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Progress in understanding error-field physics in NSTX spherical torus plasmas

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J.E. Menard, PPPL
for the NSTX Research Team

Error Field Workshop
Friday, November 16, 2007
Rosen Centre Hotel - Orlando, Florida

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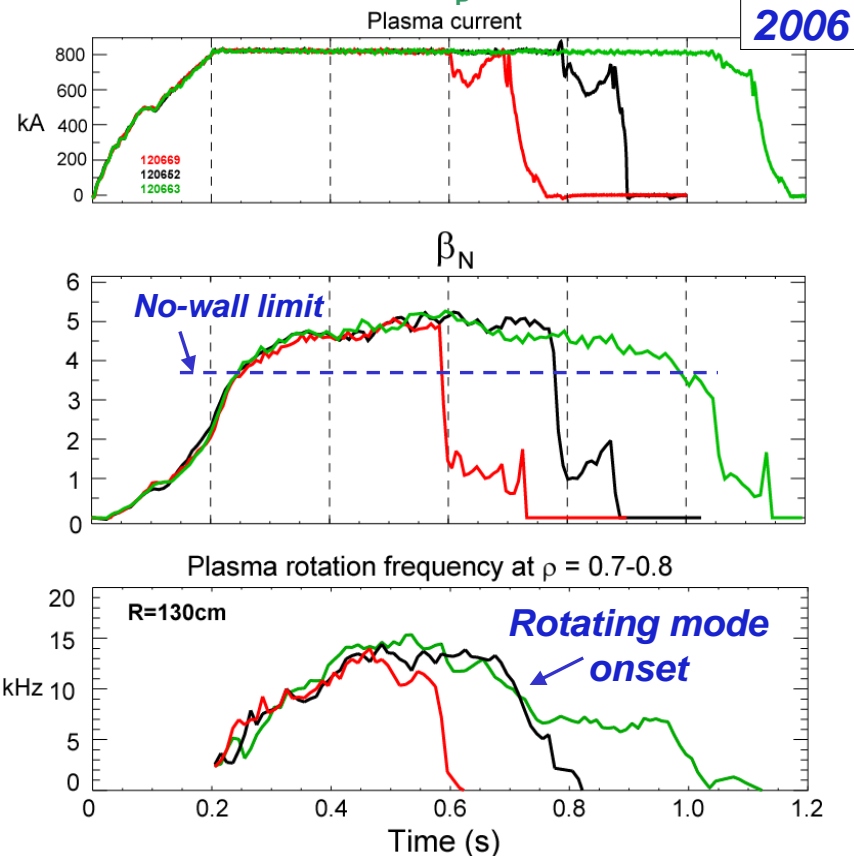
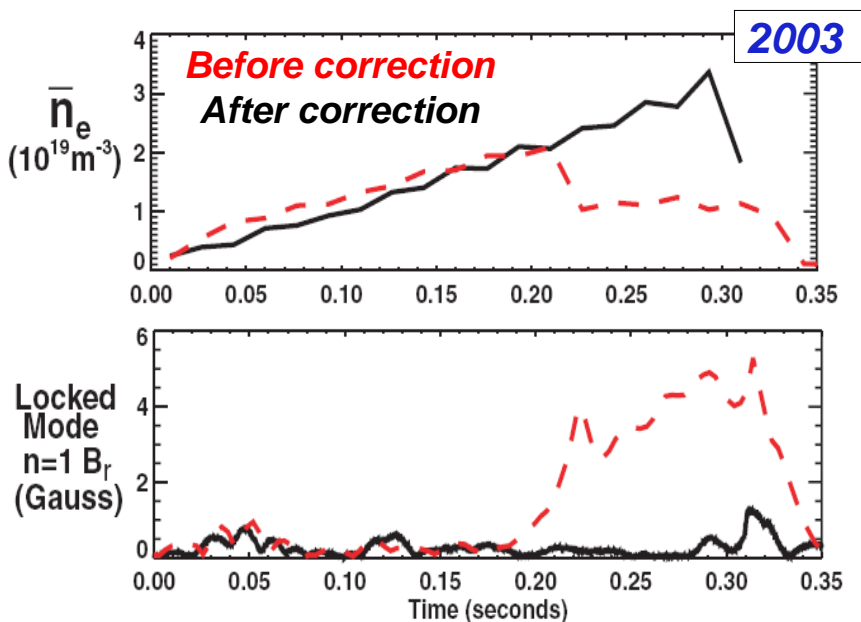
Detection and correction of small (<0.1%) low-n deviations from axisymmetry can significantly improve plasma performance



- Correction of n=1 PF coil error fields allowed stable operation at low density w/o mode locking

- Correction of n=1 TF coil error field → extended stable operation with $\beta > \beta_{\text{no-wall}}$

- **No error field control during high β_N phase**
- **TF-EFC**
- **TF-EFC + active n=1 B_p feedback**

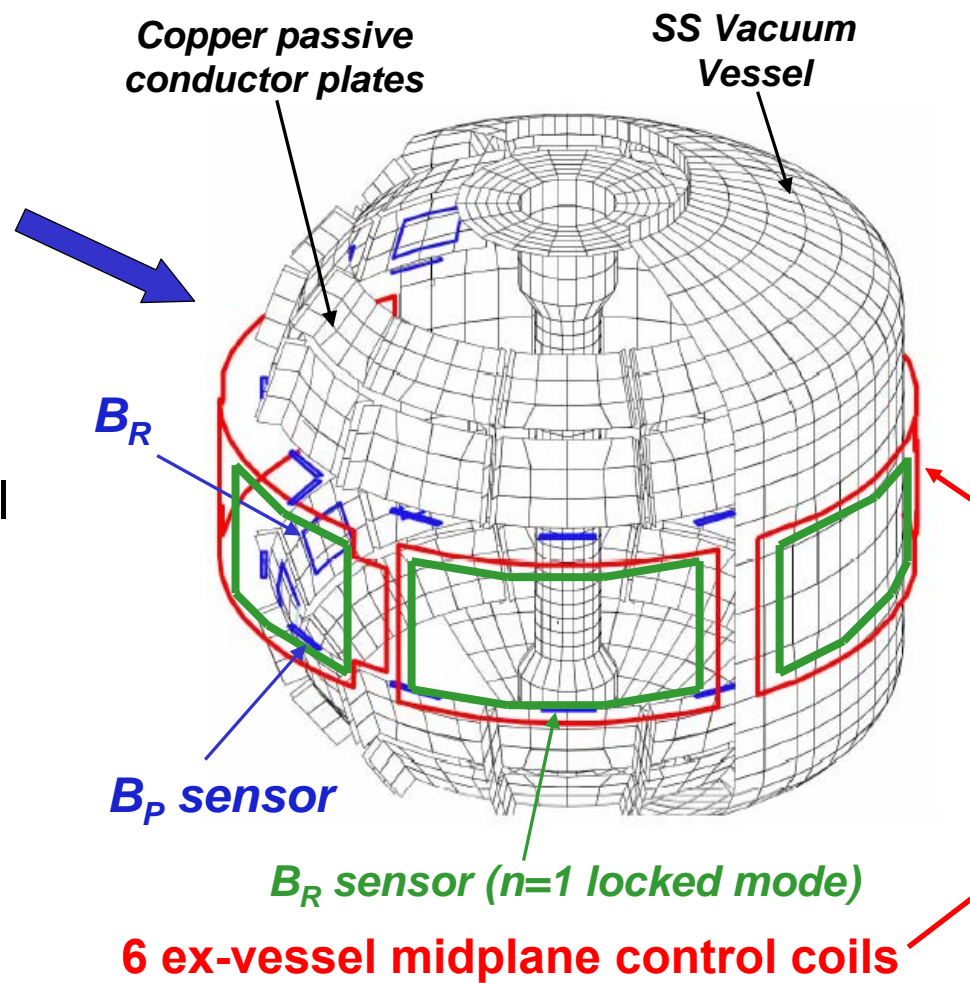


- Subsequently, sustained high- β operation was routinely achieved, however rotation decay during discharge still observed

Effective EF and RWM control relies heavily on robust detection of small ($\sim 1\text{G}$) non-axisymmetric magnetic fields



- NSTX has powerful low-f mode detection capabilities:
 - 54 sensors, 2 components of B :
 - 30 radial (B_R) and 24 poloidal (B_P)
 - 6 B_R 's are ex-vessel saddle coils
 - Toroidal mode-numbers $n=1, 2, 3$
 - Only $n=1$ used in real-time thus far
- In FY06 only B_{P-U} used for control
 - Limited by available run time
- In FY07 several new RWM/EF sensor combinations tested :
 - $B_{P-U} + B_{P-L}$
 - $B_{R-U} + B_{R-L}$
 - $B_{P-U} + B_{P-L}$ with spatial offset
 - All sensors in combination
- $B_{P-U} + B_{P-L}$ discussed in this talk



VALEN Model of NSTX (Columbia Univ.)

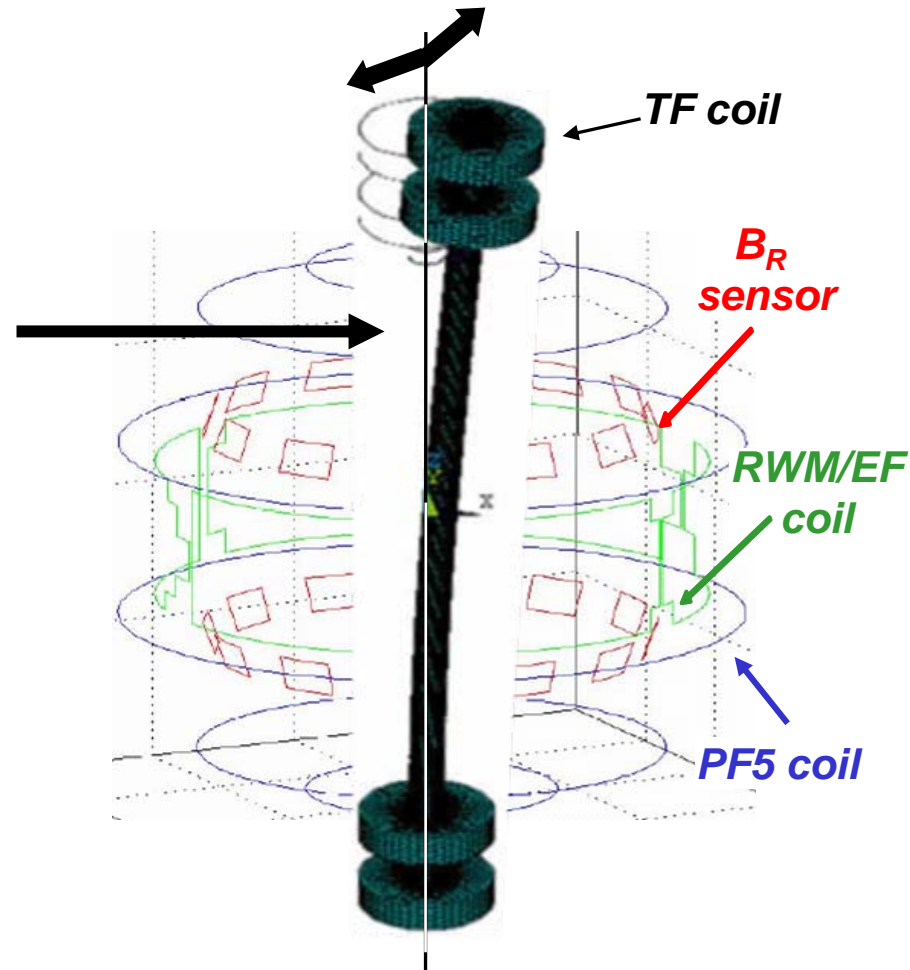
The NSTX low-frequency mode detection system has been instrumental in identifying vacuum error fields



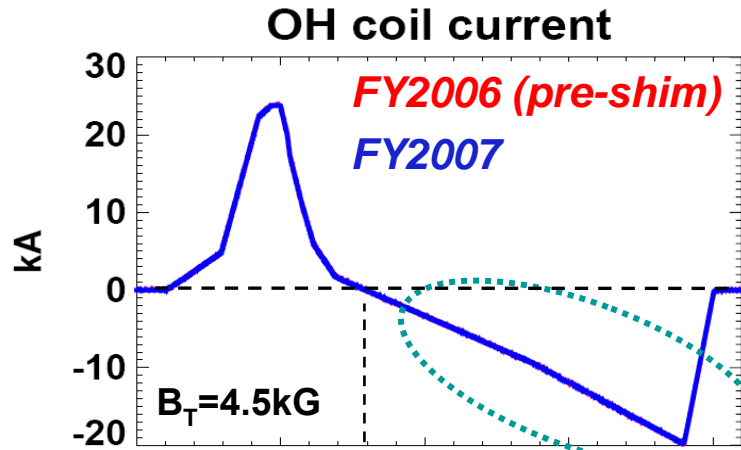
Error field detection & correction timeline:

- **2001** – Primary vertical field coil (PF5) identified as $n=1$ EF source, and was corrected in 2002 → sustained high β
- **2006** – Determined force (from OH leads) at top of machine induces **TF coil motion 1-2 mm at midplane relative to PF coils** → $n=1$ B_R EF at outboard midplane
- **2007** – shimmed TF w.r.t. OH to minimize relative motion of OH and TF
 - $n=1$ EF reduced, but not eliminated
- **2008-2009** – will improve connections at OH lead area to reduce forces and EF

(Displacement exaggerated to show tilting motion)

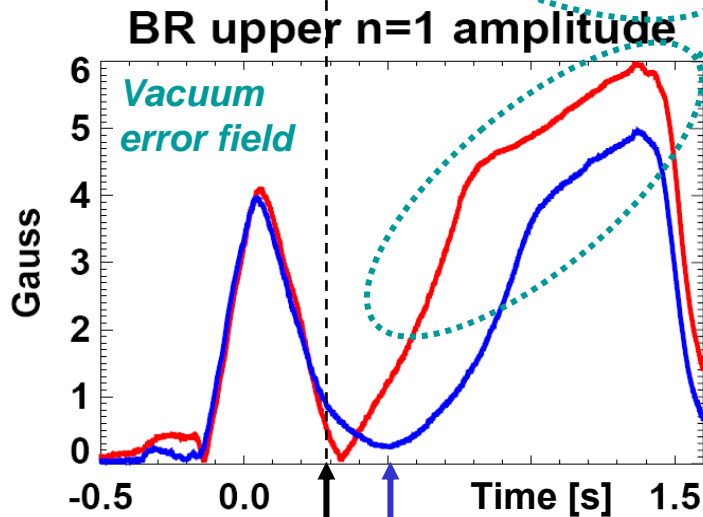


$n=1$ EF from TF coil motion is $\propto I_{OH} \times I_{TF}$, but has additional time lags and non-linearities which complicate correction

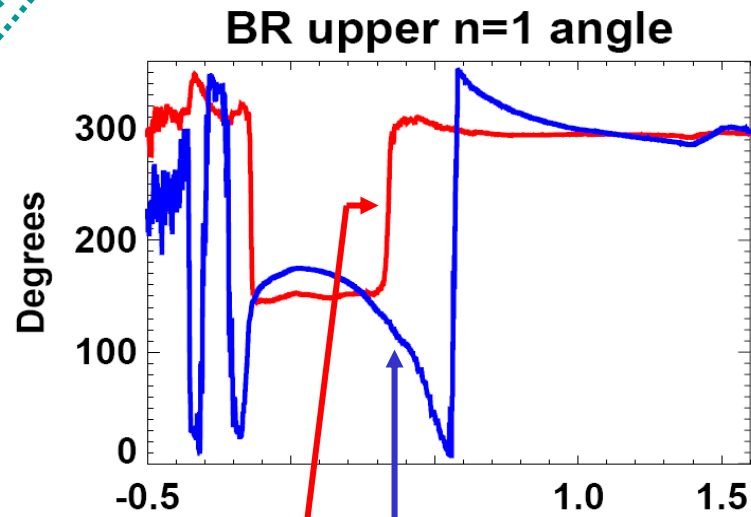


TF motion produces 4-6 Gauss peak $n=1$ EF at outboard side of vessel

EF amplitude changes slope with linear I_{OH} ramp at fixed I_{TF}



OH zero crossing precedes minimum EF by 0.2s



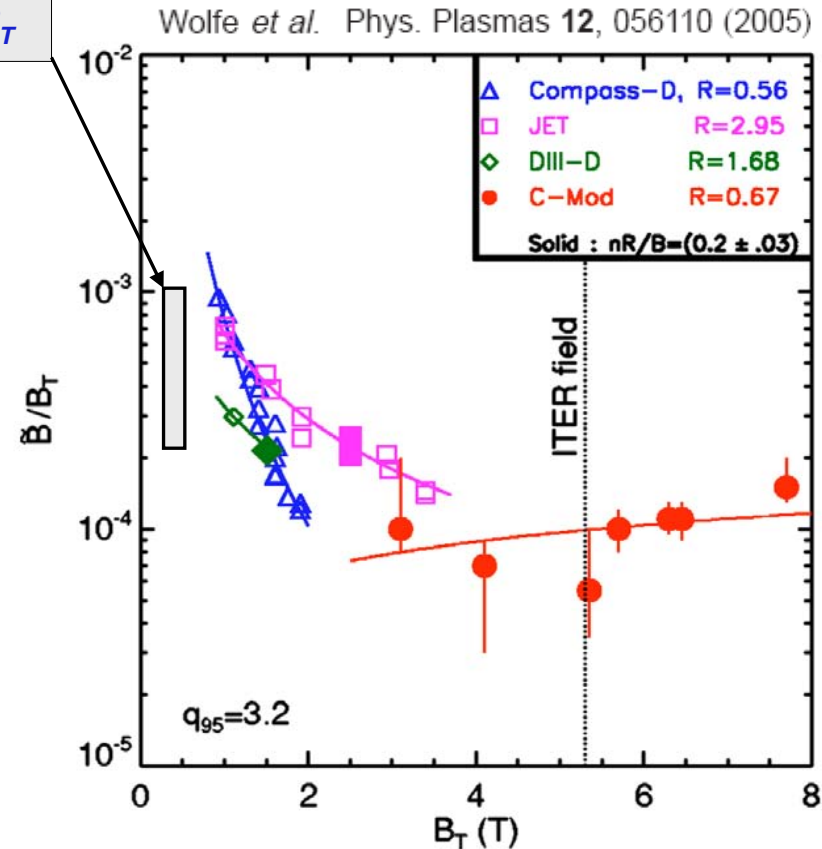
EF phase flips more slowly and in opposite direction following shimming

NSTX locked mode (LM) studies test locking theories in an extended parameter regime, and establish scalings for the ST



NSTX LM data extends database to low B_T

- **OHxTF EF model used to estimate the intrinsic EF in calculation of total**
- Linear $n=1$ EF ramp applied by EF coils to induce LM – detect w/ magnetics
- Span factor of 4 in $n_e = 0.5 - 2 \times 10^{19} \text{m}^{-3}$
- Span nearly factor of 2 in $B_T = 3 - 5.5 \text{kG}$
- Best fit to data obtained using core shear variable $dq/d\rho|_{q=2}$
 - Commonly used q_{95} not well correlated with shear due to $q_0 > 1$ (no sawteeth)



NOTE: Scaling form used here: $B_{21}(\text{lock}) / B_T \propto n^{\alpha_n} B_T^{\alpha_B} q^{\alpha_q} R^{\alpha_R}$

Analysis of error fields has improved significantly with recent Ideal Perturbed Equilibrium Code - IPEC (from DCON+VACUUM)



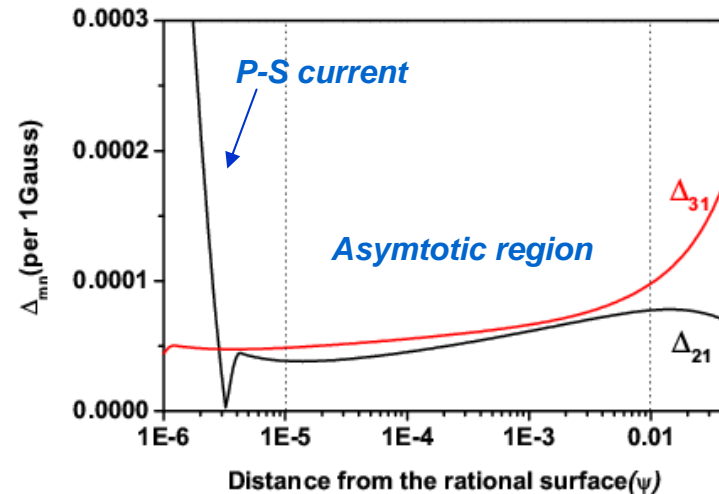
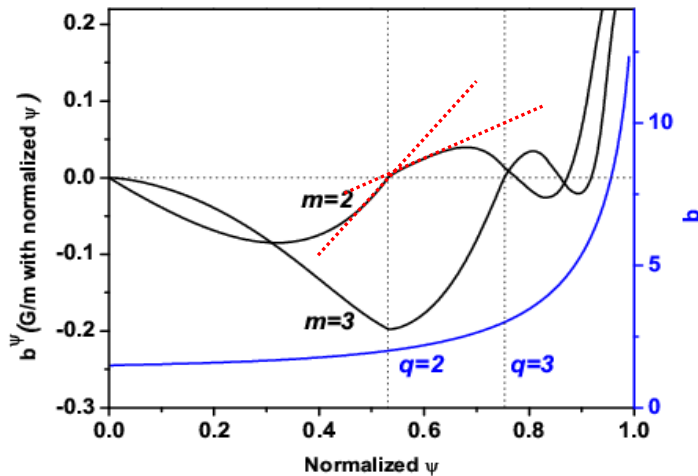
- ❑ IPEC finds perturbed equilibrium $\vec{f}_{ideal}(\vec{\xi}) = \vec{0} = \vec{\nabla}\delta p + \delta\vec{J} \times \vec{B} + \vec{J} \times \delta\vec{B}$ from an axisymmetric equilibrium $\vec{\nabla}P = \vec{J} \times \vec{B}$ given an external perturbation $\delta\vec{B}^x$
- ❑ Ideal MHD constraint does not allow islands, so 3D equilibrium has singular currents to preserve magnetic topology - $(\delta\vec{B} \cdot \vec{\nabla}\psi)_{mn} = 0$ at $q = m/n$

$$\Delta_{mn} = \left[\frac{\partial}{\partial\psi} \left(\frac{\delta\vec{B} \cdot \vec{\nabla}\psi}{\vec{B} \cdot \vec{\nabla}\phi} \right) \right]_{mn} \rightarrow \vec{j}_s = \frac{\Delta_{mn} i m e^{i(m\theta - n\phi)}}{\mu_0 n^2 \left(\oint dS B^2 / |\vec{\nabla}\psi|^3 \right)} \delta(\psi - \psi_{mn}) \vec{B} \rightarrow (\delta\vec{B} \cdot \hat{n})_{mn}$$

Jump of derivative of radial field

Parallel singular current preventing magnetic islands from opening

Total resonant B_{\perp} driving magnetic islands (w/o rotation)



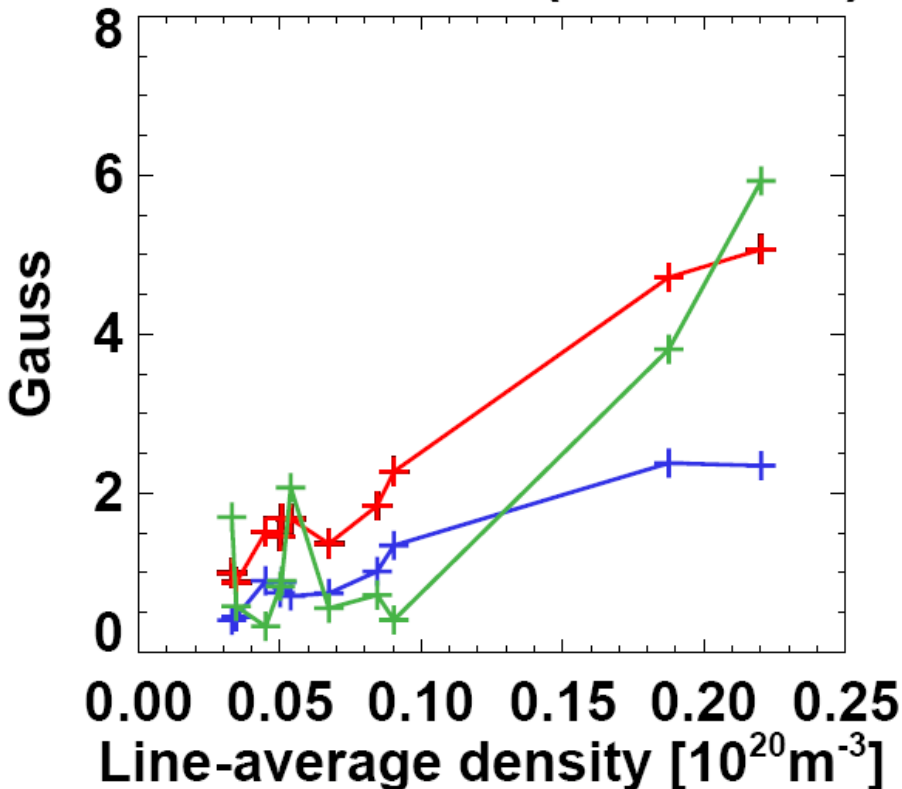
• IPEC: J.-K. Park, PoP 052110 (2007), Locked mode: J.-K. Park, PRL 195003 (2007)

Locking field from IPEC ($\delta B_{\perp}^{2,1}$ at $q=2$) exhibits more deviation from density linearity than vacuum field calculations

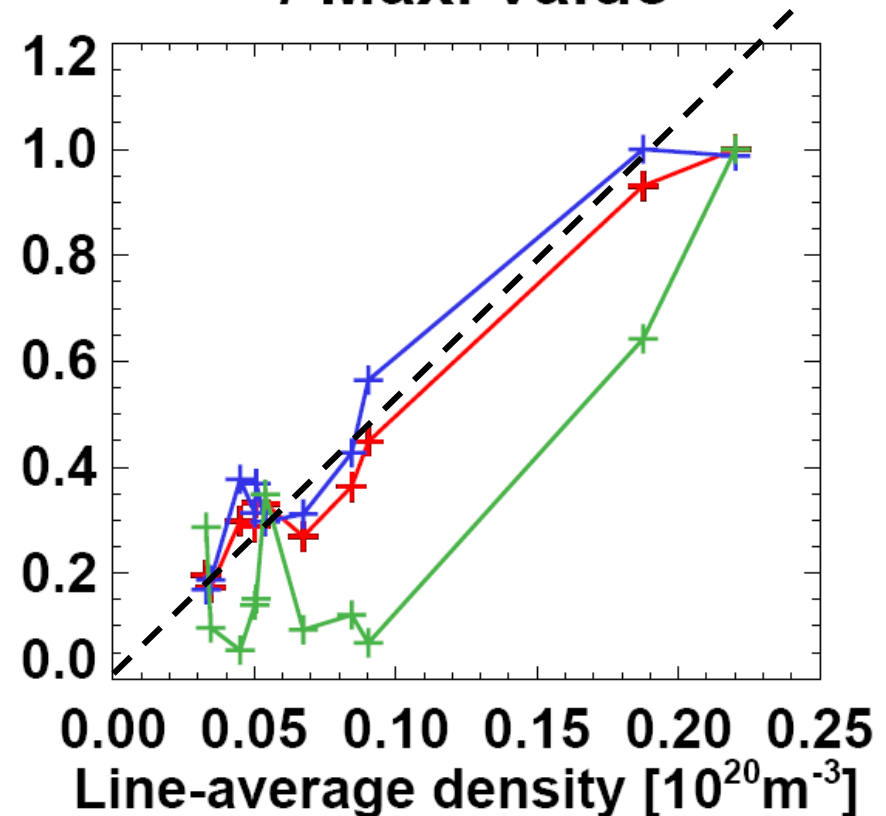


Vacuum δB_{\perp} (most commonly used)
Vacuum perturbed helical flux $\delta \psi_h$
Include plasma response (IPEC)

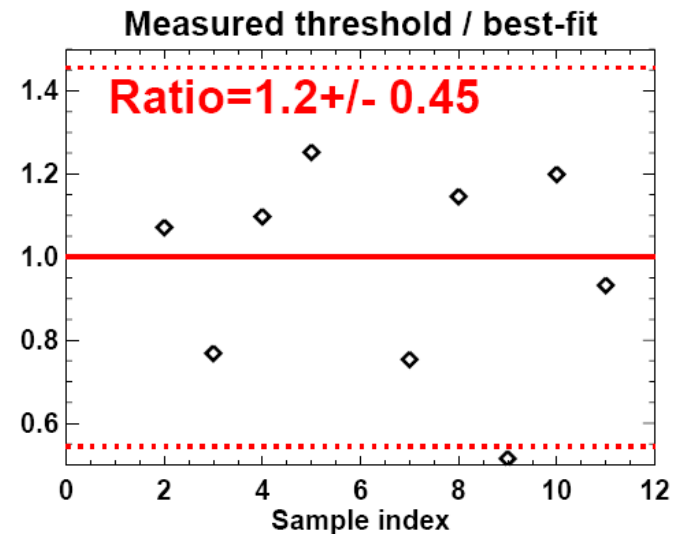
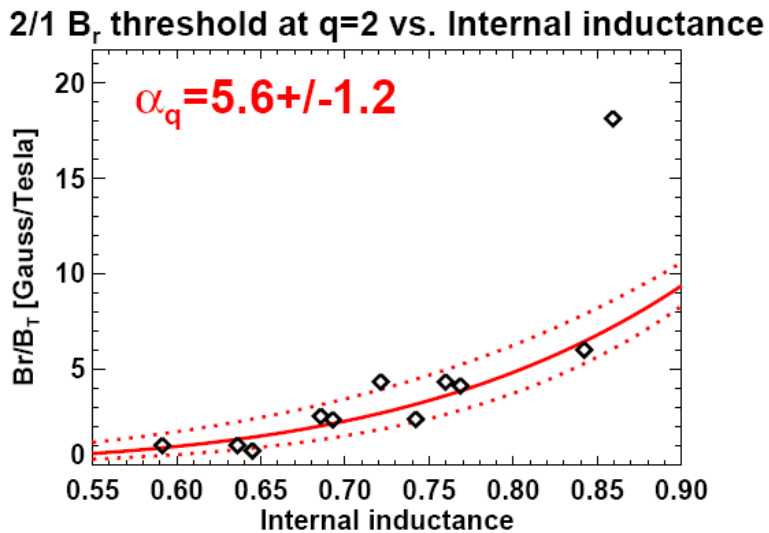
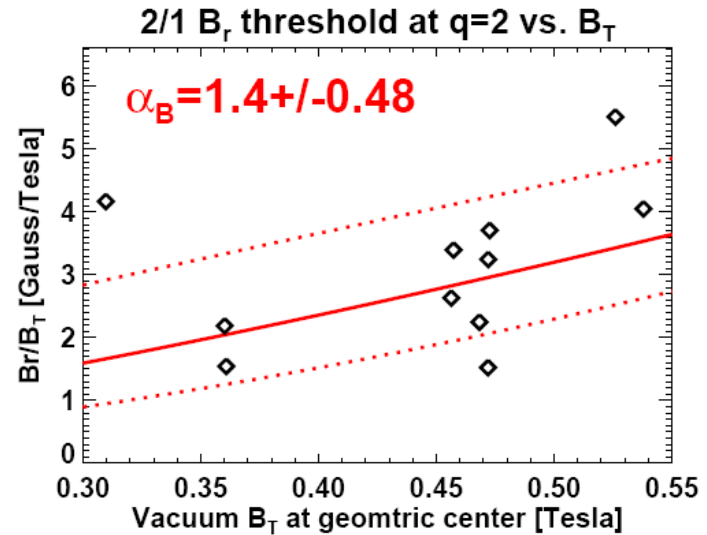
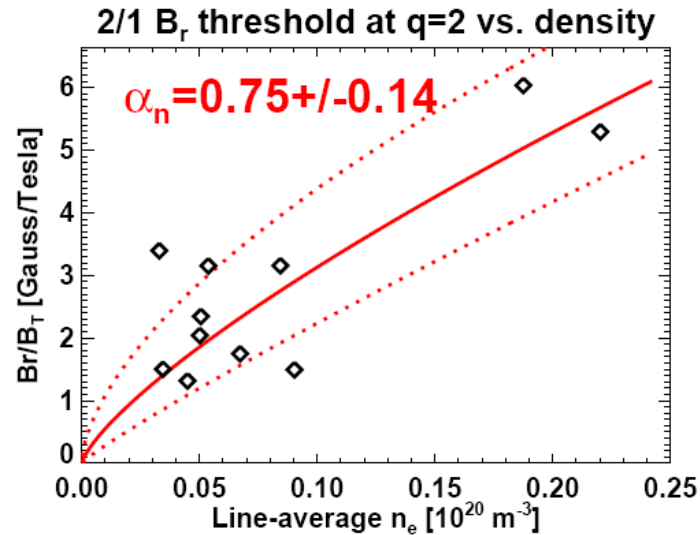
Resonant $\delta B(n=1, m=2)$



Resonant $\delta B(n=1, m=2)$ / Max. value

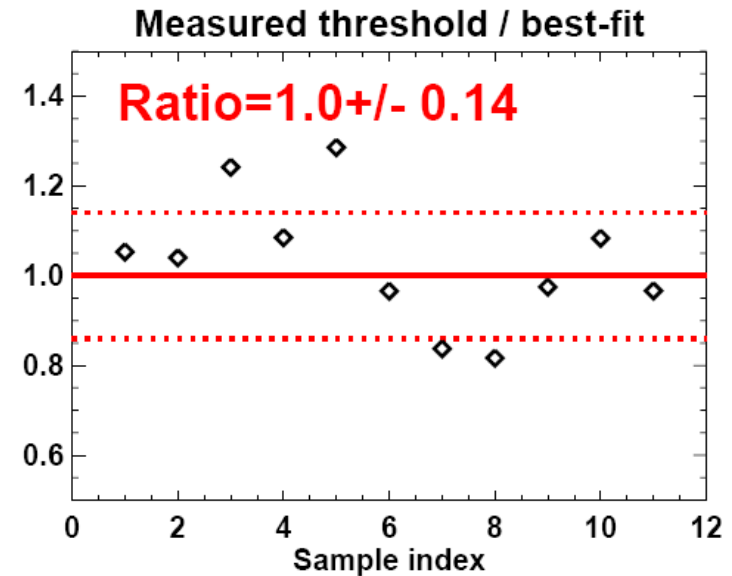
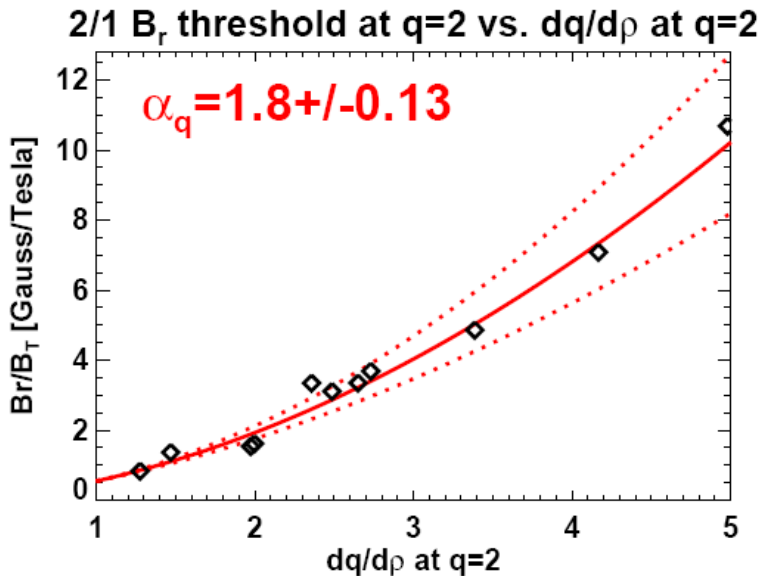
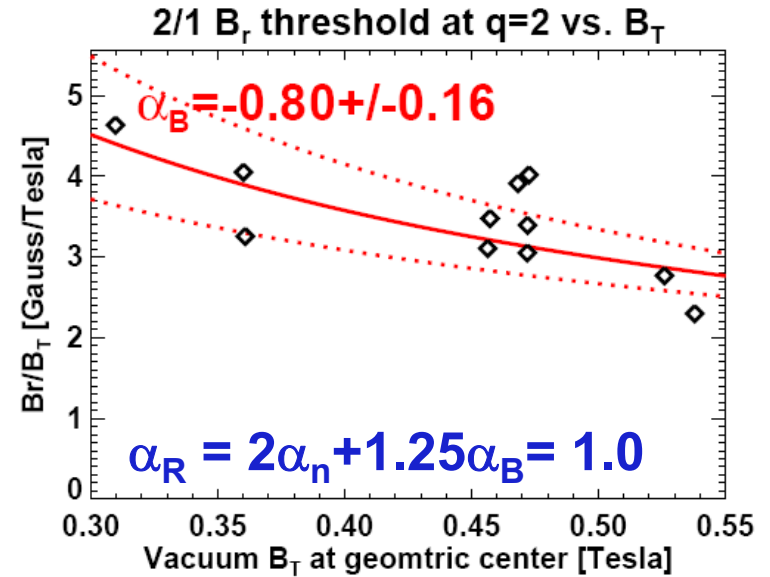
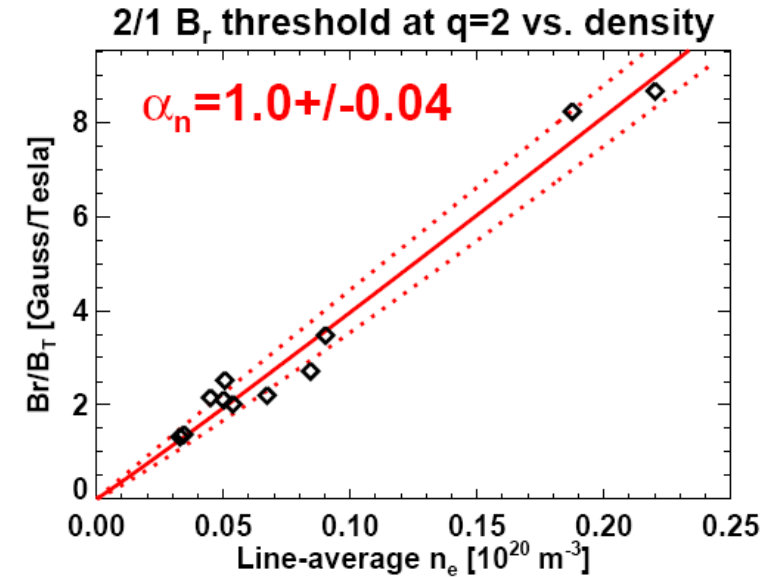


Locking threshold fit using IPEC $\delta B_{\perp}^{2,1}$ at $q=2$ cannot be well fit using internal inductance for q -shear variable

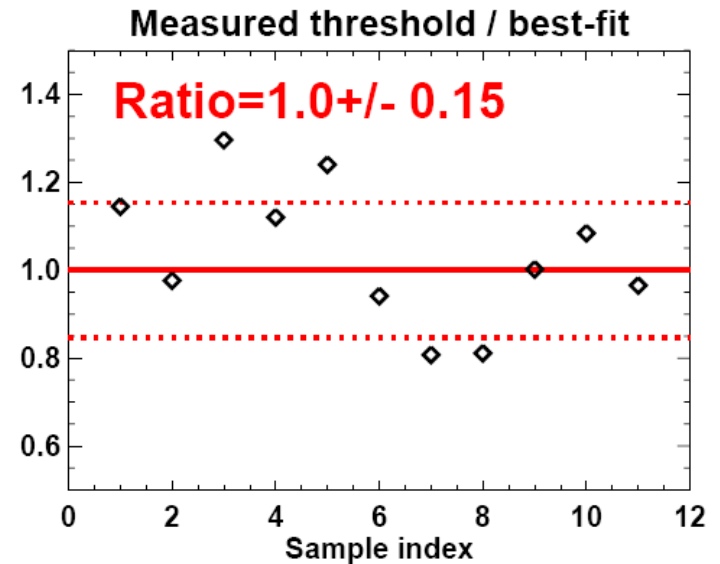
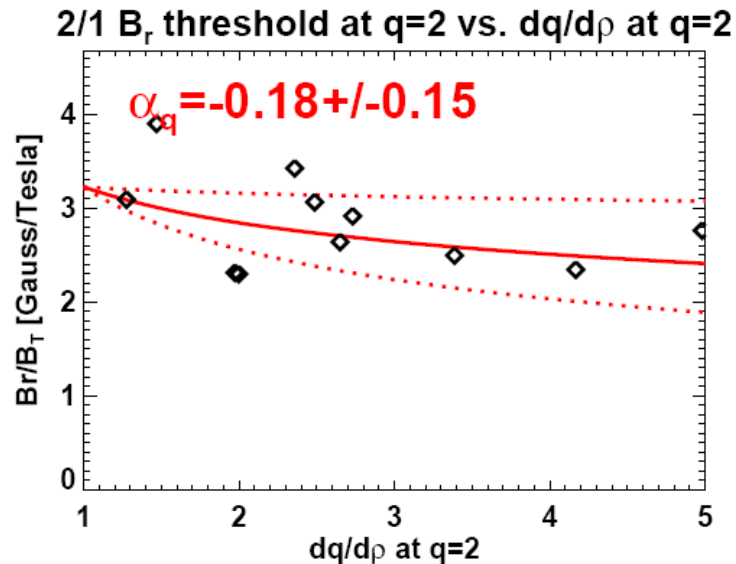
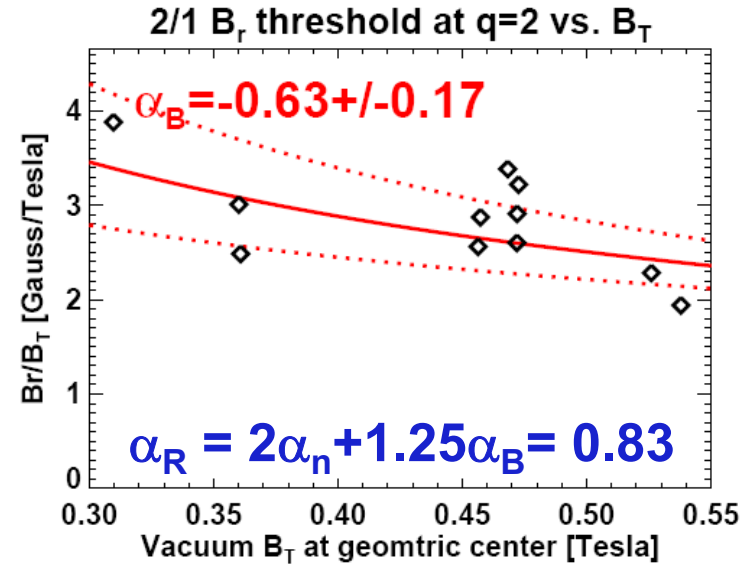
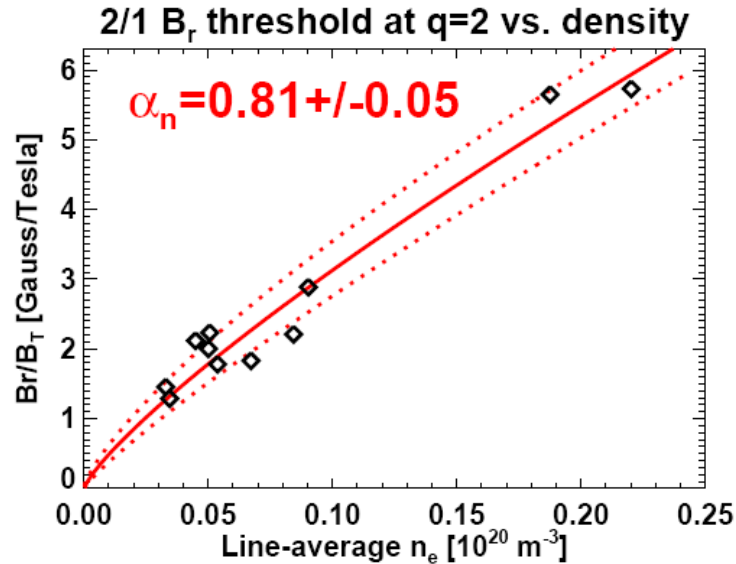


- Similar poor fit obtained using q_{95}

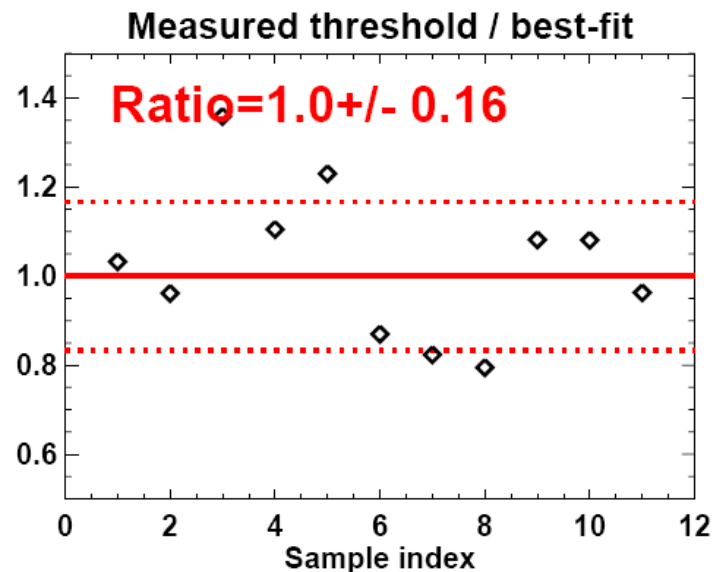
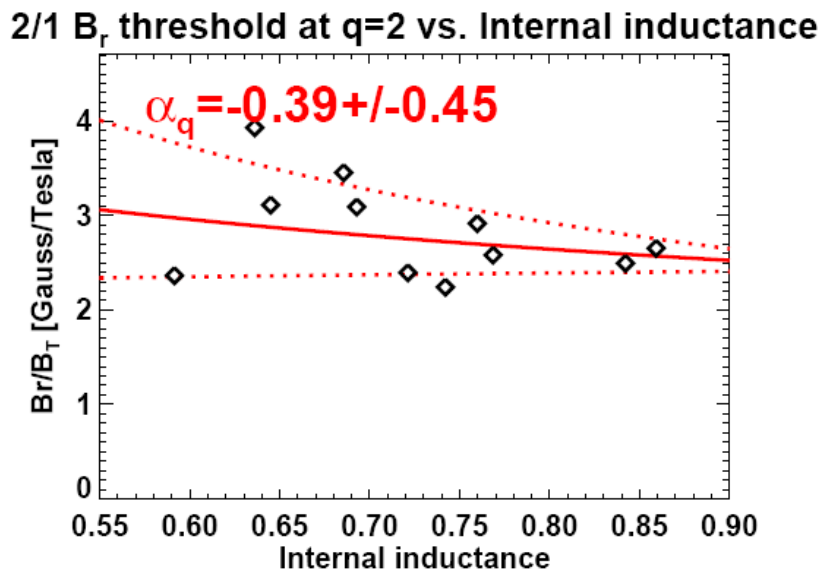
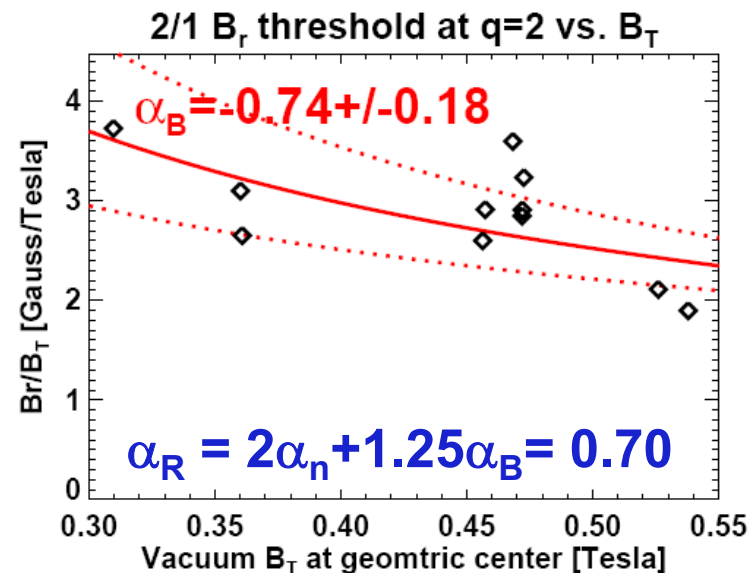
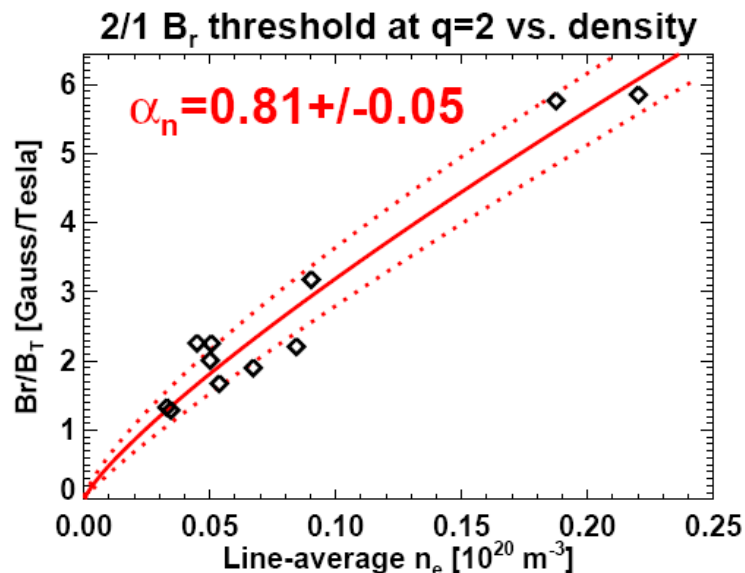
Locking threshold fit using IPEC $\delta B_{\perp}^{2,1}$ at $q=2$ has lowest fitting error if local shear at $q=2$ is used for q -shear variable



Locking threshold fit using vacuum $\delta B_{\perp}^{2,1}$ at $q=2$ has reduced α_n , $|\alpha_B|$, α_R and much weaker dependence on $dq/d\rho|_{q=2}$



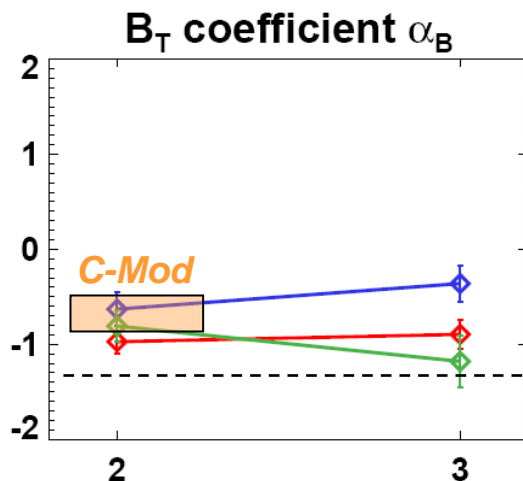
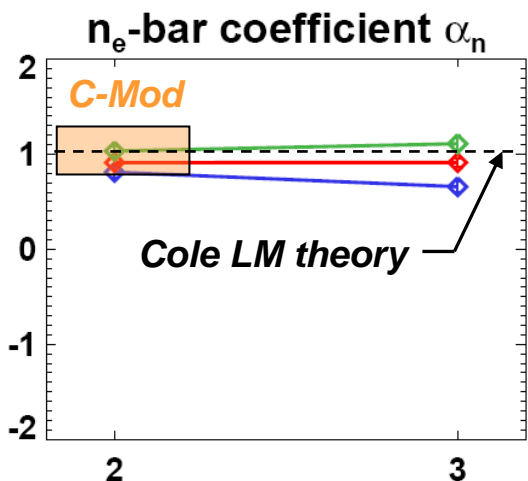
Unlike IPEC case, locking threshold fit using vacuum $\delta B_{\perp}^{2,1}$ at $q=2$ can be fit using internal inductance for q-shear, but $\alpha_R \ll 1$



NSTX data shows linear density scaling and inverse B_T dependence consistent with higher-A, B_T tokamaks and recently improved LM theory



Data also allows assessment of impact of different calculations of perturbed B-field:



Vacuum δB_{\perp} (most commonly used)
Vacuum perturbed helical flux $\delta \psi_h$
Include plasma response (IPEC)

Assume size scaling coefficient:

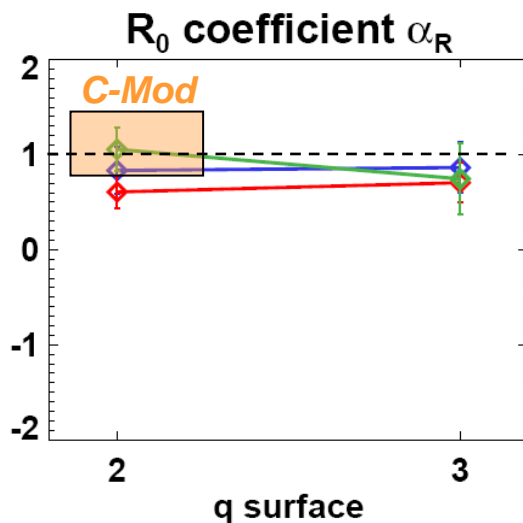
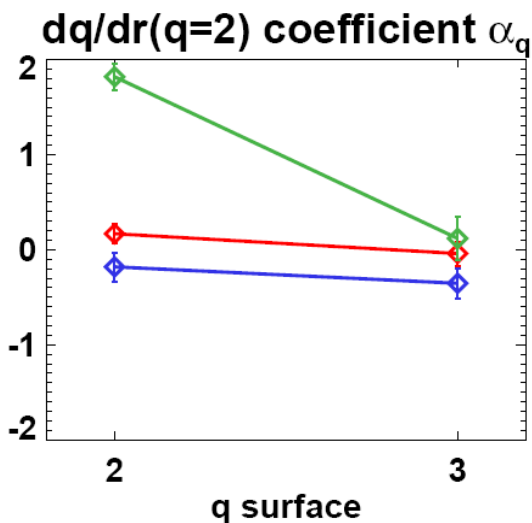
$$\alpha_R = 2\alpha_n + 1.25\alpha_B$$

(Connor-Taylor invariance)

Mean coefficients using q=2 and 3:

$\alpha_n = 0.73$	$\alpha_B = -0.50$	$\alpha_R = 0.85$
$\alpha_n = 0.91$	$\alpha_B = -0.93$	$\alpha_R = 0.66$
$\alpha_n = 1.07$	$\alpha_B = -0.99$	$\alpha_R = 0.90$

IPEC-derived coefficients are the most consistent with recent theory by A. Cole:



$$\left| \frac{b_{r,nm}^{vac}}{B_{\phi}} \right|_{crit} \propto n_e B_{\phi}^{-1.3} R_0 \tau_V^{-1/2} \sigma.$$

PRL 99, 065001 (2007)

Extrapolation to ITER from NSTX data illustrates the importance of the plasma response, and has favorable projection for ITER

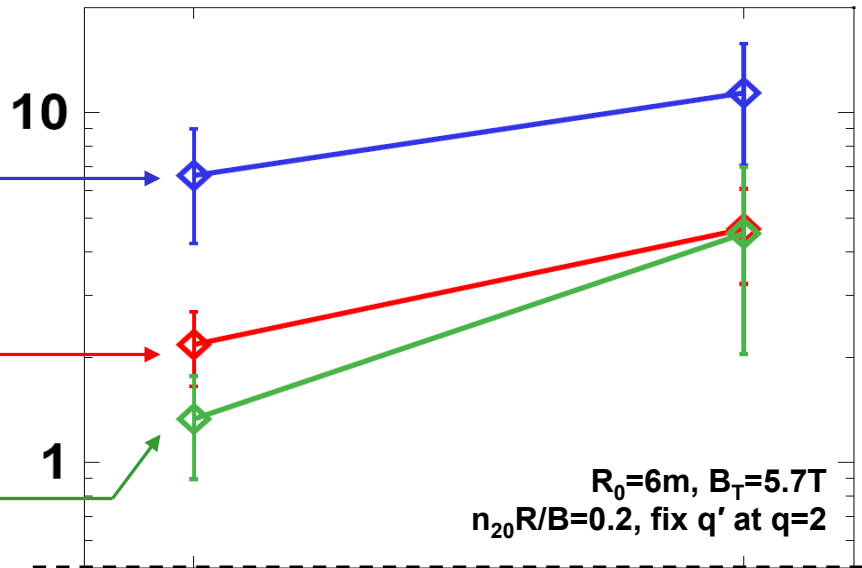


Vacuum δB_{\perp}^{mn} (most commonly used) threshold **2-5 × higher** than IPEC
 → Vacuum δB_{\perp}^{mn} **not valid** for NSTX

Vacuum $\delta \psi_h^{mn} \propto (|\nabla \psi| R^2 B_{\perp})^{mn}$ threshold **1-2 × higher** than IPEC

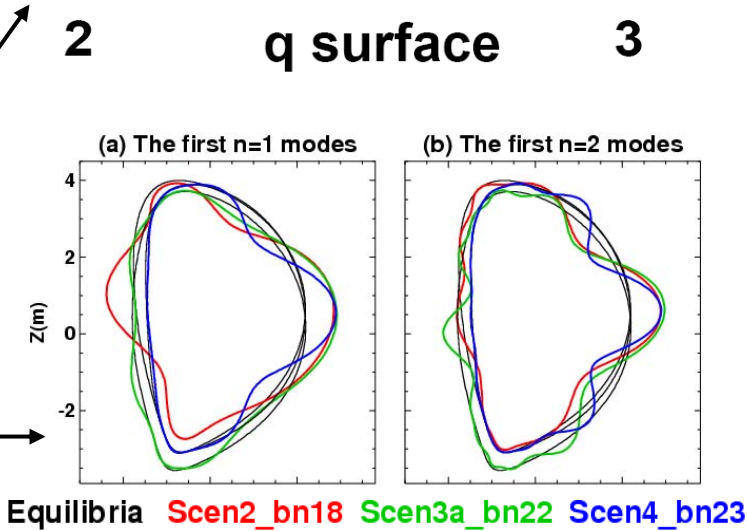
Include plasma response (IPEC)

ITER Threshold B_r/B_T [G/T]

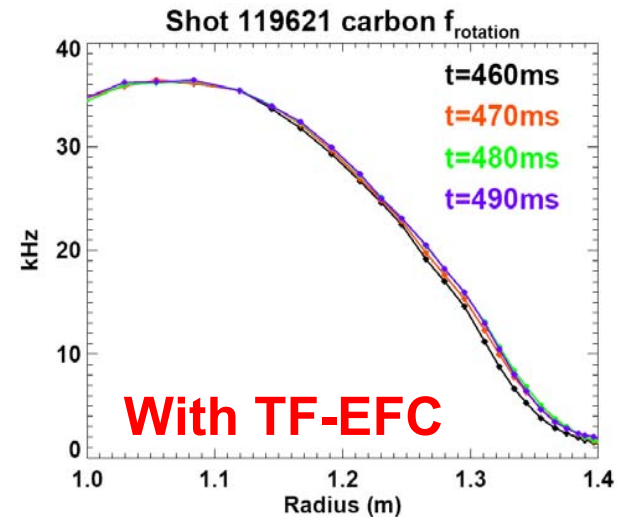
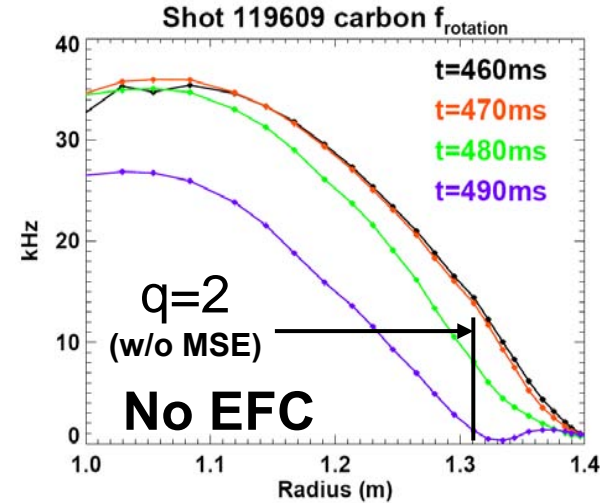
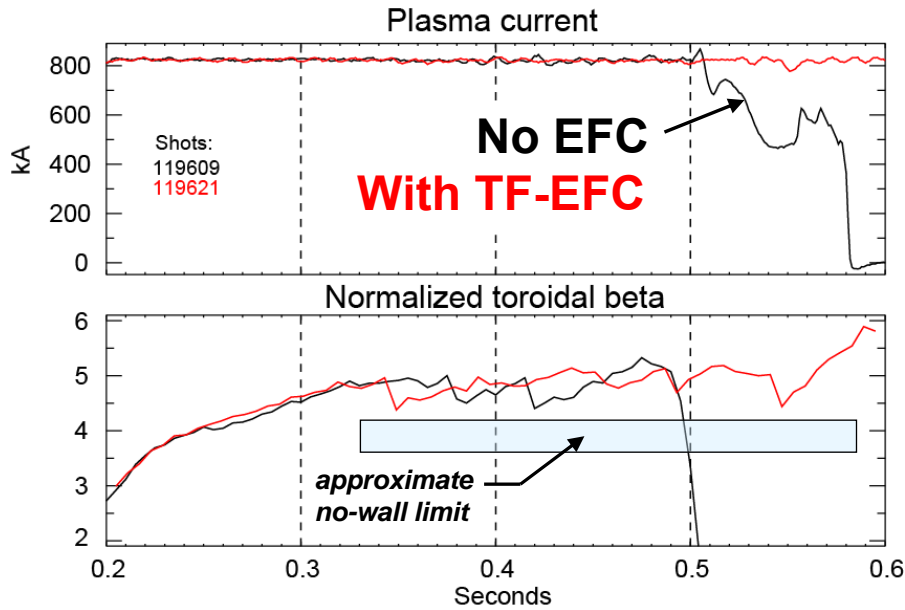


Minimum threshold $B_r/B_T = 1-4$ G/T is **2-3× higher** than minimum EF correction capability of ITER (**favorable result**)

Beginning to use IPEC to model optimal multi-scenario EF mitigation for ITER



At high β , EF correction can aid sustainment of high toroidal rotation needed for passive (rotational) stabilization of the RWM



- Use real-time $I_{\text{OH}} \times I_{\text{TF}}$, incorporate observed time-lag and non-linearity of EF
- Empirically minimize rotation damping near $q=2-3$ for 100-200ms of reference shot
 - Extrapolate in time, balance $m=2$ against $m=0$ (**non-resonant!**) of EF from moving TF
 - Correction coefficients must be altered for different $q(\rho, t)$, startup, shape, etc.

Algorithm did not work well in 2007 – in part due to more complicated time dependence of TF-EF

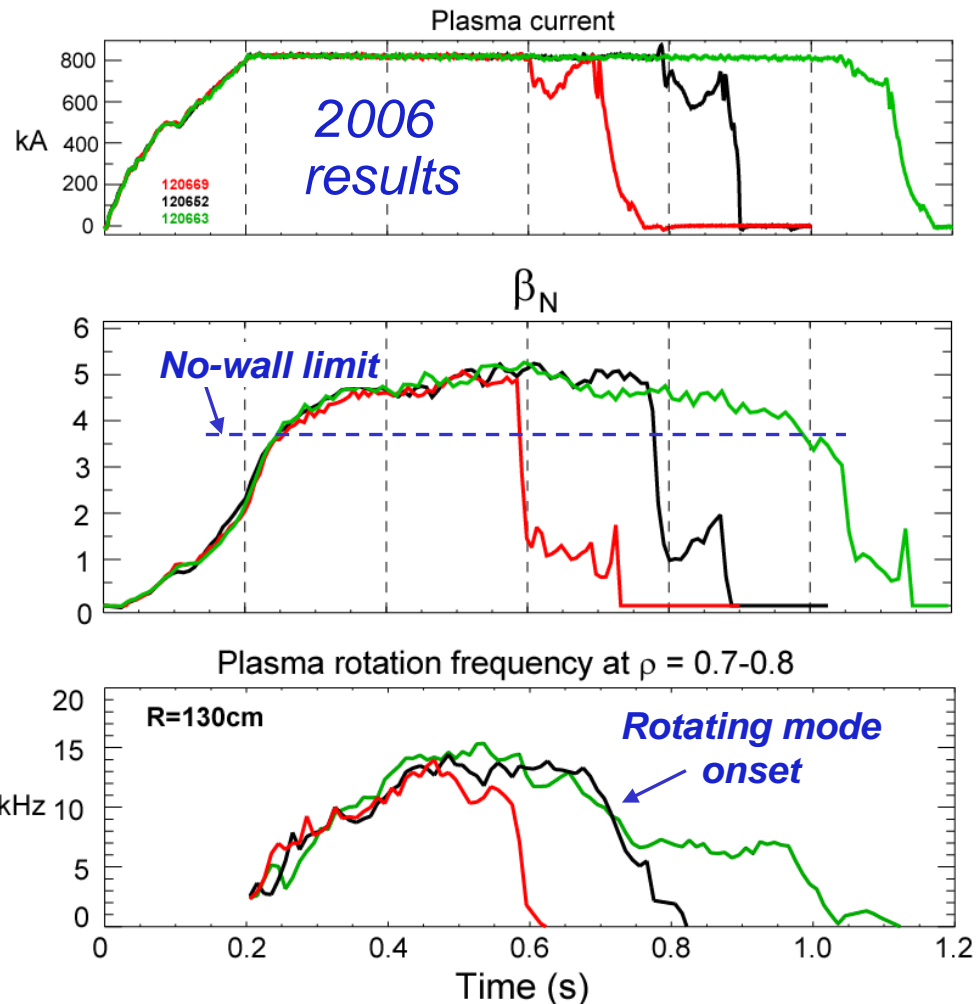
2006 - combination of pre-programmed TF-EFC + n=1 feedback (B_{P-U} sensors) was required to maximize rotation and pulse-length



- Feedback alone (not shown) extended pulse amount similar to that achieved with TF-EFC alone
 - Combination was best
- Gain limited by noise and offsets
- Mode “deformation” also observed
 - RFA/RWM would appear in lower array but not upper (or vice-versa)

- “noise” and “deformation” motivate improved mode detection in 2007:
 - Use optimal combination of U & L
 - Maximize sensitivity to RFA/RWM
 - Decrease sensitivity to deformation
 - Also try B_R for EF detection, control
 - Also try mixture of B_R and B_P

- **No error field control during high β_N phase**
- **TF-EFC**
- **TF-EFC + active n=1 B_{P-U} feedback**

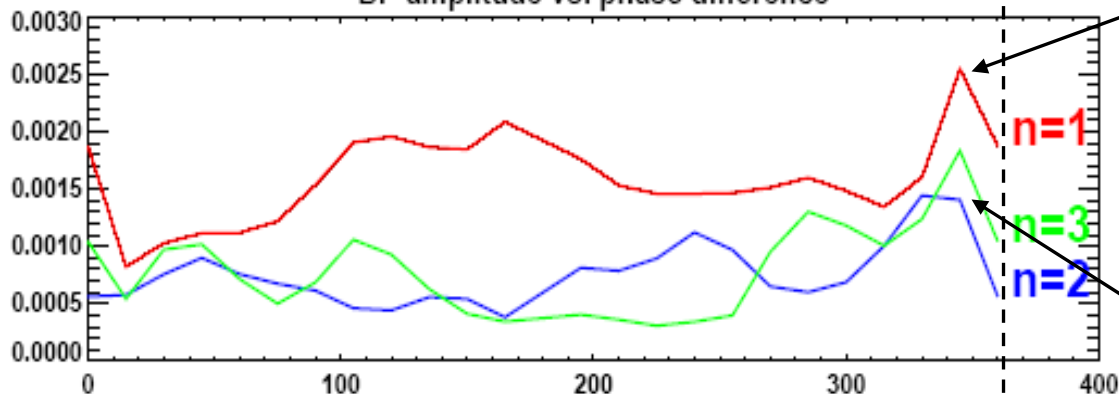


Optimized B_p sensor usage improves detection of low-f $n=1$ mode, enabling improved feedback suppression of RFA and RWMs



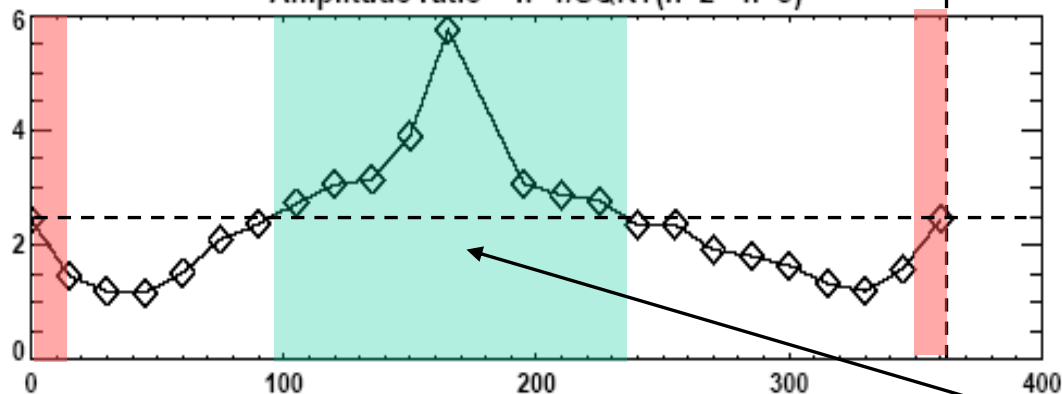
Scan phase shift between B_{p-U} and B_{p-L} : 360°

BP amplitude vs. phase difference



- Detected $n=1$ amplitude is highest near 0° phase shift
 - Consistent with simple up-down average with small offset due to mode helicity + sensor separation
- But, $n > 1$ components are also detected for “pure” $n=1$ mode
 - mode finite amplitude effects
 - eddy currents
 - conducting wall non-axisymmetry
 - sensor/detection imperfections

Amplitude ratio = $n=1/\text{SQRT}(n=2 * n=3)$

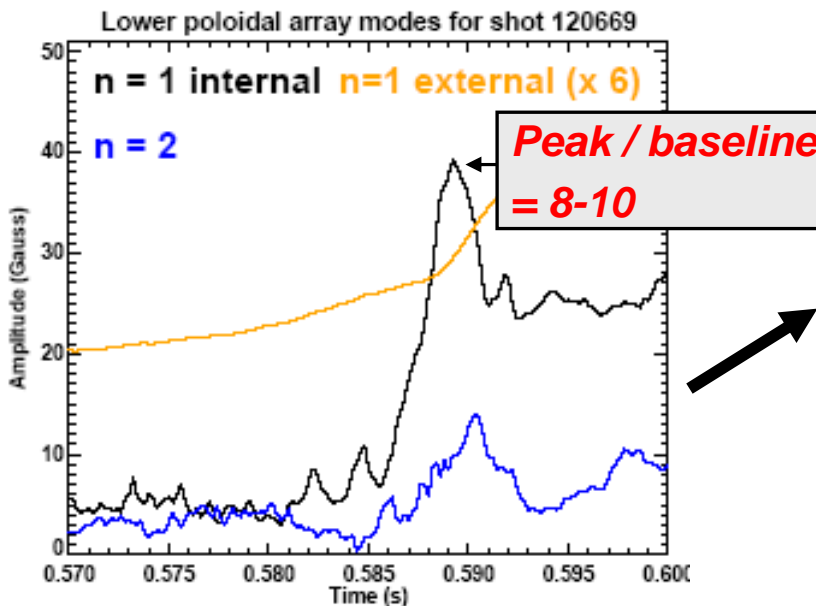
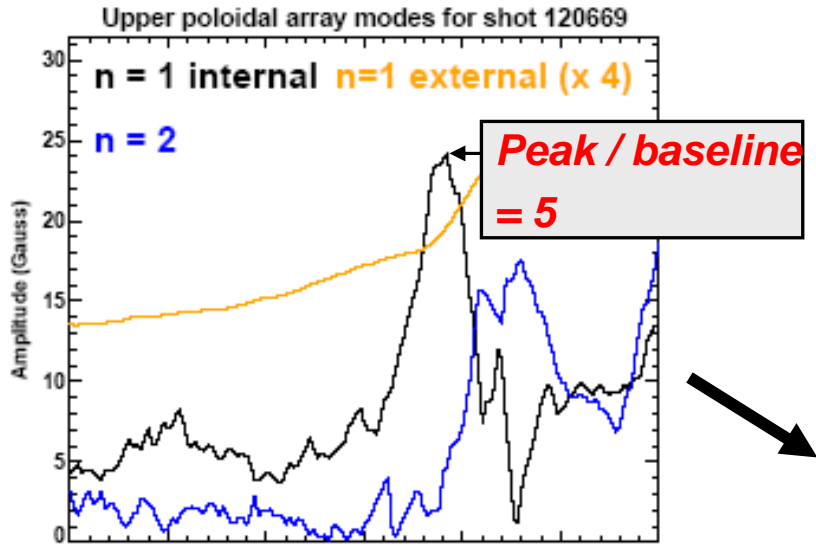


- Improved discrimination between $n=1$ and $n > 1$ obtained with different U-L phase shift range
 - $150\text{-}160^\circ$ is found to be optimal
 - Wider range of $n=1$ discrimination

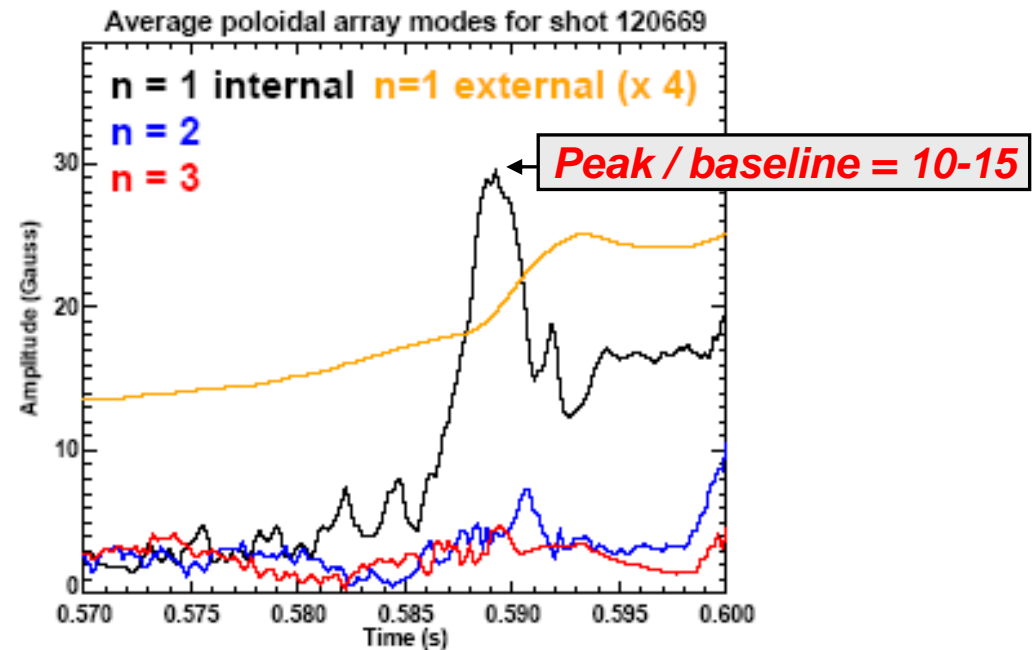
Relative phase shift between upper and lower B_p sensors [Degrees]

Optimal shift increases $n=1$ signal / baseline by $2\text{-}3 \times \rightarrow$ higher stable feedback gain

Optimal U/L average of B_p signals improves mode-ID sensitivity



Optimal upper-lower average increases amplitude / baseline factor of 2-3 \rightarrow higher feedback gain possible



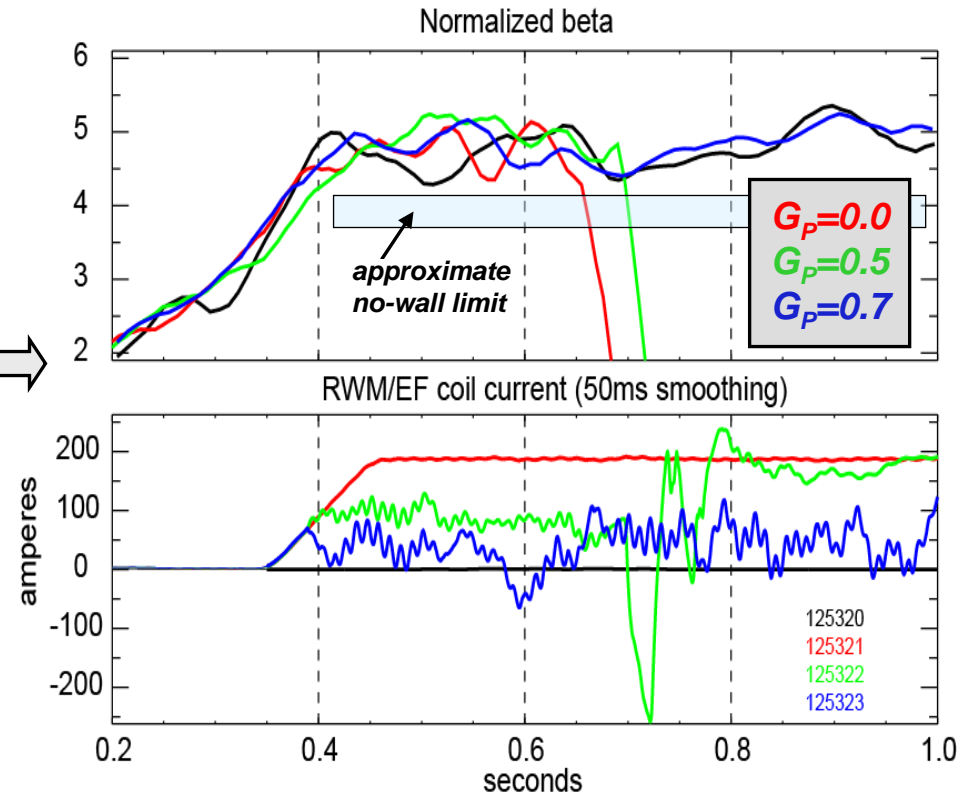
In 2007, using optimized B_p sensors in control system allowed feedback to provide most/all $n=1$ error field correction at high β



- Previous $n=1$ EF correction required a priori estimate of intrinsic EF
- Additional sensors \rightarrow detect modes with RWM helicity \rightarrow increased signal to noise
- Improved detection \rightarrow higher gain \rightarrow EF correction using only feedback on RFA

EFC algorithm developed in FY07:

- Use time with minimal intrinsic EF and RWM stabilized by rotation
- Intrinsic Ω_ϕ collapse absent in 2007 \rightarrow purposely apply $n=1$ EF to reduce rotation, destabilize RWM
- Find corrective feedback phase that reduces applied EF currents
- Increase gain until applied EF currents are nearly completely nulled and plasma stability restored
- Then turn off applied error field (!)



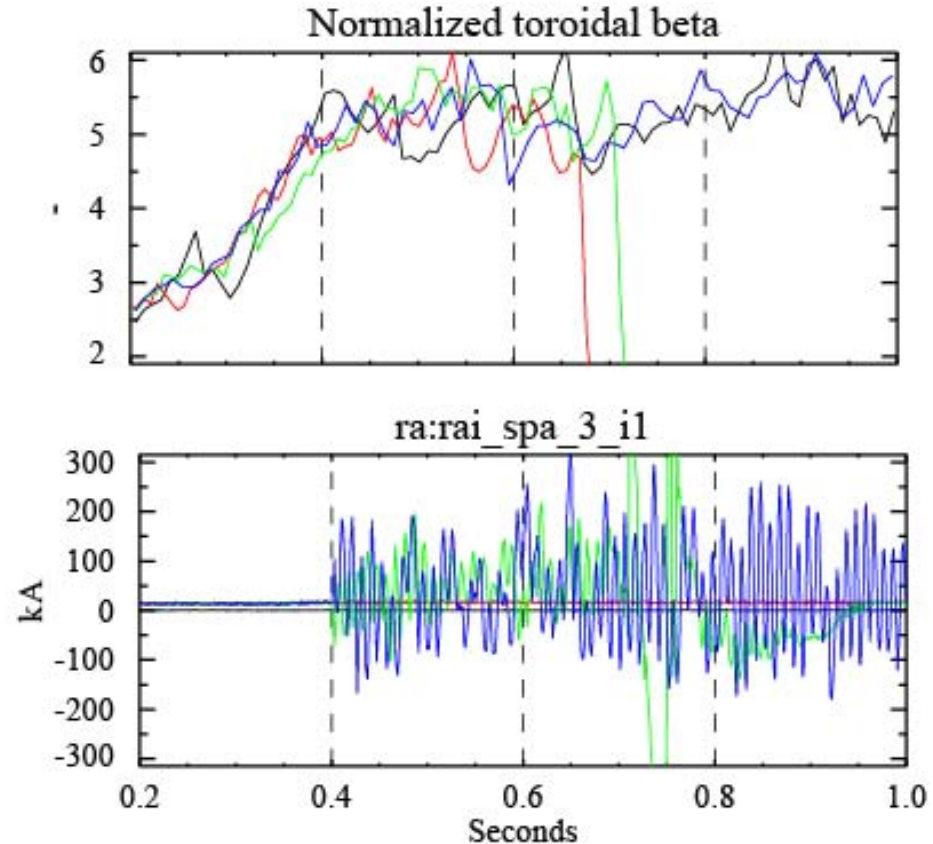
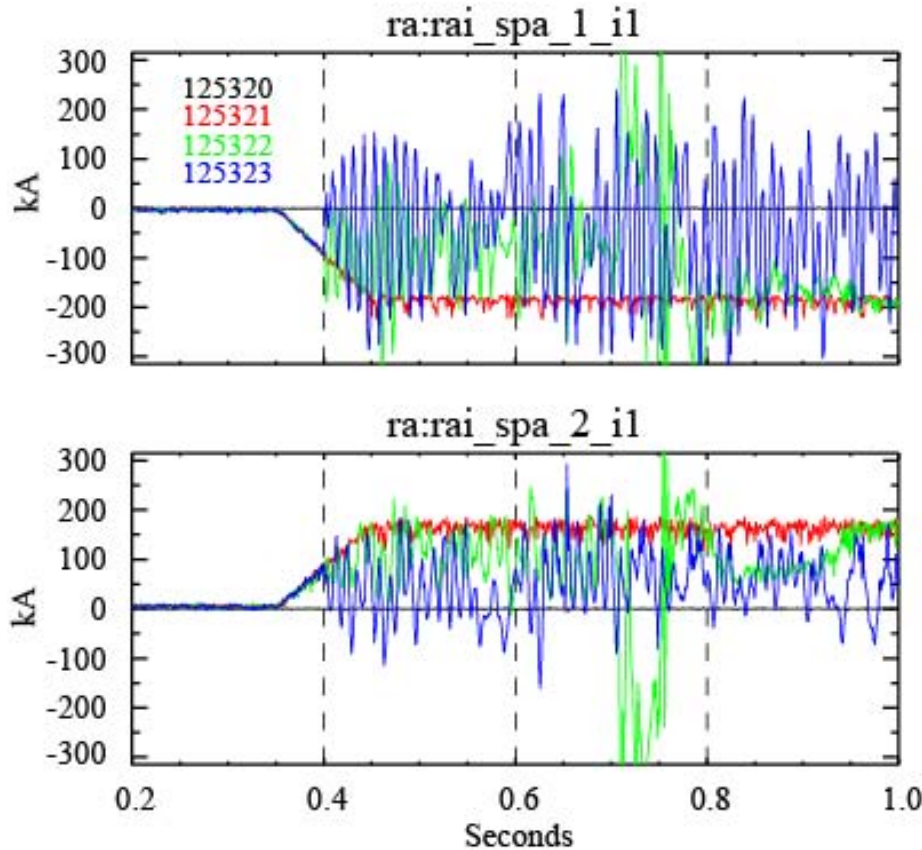
\rightarrow Use same gain/phase settings to suppress RFA from intrinsic EF and any unstable RWMs

Optimal phase difference $\delta=270^\circ$ between measured U/L avg B_p & applied B_R minimizes all time-averaged currents simultaneously

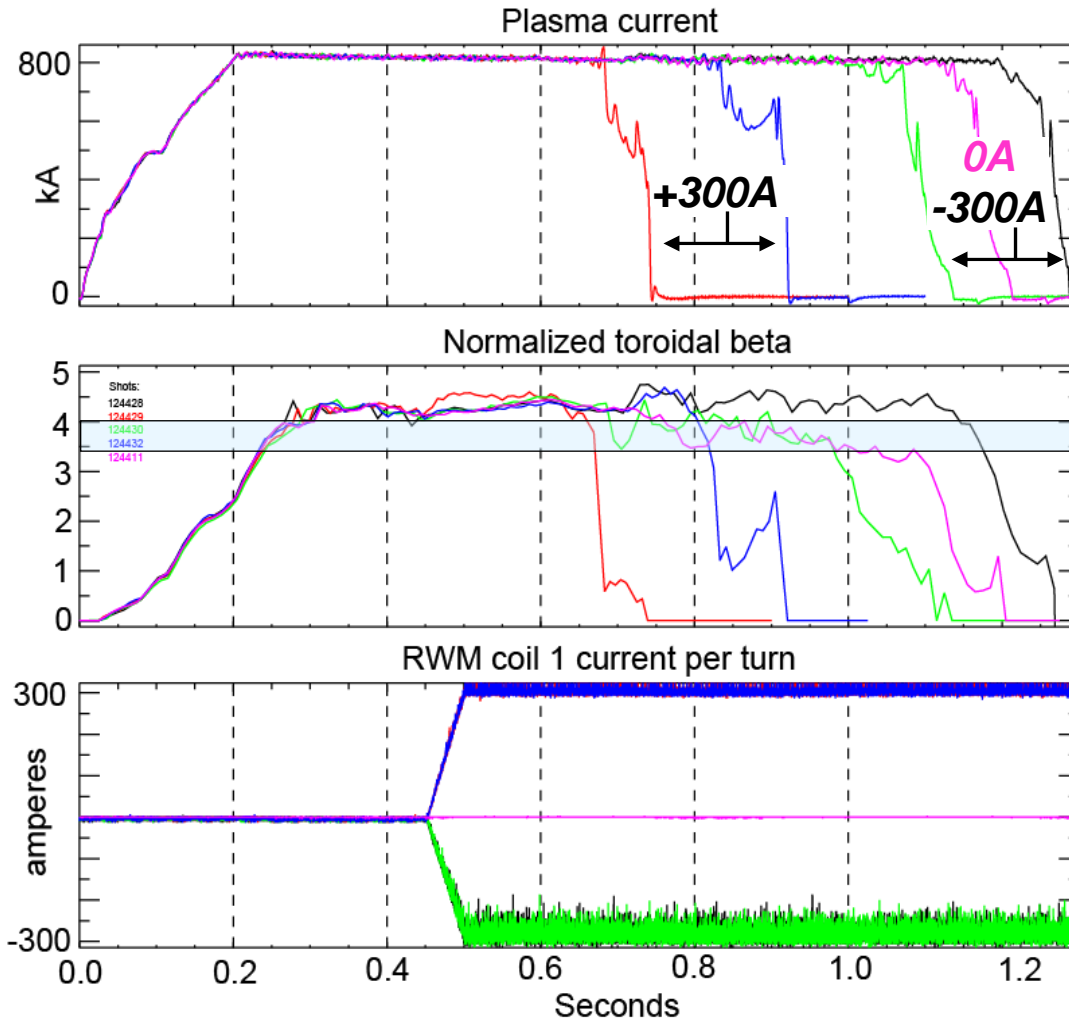


- Again, sufficient gain is required:

$G_p=0.0$ $G_p=0.5$ $G_p=0.7$



NEW: Discovered high- n error fields ($n=3$) important at high β_N



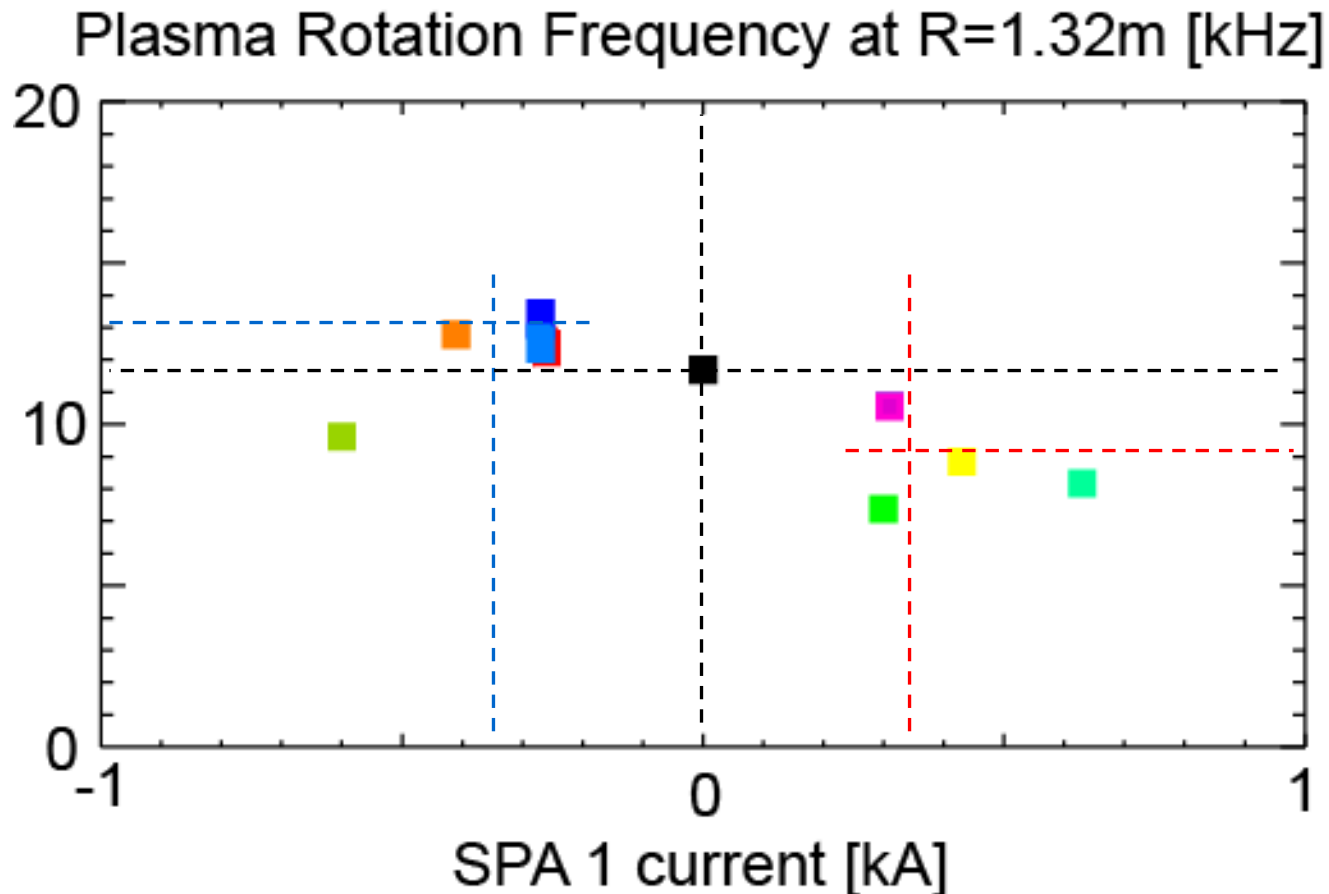
- Pulse-length depends on polarity of applied $n=3$
 - Anti-corrective polarity disrupts I_p and β
- Plasmas operate above $n=1$ no-wall limit \rightarrow RFA
 - slows rotation \rightarrow
 - destabilizes $n=1$ RWM
- Correction current magnitude for $n=3$ similar to that for $n=1$ correction
 - Applied $n=3$ $|B_R|$ is ≈ 6 G at outboard midplane
 - Fortuitous phase match between intrinsic $n=3$ EF and field coils can apply
- Assessing $n=3$ EF sources...

• $n > 1$ error fields not commonly addressed in present devices, or in ITER

Outboard Ω_ϕ changes by 30-40% with n=3 polarity flip



- Optimal n=3 current magnitude = 300-400A
- Coil shape data indicates VF coil (PF5) produces some n=3 EF
 - Need to assess if PF5 EF is consistent with empirical correction below

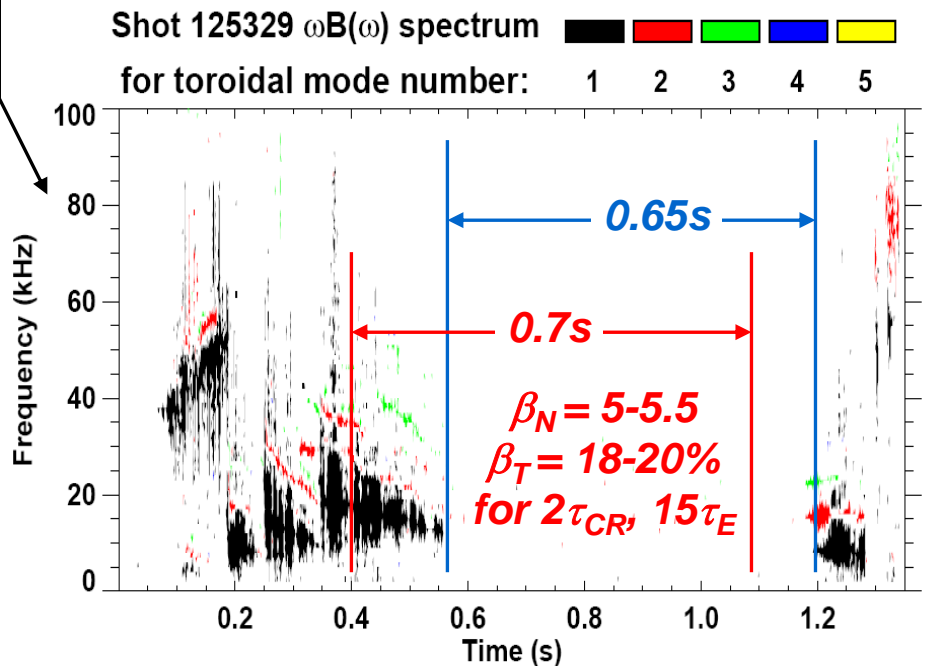


Simultaneous multiple-n correction improves performance

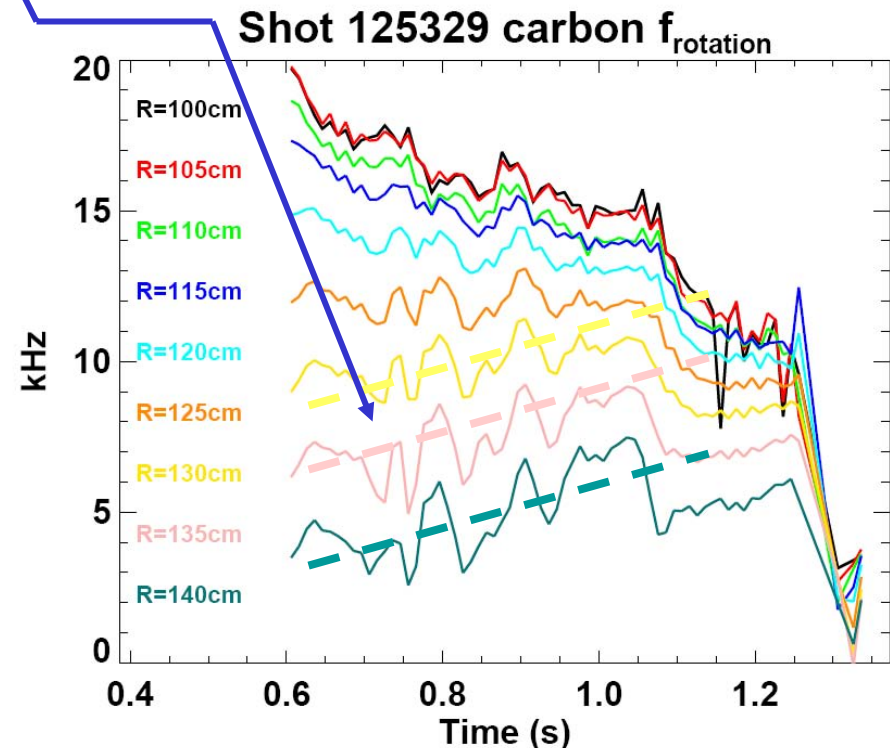
(Optimized feedback control of n=1 B_p RFA + pre-programmed n=3 correction)



- Record pulse-length at I_p=900kA, with sustained high-β
- Long period free of core low-f MHD activity
- Plasma rotation sustained over same period
 - Core rotation decreases with increasing density (f_{GW} → 0.75), but...
 - R > 1.2m rotation slowly **increases** until large ELM at t=1.1s



For reference: $\tau_{CR} \approx 0.3s$, $\tau_E = 40-50ms$



NSTX experiments have improved the understanding of magnetic error fields and their correction at low and high β



- Low density, low- β locked mode studies highlight the importance of plasma response and toroidicity, and predict favorable locking thresholds for ITER
- Multiple- n ($n = 1, 3$) EF correction improves sustained high- β_N operation
- General geometry corrections to particle orbit times can significantly modify the RWM critical rotation calculated by MARS-F – up to 50% variation in NSTX
- Present semi-kinetic damping theory generally under-predicts critical rotation
→ explore mechanisms that might decrease dissipation

We invite you to participate in and submit experimental ideas to the NSTX Research Forum, Nov. 27-29, 2007, <http://nstx-forum-2008.pppl.gov>