

# Lower Hybrid Current Profile Control Studies in Alcator C-Mod

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## Motivation

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- Quasi-steady state operation at the  $\beta$ -limit is achievable with RF current drive in C-Mod
  - $t_{\text{pulse}} \simeq (5 - 7) \text{ s}$  @  $B_0 \simeq (4 - 5) \text{ T}$
  - $t_{\text{pulse}}/\tau_{\text{L/R}} \simeq 2$  @  $T_e(0) \simeq 5 \text{ keV}$
- Increased  $\beta$ -limits due to plasma shaping ( $\kappa_x \lesssim 1.8$ ,  $\delta_x \lesssim 0.8$ )
- Full RF current drive with effective current profile control and high bootstrap current fraction ( $f_{\text{BS}}$ ) is possible:
  - Compact size ( $R_0 = 0.67 \text{ m}$ )
  - (4–8) MW of (40–80) MHz RF power for ICRH
  - 3 MW of 4.6 GHz LHCD power

# Role of Lower Hybrid Current Drive in Advanced Tokamak Physics Experiments in C-Mod

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- Efficient off-axis ( $r/a \gtrsim 0.5$ ) current generation with  $\eta_{\text{CD}} \simeq 0.1 - 0.15$  ( $10^{20}$  A/W/m<sup>2</sup>) allows:
  - Access to second stability regime as  $q(\psi) > 2$
  - Access to enhanced confinement modes as  $q(\psi)$  becomes non-monotonic and local magnetic shear is reduced
- Expect rapid thermalization of fast electron tail for  $\epsilon_{\text{F}} \simeq 50$  keV and  $n_e \simeq 1 - 1.5 \times 10^{20}$  m<sup>-3</sup>

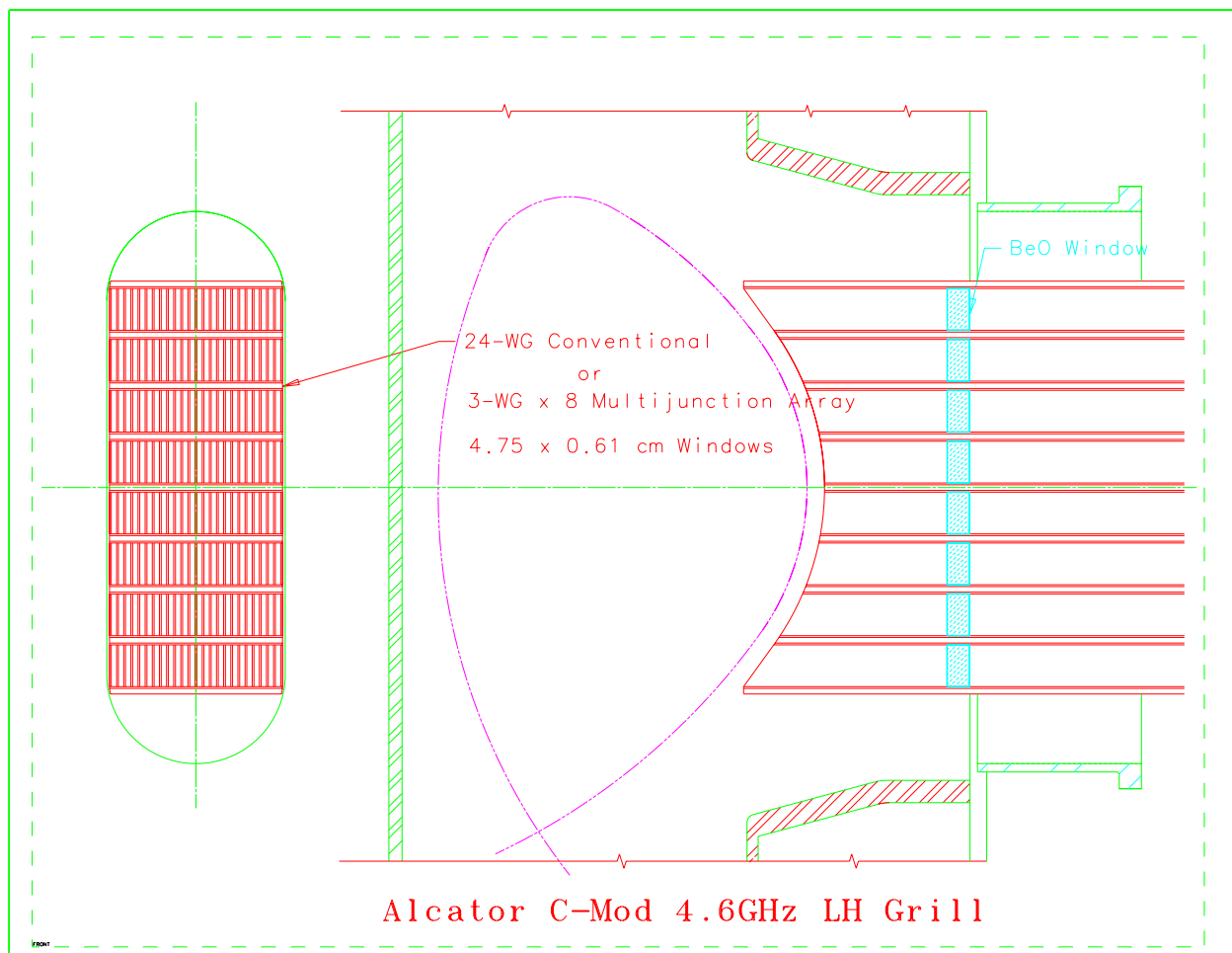
## Overview of Numerical Models

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- Current drive and MHD equilibrium code - ACCOME (MIT - JAERI - LLNL)
  - Noncircular MHD solver (SELENE)
  - Non-inductive current density source terms
    - Lower hybrid current drive (LHCD)
    - ICRF fast wave current drive (FWCD)
    - Bootstrap current
  - Pressure profiles are assumed in model - no transport
- Current drive modules iterate with MHD solver to obtain self-consistent MHD equilibrium
- Equilibria from ACCOME are analyzed for ideal stability:
  - JSOLVER / PEST II - (PPPL)
  - CAXE / KINX - (Keldysh Institute)

# Lower Hybrid Grill - 24 Waveguides Conceptual Design

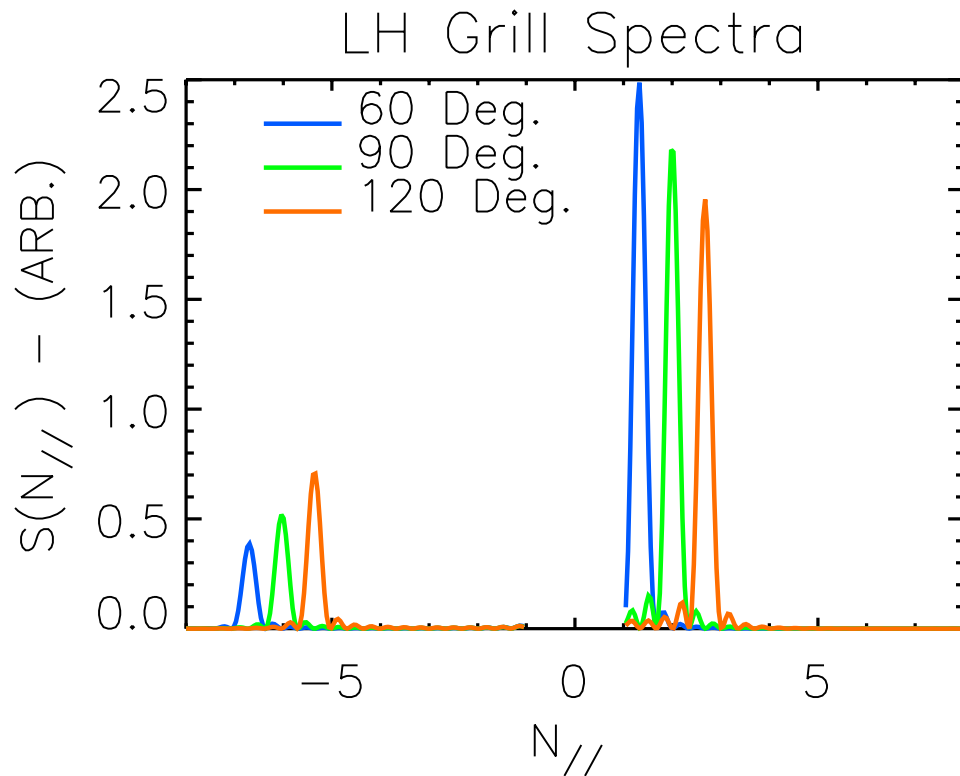
$$f_0 = 4.6 \text{ GHz}$$



# Lower Hybrid Grill Spectra - 24 Waveguides

$f_0 = 4.6$  GHz, (4.755 cm  $\times$  0.61 cm) Windows

(0.2 cm Wall Thickness)



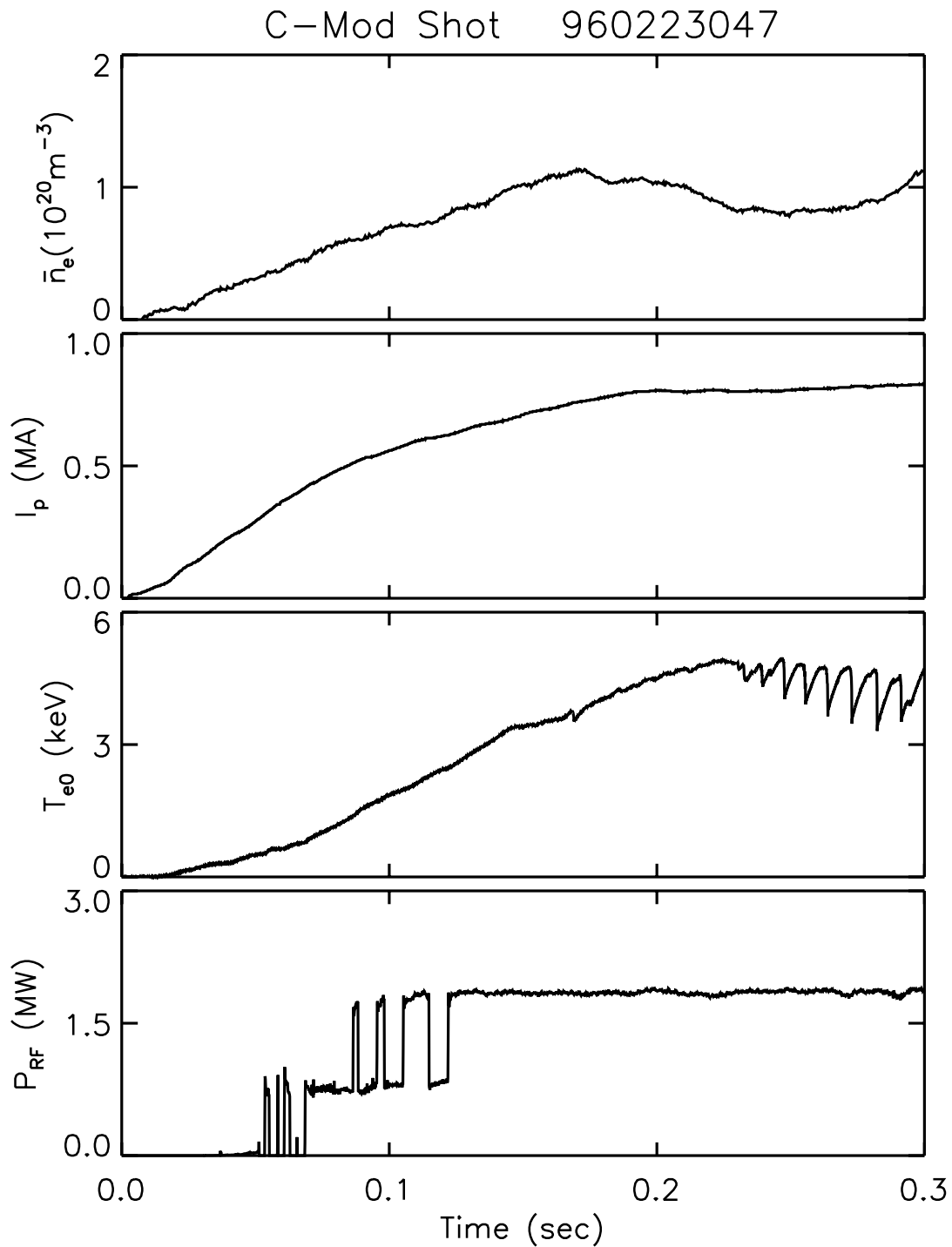
Grill Spectra calculated using a LH coupling code (M. Brambilla).

## Summary of Operating Scenarios

	Start Up		$\beta$ -Limit	
$H_{\text{ITER-89P}}$	1.0	1.0	2.50	2.50
$P_{\text{ICH}}(\text{MW})$	2.0	4.0	5.0	5.0
$\beta_{\text{N}}$	1.3	1.6	2.9	3.0
$I_{\text{p}}(\text{MA})$	0.69	0.84	0.98	0.81
$f_{\text{bs}}$	0.41	0.45	0.70	0.74
$P_{\text{LH}}(\text{MW})$	3.0	3.0	2.4	3.0

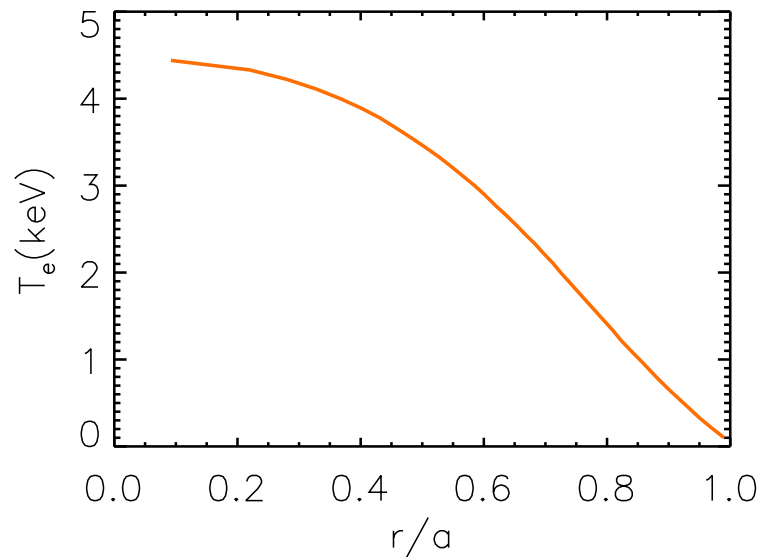
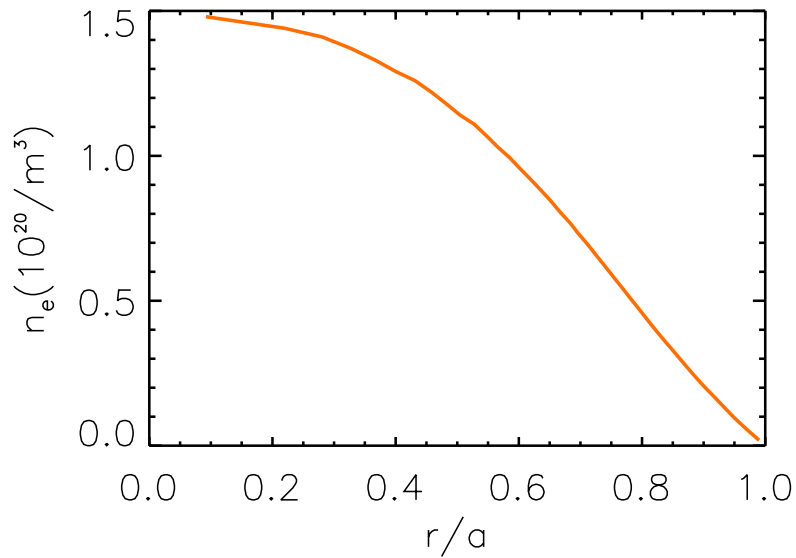
# Start Up Modelled Using C-Mod Data for Current Ramp Plus High Power ICRH

D(H) at  $B_0 = 5.3$  T,  $f_0 = 80$  MHz



## Plasma Profiles for Start Up with Reverse Shear

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3} \quad T_e(0) = 4.5 \text{ keV} \quad B_0 = 4.4 \text{ T}$$



$$p(\psi) = p(0)(1 - \psi)^2$$

$$n(\psi) = n(0)(1 - \psi)$$

$$T(\psi) = T(0)(1 - \psi)$$

$$H_{\text{ITER-89}} \simeq 1.0$$

$$P_{\text{ICRF}} \simeq 2.0 \text{ MW}$$

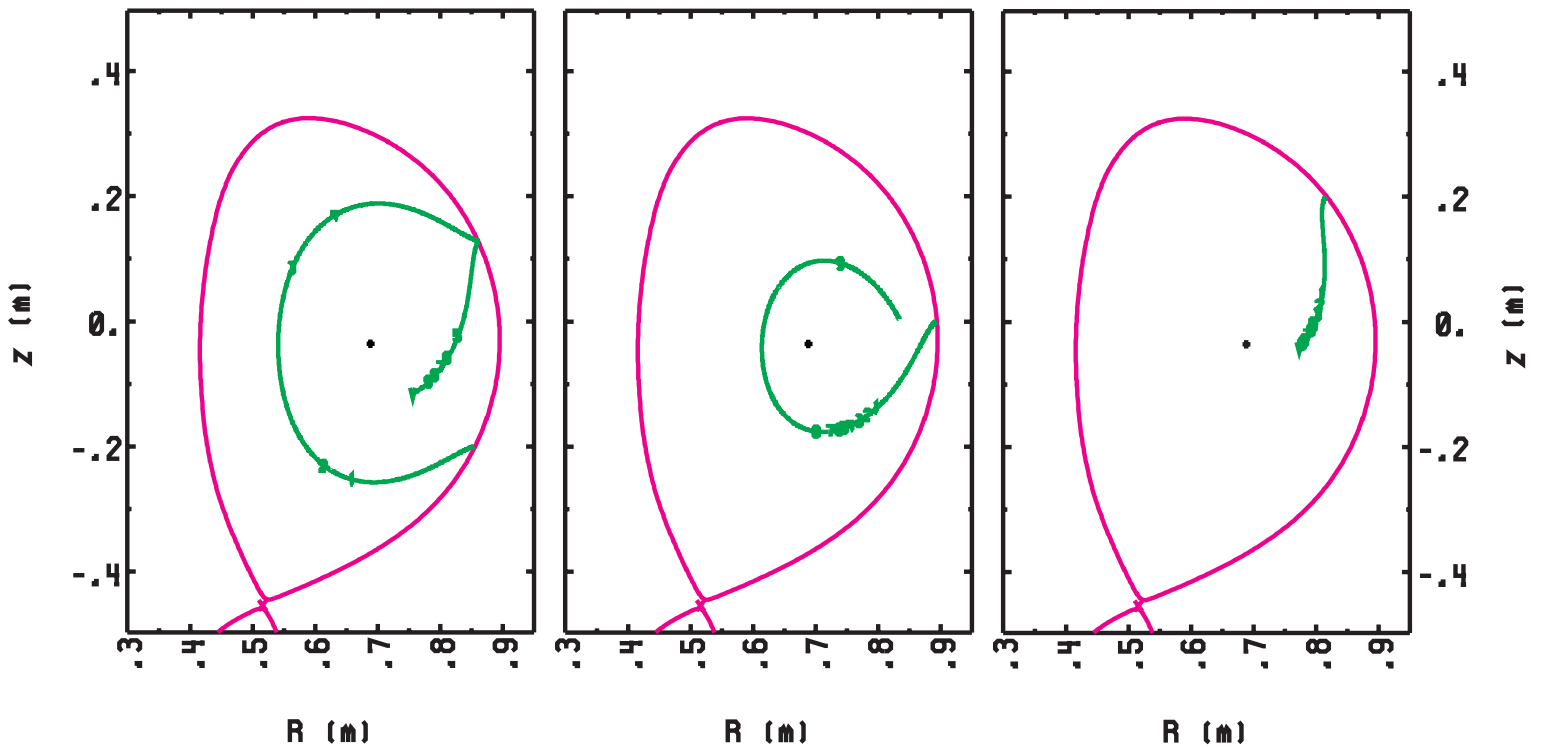
# C-Mod Start Up with Reverse Shear - ( $\beta_N = 1.3$ )

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 4.5 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 2.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 1.0$$

Lower Hybrid Ray Trajectories ( $n_{\parallel}^0 = 2.75$ )

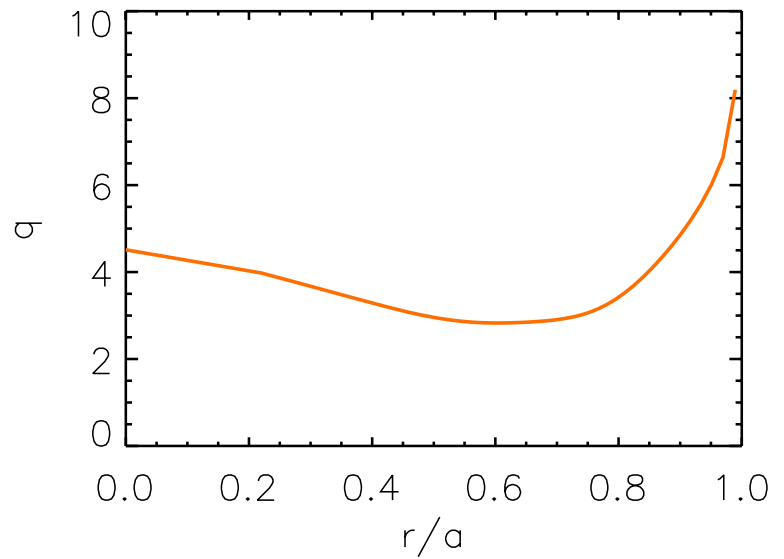
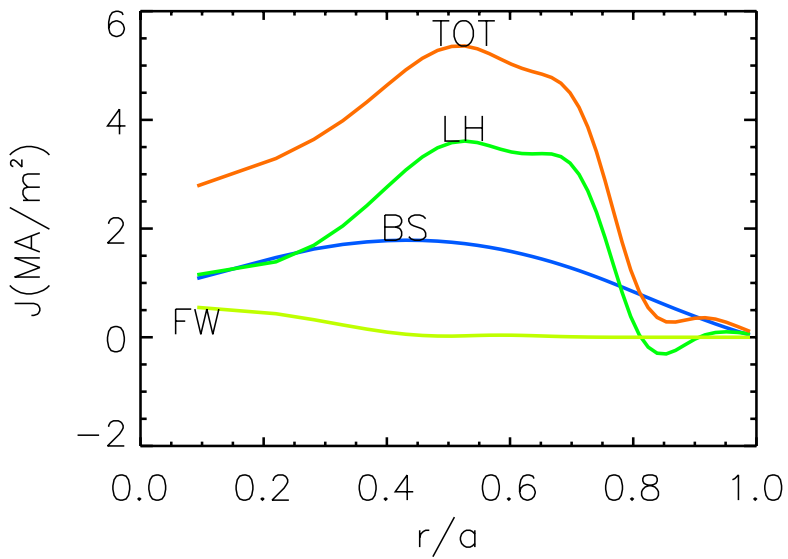
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## C-Mod Start Up with Reverse Shear - ( $\beta_N = 1.3$ )

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 4.5 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 2.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 1.0$$



$$I_p = 0.69 \text{ MA} \quad (f_{\text{BS}} = 0.41)$$

$$I_{\text{LH}} = 0.39 \text{ MA}$$

$$P_{\text{LH}} = 3 \text{ MW} \quad (n_{\parallel}^0 = 2.75)$$

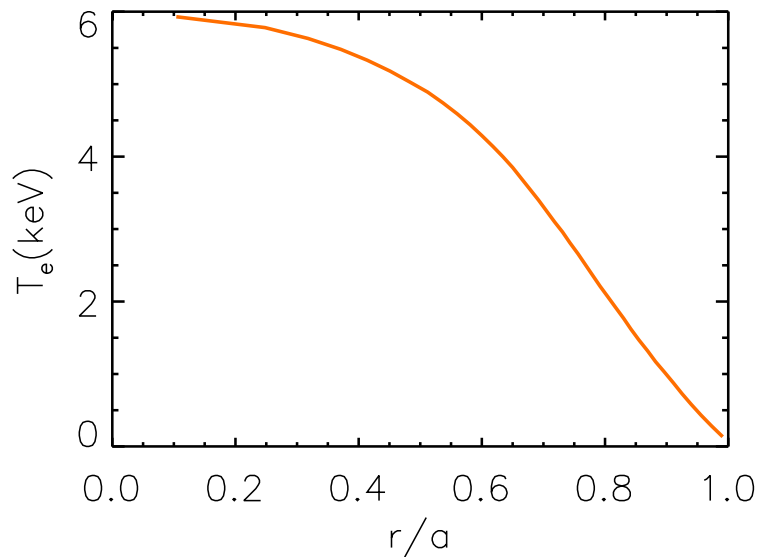
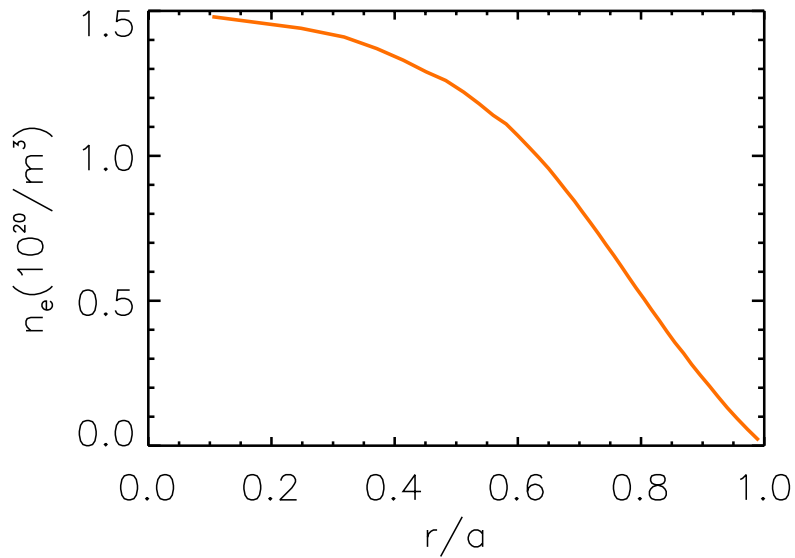
$$q_0 = 4.47 \quad q_{\text{min}} = 2.83$$

$$\beta_t = 0.88\%$$

$$p(0)/\langle p \rangle = 3.17$$

## Plasma Profiles for Start Up with Reverse Shear

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3} \quad T_e(0) = 6.0 \text{ keV} \quad B_0 = 4.4 \text{ T}$$



$$p(\psi) = p(0)(1 - \psi)^2 \quad H_{\text{ITER-89}} \simeq 1.0 - 1.5$$

$$n(\psi) = n(0)(1 - \psi) \quad P_{\text{ICRF}} \simeq 4.0 \text{ MW}$$

$$T(\psi) = T(0)(1 - \psi)$$

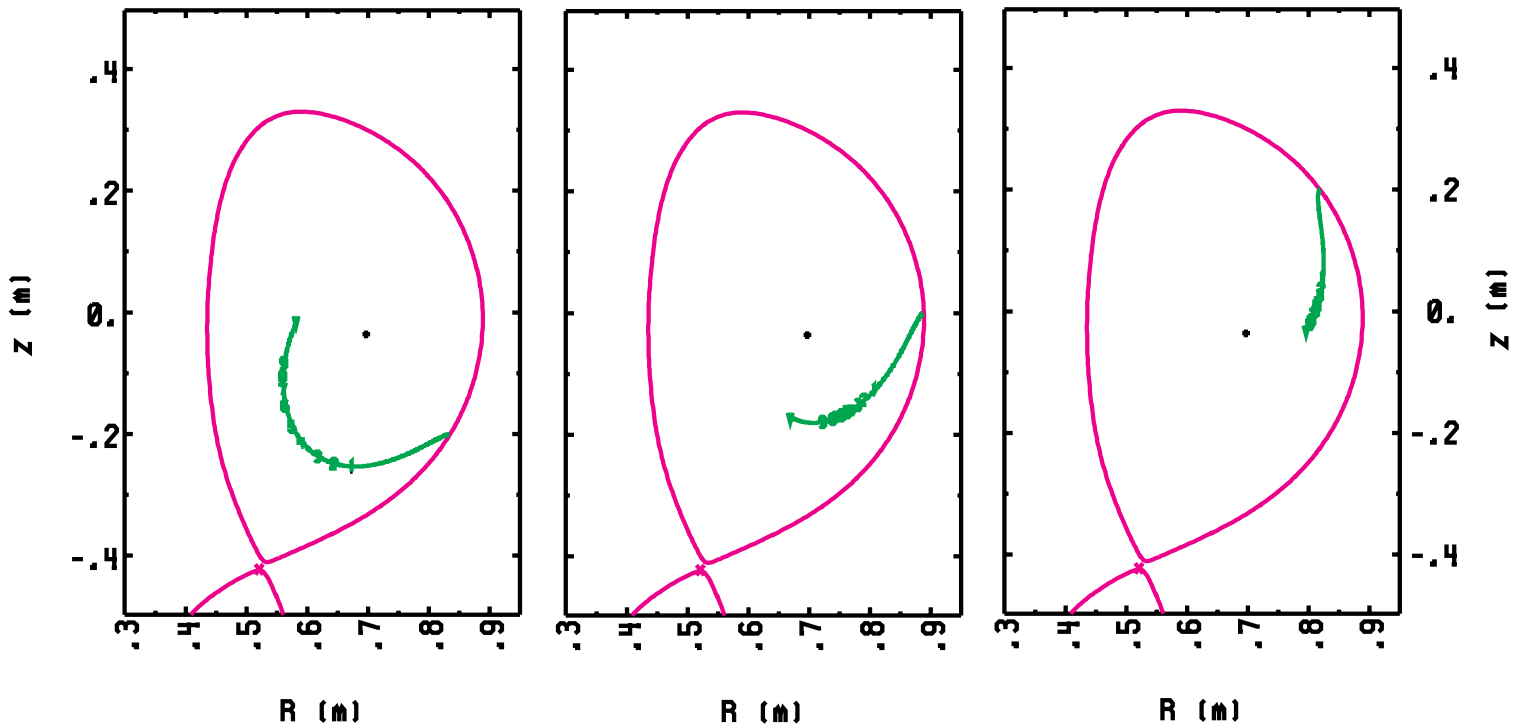
# C-Mod Start Up with Reverse Shear - ( $\beta_N = 1.6$ )

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 6.0 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 4.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 1.0 - 1.5$$

Lower Hybrid Ray Trajectories ( $n_{\parallel}^0 = 2.75$ )

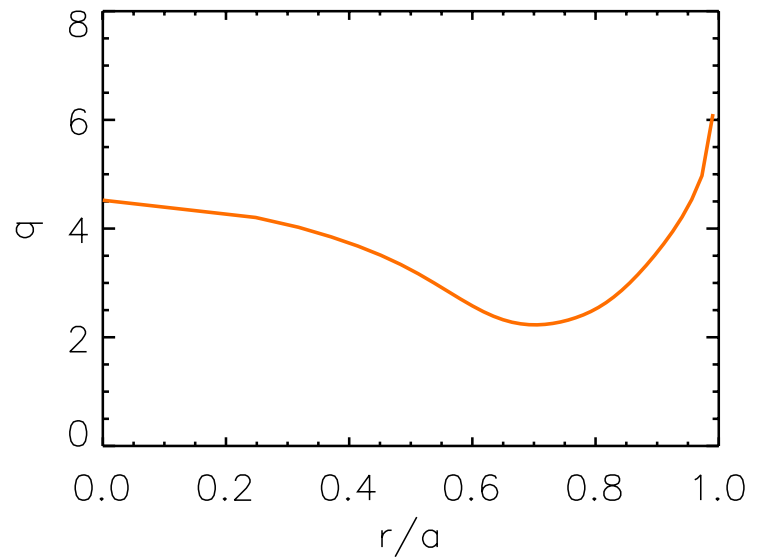
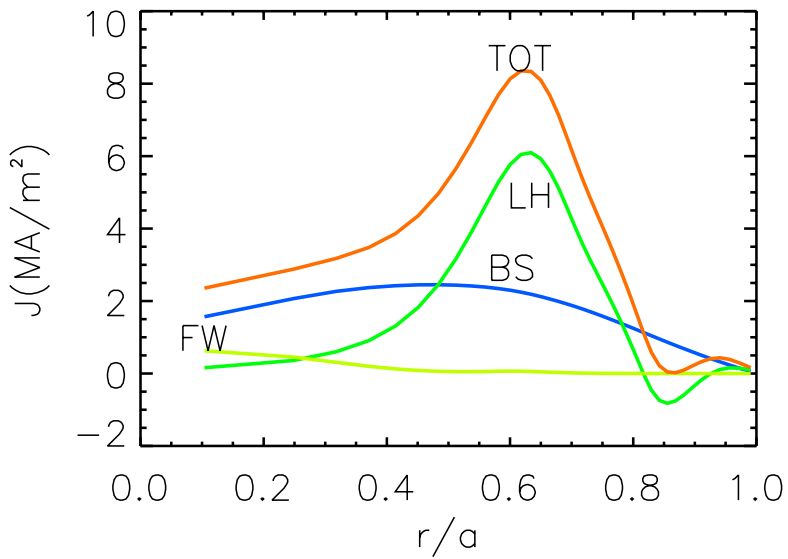
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# C-Mod Start Up with Reverse Shear - ( $\beta_N = 1.6$ )

$$n_e(0) = 1.5 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 6.0 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 4.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 1.0 - 1.5$$



$$I_p = 0.84 \text{ MA} \quad (f_{\text{BS}} = 0.45)$$

$$I_{\text{LH}} = 0.45 \text{ MA}$$

$$P_{\text{LH}} = 3 \text{ MW} \quad (n_{\parallel}^0 = 2.75)$$

$$q_0 = 4.49 \quad q_{\text{min}} = 2.23$$

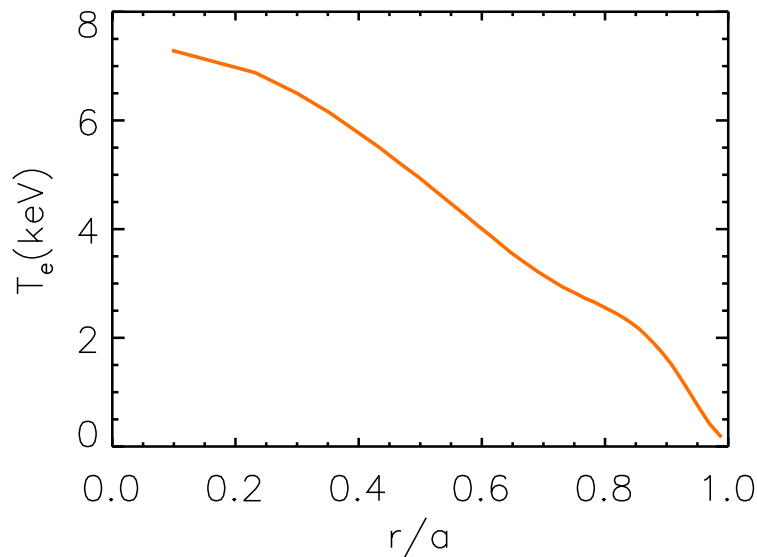
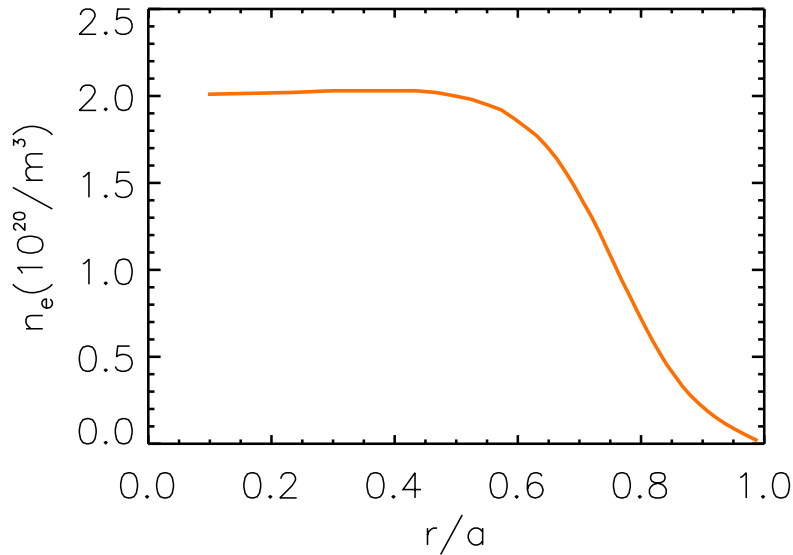
$$\beta_t = 1.33\%$$

$$p(0)/\langle p \rangle = 2.81$$

# Plasma Profiles for Reverse Shear Near the $\beta$ -limit

$$n_e(0) = 2.0 \times 10^{20} \text{ m}^{-3} \quad T_e(0) = 7.5 \text{ keV} \quad B_0 = 4.0 \text{ T}$$

*Plasma Profiles Simulate a Transport Barrier*



$$p(\psi) = p(0)(1 - \psi)^2 \quad H_{\text{ITER-89}} \simeq 2.5$$

$$n(\psi) = p(\psi)/T(\psi) \quad P_{\text{ICRF}} \simeq 5.0 \text{ MW}$$

$$T(\psi) = T(0) \left[ \frac{2}{3}(1 - \psi)^{5/2} + \frac{1}{3}(1 - \psi^8)^{3/2} \right]$$

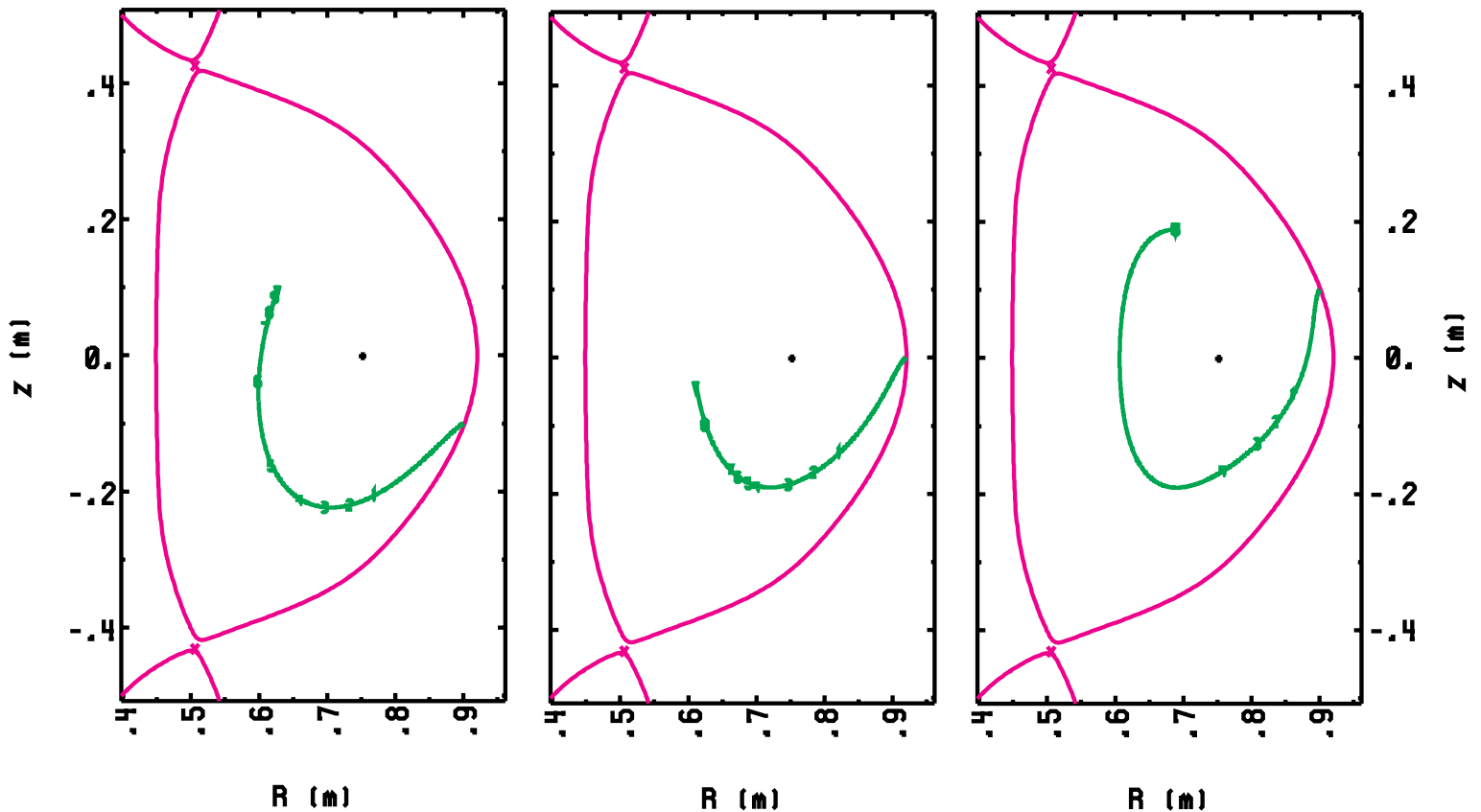
# Reverse Shear Mode Near the $\beta$ -limit ( $\beta_N = 3.0$ )

$$n_e(0) = 2.0 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 7.5 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 5.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 2.5$$

Lower Hybrid Ray Trajectories ( $n_{\parallel}^0 = 2.75$ )

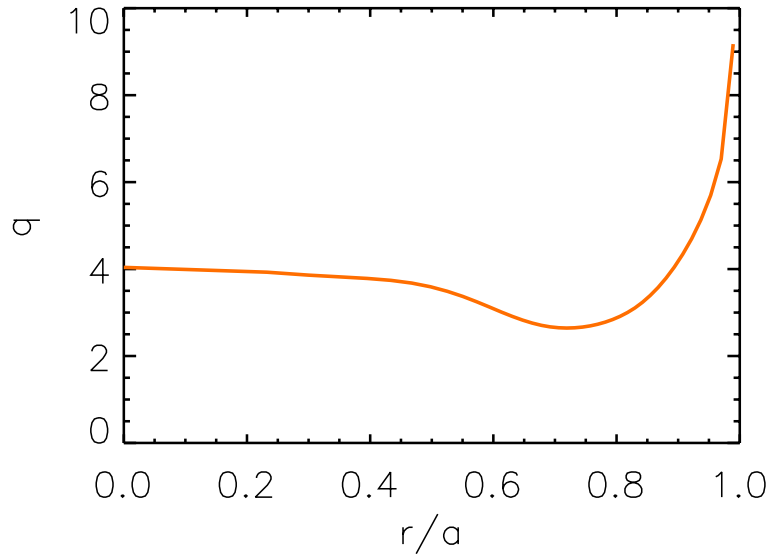
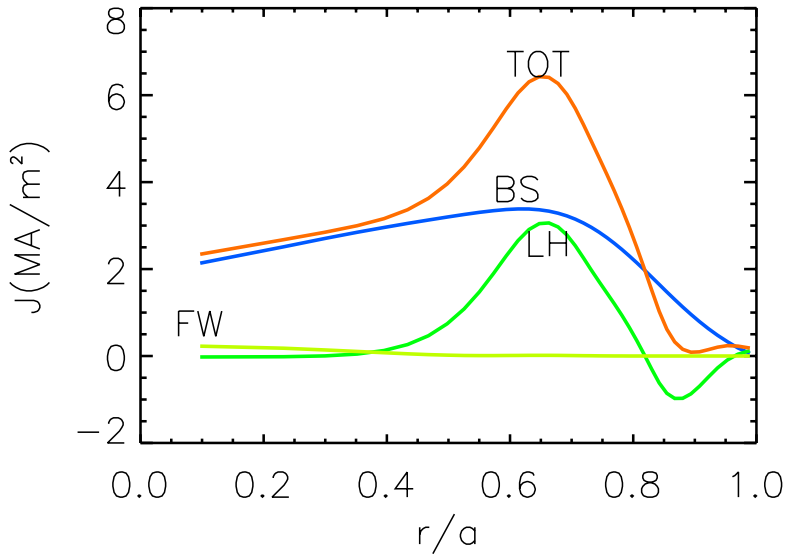
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## Reverse Shear Mode Near the $\beta$ -limit ( $\beta_N = 3.0$ )

$$n_e(0) = 2.0 \times 10^{20} \text{ m}^{-3}, \quad T_e(0) = 7.5 \text{ keV}$$

$$P_{\text{ICRF}} \simeq 5.0 \text{ MW} \quad H_{\text{ITER-89}} \simeq 2.5$$



$$I_p = 0.81 \text{ MA} \quad (f_{\text{BS}} = 0.74)$$

$$I_{\text{LH}} = 0.19 \text{ MA}$$

$$P_{\text{LH}} = 3 \text{ MW} \quad (n_{\parallel}^0 = 3.00)$$

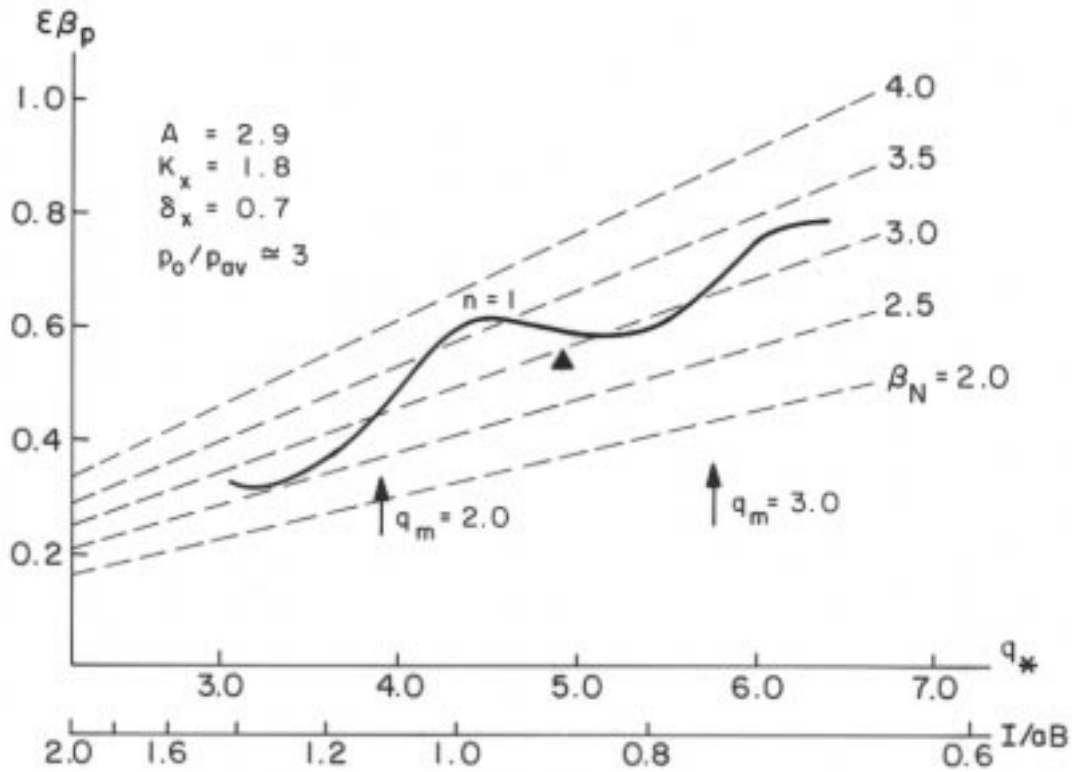
$$q_0 = 3.95 \quad q_{\text{min}} = 2.65$$

$$\beta_t = 2.60\%$$

$$p(0)/\langle p \rangle = 2.90$$

# Ideal MHD Stability Analysis Using PEST-II

Analyze ACCOME equilibrium at  $\beta_N \simeq 3.0$



- Results with  $r_{\text{wall}} = \infty$

$\beta_{N_{\text{crit}}} \simeq 3.7 \rightarrow$  set by  $n = 1$  external kink mode

- Results with  $r_{\text{wall}} = 1.3 a$

$\beta_{N_{\text{crit}}} \simeq 4.5 - 5.0 \rightarrow$  set by  $n = 3$  external mode

# Time Dependent Modelling

## (Work in Progress)

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- Use TRANSP to simulate LH current profile control in experimental discharge with  $I_p$  ramp plus ICRH.

ICRH  $\implies$  FPPRF module

LHCD  $\implies$  LSC Code (D. Ignat)

- **Goals:**

Show that off-axis LHCD can be used to sustain a RS discharge with  $q(\psi) > 2$ .

Study sensitivity of LHCD profile to changes in  $n_e(r, t)$ ,  $T_e(r, t)$ ,  $T_i(r, t)$ .

Use  $\chi_e(r, t)$  from previous TRANSP analysis of a C-Mod shot to predict  $T_e(r, t)$  in presence of LH electron heating.

## TRANSP / LSC Modelling Set-Up

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- $I_p$  ramped up from 200 kA to 800 kA
- ICRF heating of bulk plasma:

$$B_0 = 5.3 \text{ T} \quad f_0 = 80 \text{ MHz}$$

$$\text{D(H)} - (95\%:5\%)$$

- Lower hybrid Current Drive

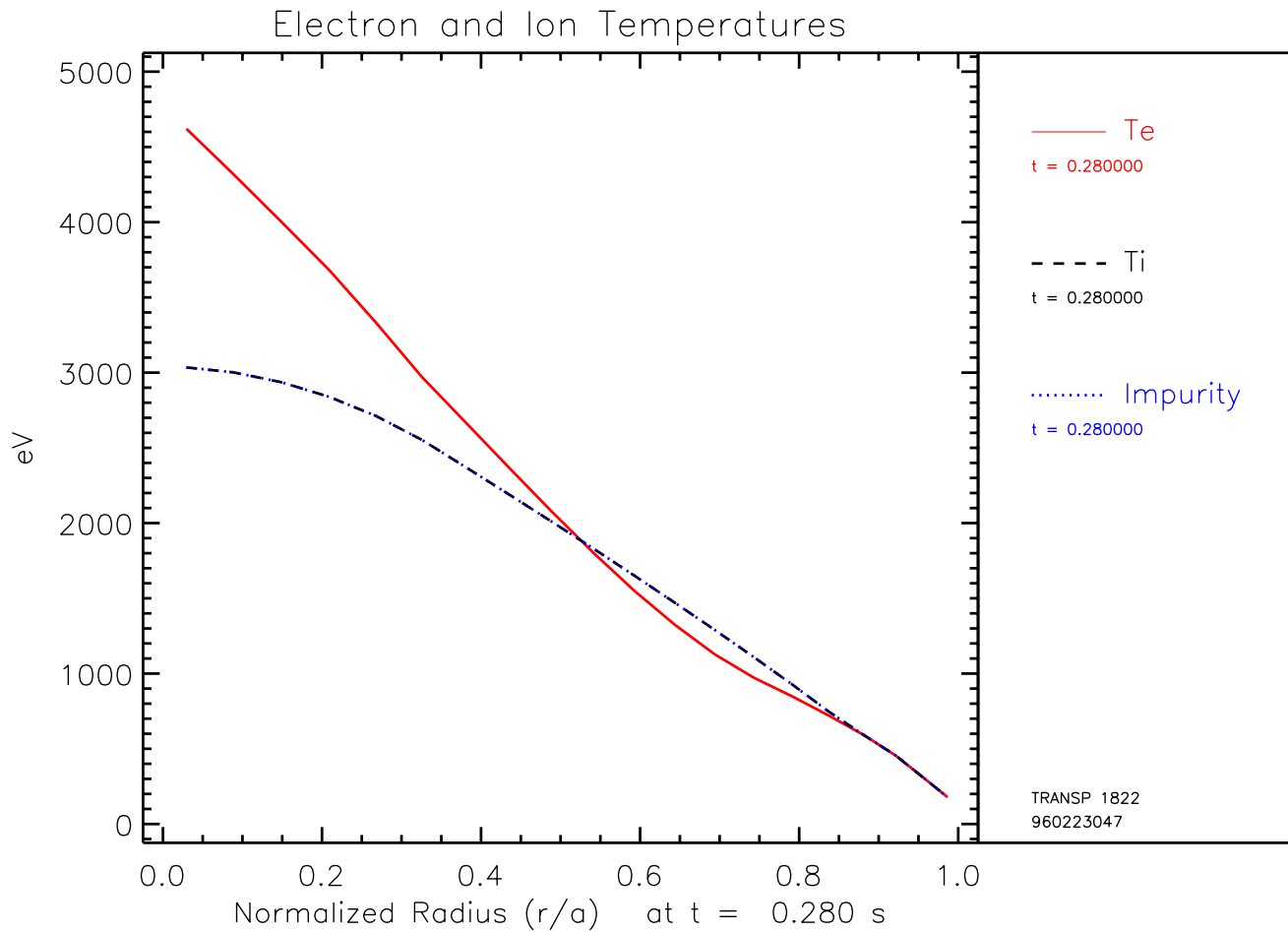
$$f_0 = 4.6 \text{ GHz} \quad P_{\text{LH}} = 2.7 \text{ MW}$$

“Compound” Lower Hybrid Spectrum

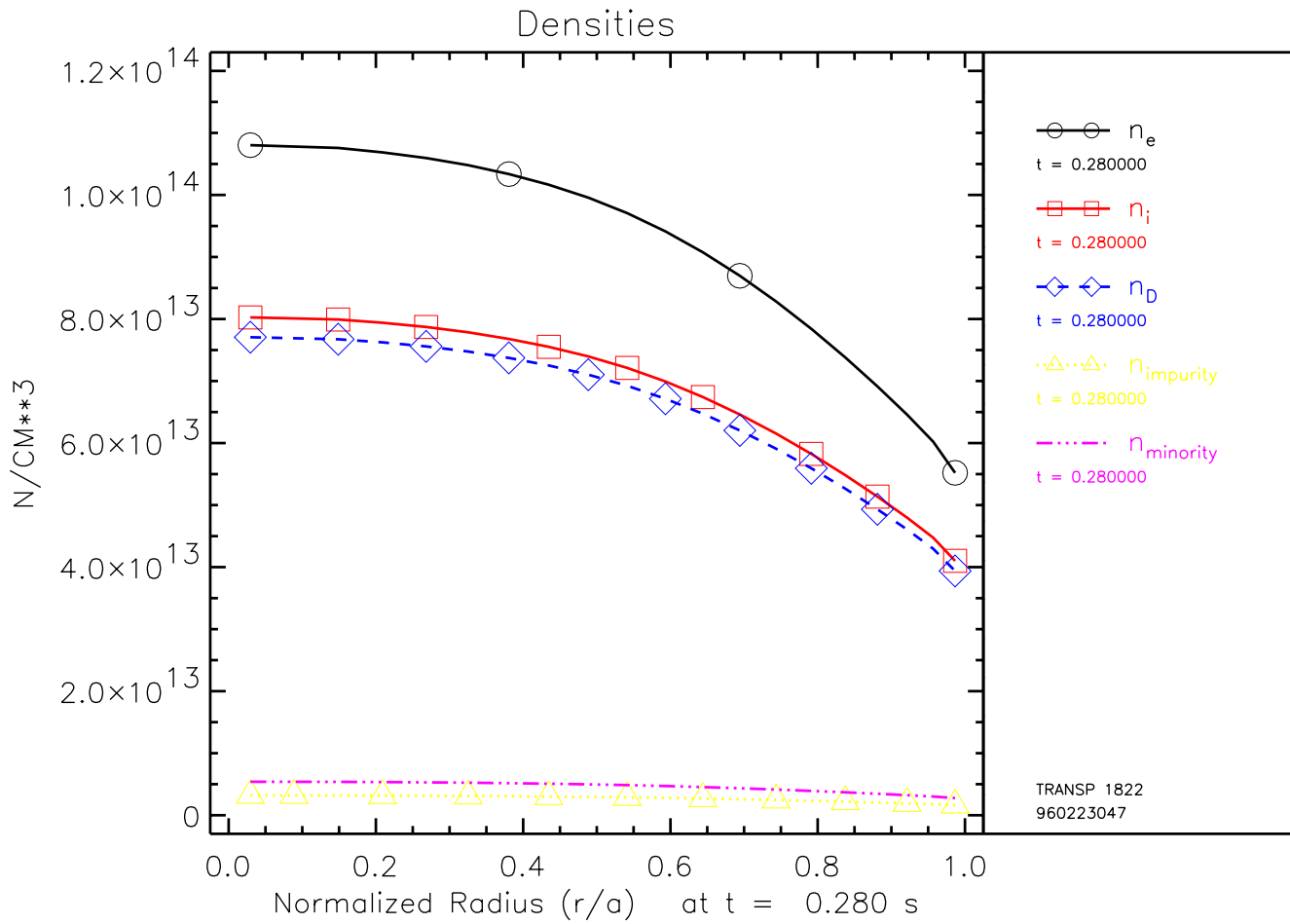
$$\rightarrow P_{\text{LH}}(n_{\parallel} = 2.75) = 2.25 \text{ MW}$$

$$\rightarrow P_{\text{LH}}(n_{\parallel} = 4.00) = 0.45 \text{ MW}$$

# Experimental Temperature Profiles Used in TRANSP / LSC Analysis

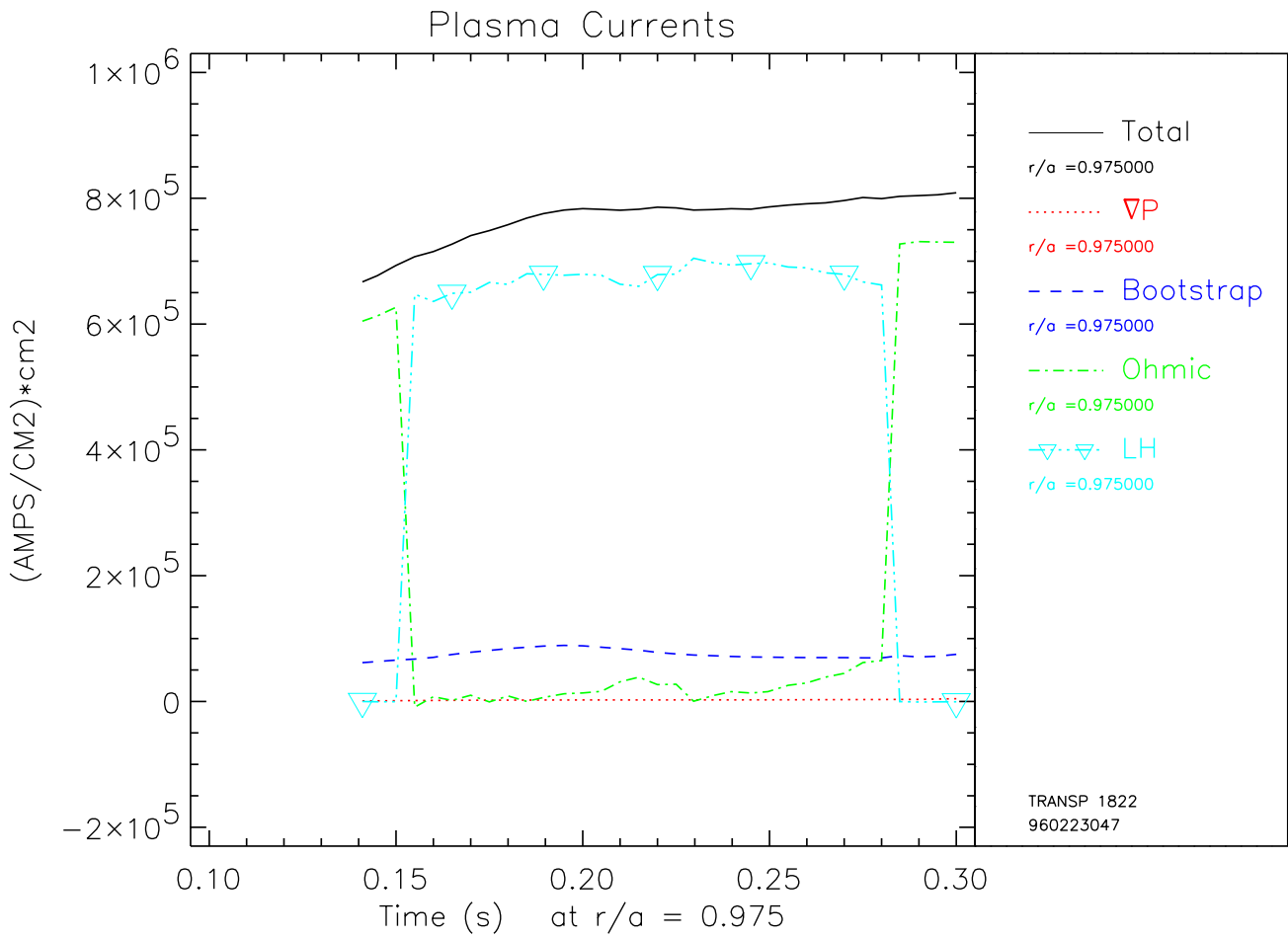


# Experimental Density Profiles Used in TRANSP / LSC Analysis



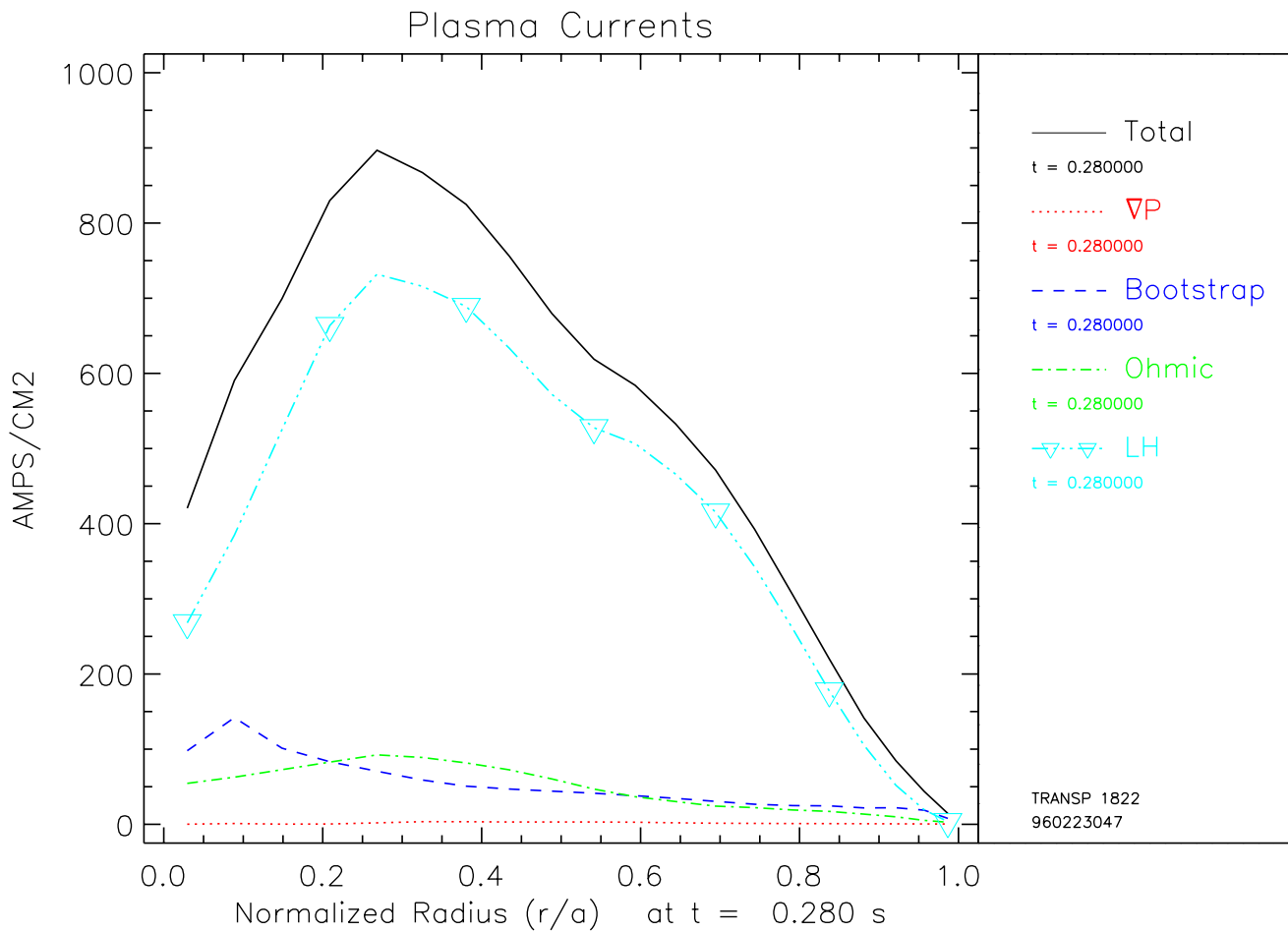
# TRANSP / LSC Modelling - Time Evolution of Currents

$$P_{LH} = 2.7 \text{ MW} \quad f_0 = 4.6 \text{ GHz}$$



# TRANSP / LSC Modelling - Current Density Profiles at 0.28 s

$$P_{LH} = 2.7 \text{ MW} \quad f_0 = 4.6 \text{ GHz}$$



C:\MODELS\TRANSPORT\SCOPES\CURRENTS.MG20

Mon Mar 8 11:56:29 1999

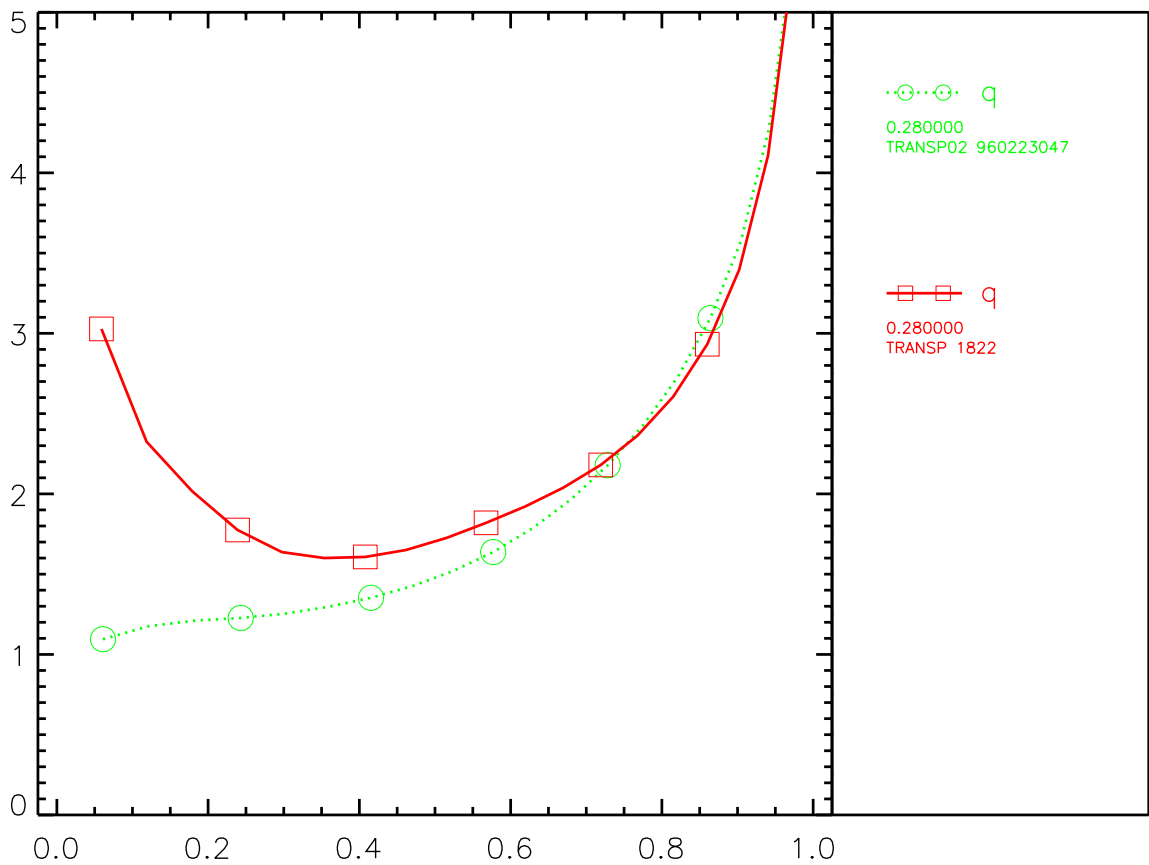
$$I_{LH} = 660 \text{ kA}$$

$$I_{BS} = 70 \text{ kA}$$

$$I_{OH} = 70 \text{ kA}$$

# TRANSP / LSC Modelling - Q-Profiles at 0.28 s

$$P_{LH} = 2.7 \text{ MW} \quad f_0 = 4.6 \text{ GHz}$$



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Solid Curve  $\implies$  OH Ramp + ICRF + LHCD

Dotted Curve  $\implies$  OH Ramp + ICRF Only

## Time Dependent Modelling - Future Work

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- Use  $\chi_e(r, t)$  from TRANSP shot analysis to **predict**  $T_e(r, t)$  with OH ramp plus ICRF plus LHCD.
- Simulate an ITB by assuming:

$$\chi_i(r, t) = \chi_i^{\text{NEO}}, \quad r \leq r(q_{\min})$$
$$\chi_i(r, t) = \chi_i^{\text{ANAL}}, \quad r > r(q_{\min})$$

# ICRF Heating Scenarios for Advanced Tokamak Operation in Alcator C-Mod

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- D(H) @ (4.0 T & 60 MHz)  
(H) – minority heating on-axis
- D( $2\Omega_{3\text{He}}$ ) @ (4.0 T & 80 MHz)  
( $2\Omega_{3\text{He}}$ ) – heating on-axis
- D(H) @ (4.4 T, 60 & 80 MHz)  
(H) – minority heating off-axis  
[ $r/a \simeq (0.35 - 0.45)$ ]

## Conclusions

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- Stationary (time) and time dependent modelling of lower hybrid current drive in Alcator C-Mod indicates that it is a promising technique for off-axis current profile control.
- Reversed shear current density profiles can be maintained using 3 MW of off-axis LHCD power as the plasma evolves from start up ( $\beta_N \simeq 1.0$ ).
- Strong plasma shaping in C-Mod has been found to result in increased ideal MHD  $\beta$ -limits relative to circular and elliptical plasmas.
- Time dependent modelling using TRANSP & LSC is now underway to determine the sensitivity of the LHRF current drive physics and system design to changes in plasma density and electron temperature.