatest weight ) follow:

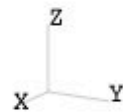
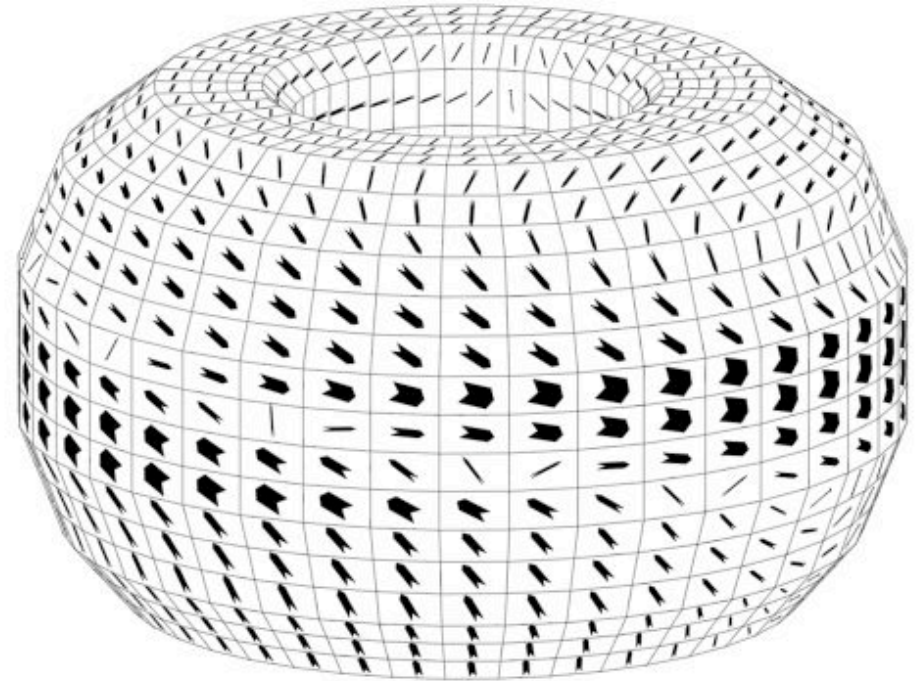
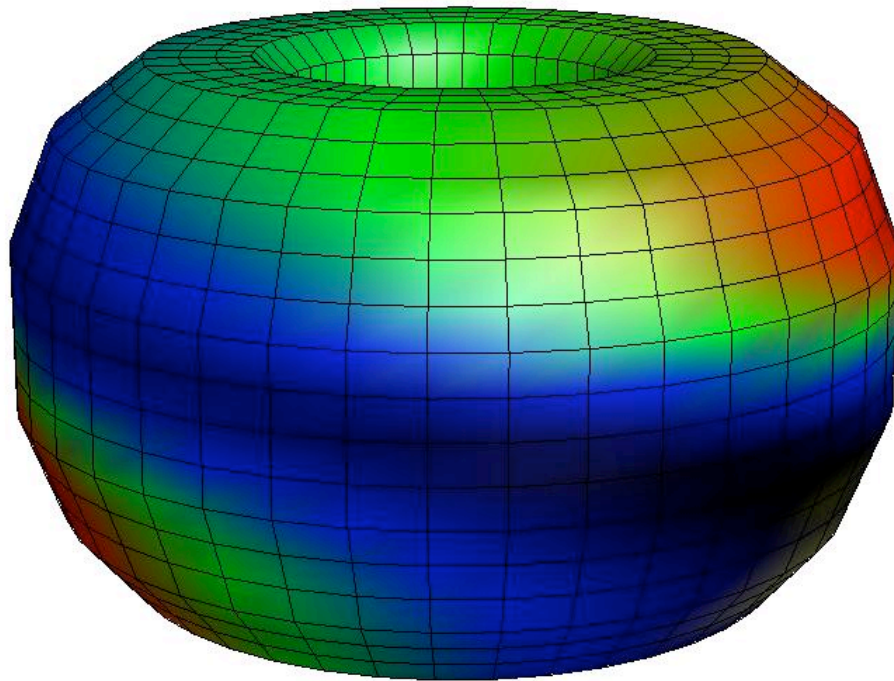


mode#1255  
wt =  $0.573e-2$   
 $0.282e-2$  s



mode#1233  
wt =  $-0.451e-2$   
 $0.207e-2$  s

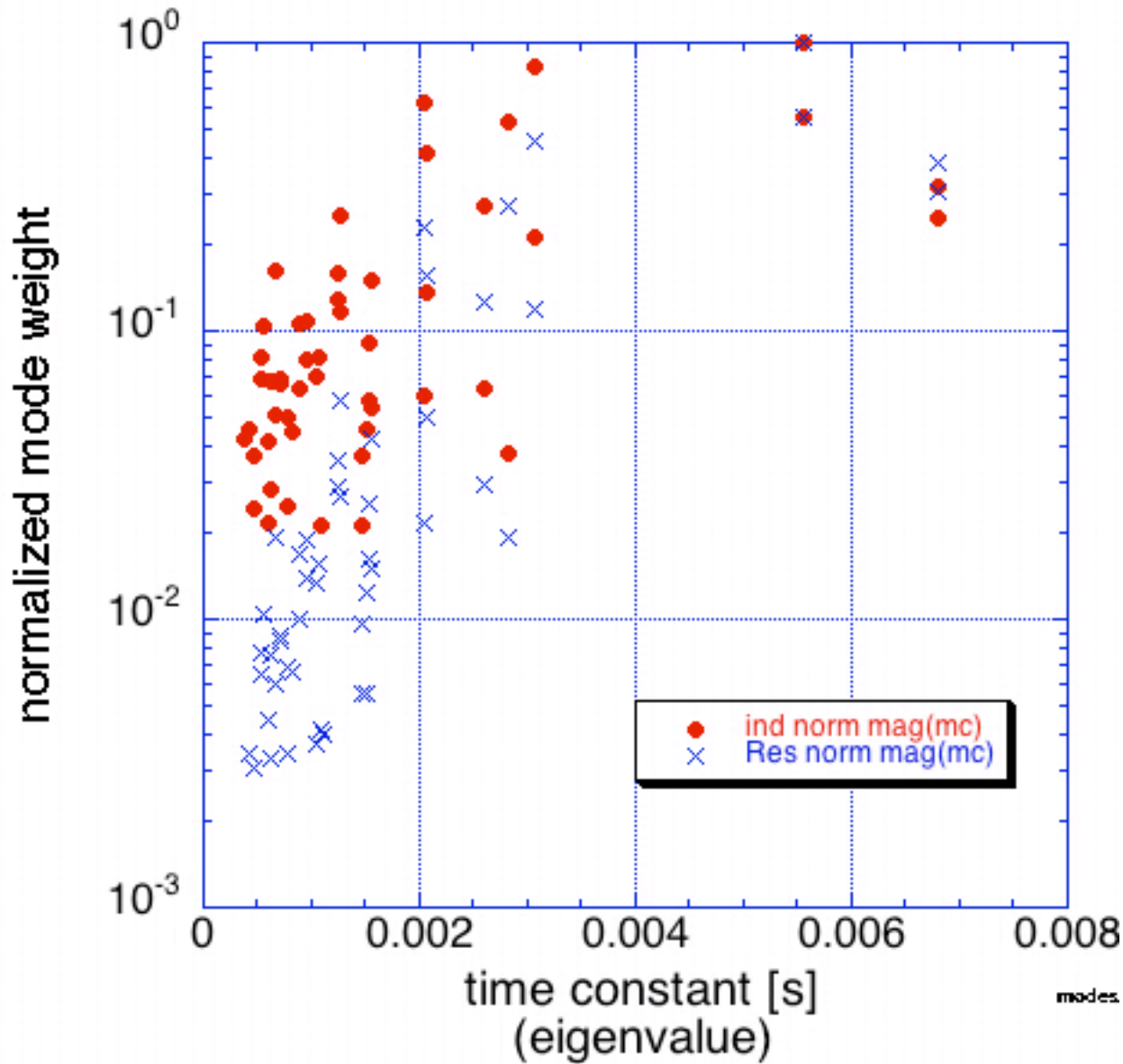
Examine steady state (resistive) response in standard DIII-D model



### 50 largest mode weights (92544)

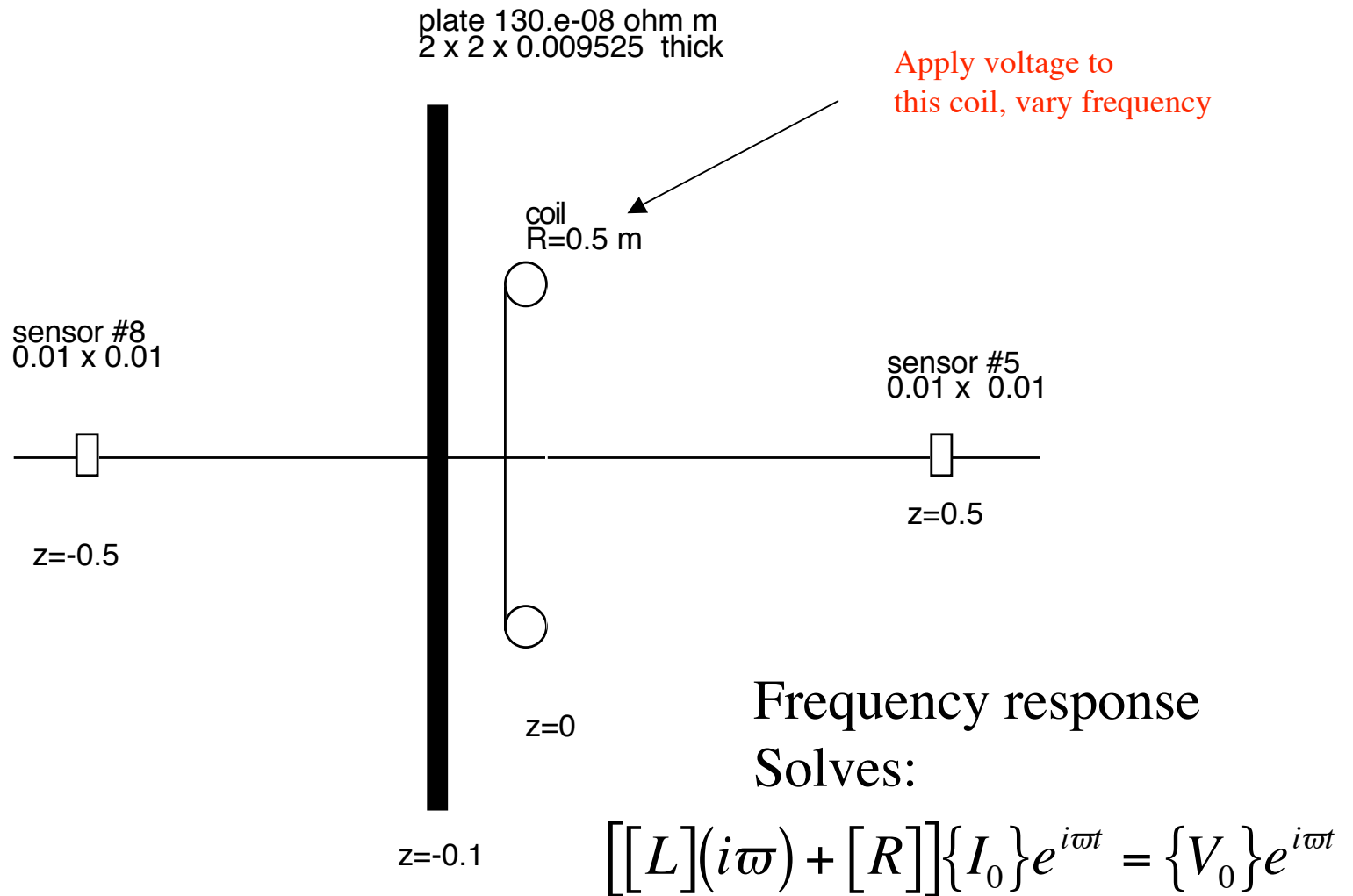
inductive limit

resistive limit



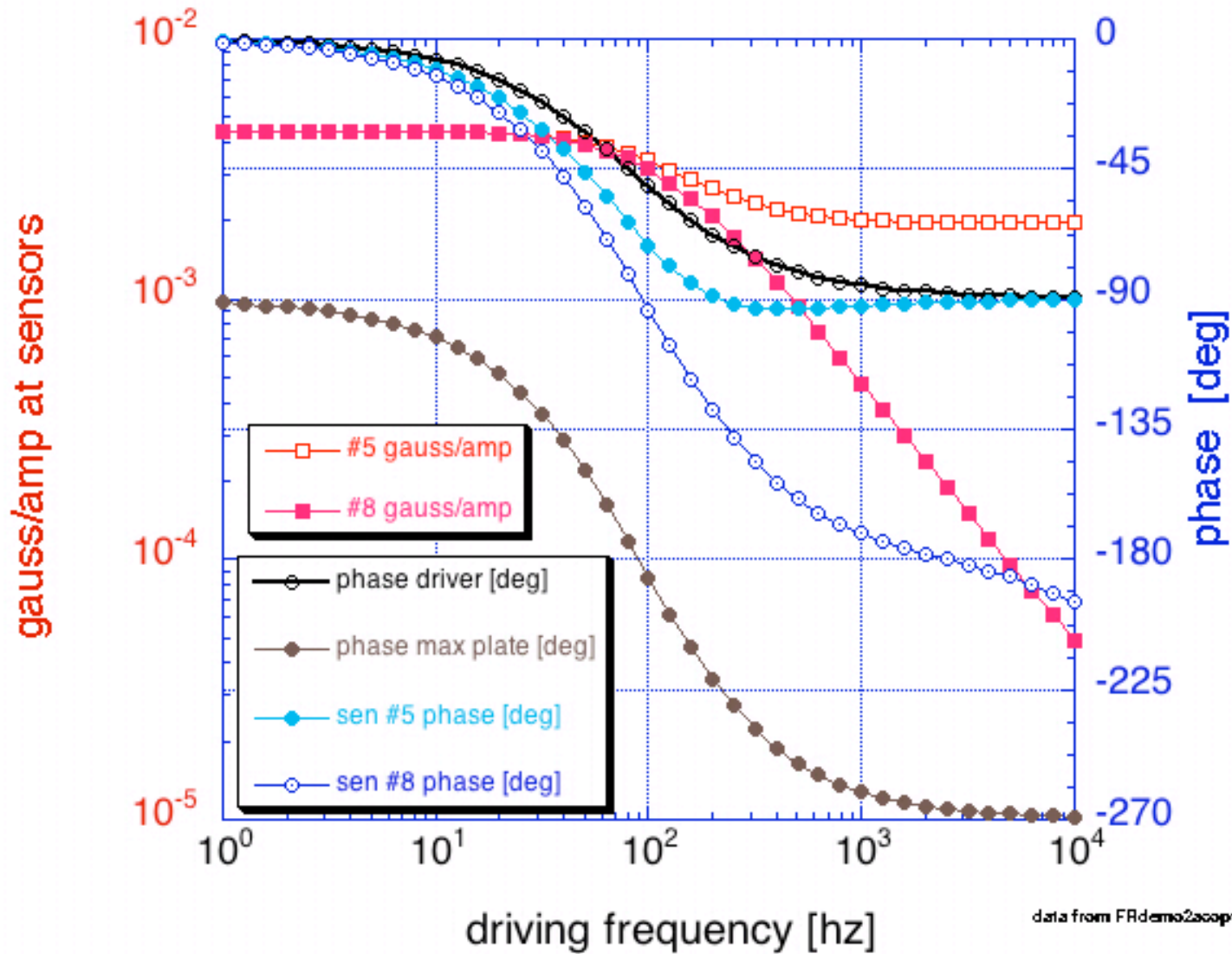
Many modes  
are important !!

Examine magnetic field penetrating a wall via frequency response of a driving coil, distributed wall model, sensors measure net axial field



frequency response calculation  
distributed wall model(many modes)  
fields & currents

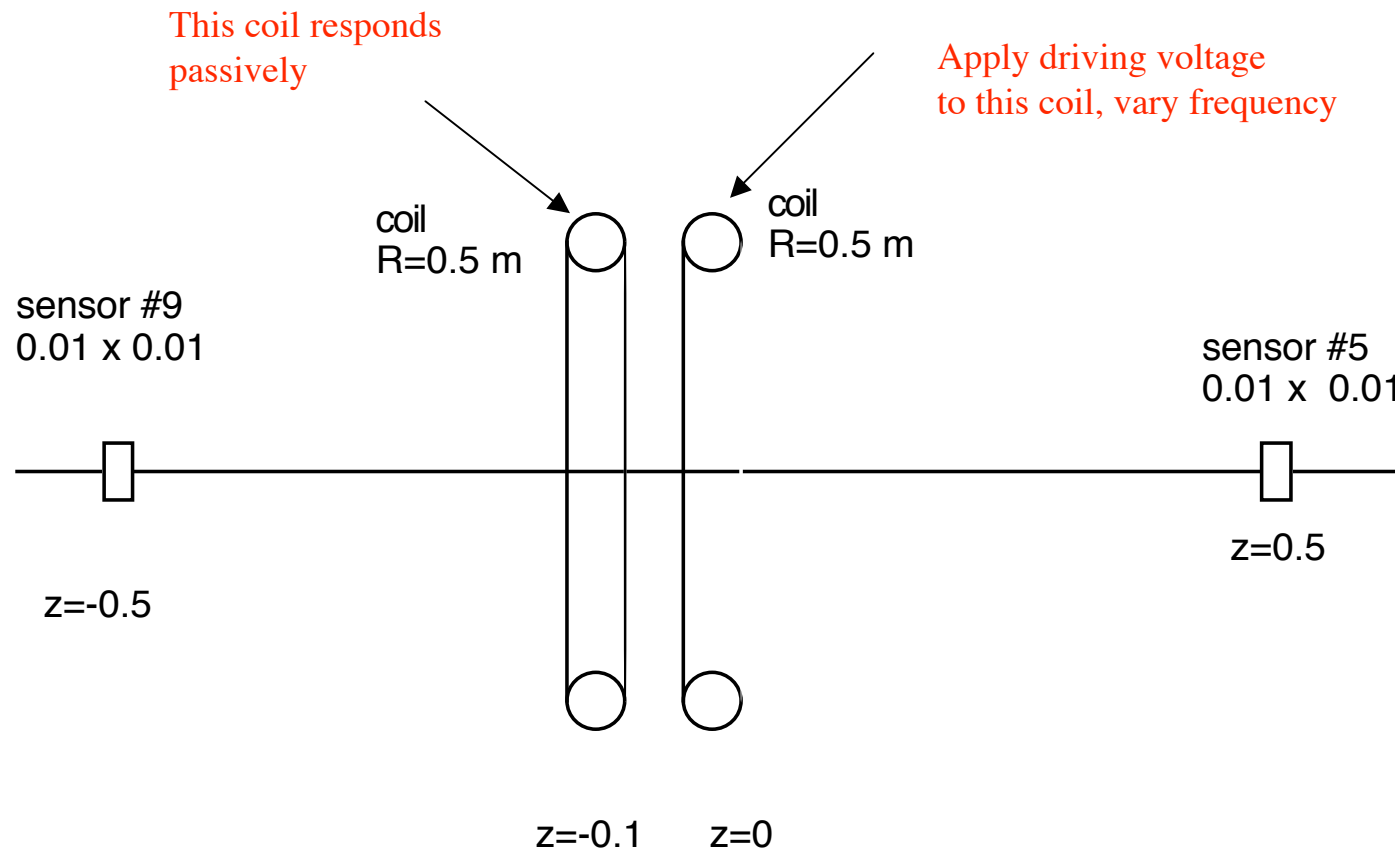
Sensor well shielded  
by distributed wall !



Skin depth  
=.009525 [m]  
~ 3.6 k hz



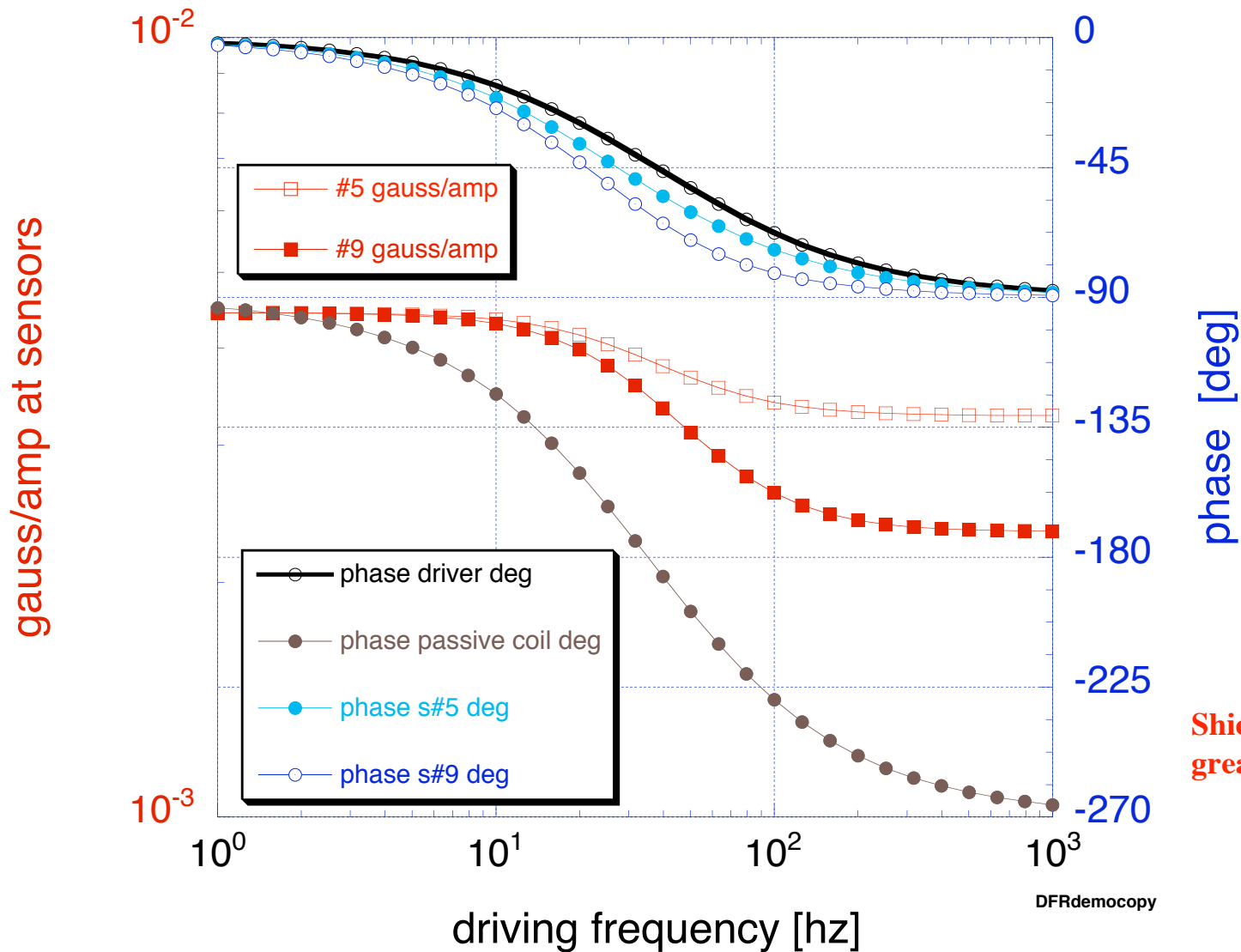
Examine magnetic field penetrating a wall via frequency response of a driving coil, the simplest wall model (a passive coil), sensors measure net axial field



Frequency response calc solves

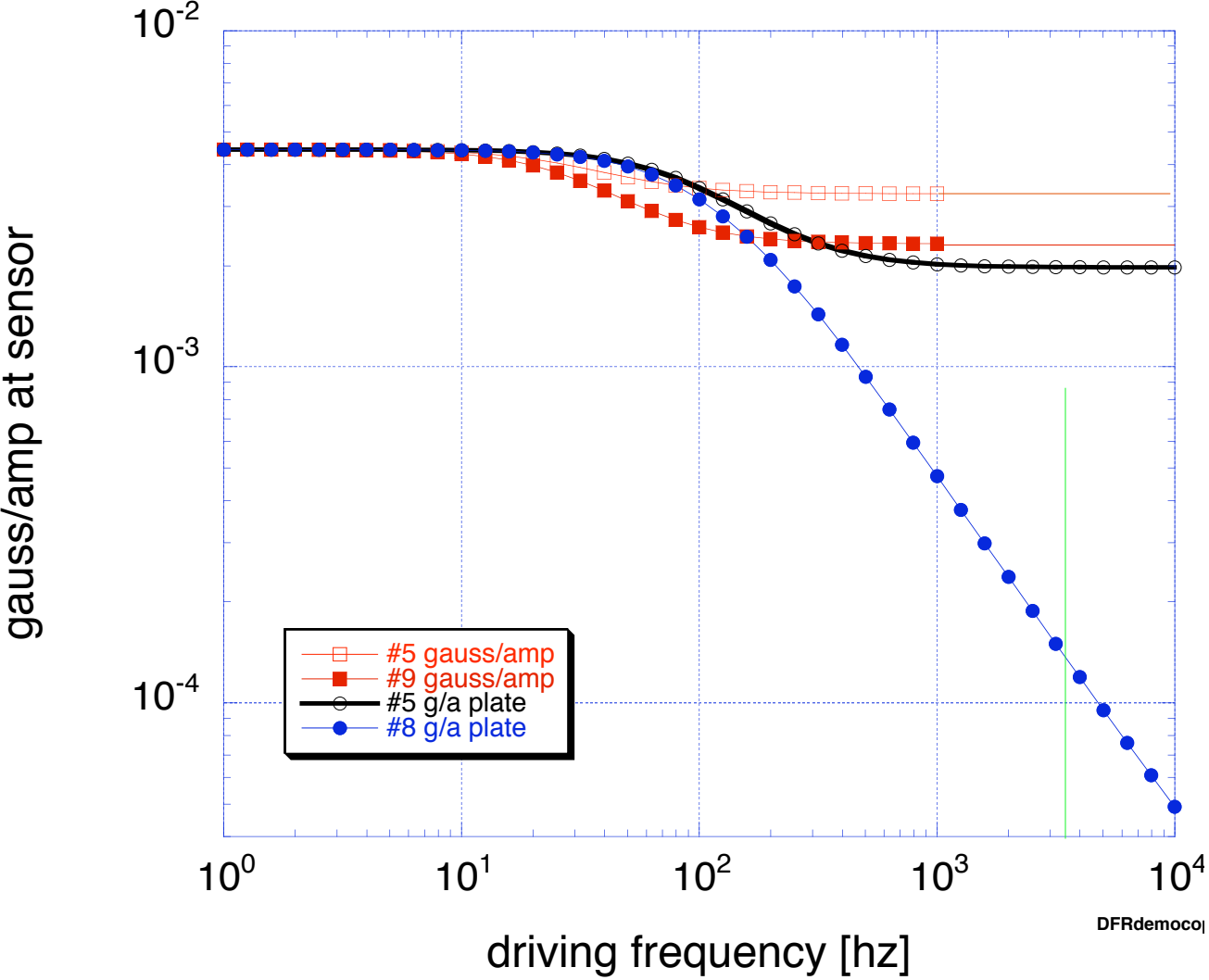
$$[[L](i\omega) + [R]]\{I_0\}e^{i\omega t} = \{V_0\}e^{i\omega t}$$

# frequency response calculations wall modeled by 1 time constant coil fields and currents



Shielding by passive coil  
greatly different !

comparison  
field penetration  
passive coil vs. plate



Distributed wall model shields much more field at interesting frequencies !

## Conclusions & Recommendations

- 1) All walls have many time constants
- 2) Current distributions may be described by sum of weighted eigenvectors, we may identify mode with the greatest contribution to the total answer
- 3) In toroidal geometry we never see an eigenvector with a helical pattern and we need many modes to well represent a helical pattern typical of a plasma mode.
- 4) Penetration of a magnetic field through a wall is not well modeled with a single wall time constant.

When using a single wall time constant proceed with caution.

Can we specify the best way to make this approximation ?