

# ARIES-RS (Reversed Shear) Advanced Tokamak Analysis and Issues

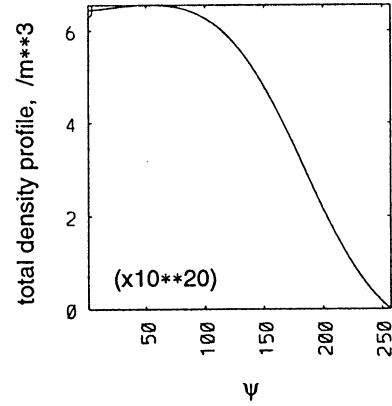
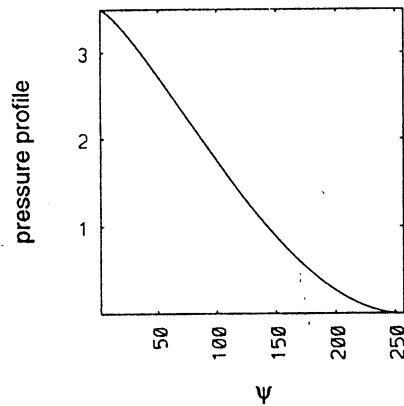
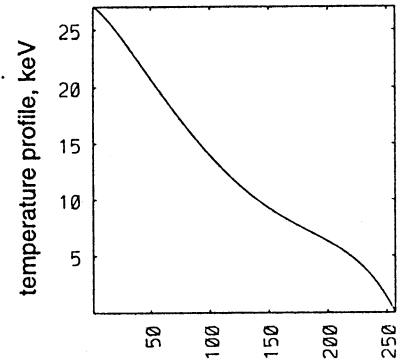
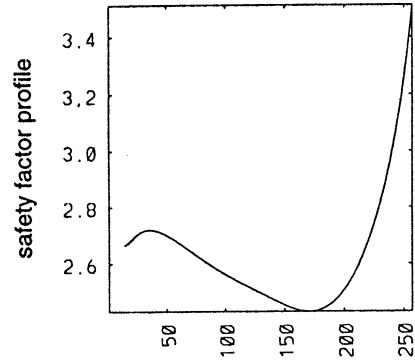
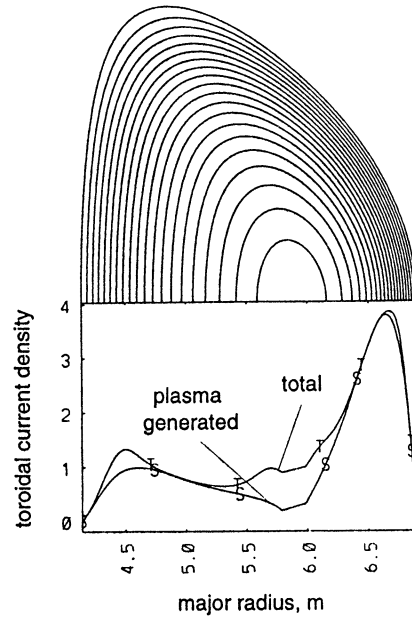
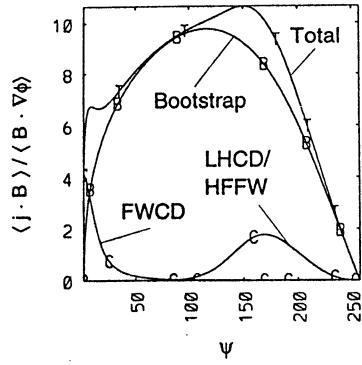
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# Introduction

- the ARIES-RS study evaluated the reversed shear configuration as a power plant to determine its potential benefits over
  - pulsed/first-stability, (PULSAR)
  - steady-state/first-stability, (ARIES-I)
  - steady-state/second-stability, (ARIES-II)
- the primary benefits of the configuration appear to be
  - high  $\beta$  (with the external kink mode stabilized) —> leading to high fusion power density and small reactor size
  - large bootstrap current and good alignment —> leading to low current drive power and therefore low recirculating power
  - sufficiently good transport that can roughly support the profiles being assumed in the stability and bootstrap calculations —> leading to energy confinement that can easily provide plasma power balance with small auxiliary input power ( $Q=25-30$ ).
  
- —> ARIES-RS utilizes the features we normally attribute to advanced tokamak plasmas, and it assumes they are obtained simultaneously in steady-state

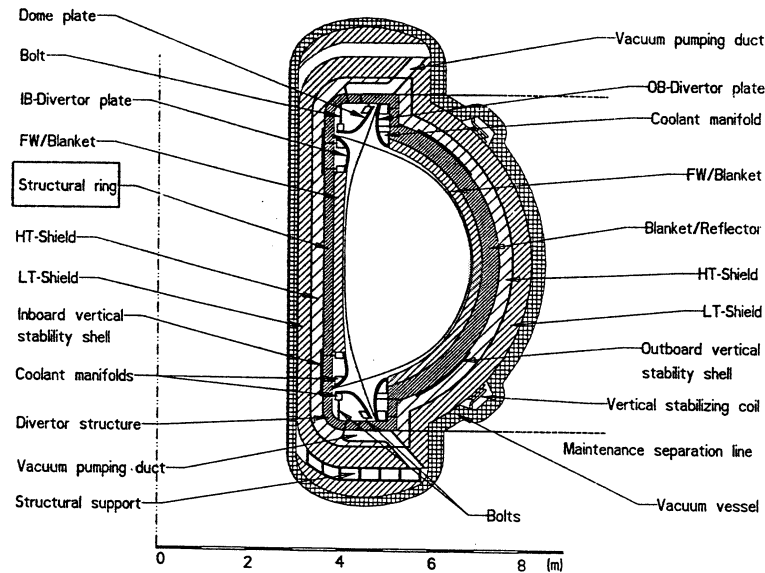


Reference reversed shear plasma configuration

$I_p$ (MA)	11.32
$B_T$ (T)	7.98
$R$ (m)	5.52
$a$ (m)	1.38
$\kappa$ (95%)	1.70
$\delta$ (95%)	0.50
$\beta_p$	2.28
$\beta$ (%)	4.96
$\beta^*$ (%)	6.18
$\beta_N$ (%)	4.83
$\beta_N^{\max}$ (%)	5.35
$q_0$ (axis)	2.80
$q_{\min}$ (minimum)	2.49
$\psi(q_{\min})$	0.69
$q_e$ (edge)	3.52
$I_{bs}$ (MA)	10.0
$I_{\nabla p}/I_p$	0.91
$I_{CD}$ (MA)	1.15
$q_*$	2.37
$l_i(3)$	0.42
$n_0/\langle n \rangle$	1.36
$T_0/\langle T \rangle$	1.98
$p_0/\langle p \rangle$	2.20
Kink wall	0.095

# Plasma Shape

- ARIES-RS shape parameters are  $\kappa_x=1.9$ ,  $\kappa_{95}=1.7$ ,  $\delta_x=0.7$ ,  $\delta_{95}=0.5$
- the plasma shape is restricted in a power plant by vertical stability/control ( $\kappa$ ) and the ability to provide an inboard divertor and adequate neutron shielding to the TF magnet ( $\delta$ )



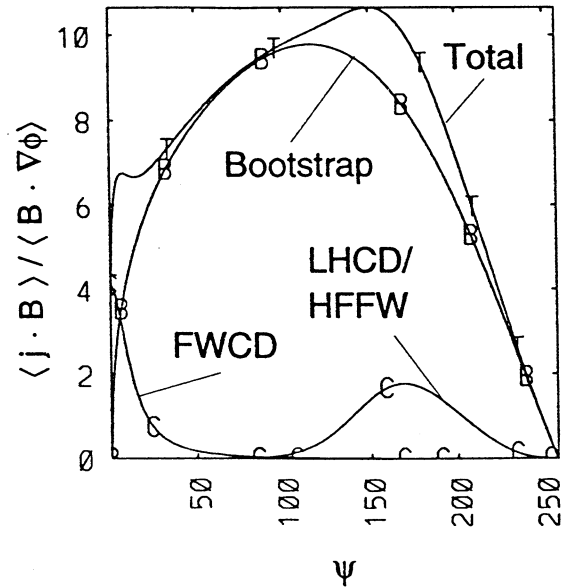
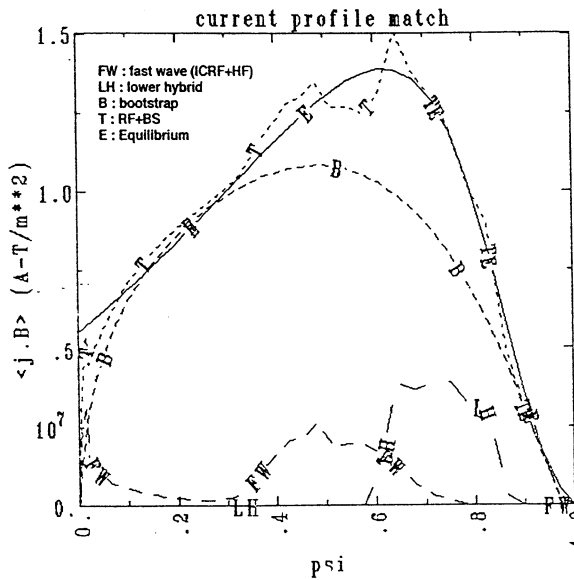
Variation of  $\beta$  with triangularity at  $A = 4.0$

$\delta$	$\beta_N^{\max}$	$\beta^{\max}$	$q_*$	$I_p$ (MA)
0.20	2.15	2.00	2.85	8.95
0.30	3.20	3.13	2.69	9.47
0.40	4.30	4.60	2.48	10.3
0.50	4.85	5.45	2.35	10.8
0.60	5.15	6.25	2.18	11.7

- $\rightarrow$  we evaluate the ideal MHD stability with the 95% shape parameters, our  $\beta$  would rise from 4.96% to 5.75% if we had used X-point parameters

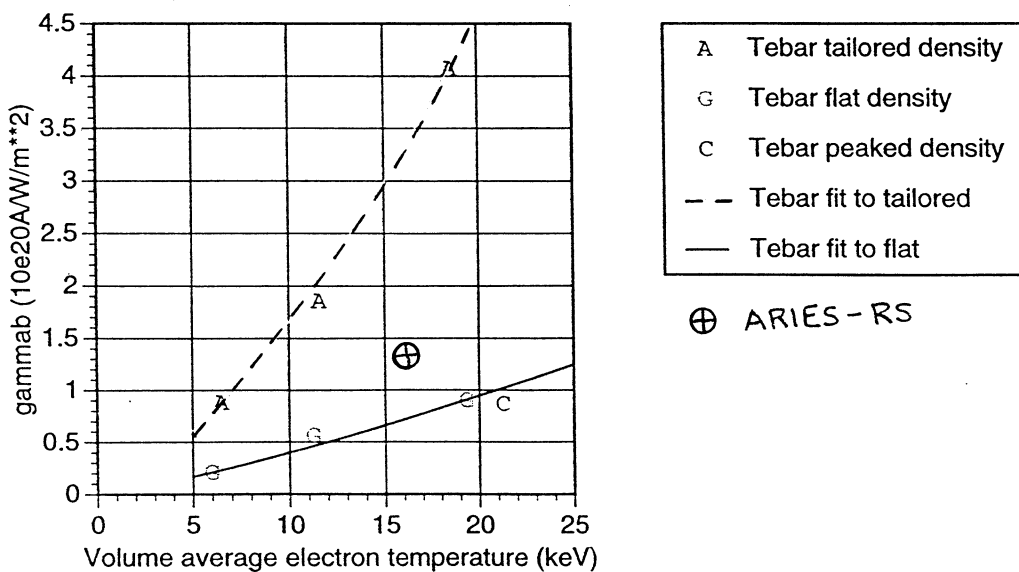
# Bootstrap Current and External CD

- use collisional Hirshman-Sigmar model for bootstrap calculations and predict the sum of bootstrap, Phirsch-Schluter, and diamagnetic currents to be 91% of the total current
- uses 3 CD systems; ICRF FW (5.5 MW), LH (35 MW), and HFFW (48 MW)
- 3 approaches were taken;
  - ideal MHD stable target plasmas were used in RF calculations to provide best fits
  - self-consistent RF/equilibrium calculations were done, and the resulting configuration checked for ideal MHD stability
  - self-consistent CD/bootstrap equilibria were calculated using the CD profiles from RF calculations, and checked for ideal MHD stability

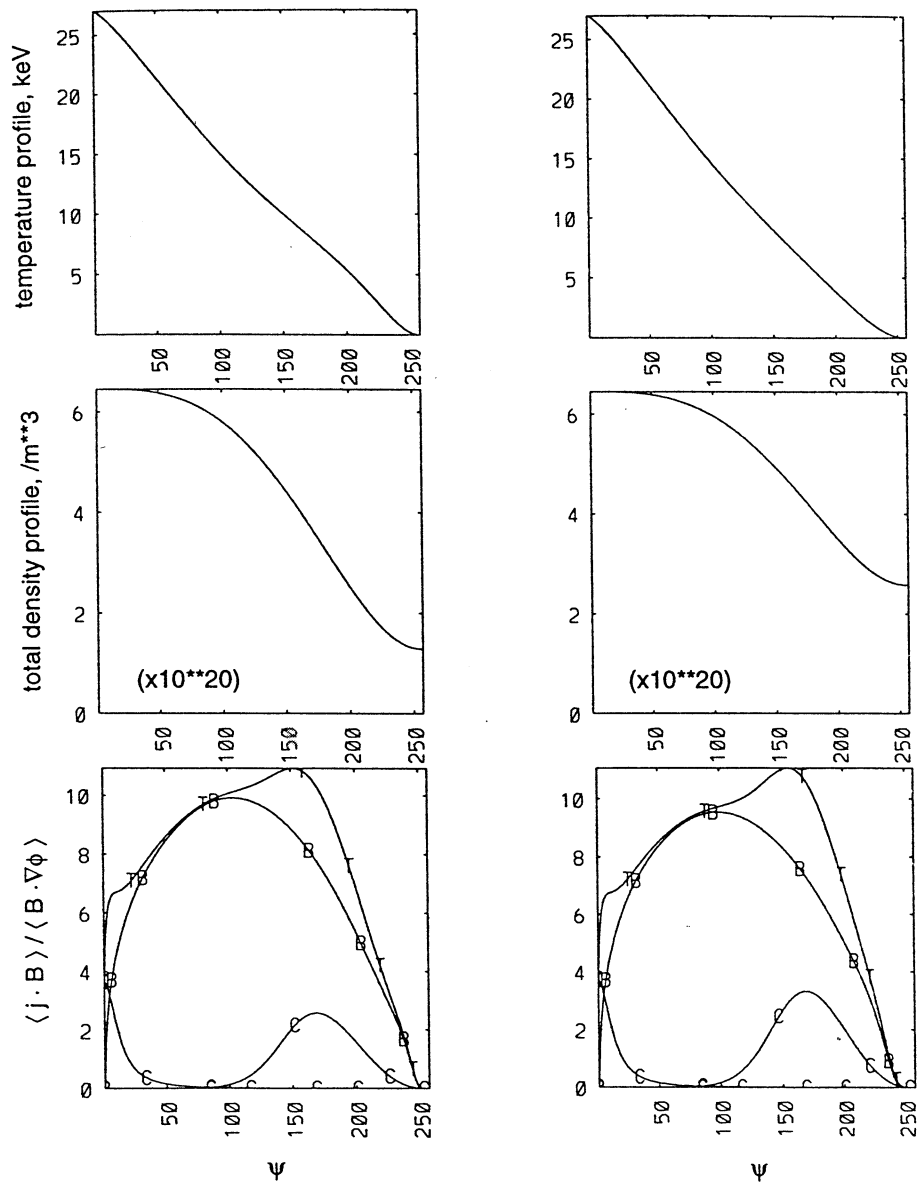


## Bootstrap Current and External CD, cont'd

- we rejected 100% bootstrap current solutions because they would require precise density and temperature profiles, and chose to make the off-axis CD a critical requirement for control of  $r(q_{min})$
- we tried to address the robustness of the configuration by scanning
  - the magnitude of temperature and density combination, and found that our bootstrap current contribution was nearly constant
  - temperature and density profiles, and found we could require as much as twice the CD we were providing, or as little as one third
  - the impact of finite edge density required for divertor operation, and found that up to 40% edge density was possible, requiring 40% more current drive, and no loss of  $\beta$ .



## Bootstrap Current and External CD, cont'd



- $\rightarrow$  the use of the collisionless bootstrap formulation can eliminate the need for off-axis current drive
- $\rightarrow$  finite edge temperature consistent with H-mode may relieve off-axis CD requirements

# Equilibrium and Ideal MHD Stability

- the maximum  $\beta$  used for ARIES-RS is 90% of the maximum  $\beta$  determined from ideal MHD stability
- for ideal MHD stability scans the current profile was prescribed by

$$\frac{\langle j \cdot B \rangle}{\langle B \cdot \nabla \phi \rangle} = j_o(1 - \hat{\psi}) + j_1 \frac{d^2 \hat{\psi}^a (1 - \hat{\psi})^b}{(\hat{\psi} - \hat{\psi}_o) + d^2} \quad (1)$$

- –  $q_o - q_{min} > 0.3$
- $q_o < 3.0$
- $q_{min} > 2.0$
- $r(q_{min})$  maximized, subject to  $q_{edge} \geq 3.5$  and a wall distance of  $0.3a$
- the pressure profile was given by

$$p = p_o(1 - \hat{\psi}^\alpha)^2 \quad (2)$$

Variation of  $\beta$  with pressure profile exponent

$\alpha$	$\beta_N^{\max}$	$\beta^{\max}$	$f_{\nabla p}$	$I_{CD}$ (MA)
1.20 <sup>a</sup>	5.77	5.95	0.78	2.28
1.30	5.35	5.54	0.89	1.20
1.40	5.00	5.17	0.89	1.19
1.50 <sup>b</sup>	4.64	4.80	0.87	1.37
1.60 <sup>b</sup>	4.36	4.50	0.87	1.36

<sup>a</sup> Bootstrap limited,  $f_{\nabla p}$  and  $I_{CD}$  correspond to  $\beta_N = 4.6$  and  $\beta = 4.74$ .

<sup>b</sup>  $T(\psi)$  and  $n(\psi)$  do not obey transport constraints.

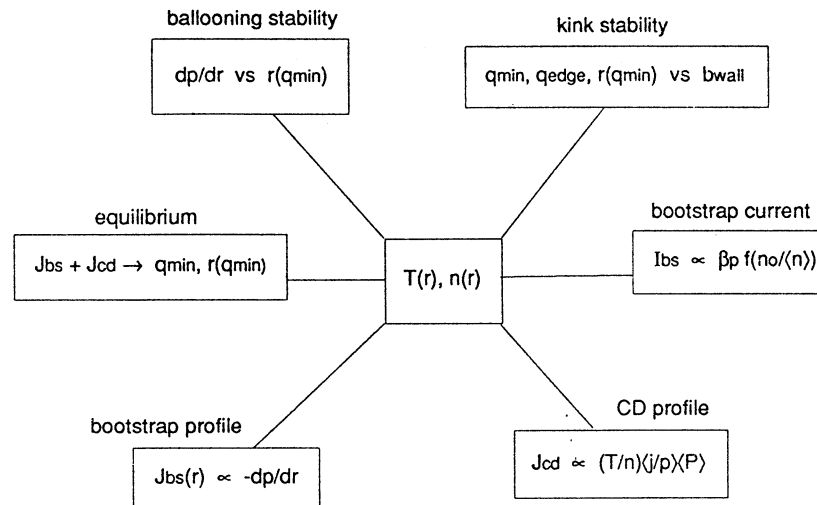
- bootstrap current alignment constraint
  - $\langle j \cdot B \rangle_{bs} \leq \langle j \cdot B \rangle_{eq}$
  - $T(\psi)$  and  $n(\psi)$  must satisfy rough transport constraint that dominant gradients fall inside or at  $r(q_{min})$

## Equilibrium and Ideal MHD Stability, cont'd

- we assume that a conducting shell and plasma rotation will stabilize the low-n kink mode
  - conducting shell assumed at  $0.3a$  for almost all analysis, and  $\beta$  limiting mode was always  $n=3$
  - stability analysis indicated that a wall only on the outboard extending poloidally from  $-85^\circ$  to  $+85^\circ$  was sufficient
  - the design of the vanadium structure/liquid lithium blanket showed that a 2 cm shell would be at  $0.1a$ , and satisfied the criteria developed by Bondeson and Ward
  - it turned out that we could not take advantage of a wall closer than  $0.25a$ , since we could not raise the ballooning limit without making the bootstrap current shift toward the axis
  - in hindsight, letting  $r(q_{min})$  shift further out and letting  $q_{edge}$  drop below 3.5, may have allowed higher  $\beta$ , but the CD implications are unclear
  - plasma rotation speed requirements were predicted to be  $2-6 \times 10^5$  m/s, while CD rotation speeds are  $\approx 10^4$  m/s
  
- $\rightarrow$  the stabilization of the low-n kink modes is critical to high  $\beta$  tokamak operation, since no second stable region exists for kink modes
  
- $\rightarrow$  no analysis of neoclassical tearing modes was done

# Plasma Transport

- no energy or particle transport analysis was done, only a rough constraint that the temperature and density profiles have their dominant gradients inside or at  $r(q_{min})$
- the profiles used in ARIES-RS provide kinetic stability to toroidal drift-type modes



- $\rightarrow$  is it possible that we can figure out how to make the reversed shear transport barrier leak, the same way we found ELM's to cause the H-mode to leak
- $\rightarrow$  it is interesting that our predictive capability for ideal MHD stability, bootstrap current, and RFCD are at a better level than our ability to predict the plasma temperature and density that underlies all of them

## Other Analysis and Issues

- radiated power from the plasma and the divertor solution
  - 20% radiated power from plasma core ( $\approx 100$  MW)
  - 80% into SOL, utilized a radiating divertor with neon impurity ( $\approx 400$  MW), where some power is also radiated in the SOL
  - $Z_{eff}$  was 2.0
  - $n_{edge}/n_o = 0.2$
  - neon enrichment in the divertor of between 2-8 was assumed
  - mantle radiation required higher  $Z_{eff}$  and  $n_{edge}/n_o$  greater than 0.4 that adversely affected the CD, MHD stability, and power balance
- analysis was done to demonstrate that we could deposit a pellet inside the  $r(q_{min})$  for fueling
- the assumed effective particle confinement time was 10 times
- the energy confinement time corresponded to an ITER-89P multiplier of 2.3
- the plasma was expected to have an H-mode edge with low amplitude/high frequency ELM's

# ARIES-RS Implications for Advanced Tokamaks

- the simultaneous achievement of
  - effective stabilization of low- $n$  external kink modes by a conducting wall/rotation or a feedback control system
  - operation near the ideal MHD  $\beta$ -limit
  - 100% non-inductive plasma current with large bootstrap current fraction
  - significant plasma shaping, but not extreme
  - global energy and particle confinement times that are not extreme
  - temperature and density profiles (and therefore pressure) that can support good ideal MHD stability and bootstrap current alignment
  - effective means for power and particle handling between the core plasma, the SOL, and the divertor
  - all in STEADY STATE
  
- -> to do all these simultaneously requires feedback control of several subsystems that interact